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The Incorporation of Carbon Nanofibres to Enhance the Properties of Hot Compacted Self-Reinforced Single-Polymer Composites

> R J Foster, P J Hine, M J Bonner & I M Ward ECCM 13 2-5th June 2008

Development of enhanced polymers



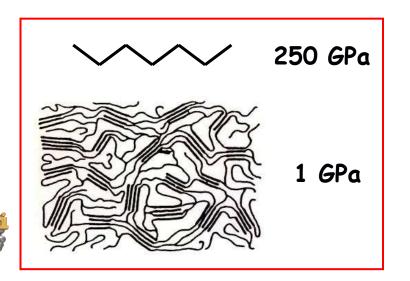
"COMMODITY" POLYMERS

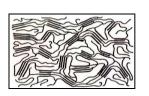
Cheap and easy to manufacture Limited mechanical properties at elevated temperatures

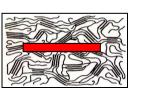
Control of molecular orientation and morphology Structure-Property Relationships between experimental results and theoretical predictions Add a reinforcement usually glass fibres:

> Control orientation and fibre length

> > 1 GPa







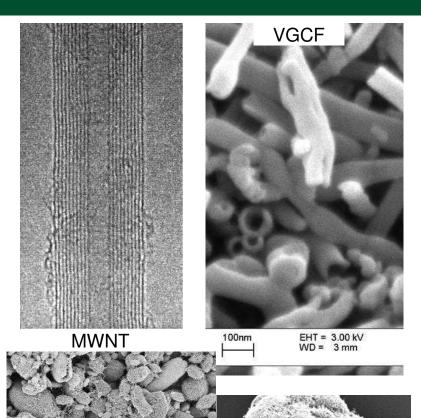
30% w/w glass filled PE: 8 GPa aligned fibres

Unfilled PE

Carbon nanotubes and nanofibres

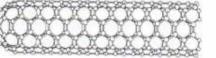


- Seamless cylinders of graphene
- Carbon-carbon bond exceptional strengths & mechanical resilience
- Vapour Grown Carbon Fibres's (VGCF/CNF)
 - Seeded in vapour, entangled mass
 - Relatively inexpensive.
- Highly Entangled fibre assembly need to disentangle whilst retaining length for best mechanical properties
- Potential blending routes include high shear mixing, solvent dispersion, ball-milling, compatiblisers and ultrasound



VGCF









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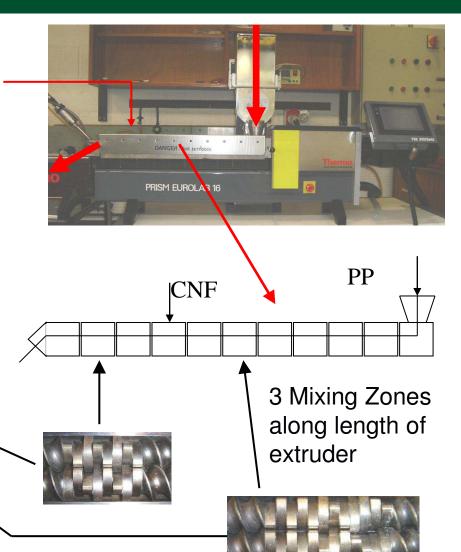
High shear mixing

Prism Twin Screw Extruder

Introduce Carbon Nanofibres (CNF) at end of 1st Extrusion (5% by volume)

Removal of material in pellet form after each extrusion –compression moulded sheet for properties testing

Re-introduce material into extruder for a 2nd & 3rd extrusion (4 & 7 Mixes)



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Properties of blended material

Number of Mixes 7 4 Both Blending 2.3 Temperatures 5% CNF by 200C Comp volume 2.2 230C Comp Isotropic Compression 200C Pure 2.1 moulded sheets made from 230C Pure pelletised material 2.0 Modulus (GPa) Static tensile testing 1.9 Young's modulus goes through clear peak after 4 1.8 mixes 1.7 Increase attributed to improved dispersion 1.6 -Decrease attributed to 白玉 reduction in CNF length 1.5 -3 Number of Extrusions ~37% increase in Young's Modulus

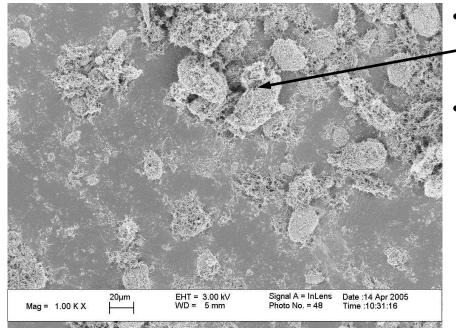


(1.55GPa to 2.12GPa)

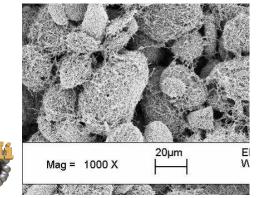
Isotropic Compression Moulded Sheets

A single mix



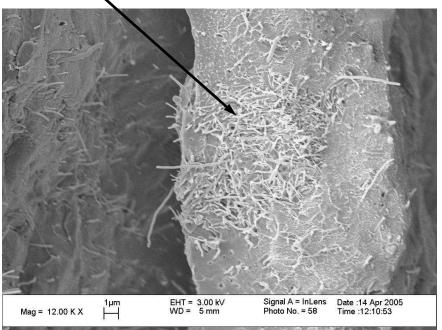


CNF blended at 200°C, 1 mix (1 extrusion)



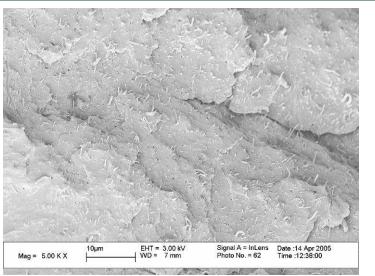
As Received CNF

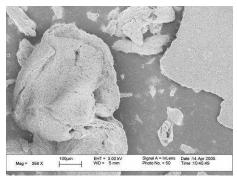
- Burning off PP matrix from material mixed once shows ball-like structures intact, similar to the as-received CNF
- Freeze fracture of composite sheet from same material shows regions of un-wetted fibres



Freeze Fracture Sample of Compression Moulded Sheet from material blended at 200°C, 1 mix (1 extrusion)

More mixes....



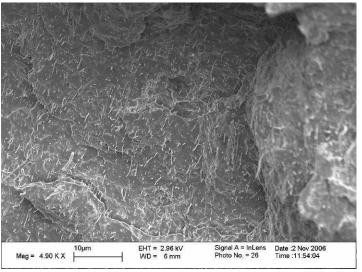


CNF 'Mats' – reaggregated fibres (4, 7 Mixes)

Freeze Fracture Sample of Compression Moulded Sheet from material blended at 200°C, 7 mixes (3 extrusions)

Freeze Fracture Sample of Compression Moulded Sheet from material blended at 200°C, 4 mixes (2 extrusions)

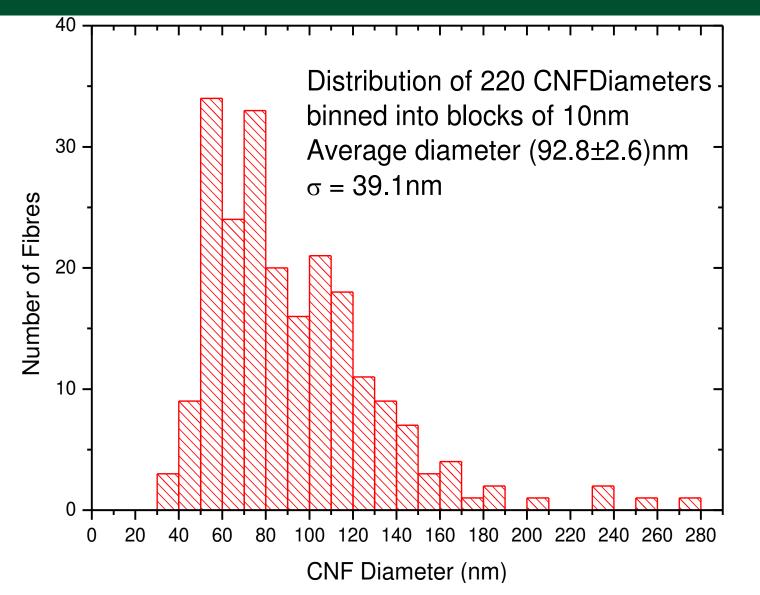




- Burning off matrix for material mixed more than once leads to reaggregation of fibres –no direct information about blending process
- Can infer that material must be well mixed and fibres must have been separated in order for them to re-aggregate
- Confirmed by freeze fracture of composite sheet
- Thus increase in Young's modulus going from 1 mix to 4 mixes is due to improved dispersion

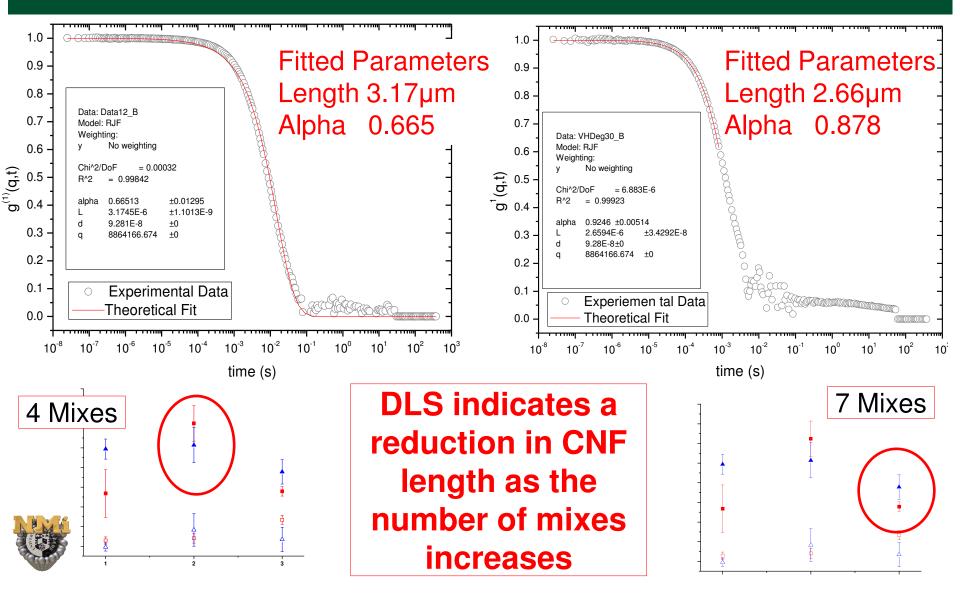
Diameter measurement







Dynamic Light Scattering



The Cox-Krenchel model

Composite Modulus modelled using Cox-Krenchel equation (modification of the rule of mixtures):

$$\mathbf{E}_{\mathrm{C}} = \eta_0 \eta_1 \mathbf{V}_{\mathrm{f}} \mathbf{E}_{\mathrm{f}} + (1 - \mathbf{V}_{\mathrm{f}}) \mathbf{E}_{\mathrm{m}}$$

 $V_{\rm f}$ = Volume fraction of fibres, $E_{\rm f}$ = Young's Modulus of fibres, $E_{\rm m}$ = Young's Modulus of matrix

 η_0 is orientation efficiency factor:

$$\eta_0 = \sum_n a_n \cos^4 \theta_n \text{ where } \sum_n a_n = 1$$

For 3D: $\eta_0 = 1/5$ and for 2D: $\eta_0 = 3/8$
 η_1 is length efficiency factor (Cox Shear Lag factor):
 $\eta_1 = 1 - \frac{\tanh(\beta 1/2)}{\beta 1/2}$

Where 1 is the length of the fibres, and β is given by:

$$\beta = \left(\frac{2\pi G_{\rm m}}{E_{\rm f} A_{\rm f} \log_{\rm e}({\rm R/r})}\right)^{\frac{1}{2}}$$

Critical Parameters -fibre length, fibre diameter and volume fraction

X



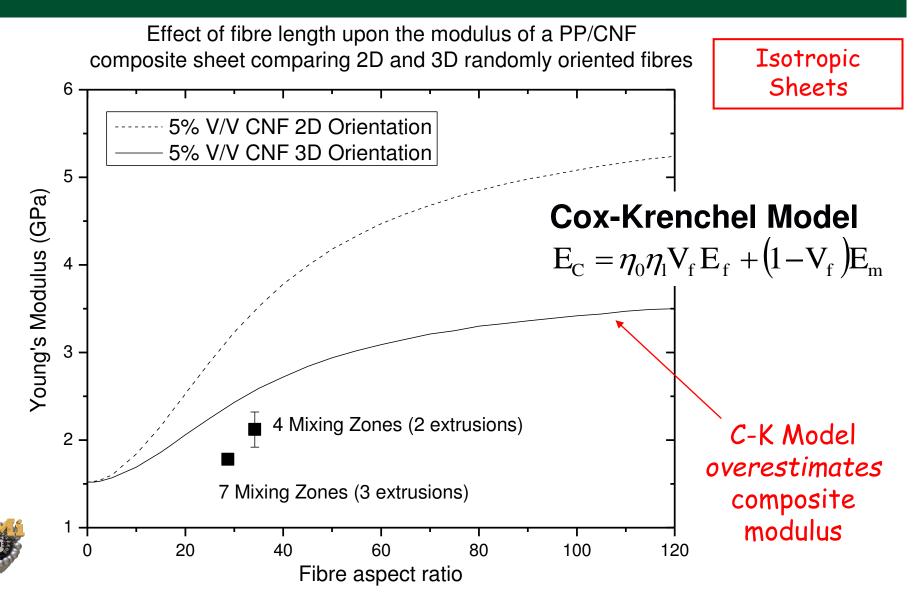
Folkes, M. J., "Short Fibre Reinforced Thermoplastics". 1985, John Wiley & Sons.

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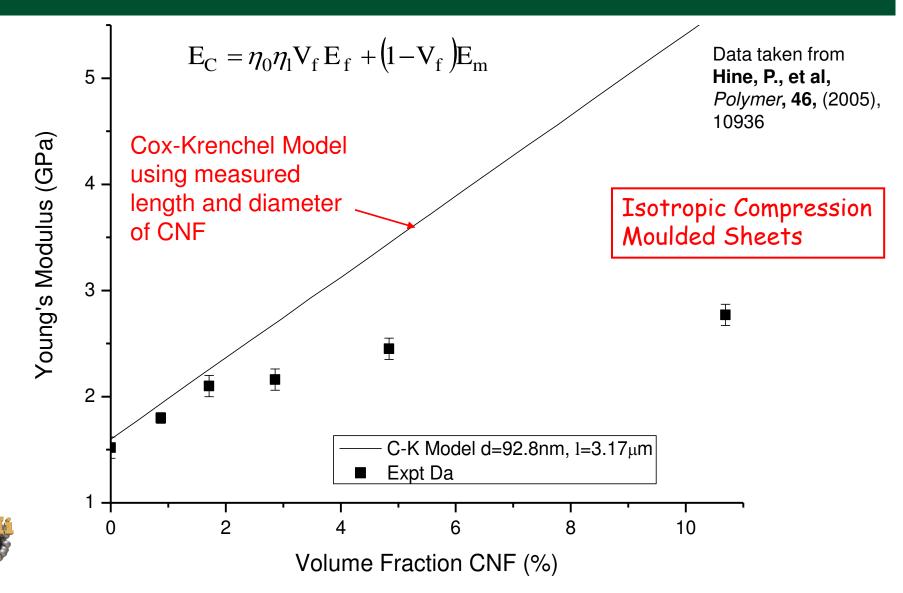
Cox-Krenchel modelling





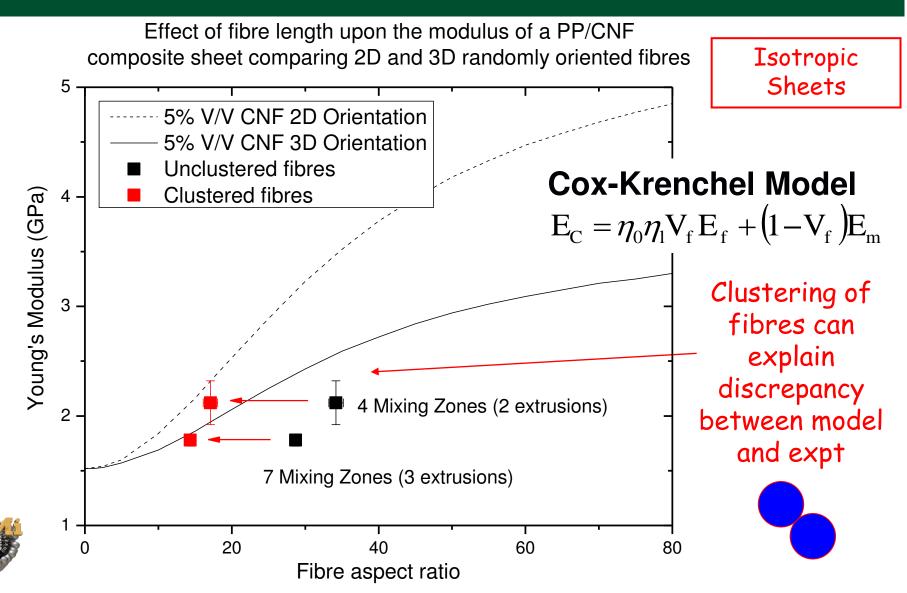
Amount of nanofiller





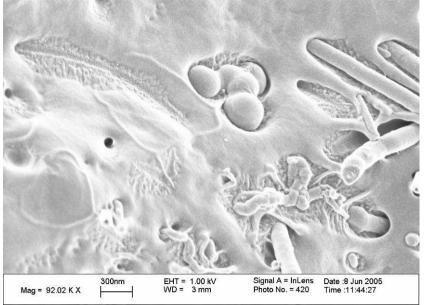
Cox-Krenchel modelling



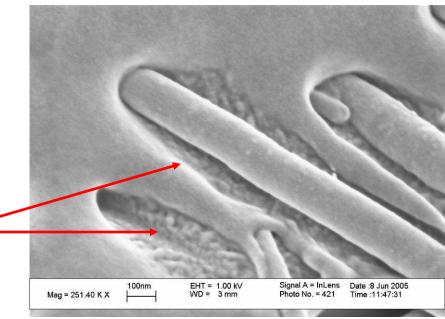


Morphology





SEM image of freeze fracture from isotropic sheet shows CNF can modify the local microstructure forming transcrystalline layer

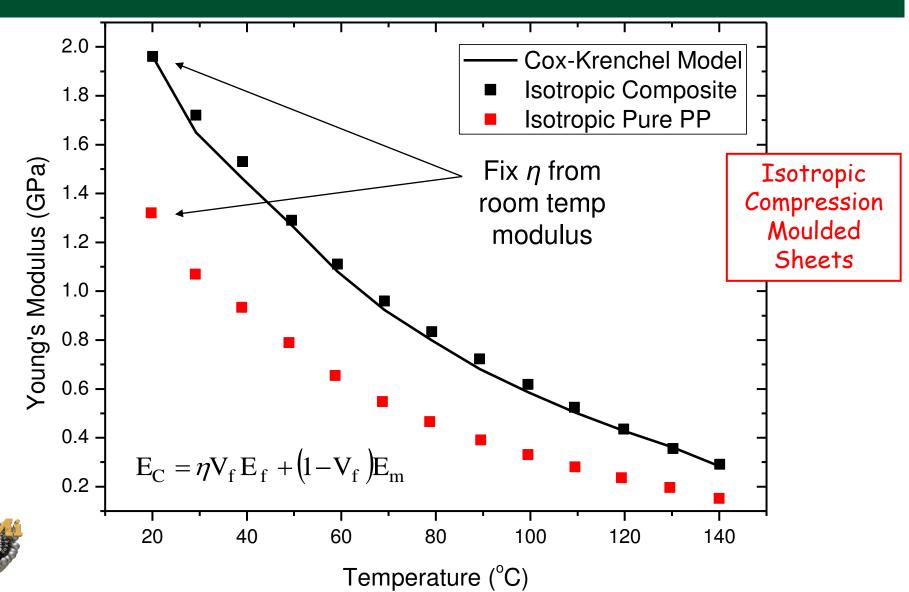


Transcrystalline layer (row aligned molecules nucleated on CNF)





Temperature performance



Hot compaction



Take an array of oriented polymer fibres or tapes.

Process at a suitable temperature to melt only the skin of the oriented elements and keep the oriented core.

On cooling the melted material freezes to bind the oriented elements together forming a single polymer composite.



Draw ratio of tapes (level of molecular orientation) controls final properties.

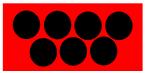
SCHEMATIC

HOT COMPACTION

Take an assembly of oriented fibres or tapes



At the compaction temperature surface melting occurs



On cooling a composite is formed of the original material and the melted phase

Ward, I. M., Hine, P. J., *Polymer*, 45, (2004), 1423

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Hot compaction

Nike Contour Shinguards







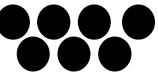


Samsonite Suitcases



Automotive Undertray

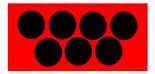
HOT COMPACTION SCHEMATIC



Take an assembly of oriented fibres or tapes



At the compaction temperature surface melting occurs



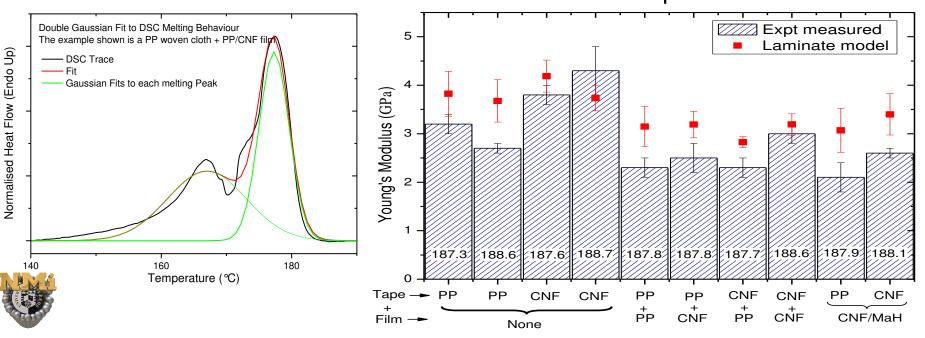
On cooling a composite is formed of the original material and the melted phase

Ward, I. M., Hine, P. J., *Polymer*, 45, (2004), 1423

Laminate Modelling

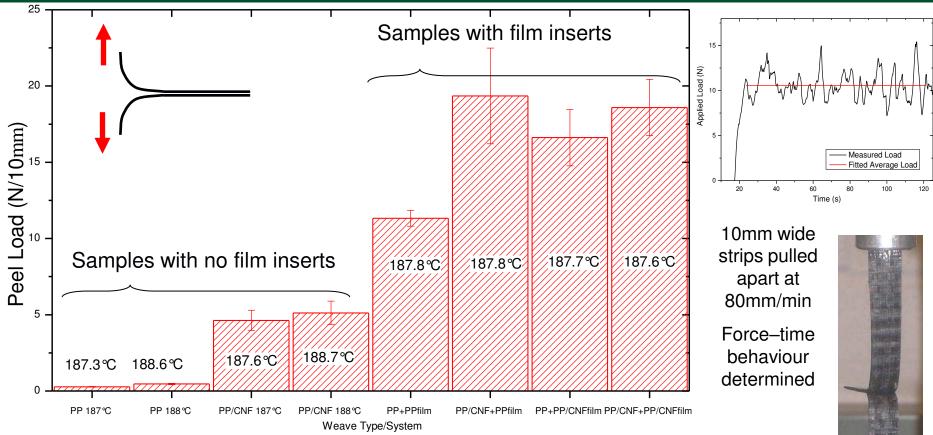
Modulus of laminate structure can be predicted from modification of the rule of mixtures:

$$E_{\text{Composite}} = \left(\frac{\text{Vol}_{\text{Oriented}}}{2}\right) E_{\text{oriented}} + \left(1 - \frac{\text{Vol}_{\text{Oriented}}}{2}\right) E_{\text{Matrix}}$$
Measure E_{oriented} (tapes) and E_{matrix} (isotropic)
Use DSC to determine the amount of material in each phase



Peel Strength (Delamination)

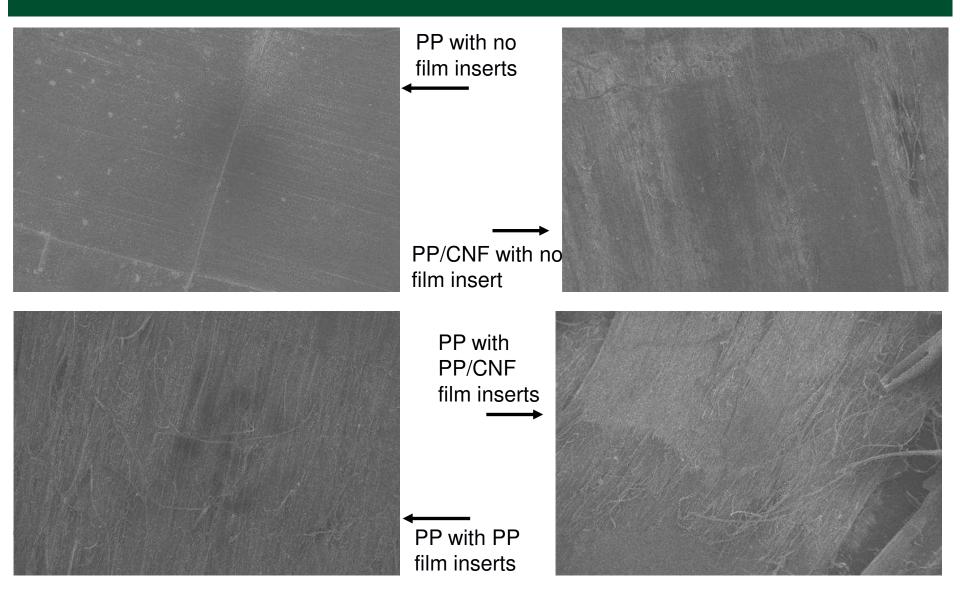




CNF dramatically improves Peel Strength of PP (from <0.5N to ~5N) HCPP with PP film increases Peel force by order of magnitude (~11N) Hot compacted nanocomposite shows further improvement (~18N) Surprisingly doesn't matter into what phase CNF are incorporated

Fracture Surfaces





Conclusions



- Polypropylene-CNF nanocomposite material successfully blended using high shear mixing. Peak in properties after 4 mixes.
- DLS and SEM analysis used to measure CNF length, diameter and dispersion – modelling gives insight into structure-property relationship
- Improved temperature performance of nanocomposite material
- Nanocomposite has been drawn and hot compacted to produce CNF reinforced single-polymer composites.
- Interlayer adhesion (peel force) of single-polymer composites improved dramatically by incorporation of CNF. Film layers of PP and PP/CNF allow further improvement.
- SEM has identified differences in the fracture surfaces. Ongoing investigation into full effect of CNF.





The authors would like to thank the Nanomanufacturing Institute for funding this study