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Structural and Thermal Effects of Hf⁴⁺ Substitution in CaZr_{1-x}Hf_xTi₂O₇ Zirconolite

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Abstract

There is a requirement to further understand the structural and thermal properties of candidate Pu wasteform materials, and moreover gain a better understanding of composition-driven variation in these properties as they can impact disposability. Zirconolite (CaZrTi₂O₇) phases are a candidate wasteform system to immobilise Pu at scale and therefore it is necessary to understand (as far as possible) the isolated influence of cation substitution on specific lattice sites. CaZr_{1-x}Hf_xTi₂O₇ is a model system for understanding the microstructural effects of Hf⁴⁺ substitution and underpin its viability as a neutron absorbing additive that could feasibly be co-immobilised with Pu. Hf⁴⁺ was capable of wholly substituting for Zr⁴⁺ at low-to-moderate concentration (i.e. x ≤ 0.60) after which some minor Hf-phase segregation was observed. Powder X-ray diffraction, Rietveld analysis and Raman spectroscopy were consistent with Hf⁴⁺ substituting in the Zr⁴⁺ site and confirmed no additional zirconolite polytypes were formed in addition to 2M. Hf L₃-edge EXAFS analysis was consistent with Hf⁴⁺ occupying the 7-fold Zr⁴⁺ site in the zirconolite-2M structure consistent with the targeted substitution scheme. The thermal diffusivity and thermal conductivity of the zirconolite ceramics was generally observed to increase with elevated Hf⁴⁺ content although no clear compositional trends were identified.

1 Introduction

Plutonium lifecycle is a key aspect of the Nuclear Decommissioning Authority (NDA) research strategy, which outlines a requirement to place all Pu currently held under UK civil safeguards 'beyond reach' [1]. As of 2025, immobilisation within a ceramic wasteform prior to geological disposal is the favoured disposition route and, as such, there are ongoing efforts to underpin a preferred immobilisation technology and develop the current understanding of the mechanical, structural and thermal properties of potential host matrices that could feasibly incorporate Pu at moderate concentration (ca. 20 wt. %). Zirconolite (CaZrTi₂O₇) is a candidate ceramic phase that has been identified as a potentially feasible wasteform for the immobilization of separated Pu, and there has been a notable body of published literature aiming to further understand its chemistry with respect to actinide incorporation, either using Pu or relevant surrogates (Ce, U, Th) and additives that will require co-immobilisation with a view to satisfy disposal criteria, namely neutron absorbing additives [2]. When considering geological disposability of radioactive waste, heat generation, radiological risk and the potential for a criticality event to occur must all be considered. As criticality can occur in both ²³⁹Pu and the ²³⁵U daughter

product there is a requirement for waste packages containing immobilised Pu to co-immobilise a suitable neutron absorber. In order to develop a robust safety case for the geological disposal of ceramic products containing Pu in the immobilised form, it is necessary to demonstrate confidence in the solid solution behaviour of neutron absorbing additives within the host wasteform structure. An improved understanding of doping limits and site substitution constraints will better inform ceramic compositions that can be formulated with Pu without leading to the formation of deleterious secondary phases containing segregated Pu. A recent review highlighted Hf⁴⁺ as a potential neutron absorbing additive in zirconolite^[3] and indeed several examples of successful Hf⁴⁺ incorporation within this phase have been reported in the wider literature. Vance et al. reported the successful substitution of Hf⁴⁺ for Zr⁴⁺ at 50 mol. % and 100 mol. % when fabricated by a solid-state route, i.e. CaZr_{0.5}Hf_{0.5}Ti₂O₇ and CaHfTi₂O₇^[4] and the synthesis of phase pure CaHfTi₂O₇ 'hafnolite' was also reported by Putnam et al.^[5]. Begg et al. reported a series of PuO₂-doped zirconolite materials under a range of processing atmospheres to favour either Pu³⁺ or Pu⁴⁺^[6]. When targeting B-site substitution i.e. CaHf_{0.9}Pu_{0.1}Ti₂O₇ a sample of 98% phase reported purity in air, with Pu⁴⁺ maintained; A-site substitution, targeting Pu³⁺ in Ca_{0.8}Pu_{0.2}HfTi_{1.8}Al_{0.2}O₇ and Pu⁴⁺ in Ca_{0.8}Pu_{0.2}HfTi_{1.6}Al_{0.4}O₇ produced 96% and 94% phase purity, respectively, when sintered in air with 100% Pu⁴⁺ valence for both materials measured by X-ray absorption spectroscopy; these data indicate that zirconolite is capable of self-charge balancing in the absence of charge modifying additives. Zhang et al. attempted the synthesis of the CaZr_{1-x}Hf_xTi₂O₇ solid solution by combustion synthesis followed by quick pressing, however despite low reported Hf leach rates (CaZr_{0.4}Hf_{0.6}Ti₂O₇ at 90 °C via MCC-1 method in deionised water: $1.11 \times 10^{-8} \text{ g} \cdot \text{m}^{-2} \cdot \text{d}^{-1}$ normalised after 42 d) a moderate perovskite yield was reported throughout the sample matrix^[7]. Further syntheses of doped CaHfTi₂O₇ ceramics and glass-ceramics have been reported in the work of Caurant et al.^[8,9]. As Hf⁴⁺ is considered a candidate neutron absorbing additive, the aim of the present work is to further underpin the incorporation behaviour of Hf⁴⁺ within the zirconolite phase, by careful examination of diffraction, microscopy and spectroscopy behaviour between the two end-member compounds CaZrTi₂O₇ and CaHfTi₂O₇.

2 Experimental Methodology

The CaZr_{1-x}Hf_xTi₂O₇ solid solution (where x = 0 – 1.00, Δx = 0.10) was fabricated by a solid-state reaction between component oxides CaTiO₃, ZrO₂, HfO₂ and TiO₂ (Merck, 99.9% trace metals basis). Precursors were calcined at 800 °C overnight prior to weighing in the required proportions and added to a Y-stabilised ZrO₂-lined milling jar, with ZrO₂ milling media and isopropanol. Each sample was homogenised by planetary ball milling at 400 rpm for a period of 20 min, with the direction changed at each 5 min interval. The powder slurry was discharged and dried at 80 °C to evaporate excess solvent and sieved through a 1 mm mesh to separate the milling media. Approximately 1 g of each composition was pressed into the walls of a stainless-steel die under a uniaxial force of 3 t and pellets were sintered in air at 1400 °C, with a dwell period at maximum temperature held for 24 h and programmed heating/cooling rates of 5 °C/min. Powder X-ray diffraction data was collected using a Bruker D2 Phaser (Cu Kα, λ = 1.5406 Å) fitted with a Lynxeye position sensitive detector and Ni filter, over the range

$10^\circ \leq 2\theta \leq 70^\circ$ with a scan rate of $0.02^\circ \text{ s}^{-1}$ and 1 s per step. Peak matching and indexing was achieved using the PDF2+ database. Each diffraction profile was analysed using the Rietveld method to extract the lattice parameters of the zirconolite phase using the Bruker TOPAS software package. The microstructure and bulk composition of each pellet was analysed using a Hitachi TM3030 microscope operating at 15 kV accelerating voltage with an approximate working distance of 8 mm. Prior to analysis each pellet was mounted in cold-setting epoxy resin and polished to a $1 \mu\text{m}$ surface finish and coated with a thin layer of conducting carbon. The microscope was fitted with a Bruker Quantax system for elemental dispersive X-ray spectrometry (EDS) analysis. X-ray absorption spectroscopy (XAS) data were collected at the Hf L₃-edge at Diamond Light Source Beamline B18 using a transmission configuration. Data were collected for compositions $x = 0.10, 0.50$ and 1.00 , representative of material with the nominal compositions corresponding to $\text{CaZr}_{0.90}\text{Hf}_{0.10}\text{Ti}_2\text{O}_7$, $\text{CaZr}_{0.50}\text{Hf}_{0.50}\text{Ti}_2\text{O}_7$ and $\text{CaHfTi}_2\text{O}_7$, respectively. The Demeter software package was used to normalise and merge multiple scans into one dataset, with the EXAFS region used to model single scattering paths generated by FEFF for the zirconolite-2M structural model (C2/c). Raman spectra were also collected on samples of $\text{CaZrTi}_2\text{O}_7$, $\text{CaZr}_{0.5}\text{Hf}_{0.5}\text{Ti}_2\text{O}_7$ and $\text{CaHfTi}_2\text{O}_7$ using a Renishaw InVia Raman microscope equipped with a 2400 mm^{-1} grating. Samples were excited using a 514.5 nm Ar laser at 5 mW power output, scanning for 45 seconds at three points on the sample surface. Data were averaged and smoothed using a Savitsky Golay filter followed by Asymmetric Least Squares background subtraction determined through sensitivity analysis of the 780 cm^{-1} spectral line position and intensity ($\lambda = 1 \times 10^6$, $p = 0.004$). Laser Flash Analysis (LFA) was performed using a Netzsch LFA 467 Hyper Flash to determine thermal diffusivity and specific heat capacity at 30, 100, 200, 300, 400 and 500°C . LFA data were collected on 13 mm disks polished to $1 \mu\text{m}$ surface finish, with material density established by He pycnometry and the Archimedes method.

3 Results and Discussion

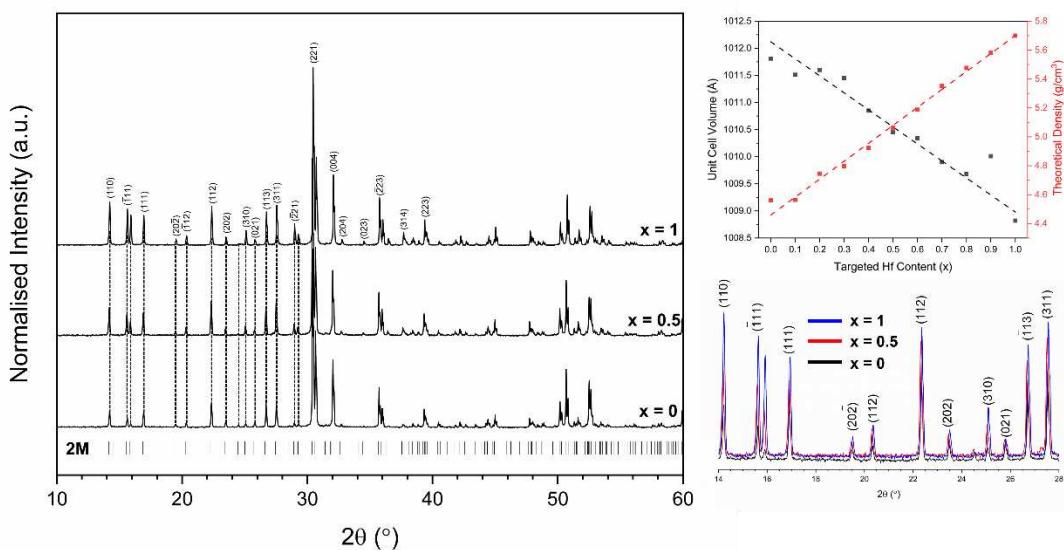


Fig. 1 Powder X-ray diffraction data for $x = 0$, 0.50 and 1.00 showing the allowed reflections for the zirconolite-2M structure and (hkl) values for selected reflections in the low 2θ range. Insets show (1) magnified reflections in the range $14^\circ \leq 2\theta \leq 28^\circ$

and (2) unit cell volume (Å³) and theoretical density (g/cm³) as a function of targeted Hf⁴⁺ content, using values calculated from Rietveld analysis of powder diffraction profiles.

A series of 11 zirconolite-hafnolite pellets were produced including both end-member compositions and first analysed by powder X-ray diffraction (**Fig. 1**) and scanning electron microscopy (**Fig. 2**) to establish phase purity and determine substitution limits of HfO₂ within the nominal solid solution CaZr_{1-x}Hf_xTi₂O₇. The observed reflections in the powder diffraction profile were all readily indexed to the zirconolite-2M structure and, with the exception of x = 0.70, 0.80 and 0.90, no visible phase separation was observed. An example of the microstructure for x = 0.80 is provided in **Fig. S1** and appears to show small Hf/Ti-rich inclusions, likely of the HfTiO₄ structure-type. The HfTiO₄ reflections were not readily indexable due to the overlap in 2θ position with the dominant (221) reflection for the 2M structure. Rietveld analysis was performed using a zirconolite-2M (C2/c) structural model, wherein the occupancy of the Zr1 site was modified to partially include Hf⁴⁺ fixed according to the target stoichiometry. The unit cell parameters and site occupancy of Ca1, Ti1, Ti2 and Ti3 sites were allowed to simultaneously refine, and the refinements all converged with good statistics (**Table 1**). It was noted that including an additional HfTiO₄ phase to the model for x = 0.70 did nothing to further improve the refinement statistics and estimated the relative phase fraction to be < 2 wt. %, hence was not included in any subsequent analysis. The relative intensity of the indexed reflections was observed to increase when data were normalised to the intensity of the dominant (221) reflection (see inset of **Fig. 1**) attributed to an increased scattering factor. As the intensity of scattered X-rays scales with Z, this effect was attributed to the progressive substitution of Hf (Z = 72) for Zr (Z = 40). The unit cell volume was observed to steadily decrease as a function of Hf⁴⁺ content (see inset of **Fig. 1**) on account of the small variation in ionic radii between Zr⁴⁺ and Hf⁴⁺ (0.78 Å and 0.76 Å in 7-fold coordination, respectively). The obtained unit cell dimensions are in good agreement with those previously reported in the literature [3]. The theoretical density of the zirconolite phase was observed to steadily increase with Hf⁴⁺ content, consistent with the density of Zr and Hf oxides (5.67 and 9.68 g/cm³, respectively).

Table 1) Unit cell parameters for the zirconolite-2M phase obtained by Rietveld analysis using a 2M (C2/c) structural model.

(x)	a (Å)	b (Å)	c (Å)	β (°)	V (Å ³)	R _{wp}	GOF
0.00	12.4447(2)	7.2728(1)	11.3726(2)	100.5760(12)	1011.81(3)	12.53	2.08
0.10	12.4416(2)	7.2725(1)	11.3723(2)	100.5712(10)	1011.51(3)	11.40	2.02
0.20	12.4451(5)	7.2719(3)	11.3712(5)	100.5820(2)	1011.60(8)	15.11	2.54
0.30	12.4402(2)	7.2725(1)	11.3728(2)	100.5713(11)	1011.45(3)	10.97	2.05
0.40	12.4369(2)	7.2715(1)	11.3704(2)	100.5650(9)	1010.85(3)	9.55	1.95
0.50	12.4358(2)	7.2711(1)	11.3675(2)	100.5633(11)	1010.45(3)	10.01	1.90
0.60	12.4340(2)	7.2714(1)	11.3675(2)	100.5626(10)	1010.34(2)	10.00	2.10
0.70	12.4318(2)	7.2704(1)	11.3660(2)	100.5616(11)	1009.90(3)	9.86	2.10
0.80	12.4311(2)	7.2703(1)	11.3643(2)	100.5595(11)	1009.68(3)	9.91	1.98
0.90	12.4327(2)	7.2717(1)	11.3650(2)	100.5647(13)	1010.01(4)	10.36	1.99

1.00	12.4267(2)	7.2694(1)	11.3599(2)	100.5557(10)	1008.82(2)	9.67	2.05
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SEM observations of the polished microstructures highlighted that high density materials were formed throughout the solid solution (**Fig. 2**). Minimal porosity was observed, and this was reflected by the obtained Archimedes and He-pycnometry density measurements, indicating %TD between $\sim 93\%$ and $\sim 98\%$. The average bulk composition of each microstructure was obtained by EDS analysis (**Table S1**) which produced average values in good agreement with the targeted composition, with each composition normalised to seven oxygen atoms per formula unit.

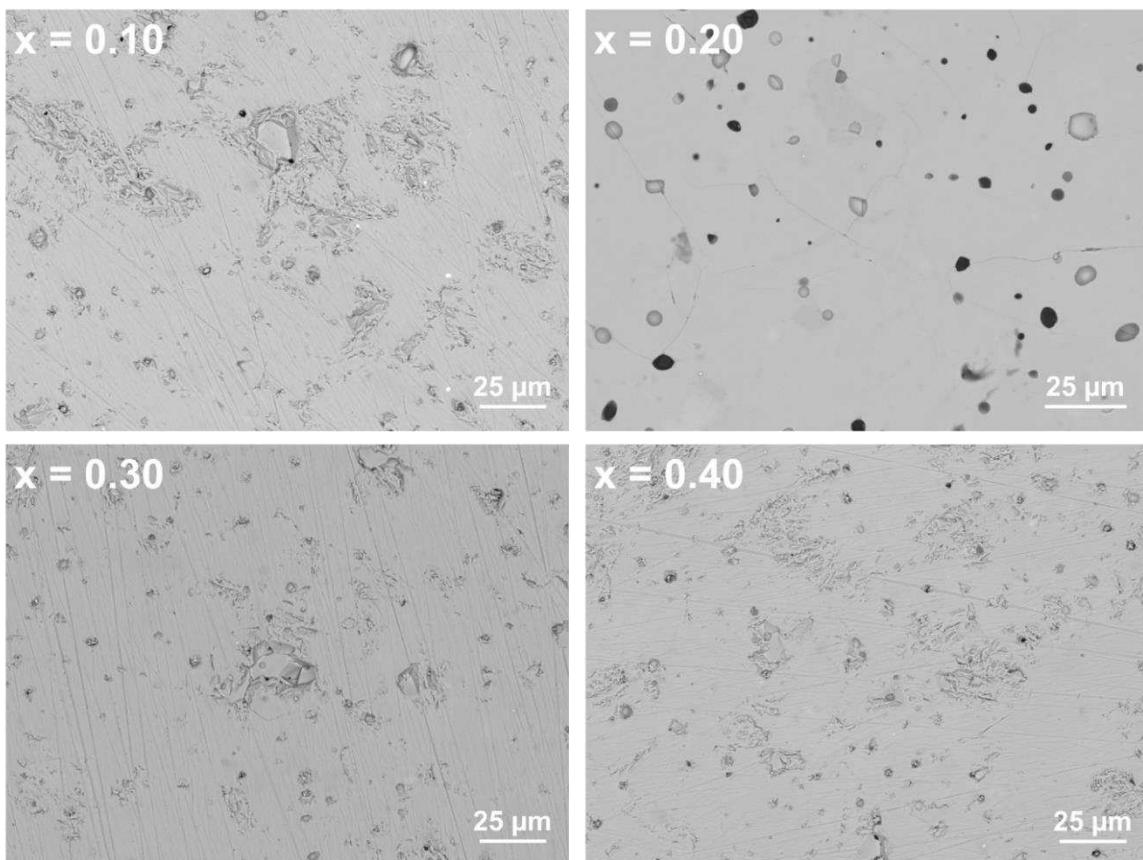


Fig. 2) Backscattered electron micrograph images of polished $0.10 \leq x \leq 0.40$ compositions detailing single phase zirconolite-2M.

The fits of Hf L₃-edge EXAFS spectra for $x = 0.1$, 0.5 , and 1.0 compositions are shown in **Fig. 3**. The Hf L₃-edge EXAFS was first fitted for the HfO₂ reference sample to determine a suitable amplitude reduction factor ΔE_0 of 1. For $x = 1.0$ (R-factor = 0.0122) the model utilised a split first O shell with 5 O backscatterers at 2.11 (1) Å and 2 O backscatterers at 2.35 (3) Å, along with 2.5 Ti backscatters (with the 0.5 degeneracy contribution accounting for the 50% statistically occupied Ti site within zirconolite-2M) at 3.28 (1) Å, 2 Ca backscatterers at 3.65 (2) Å, 1 Hf backscatterer at 3.90 (3) Å, and 2 Ca backscatterers at 4.06 (3) Å. For $x = 0.5$ (R-factor = 0.0164), a very similar best fit model was used, however both Zr and Hf scattering paths were included, each with amplitude reduction factors (S_0^2)

scaled by a factor of 0.5, as degeneracies below 1 are known to produce unstable fits in Artemis. The model included 5 O backscatterers at 2.12 (1) Å, 2 O backscatterers at 2.35 (2) Å, 2.5 Ti backscatterers at 3.25 (2) Å, 2 Ca backscatterers at 3.49 (4) Å, 0.5 Hf backscatterers at 3.70 (3) Å, 0.5 Zr backscatterers at 3.47 (3) Å, and 2 Ca backscatterers at 4.16 (4) Å. For $x = 0.1$ (R-factor = 0.0115), a narrower Hanning window function was used due to the reduced signal to noise ratio from the Hf L₃-edge (low Hf concentration). This resulted in fewer scattering paths being included to prevent over-parameterising and hence over-constraining the model within the fitted window. While ideally, a similar model would be used between all compositions, this compromise was required to produce an acceptable best fit model. The paths included were 5 O backscatterers at 2.12 (1) Å, 2 O backscatterers at 2.35 (3) Å, and 2.5 Ti backscatterers at 3.27 (1) Å.

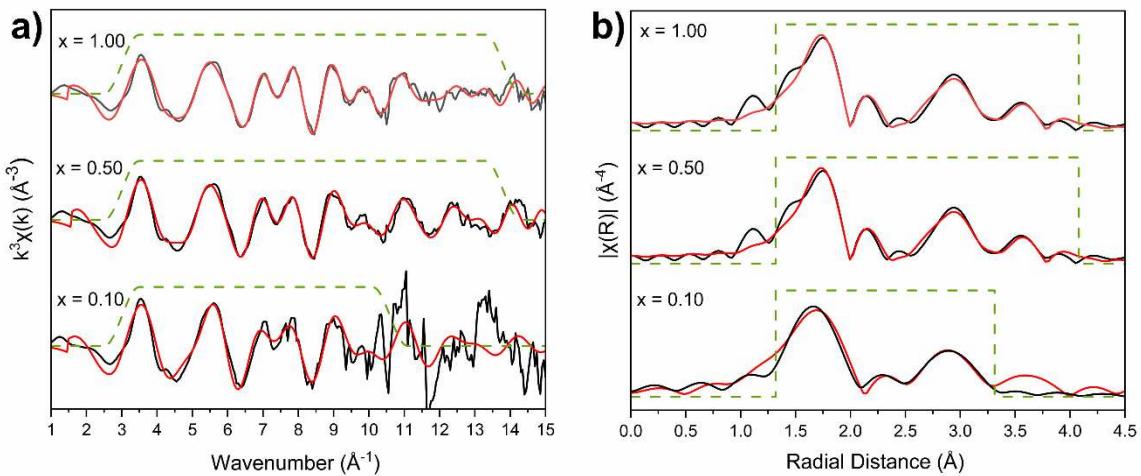


Fig. 3 a. Hf L₃ k^3 weighted EXAFS. b. Fourier transform of the k^3 -weighted EXAFS. Black lines are data, red lines are best fit models, green dashed lines show the Hanning window function.

Table S2 summarises the parameters used to produce the discussed fits. All three fits use a scattering model that corresponds well to the known structure of zirconolite-2M giving confidence to the outputted atomic positions and resulted in low R-factors (< 0.02) indicating the quality of the fit is strong. For all three compositions the total degeneracy for the first oxygen shell around Hf⁴⁺ was found to be 7. Bond valance sums (b.v.s.) were calculated for the first oxygen shell of Hf⁴⁺, which were found to be acceptably close to 4 v.u. (valance units) for each model, confirming chemical plausibility. First oxygen shell b.v.s. of each model are presented within **Table S2**, also shown are the percentage of variables used for fitting out of the available independent data points within the fitting windows, fits using >70% of available data points risk being over constrained. Overall, the results of these fits support the proposed solid solution mechanism whereby Hf⁴⁺ largely replaces Zr⁴⁺ in the 7-fold coordinated oxygen environment, although a small degree of Ti/Zr site mixing is expected in all cases. The radial distance of the oxygen scatters can be seen to increase slightly with Hf content, indicating that the first oxygen shell expands slightly when Zr⁴⁺ is replaced with Hf⁴⁺. Confidence in these results is given by the quality of the fits to the data.

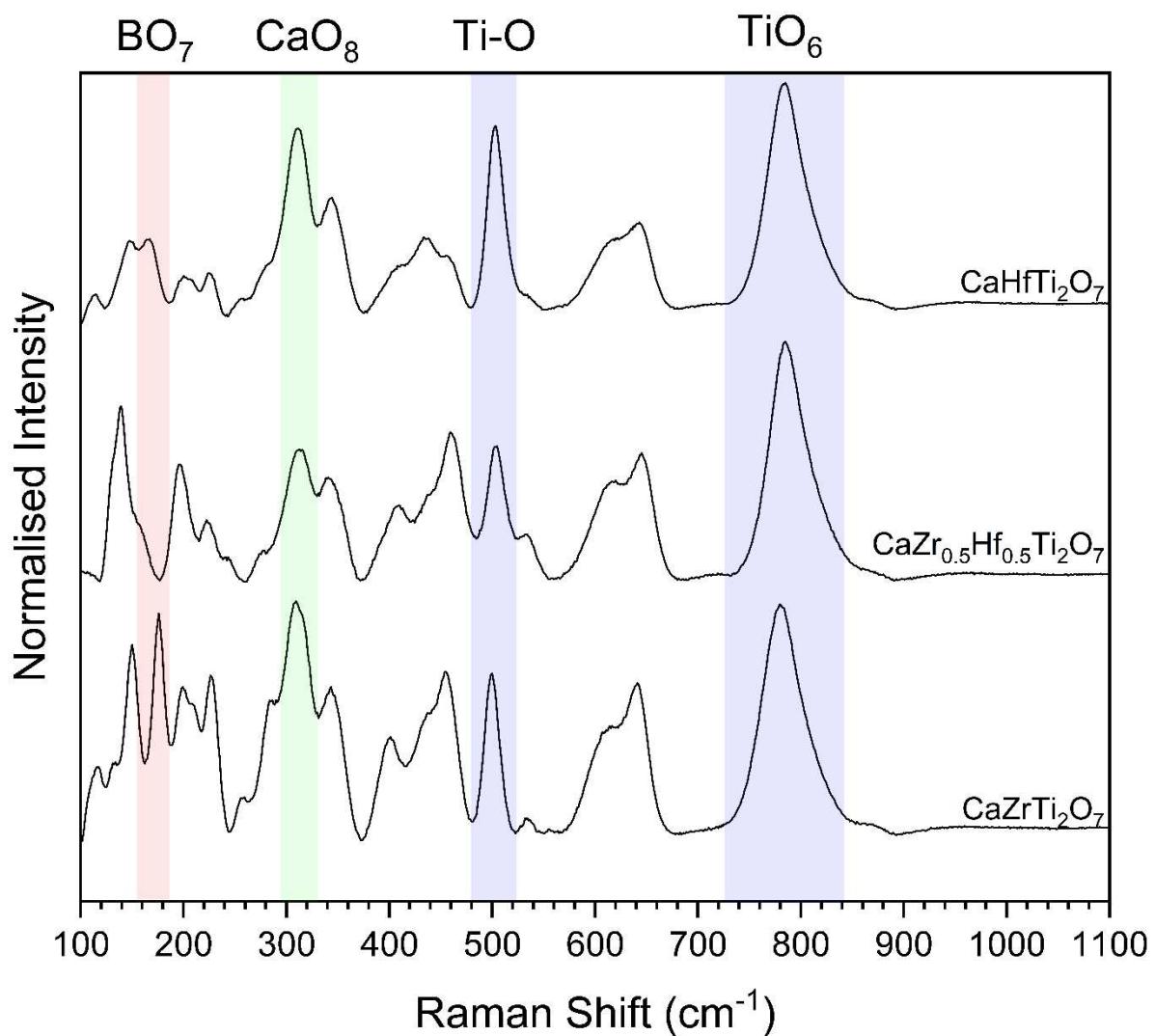


Fig. 4) Raman spectra for $\text{CaZrTi}_2\text{O}_7$, $\text{CaZr}_{0.5}\text{Hf}_{0.5}\text{Ti}_2\text{O}_7$ and $\text{CaHfTi}_2\text{O}_7$

Raman spectra (**Fig. 4**) showed a series of peaks with endmembers being particularly similar in observed vibrational modes. Whilst the Raman spectra of zirconolite has not been formally assigned, the dominant 780 cm^{-1} peak, consistent with the symmetric stretching of TiO_6 polyhedra, is present across the series alongside the characteristic Ti-O torsional vibration at 500 cm^{-1} [10, 11]. The doublet of peaks at 615 cm^{-1} and 640 cm^{-1} are also present across all samples and are typical of zirconolite-2M Raman spectra [12, 13]. The peaks centred around 314 cm^{-1} , which is associated with the CaO_8 polyhedral vibrations, specifically those in the $250 - 380\text{ cm}^{-1}$ remain largely unchanged except for subtle broadening which can be attributed to the poorer sinterability of HfO_2 [11]. The most significant changes in the Raman spectra are within the $100 - 240\text{ cm}^{-1}$ region, with the 179 cm^{-1} peak at the Zr endmember, typically associated with ZrO_7 vibration (or more generally BO_7 when considering the ABC_2O_7 general structure) red-shifting to 165 cm^{-1} with Hf. This indicates a lower frequency vibration, likely due to the larger atomic mass of the Hf ion. These data indicate a complete substitution of Zr for Hf whilst retaining the monoclinic 2M polytype of zirconolite and confidently demonstrate the dependency of the 179 cm^{-1} spectral line to the intrinsic vibration of ZrO_7 polyhedra.

The thermal properties of a ceramic wasteform govern how the material dissipates radiogenic decay heat from the decay of isotopes such as ^{239}Pu , and could therefore have an effect on material performance. An increased understanding of the thermal and mechanical properties, and such a dependence on composition, is necessary to predict the evolution of key wasteform properties in the disposal environment. This can be further influenced by factors such as the loading, design and geometry of waste packages. The thermal conductivity and diffusivity and specific heat capacity of samples corresponding to $x = 0, 0.5$ and 1 (i.e. $\text{CaZrTi}_2\text{O}_7$, $\text{CaZr}_{0.5}\text{Hf}_{0.5}\text{Ti}_2\text{O}_7$ and $\text{CaHfTi}_2\text{O}_7$) were measured by the Laser Flash method (**Fig. 5**). Both the thermal diffusivity (α) and conductivity (k) were observed to increase with elevated Hf^{4+} content (**Table 2**) although there is not entirely a clear compositional trend. A literature survey identified limited comparable data sets for the diffusivity and conductivity values for stoichiometric zirconolite and related phases, these are summarised in **Table 2**. Buykx [14] reported both thermal diffusivity (23 °C to 650 °C) and thermal conductivity (23 °C to 475 °C) for $\text{CaZrTi}_2\text{O}_7$ using the LFA method. The reported thermal conductivity and diffusivity values are both higher across the temperature range than those observed in the present work. Additionally, thermal conductivity was shown to increase slightly with temperature, a trend not observed here. Yin et al. [15] reported thermal conductivities measured by LFA at 25 °C for $\text{Ca}_{1-x}\text{Zr}_{1-x}\text{Nd}_{2x}\text{Ti}_2\text{O}_7$ ($0 \leq x \leq 0.3$), which ranged between 1.51 to 1.67 W/mK, with no apparent compositional trend. **Table 3** compiles the specific heat capacity (C_p) values for zirconolite systems reported in the literature, along with the results of the present work. Variations in LFA methodology may have contributed to the inconsistencies observed both within the existing literature, and in comparison, with the results of this study. The LFA method for insulating materials is sensitive to both the sample's dimension-to-thickness ratio, and coating procedure which is difficult to normalise. Moreover, the presence of the $(\text{Hf/Ti})\text{O}_4$ impurity phase in the $x = 1$ sample will likely impact a true measurement of conductivity/diffusivity, potentially due to variations in heat capacity and thermal expansion coefficients. Further work will seek to corroborate the influence of both composition and grain size on the thermal properties of zirconolite pellets, including those doped with realistic quantities of Pu surrogates.

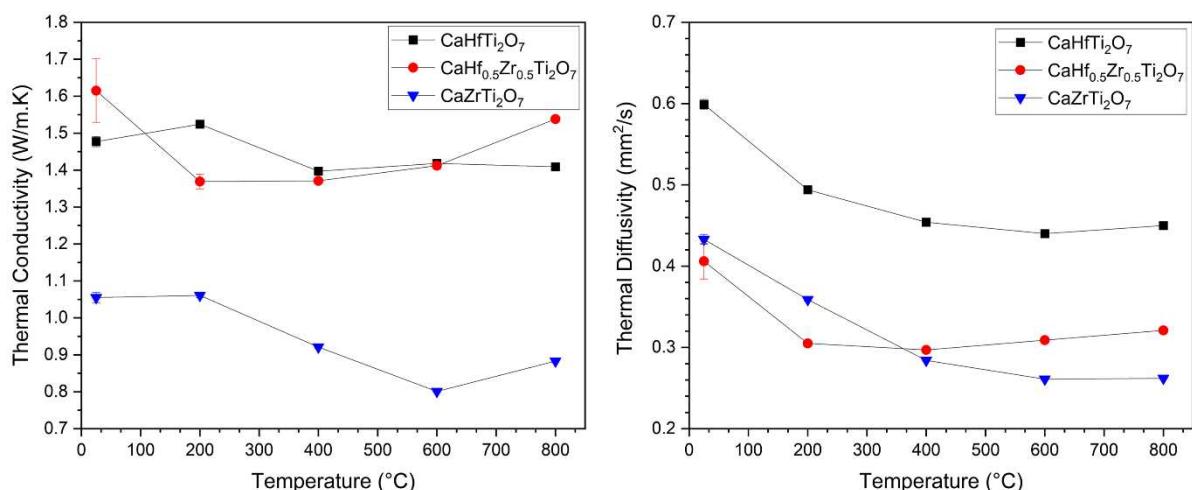


Fig. 5) Measured thermal diffusivity and conductivity for $x = 0, 0.50$ and 1.00 ceramics in the $\text{CaZr}_{1-x}\text{Hf}_x\text{Ti}_2\text{O}_7$ system

Table 2) Thermal diffusivity and conductivity values for zirconolite materials identified in the wider literature

Composition	Thermal Diffusivity (mm ² /s)	Thermal Conductivity (W/mK)	Temperature (°C)	Ref.
CaZrTi ₂ O ₇	0.43 ± 0.01	1.06 ± 0.01	25	
	0.36 ± 0.01	1.06 ± 0.01	200	
	0.28 ± 0.01	0.92 ± 0.01	400	Present work
	0.26 ± 0.01	0.80 ± 0.01	600	
	0.26 ± 0.01	0.89 ± 0.01	800	
CaZr _{0.5} Hf _{0.5} Ti ₂ O ₇	0.41 ± 0.02	1.62 ± 0.09	25	
	0.31 ± 0.01	1.37 ± 0.02	200	
	0.30 ± 0.01	1.37 ± 0.01	400	Present work
	0.31 ± 0.01	1.41 ± 0.01	600	
	0.32 ± 0.01	1.54 ± 0.01	800	
CaHfTi ₂ O ₇	0.60 ± 0.01	1.48 ± 0.01	25	
	0.50 ± 0.01	1.52 ± 0.01	200	
	0.45 ± 0.01	1.40 ± 0.01	400	Present work
	0.44 ± 0.01	1.42 ± 0.01	600	
	0.45 ± 0.01	1.41 ± 0.01	800	
CaZrTi ₂ O ₇	0.88 (0.044)	2.11 (0.25)	23	
	0.83 (0.037)	2.31 (0.28)	160	
	0.79 (0.040)	2.34 (0.28)	305	[14]
	0.79 (0.040)	2.42 (0.29)	475	
	0.85 (0.043)	-	650	
CaZrTi ₂ O ₇		1.57		
Ca _{0.95} Zr _{0.95} Nd _{0.1} Ti ₂ O ₇		1.50		
Ca _{0.90} Zr _{0.90} Nd _{0.2} Ti ₂ O ₇		1.67		[15]
Ca _{0.85} Zr _{0.85} Nd _{0.3} Ti ₂ O ₇	-	1.52	25	
Ca _{0.80} Zr _{0.80} Nd _{0.4} Ti ₂ O ₇		1.52		
Ca _{0.70} Zr _{0.70} Nd _{0.6} Ti ₂ O ₇		1.66		

Table 3) Specific heat capacity values for zirconolite and related Hf-solid solutions reported in the wider literature

Composition	Method	C _p (J / kg·K)	Temperature (°C)	Ref.
CaZrTi ₂ O ₇	LFA	0.593	25	Present work
CaZr _{0.5} Hf _{0.5} Ti ₂ O ₇	LFA	0.809	25	Present work
CaHfTi ₂ O ₇ + < 2wt% Hf/Ti Rich Impurities	LFA	0.448	25	Present work
CaZrTi ₂ O ₇	LFA	0.55	21.85 (295 K)	[14]
CaZrTi ₂ O ₇ + Excess ZrO ₂	Adiabatic Calorimetry	0.62	25	[16]
CaZrTi ₂ O ₇	Adiabatic Calorimetry	0.62	25	[17]
CaZr _{0.26} Hf _{0.74} Ti ₂ O ₇	Adiabatic Calorimetry	0.51	25	[18]
CaHfTi ₂ O ₇	Adiabatic Calorimetry	0.49	25	[18]
CaZrTi ₂ O ₇	GULP Potential Models	0.55	21.85 (295 K)	[19]
CaZrTi ₂ O ₇	Drop Calorimetry	0.62	25	[20]
CaZrTi ₂ O ₇	Drop Calorimetry	0.67	25	[21]

4 Conclusions

The UK separated Pu inventory could potentially be managed by a strategy of immobilisation proceeded by permanent geological disposal. The NDA seeks to further its understanding of the thermal and structural properties of potential ceramic wasteforms, for which zirconolite (CaZrTi₂O₇) is a candidate, inclusive of a further underpinning of the substitution behaviour of potential neutron absorbing additives within the zirconolite structure. This also constitutes a requirement to understand the isolated effects of cation substitution within specific lattice sites. To this end, the CaZr_{1-x}Hf_xTi₂O₇ system was fabricated and demonstrated complete solid solubility of Hf⁴⁺ at low-to-moderate concentration ($x \leq 0.60$) confirmed by powder X-ray diffraction, electron microscopy and Raman spectroscopy. Our data provide underpinning evidence that Hf⁴⁺ successfully substitutes for Zr⁴⁺ in the zirconolite structure, without promoting polytype transformations or (at low to moderate concentrations) resulting in phase segregation. Rietveld analysis of the diffraction data was consistent with Hf⁴⁺ occupying Zr⁴⁺ sites within the zirconolite structure. Complementary Hf L₃-edge EXAFS fitting of Hf-substituted zirconolite (reported within for the first time) were consistent with this substitution mechanism. The thermal diffusivity and conductivity were also observed to vary with Hf⁴⁺ content yet no clear compositional trends were identified, highlighting the requirement for further systematic study in this area using a larger data set with more granular compositional intervals. These data contribute to a more holistic understanding of the zirconolite system and will further inform potential solid solution regimes for materials containing Pu and neutron absorbing additives. Further work will seek to understand the thermal and structural

properties in wasteforms containing a realistic Pu surrogate fraction, with a view to better inform disposability.

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6 Author contributions

AM: Formal analysis, investigation, data curation, original draft preparation. AAF: Formal analysis, investigation, data curation. LTH: Formal analysis, investigation, data curation. MM: Formal analysis, investigation, data curation. IA: Formal analysis, investigation, data curation. AHR: Formal analysis, investigation, data curation. MCS: IA: Formal analysis, investigation, data curation. LRB: Conceptualisation, investigation, resources, supervision, project administration, funding acquisition.

7 Data Availability

The data to support the findings of this study are available from the corresponding author upon reasonable request.

8 Declarations

Conflict of interest: The authors declare no known conflicts of interest.

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