

# Multiobjective Eco-Driving Speed Optimization with Real-time Traffic: Balancing Fuel, NO<sub>x</sub>, and Travel Time

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## Abstract

Optimizing driving velocity profiles is crucial for reducing vehicle fuel consumption and NO<sub>x</sub> emissions without altering core vehicle components. While many studies have addressed eco-driving, most have focused solely on minimizing fuel consumption or have treated NO<sub>x</sub> emissions separately, resulting in distinct, non-integrated speed profiles, and have often neglected the influence of real-time traffic. To overcome these limitations, this paper introduces a novel Multiobjective Speed Profile Optimization (MO-SPO) framework for eco-driving that simultaneously minimizes fuel consumption, NO<sub>x</sub> emissions, and travel time while accounting for surrounding traffic. Two solution approaches are developed and compared: a two-phase Model Predictive Control (MPC) method and a newly proposed Deep Reinforcement Learning (DRL) method that directly integrates multiple objectives and real-time traffic constraints into the speed control policy.

Simulation results on a UK highway segment, with vehicle dynamics and engine characteristics derived from GT-SUITE data, demonstrate the benefits of the proposed framework. For instance, at one representative Pareto point, results indicate that the DRL approach achieves up to 10% lower fuel consumption and 16% lower NO<sub>x</sub> emissions compared to MPC-based methods while reducing travel time by approximately 5%. In addition, the DRL method maintained safer headway distances, offering more robust eco-driving strategies in dynamic traffic environments.

This work is the first to apply multiobjective optimization to generate integrated speed profiles that consider fuel, NO<sub>x</sub>, and travel time simultaneously under realistic traffic conditions.

**Keywords**— eco-driving speed profile optimisation; fuel consumption; NO<sub>x</sub> emission; multiobjective optimization; model predictive control; deep reinforcement learning

# 1 Introduction

Rapid urbanization and the steady increase in global vehicle ownership have heightened concerns about energy consumption and air pollution in the transportation sector (Placek, 2022). Although research and industry efforts have led to the development of more efficient powertrain systems and alternative-fuel vehicles (Pickl, 2019; Alam et al., 2010; Jia et al., 2016), conventional internal combustion engine (ICE) vehicles still dominate the roads and contribute significantly to environmental problems, particularly through emissions of nitrogen oxides (NO<sub>x</sub>). Prolonged exposure to NO<sub>x</sub> is linked to photochemical smog, acid rain formation, and particulate matter (PM), such as PM<sub>2.5</sub> and PM<sub>10</sub>, which pose direct risks to public health (Haakman et al., 2020; Chossière et al., 2017; Liu et al., 2022). Additionally, repeated studies indicate that vehicle-related emissions are a major source of air pollution, leading to an estimated 7,500 premature deaths annually in the UK alone (Ježek et al., 2015).

Besides the health and environmental concerns, the global rise in fuel prices and the finite nature of petroleum supply have consistently underscored the economic imperative to minimise vehicle fuel consumption (Pickl, 2019). As a result, numerous strategies have been explored to reduce both emissions and energy usage, ranging from traffic signal optimisation (Osorio and Nanduri, 2015) and cooperative driving (Kamal et al., 2022; Kong and Ma, 2024) to the development of hybrid and electric vehicle technologies. Among these, optimizing driving velocity profiles stands out as a highly cost-effective method, since it does not require retrofitting vehicles with new hardware or redesigning powertrains (Wang et al., 2022). Instead, it focuses on modifying driver behavior—speed, acceleration, braking—to achieve more efficient and cleaner operation.

A substantial body of literature has investigated velocity profile optimisation from various angles (Cui et al., 2021; Hamednia et al., 2022; Jia et al., 2022; Nie et al., 2022; Lot et al., 2025). Most of these studies concentrate on single-objective formulations, typically aiming to minimise fuel consumption under specific constraints such as road safety and rules. Although effective in reducing fuel consumption, these methods often overlook or only superficially address NO<sub>x</sub> emissions—an omission that is partly attributable to the complexities in accurately modelling and incorporating NO<sub>x</sub> in optimisation frameworks (Fernández-Yáñez et al., 2021). The incorporation of NO<sub>x</sub> is indeed technically more challenging, involving additional engine and aftertreatment parameters whose dynamic behavior is less straightforward to predict compared to fuel consumption. Consequently, comprehensive studies that jointly optimise fuel and NO<sub>x</sub> remain sparse.

A few exceptions exist. For instance, Fernández-Yáñez et al. (2021) investigated speed profile generation while considering both fuel and NO<sub>x</sub>, yet it treated each objective separately, yielding distinct profiles optimised exclusively for fuel or NO<sub>x</sub>. More recently, Yuval et al. (2023) employed multi-objective optimisation to integrate fuel consumption and NO<sub>x</sub> objectives simultaneously. While this represents a meaningful advance, it primarily addresses traffic-free conditions and is built on a shortest-path method (Ozatay et al., 2014) without incorporating real-world traffic flow. The absence of traffic considerations limits the real-life applicability of such solutions, since constraints like headway distance, dynamic speed limits, and surrounding vehicles' behaviors significantly influence feasible speed profiles.

70 Against this backdrop, our work aims to close the gap by proposing a multiobjective speed profile  
71 optimisation (MO-SPO) framework that jointly minimises fuel consumption, NO<sub>x</sub> emissions, and travel  
72 time while explicitly accounting for surrounding traffic. Travel time is included as a third objective to reflect  
73 practical stakeholder needs, since drivers and freight operators often balance economic, environmental, and  
74 time-efficiency goals. By framing these objectives within a multiobjective optimisation perspective, we  
75 avoid the pitfalls of blending incommensurable objectives (e.g., fuel vs. NO<sub>x</sub>) into a single scalar function  
76 (Ehrgott, 2005). Instead, we derive a Pareto front—a set of optimal solutions—where no objective can be  
77 improved without compromising at least one other. This approach provides a flexible decision-making tool  
78 for diverse user preferences, allowing stakeholders to select solutions that best align with their priorities.

79 From a methodological perspective, applying multiobjective optimisation to real-time speed generation  
80 in the presence of dynamic traffic is notably challenging. While traditional MPC can handle certain multi-  
81 objective problems by aggregating objectives into a single cost function, its sequential decision-making na-  
82 ture and reliance on finite-horizon optimization can limit its capacity to capture global trade-offs (Rawlings  
83 et al., 2017). In contrast, reinforcement learning — grounded in the convergence properties of Bellman’s  
84 equations—offers a holistic, global approach that naturally considers long-term interactions among multiple  
85 objectives, making it more suitable for truly complex multi-objective optimization scenarios. Therefore, we  
86 propose and compare two alternative approaches:

87 (i) **Two-Phase MPC:**

- 88 • **Phase-1:** Solve a traffic-free problem to obtain an “ideal” Pareto front that captures trade-offs  
89 between fuel consumption, NO<sub>x</sub>, and travel time in an uncongested environment.
- 90 • **Phase-2:** Integrate the sampled Pareto-optimal solutions into a real-time MPC framework, bal-  
91 ancing the objectives and constraints in the presence of surrounding traffic.

92 (ii) **Multiobjective Deep Reinforcement Learning (DRL):**

- 93 • Simultaneously considers real-time traffic dynamics and user-defined weight preferences for fuel,  
94 NO<sub>x</sub>, and travel time.
- 95 • Exploits the compatibility between multiobjective optimization and reinforcement learning (Mof-  
96 faert and Nowé, 2014; Li et al., 2021), enabling an agent to learn speed control policies that yield  
97 different Pareto-optimal solutions.

98 We demonstrate the practicality and effectiveness of these two approaches using a highway segment  
99 in southern England based on both simulated and real-world traffic data. The vehicle’s powertrain char-  
100 acteristics and emission rates are modelled based on GT-SUITE simulation data (Gamma Technologies),  
101 enabling a realistic and detailed representation of fuel consumption and NO<sub>x</sub> generation. Although the two-  
102 phase MPC method offers a comparatively more straightforward integration of multiobjective solutions into  
103 an MPC framework, our results indicate that multiobjective DRL provides greater flexibility and superior  
104 performance in simultaneously balancing the three objectives. However, its reliance on training data and

105 computational resources may limit its applicability to completely new traffic scenarios without additional  
106 training.

107 By shedding light on the strengths and limitations of these two approaches, this paper aims to contribute  
108 both methodologically and practically to the ongoing pursuit of greener transportation. The proposed frame-  
109 work illustrates how multiobjective optimisation can be leveraged to deliver not just a single solution, but an  
110 entire spectrum of speed profiles that can be tailored to different priorities and real-time traffic conditions.

111 To summarize, the primary innovations of our approach are summarized as follows:

- 112 • **Integrated Multiobjective Optimization:** Simultaneously minimizes fuel consumption, NO<sub>x</sub> emis-  
113 sions, and travel time, overcoming the limitations of single-objective approaches.
- 114 • **Real-Time Traffic Integration:** Explicitly incorporates real-world traffic dynamics to generate prac-  
115 tical, adaptive speed profiles.
- 116 • **Dual Methodology:** Proposes both a two-phase MPC and a multiobjective DRL approach, offering  
117 flexible solutions to eco-driving challenges.
- 118 • **Enhanced Performance:** The DRL method demonstrates significant improvements over MPC, vali-  
119 dated through UK highway cases.

120 The remainder of the paper is organised as follows. Section 2 provides an in-depth literature survey of  
121 eco-driving and optimal speed profile generation. Section 3 presents the vehicle modelling and the relation-  
122 ships between engine power, fuel consumption, and NO<sub>x</sub> emission. Section 4 introduces the multiobjective  
123 problem formulation and details the two proposed solution approaches. Section 5 discusses the experimen-  
124 tal setup, results, and a comparison of the approaches. Finally, Section 6 draws conclusions and outlines  
125 directions for future research, including advanced multiobjective reinforcement learning techniques and the  
126 incorporation of other emissions such as PMs and CO<sub>x</sub>.

## 127 **2 Related work**

### 128 **2.1 Conventional approaches for energy focused eco-driving**

129 Generating an optimised driving speed profile provides an effective way for reducing energy consumption  
130 and emission of pollutants. Various approaches have been proposed for eco-driving, in particular for gen-  
131 erating speed profiles that minimise total fuel consumption. Typical conventional solution approaches used  
132 for generating optimal speed profiles include analytical/exact methods (e.g., mathematical programming or  
133 dynamic programming) and optimal control methods (e.g., MPC and its variants).

134 The concept of “Look-ahead Control” has been widely used in some works (Eriksson et al., 2019), which  
135 demonstrates the advantage of using available information on future disturbances. For instance, Sharma  
136 et al. (2021) minimized fuel consumption of a heavy-duty vehicle by predicting the speed of the leading  
137 vehicle based on its uphill deceleration, achieving up to 8% fuel savings in real road scenarios. Other sim-  
138 ilar studies include Hellström et al. (2009) for minimising fuel consumption of heavy diesel trucks, Kamal

139 et al. (2022) for predicting the states of the preceding vehicle in urban scenarios at an adaptive look-ahead  
140 time step, etc. This advantage has been further applied in the cooperative driving scenario which employs  
141 aerodynamic drag reduction of platoons. For instance, Zhai et al. (2019) proposed an ecological cooper-  
142 ative look-ahead control strategy based on distributed model predictive control (DMPC) for a platoon of  
143 automated vehicles on freeways with varying slopes, combining eco-driving and platooning technologies to  
144 maximize fuel efficiency. Kong and Ma (2024) developed a cooperative eco-driving and energy manage-  
145 ment control strategy for heterogeneous vehicle platoons at multiple signalized intersections, leveraging a  
146 soft actor-critic (SAC)-based approach to optimize ecological velocity, safe inter-vehicle distance, and en-  
147 ergy efficiency while maximizing fuel economy and driving comfort. With the help of emerging vehicular  
148 communication technologies, a distributed optimal control scheme Liu et al. (2017) is proposed to achieve  
149 cooperative highway driving at the level of individual vehicles, which demonstrates the improvement of fuel  
150 economy and traffic efficiency.

151 For long-haul applications, two-stage hierarchical frameworks decouple global route planning from lo-  
152 cal speed optimization. For instance, Hamednia et al. (2022) proposed a bi-level optimization approach  
153 where gear selection is pre-optimized offline, and a nonlinear dynamic program is solved online. By lever-  
154 aging Pontryagin’s Maximum Principle and a model predictive control framework, the method achieves up  
155 to 11.60% energy savings compared to average driving cycles. Furthermore, integrating advanced ICT tech-  
156 nologies, such as cloud-based systems, can enhance real-time perception and decision-making. For example,  
157 Schlechtendahl et al. (2017) introduced the concept of control system as a service (CSaaS), enabling cloud-  
158 deployed optimization. Jia et al. (2022) developed an enhanced cloud-based predictive cruise control (PCC)  
159 system, combining deep learning-based traffic prediction with adaptive MPC to optimize speed profiles un-  
160 der varying traffic conditions. Their method, tested on a UK highway segment, demonstrated improved fuel  
161 efficiency for heavy-duty vehicles (HDVs) by leveraging real-time traffic data and advanced computational  
162 techniques. In addition, Nie et al. (2022) coupled gradient-based MPC for speed planning with MPC-based  
163 energy allocation in fuel cell hybrids, reducing traction power by 2.65% and battery degradation by 8.14%.  
164 Khalatbarisoltani et al. (2023) propose a two-level eco-driving strategy for Connected Fuel Cell Vehicles  
165 (C-FCVs) to optimize speed trajectories and powertrain operation, addressing computational challenges and  
166 real-time traffic complexities. The top layer integrates an LSTM-based traffic predictor and an MPC frame-  
167 work to optimize speed while considering hydrogen consumption, ride comfort, and traffic efficiency, while  
168 the bottom layer employs decentralized MPC to allocate power optimally between fuel cells and the battery.  
169 Simulation results demonstrate that this strategy enhances ride comfort, reduces hydrogen consumption by  
170 7.28%, and mitigates component degradation by 5.33%.

171 Drive cycle optimisation was also considered in some researches to minimise vehicle’s fuel consump-  
172 tion. Mensing et al. (2011) minimise a light-duty vehicle’s fuel consumption, which demonstrates a 16%  
173 decrease relative to the New European Driving Cycle (NEDC) while preserving travel time and adhering  
174 to speed regulations. Cui et al. (2021) proposes a Simulated Annealing (SA)-based method to develop  
175 driving cycles that better align with real-world speed-acceleration patterns, reducing errors by up to 23%  
176 compared to traditional methods and improving fuel consumption estimation accuracy. Additionally, Lot

177 et al. (2025) proposed an optimal control formulation for eco-driving in front-wheel drive electric vehicles,  
178 integrating driver preferences—such as desired speed, following distances, and smooth acceleration—with  
179 energy efficiency goals, using a simplified polynomial approximation of vehicle losses and relaxed regener-  
180 ative braking constraints. Testing on a 25km simulated journey shows 21% energy savings with only a 7%  
181 reduction in average speed, and 10–15% energy savings in car-following scenarios without speed reduction.

## 182 **2.2 Reinforcement learning based approaches**

183 Recent advancements in cloud computing and artificial intelligence have enabled the integration of machine  
184 learning techniques, particularly reinforcement learning (RL), with traditional optimization frameworks to  
185 address vehicle energy management challenges. Unlike conventional methods that often rely on heuristic  
186 rules or static models, RL-based approaches demonstrate unique capabilities in solving complex optimiza-  
187 tion and optimal control problems through data-driven exploration of state-action spaces. This subsection  
188 systematically reviews emerging RL methodologies and their applications across diverse energy optimiza-  
189 tion scenarios.

190 **Hierarchical Control Architectures** A prominent trend involves hierarchical frameworks that decom-  
191 pose energy management tasks into coordinated layers. Hu and Li (2021) developed an adaptive hierarchi-  
192 cal energy management system (EMS) combining deep deterministic policy gradient (DDPG) with equiv-  
193 alent consumption minimization strategy (ECMS) knowledge. This hybrid approach achieves near-optimal  
194 fuel consumption comparable to dynamic programming (DP) benchmarks while outperforming PID-based  
195 ECMS and rule-based strategies. The framework’s efficient exploration mechanism demonstrates particu-  
196 lar promise for real-world applications requiring safe online learning. Extending this concept, Dong et al.  
197 (2023) proposed a three-layer flexible eco-cruising strategy (FECS) featuring: 1) Dijkstra-based lane plan-  
198 ning considering long-term traffic impacts, 2) trigonometric speed optimization for energy savings, and 3)  
199 robust trajectory tracking with safety guarantees. Stochastic simulations reveal significant cost reductions  
200 in moderate-flow and free-flow traffic scenarios.

201 **Multi-Objective Optimization** Addressing the inherent trade-offs in vehicular energy systems, Yang et al.  
202 (2023) formulated hybrid electric vehicle energy management as a general-sum stochastic game solved  
203 through multi-agent RL (MARL). By modeling the engine-generator set and hybrid energy storage system  
204 as competing agents, their framework achieves Nash equilibrium solutions balancing fuel economy, battery  
205 degradation, and ultracapacitor state of charge. The MARL approach demonstrates superior performance  
206 over single-agent RL and DP in maintaining balanced objective optimization. Similarly, Xia Jiang and Li  
207 (2023) established a hierarchical Markov Decision Process (MDP) integrating car-following, lane-changing,  
208 and RL policies for electric connected vehicles. SUMO simulations at signalized intersections show sub-  
209 stantial energy savings while maintaining safe interactions with human-driven vehicles.

210 **Partial Observability and Complex Environments** For realistic traffic scenarios with limited informa-  
211 tion, Yang et al. (2024) developed autonomous eco-driving strategies using DDPG, PPO, and SAC algo-  
212 rithms combined with hybrid car-following models. Their framework enables connected and automated  
213 vehicles (CAVs) to optimize safety, energy efficiency, and ride comfort simultaneously when navigating  
214 signalized intersections. Comparative analyses reveal that the HybridSAC variant surpasses human drivers  
215 and traditional models (Trigo, IDM) across all performance metrics. Addressing partial observability, Zhu  
216 et al. (2024) framed multi-power-source CAV control as a Partially Observable MDP (POMDP) solved via  
217 proximal policy optimization (PPO). The developed controller reduces fuel consumption by 17% versus  
218 human drivers while maintaining comparable travel times.

219 **Integrated Decision-Making Architectures** Recent innovations emphasize unified frameworks for si-  
220 multaneous longitudinal and lateral control. Li et al. (2024b) introduced an attention-enhanced Twin De-  
221 layed DDPG (TD3) architecture incorporating multi-head self-attention and hybrid action representation.  
222 This integration achieves 42.18% stability improvement over prior methods while delivering 30.25% energy  
223 efficiency gains. Building on this, Fan et al. (2024) proposed a TD3-based eco-driving strategy combining  
224 lane preference scoring with longitudinal speed planning. Their SUMO simulations demonstrate synergistic  
225 benefits: longitudinal control alone reduces travel time by 7.94% or energy consumption by 18.15%, while  
226 integrated lateral decisions further decrease both metrics by 5.7% and 1.75% respectively.

227 **Customized Multi-agent and Deep Learning Techniques** Khalatbarisoltani et al. (2024) proposes a de-  
228 centralized health-conscious learning-based integrated thermal and energy management (ITEM) system for  
229 hybrid electric vehicles (HEVs) that optimizes fuel consumption, driver comfort, and battery lifetime using a  
230 multi-agent deep reinforcement learning (MADRL) framework with long short-term memory (LSTM). The  
231 MADRL approach outperforms rule-based and single-agent strategies, reducing battery degradation by 48%  
232 while maintaining cabin comfort. Experimental validation through hardware-in-the-loop (HIL) testing con-  
233 firms the reliability of the proposed method, with battery and cabin temperature deviations from simulation  
234 results remaining within 0.45 and 0.85 degrees, respectively. Jia et al. (2025) propose a predictive energy  
235 management system (PEMS) for fuel cell hybrid electric buses (FCHEBs) using a twin delayed deep deter-  
236 ministic policy gradient (TD3) algorithm, integrating future driving conditions and a predictive passenger  
237 model to optimize operational costs. Experimental results show that the TD3-based PEMS reduces com-  
238 prehensive operational costs by 5.92% compared to conventional TD3-based EMS with a fixed passenger  
239 count.

### 240 **2.3 Energy and emission focused eco-driving**

241 The analysed papers suggest a predominant focus on energy consumption when generating speed profiles for  
242 vehicles. Most of the reviewed literature emphasises energy use, sometimes considering travel time, while  
243 neglecting the assessment of NOx emissions due to its inherent technical complexities in quantification. In  
244 Fernández-Yáñez et al. (2021) explores speed profile generation considering both fuel and NOx, producing

245 separate optimal profiles for each objective. It shows that optimising for fuel does not necessarily reduce  
246 NO<sub>x</sub>, and the study achieves significant reductions in both fuel consumption and NO<sub>x</sub> emissions through  
247 dynamic programming.

248 Huang et al. (2021) investigate the impact of driver behavior on real driving emissions (RDE) using  
249 a portable emission measurement system with 30 drivers (15 novice, 15 experienced) driving the same  
250 diesel vehicle on the same route. Results show that novice drivers are generally more aggressive, leading to  
251 slightly higher mean fuel consumption (2%) and significantly higher NO<sub>x</sub> (17%) and PM (29%) emissions  
252 than experienced drivers. However, individual driver differences play a more significant role than experience  
253 level, suggesting that adopting eco-driving skills could substantially reduce fuel consumption and emissions  
254 for the worst-performing drivers.

255 Tang et al. (2021) present a strategy for managing energy and emissions based on a deep Q-network  
256 (DQN) as applied to dynamic programming (DP) as an optimal reference point. Two distributed deep re-  
257 inforcement learning (DRL) algorithms, namely asynchronous advantage actor-critic (A3C) and distributed  
258 proximal policy optimisation (DPPO), were employed to propose EMSs. Afterwards, emission optimisa-  
259 tion was incorporated to propose distributed DRL-based E&EMSs. Through simulation results, three control  
260 strategies based on deep reinforcement learning (DRL) show outstanding computational efficiency and near-  
261 optimal fuel economy. Compared to DQN, two distributed DRL algorithms improve learning efficiency by  
262 four times.

263 Guo et al. (2022) introduces an advanced energy management strategy for fuel cell hybrid vehicles based  
264 on a dueling-double-deep Q-network (D3QN). The primary challenge addressed is achieving an effective  
265 trade-off between system degradation and hydrogen consumption, while minimizing computational costs  
266 across diverse operational environments.

267 Yuan et al. (2022) quantify the fuel use and emission reduction potential of eco-driving for light-duty  
268 gasoline vehicles (LDGVs) using three million seconds of real-world driving data from 160 drivers across  
269 eight routes and 199 segments. Using a Vehicle Specific Power modal model, results show that route-level  
270 eco-driving can reduce fuel use and emissions by 6% to 40% compared to average driving. While eco-  
271 driving generally leads to simultaneous fuel and emission reductions, trade-offs exist, highlighting the need  
272 for strategic decision-making in LDGV eco-driving.

273 Jia et al. (2023) propose a novel cost-minimization energy management strategy that integrates thermal  
274 safety, degradation awareness of lithium-ion batteries, and fuel cell aging suppression to balance durabil-  
275 ity and hydrogen consumption. Using an enhanced self-learning stochastic Markov predictor for speed  
276 prediction, the strategy reduces battery aging by 34.8% and total operating costs by 12.3% compared to  
277 conventional methods.

278 Han et al. (2024) propose an energy management strategy that integrates a battery preheating tech-  
279 nique—supported by a high-precision electro-thermal-aging model, grid- and battery-powered preheating  
280 methods, and optimization algorithms (PSO and PMP)—to determine optimal preheating times and manage  
281 energy effectively. Simulation results demonstrate that at -20°C, preheating can reduce energy usage by  
282 approximately 44–48% compared to non-preheating scenarios.



283 Wang et al. (2024) introduces an advanced energy system combining a solid oxide fuel cell (SOFC) with  
284 compressed air energy storage CAES to generate compressed air, electrical power, and heat. The system’s  
285 performance was assessed and optimized using regression-based machine learning models, focusing on three  
286 key process variables: temperature, current density, and utilization factor.

287 The closest work relevant to our paper is given by Yuval et al. (2023), where an approach using mul-  
288 tiobjective optimisation was introduced, aiming to create optimised speed profiles while simultaneously  
289 considering fuel consumption, NOx emissions and travel time under traffic-free conditions. This method  
290 represents a more favourable approach for handling problems featuring multiple objectives that cannot be  
291 directly compared. Rather than combining these objectives into a single weighted metric, the proposed ap-  
292 proach offers a collection of non-dominated solutions (Pareto front). Each solution within this set reflects  
293 varying preferences concerning the importance of fuel, NOx and time. A standard shortest path model  
294 similar to Ozatay et al. (2014) was designed to implicitly address several constraints, and was solved using  
295 linear programming. By obtaining the Pareto front for the three objectives, this approach provides a range of  
296 options for users or driving guidance systems to select tailored strategies according to their specific require-  
297 ments. However, the study in Yuval et al. (2023) only considers traffic-free scenarios, which significantly  
298 narrows its applicability in real-world situations.

## 299 **2.4 Contributions of our work**

300 Our work distinguishes itself from the existing literature by addressing a critical gap: while many eco-  
301 driving studies focus solely on fuel consumption or treat NOx emissions separately—often overlooking  
302 the impact of real-time traffic—our paper presents the first multiobjective framework that optimizes speed  
303 profiles for fuel consumption, NOx emissions, and travel time in an integrated manner. Unlike conven-  
304 tional approaches, which typically generate isolated or non-integrated speed profiles using methods such  
305 as dynamic programming, MPC, or even single-objective reinforcement learning, our Multiobjective Speed  
306 Profile Optimization (MO-SPO) framework incorporates both a two-phase MPC and a novel DRL method  
307 that explicitly account for dynamic traffic constraints.

## 308 **3 Vehicle modelling**

309 In this part, we present the longitudinal vehicle dynamics model, along with employing simulated data to  
310 establish connections between engine power, fuel usage, and NOx emissions. By considering the vehicle’s  
311 dynamics, the power output can be precisely computed by factoring in the road slope, road condition, and  
312 the driver’s actions, indicated by changes in speed over a specific duration and the resulting acceleration.

### 313 **3.1 Vehicle dynamics**

314 In our research, we utilize a vehicle’s longitudinal dynamics model, following the convention from previous  
315 work such as Ozatay et al. (2014); Jia et al. (2022); Fernández-Yáñez et al. (2021); Yuval et al. (2023).

316 We use  $M_e$  to denote the effective mass of the vehicle, which accounts for both the vehicle's actual mass  
 317 and the rotational inertia of its wheels. The term  $\frac{dv}{dt}$  represents the vehicle's acceleration, describing the  
 318 rate of change of its velocity  $v$  over time. The forces acting on the vehicle include  $F_{eng}$  for the tractive  
 319 force generated by the engine,  $F_{brk}$  for the braking force,  $F_{rol}$  for the rolling resistance force,  $F_{aro}$  for the  
 320 aerodynamic resistance force, and  $F_{grd}$  for the road grade resistance force. The rolling resistance force  $F_{rol}$   
 321 is calculated using the vehicle mass  $M_v$ , gravitational acceleration  $g$ , rolling resistance coefficient  $C_r$ , and  
 322 the cosine of the road gradient  $\theta(t)$ . The aerodynamic resistance force  $F_{aro}$  depends on the air density  $\rho$ ,  
 323 frontal area  $A_f$ , aerodynamic drag coefficient  $C_d$ , and the square of the vehicle's speed  $v(t)$ . The road grade  
 324 resistance force  $F_{grd}$  is determined by the vehicle mass  $M_v$ , gravitational acceleration  $g$ , and the sine of the  
 325 road gradient  $\theta(t)$ . Finally, the effective mass  $M_e$  incorporates the vehicle mass  $M_v$  and the rotational inertia  
 326 of the wheels, calculated using the number of wheels  $N_w$ , rotational inertia of each wheel  $J_w$ , and wheel  
 327 radius  $R_w$ . The complete model reads,

$$M_e \frac{dv}{dt} = F_{eng} - F_{brk} - F_{rol} - F_{aro} - F_{grd}. \quad (1)$$

$$F_{rol} = M_v g C_r \cos(\theta(t)). \quad (2)$$

$$F_{aro} = \frac{1}{2} \rho A_f C_d v(t)^2. \quad (3)$$

$$F_{grd} = M_v g \sin(\theta(t)). \quad (4)$$

$$M_e = M_v + N_w \frac{J_w}{R_w^2}. \quad (5)$$

332 The vehicle's resulting force can be straightforwardly calculated by applying Eq (1) to (5). The term  
 333 representing the overall force generated by the vehicle, denoted as  $F_{veh} := F_{eng} - F_{brk}$ , is established. To  
 334 calculate the tractive force  $F_{eng}$  and braking force  $F_{brk}$ , we operate under the assumption that efficient driving  
 335 avoids simultaneous use of throttle and brake, a premise found in various pertinent studies like Fernández-  
 336 Yáñez et al. (2021) and Yuval et al. (2023). This assumption assumes that at any given time, either  $F_{eng}$  or  
 337  $F_{brk}$  must be zero, determined as follows: When  $F_{veh} \geq 0$ , then  $F_{eng} = F_{veh}$  and  $F_{brk} = 0$ ; if  $F_{veh} < 0$ , then  
 338  $F_{eng} = 0$  and  $F_{brk} = F_{veh}$ .

339 After determining the tractive force  $F_{eng}$ , we establish the engine power  $P_{eng}$  using the predetermined  
 340 vehicle specifications. Subsequently, fuel consumption and NOx emissions are derived from this engine  
 341 power. We will now elaborate on this process.

### 342 3.2 Fuel and NOx rate functions based on simulation

343 Based on of the simulated vehicle, we applied a third-order polynomial fit to establish the relationships  
 344 between NOx rates  $\dot{m}_N$  and engine power  $P_{eng}$ , and a first-order polynomial fit was used to simulate between  
 345 fuel  $\dot{m}_f$  and engine power  $P_{eng}$ . These relationships are derived from simulation data obtained through  
 346 experiments conducted using the GT-SUITE (Gamma Technologies) package. Appendix A1 elaborates the  
 347 simulation environment and vehicle modules used for deriving such relationships.

348 In this study, the GT-SUITE powertrain and emission model parameters were adopted from the rigor-  
 349 ously validated work of Gao et al. (2021). Their validation process included experimental comparisons un-  
 350 der diverse driving conditions, such as the Worldwide Harmonized Light Vehicles Test Cycle (WLTC), and  
 351 covered critical scenarios like cold-start emissions, SCR/ACCT system efficiency, and thermal dynamics of  
 352 after-treatment systems. Specifically, fuel consumption and NOx emission simulations were benchmarked  
 353 against experimental data, showing strong agreement (e.g., minor deviations in NOx rates and fuel con-  
 354 sumption trends). By leveraging this pre-validated model, we ensure that our eco-driving analysis reflects  
 355 real-world powertrain and emission behaviors across the operational scenarios examined in this work.

356 For NOx, the relationship is:

$$\dot{m}_f = \alpha_1 P_{eng}^3 + \alpha_2 P_{eng}^2 + \alpha_3 P_{eng} + \alpha_4, \quad P_{eng} \geq 0, \quad (6)$$

357 where  $\alpha_1 = 9.207 \times 10^{-20}$ ,  $\alpha_2 = 1.663 \times 10^{-14}$ ,  $\alpha_3 = 2.076 \times 10^{-10}$ , and  $\alpha_4 = 4.204 \times 10^{-7}$ . The  $R^2$  of the  
 358 fitting is 0.97.

359 For fuel, the relationship is:

$$\dot{m}_N = \beta_1 P_{eng} + \beta_2, \quad P_{eng} \geq 0, \quad (7)$$

360 where  $\beta_1 = 5.937 \times 10^{-8}$ ,  $\beta_2 = 0.0001002$ . The  $R^2$  of the fitting is 0.94.

361 The situation of negative engine power (i.e.,  $P_{eng} < 0$ ) did not happen in our experiments, since  $F_{eng} \geq 0$   
 362 and  $v(s) \geq 0$  always hold. If it is to be included, as in several other research cases (Rakha et al., 2011;  
 363 Wang and Rakha, 2017), a common practice is to set an additional condition such that  $\dot{m}_f = \alpha_0$  and  $\dot{m}_N = \beta_0$   
 364 if  $P_{eng} < 0$ , which can be easily incorporated into our model if needed. Based on Eq (6) and (7), the  
 365 static relationships of fuel consumption and NOx emissions with both zero and varying road grades while  
 366 maintaining a constant vehicle speed are illustrated in Figure 1. Note that since the road grade typically  
 367 varies along the observed journey section, these static relationships provide only idealised results.

## 368 4 Problem formulation and two alternative solution approaches

369 In this section, we first introduce the fundamentals of multiobjective optimisation and the overall speed  
 370 profile generation problem as an optimal control problem. We then delve into the two alternative solution  
 371 approaches both offering innovative ways to tackle the challenge of simultaneously optimising fuel con-  
 372 sumption, NOx emissions, and travel time considering surrounding traffic. The first approach is based  
 373 on traditional optimisation and control. It divides the problem into two phases, applying multiobjective  
 374 optimisation in a traffic-free scenario and then using model predictive control to address real-time traffic  
 375 scenarios. The second approach combines multiobjective deep reinforcement learning with real-time traffic  
 376 considerations, allowing for direct weighting of preferences to obtain optimised speed profiles. Through  
 377 these approaches, we aim to enhance eco-driving strategies and promote more sustainable and efficient  
 378 transportation solutions.

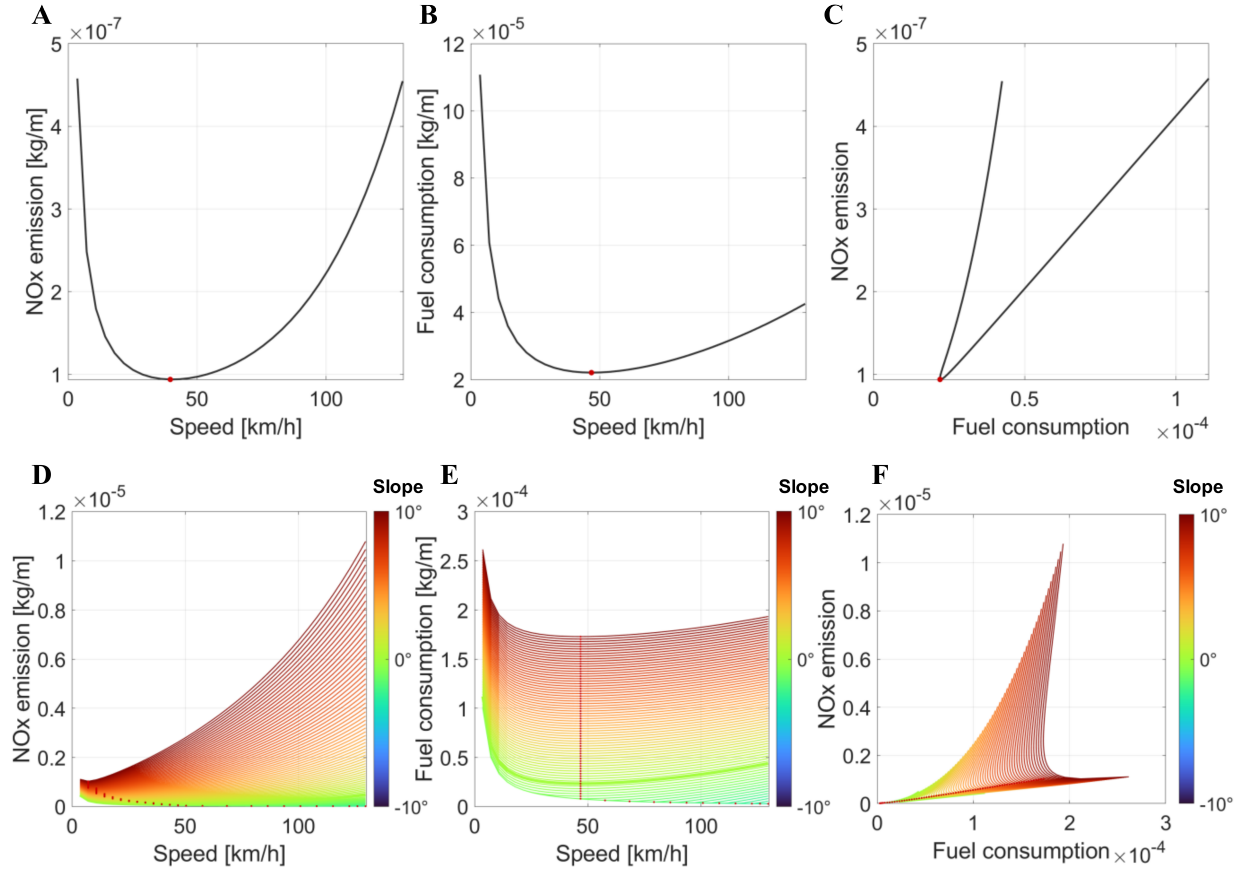


Figure 1: Investigating the relationship between NOx emissions and fuel consumption at a constant vehicle speed and varying road gradients. A-C: Fuel consumption (A) and NOx emissions (B) are examined with respect to a constant vehicle speed on a flat road. The relationship between fuel consumption and NOx emissions is shown in C. The red dots indicate the minimum values. D-F: Similar analyses to A-C are conducted, but with a range of constant road slopes from  $-10^\circ$  to  $10^\circ$ .

#### 379 4.1 Multiobjective optimisation

380 Multiobjective optimisation (Ehrgott, 2005) is a technique used to handle problems with multiple, often  
 381 incomparable, objectives. Instead of seeking a single optimal solution, it aims to find a set of solutions  
 382 known as the Pareto front, where no other solution can improve one objective without sacrificing another.  
 383 This approach provides decision-makers with a range of trade-off options, allowing them to select the most  
 384 suitable solution according to their preferences and requirements.

385 The modelling of multi-objective optimization for eco-driving is of paramount importance due to the  
 386 diverse and often conflicting preferences of users, as well as the inherent uncertainties in real-world driving  
 387 scenarios (Li et al., 2024a; Chen et al., 2018). Traditional eco-driving strategies typically prioritize single  
 388 objectives, which may not adequately address the multifaceted priorities of drivers. For instance, while some  
 389 drivers may prioritize energy efficiency, others may place greater emphasis on minimizing travel time or en-  
 390 hancing driving comfort. This paper underscores the necessity of integrating multiple objectives, including

391 fuel consumption, NOx emissions, and travel time, into a cohesive framework to deliver tailored eco-driving  
 392 recommendations. Additionally we highlight the critical role of accounting for real-time dynamics in traffic  
 393 conditions, where the unpredictable behaviors of leading vehicles can significantly influence energy effi-  
 394 ciency, NOx emission and travel time. Addressing these complexities is crucial for the widespread adoption  
 395 of eco-driving practices, where real-time adaptability and user satisfaction are key to achieving both envi-  
 396 ronmental and operational goals.

397 Let there be  $K$  distinct objectives, each representing an aspect to be minimized and denoted by  $z_k(x)$ ,  $k =$   
 398  $1, \dots, K$ , and these objectives are not directly comparable:

$$\text{minimize } \{z_1(x), z_2(x), \dots, z_K(x)\}. \quad (8)$$

399 Solution  $x$  is said to *dominate* solution  $x'$  if  $x$  is better than or the same as  $x'$  for all objectives, i.e.,  $z_k(x) \leq$   
 400  $z_k(x')$ ,  $\forall k = 1, \dots, K$ , and there exists at least one objective where  $x$  is strictly better than  $x'$ , i.e.,  $\exists k : z_k(x) <$   
 401  $z_k(x')$ . A non-dominated (efficient) solution refers to a feasible solution within a set that is not surpassed by  
 402 any other feasible solutions. The collection of all these non-dominated solutions is termed the Pareto-optimal  
 403 set. The boundary delineated by the points derived from this Pareto-optimal set is known as the Pareto front  
 404 (frontier). In multiobjective optimisation problems, the goal is to discover a diverse set of solutions situated  
 405 along this Pareto front. Common methods used to generate a Pareto front include techniques like weighted  
 406 sum,  $\epsilon$ -constraint, and weighted metric methods (Ehrgott, 2005).

## 407 **4.2 Speed profile generation as an optimal control problem**

### 408 **4.2.1 Original optimal control problem**

409 In this section, we outline the overall optimal control problem focused in our research. The aim is to generate  
 410 a speed profile that minimises specific objectives throughout a total distance travelled, denoted as  $S$ . As the  
 411 longitudinal model operates within the spatial domain, we apply the following domain transformations:  
 412  $dt = \frac{ds}{v(s)}$  and  $\frac{dv}{dt} = \frac{dv}{ds} \frac{ds}{dt} = \frac{dv}{ds} v$ , in a way that the distance travelled  $s$  becomes an independent variable  
 413 and  $\dot{m}(t)dt = \frac{\dot{m}(s)}{v(s)} ds$  corresponds to a rate  $\dot{m}(t)$  originally measured with respect to time. When the travel  
 414 velocity  $v(s)$  is known, the engine power ( $P_{eng}(s) = \frac{F_{eng}}{v(s)}$ ) can be exclusively determined using Eq (1)–(5)  
 415 provided that the velocity and acceleration are identifiable. Subsequently, the fuel consumption and NOx  
 416 emission rates can be computed using Eq (6) and (7). Three objectives are identified in our multiobjective  
 417 optimisation framework:

418 (i) Total fuel consumption:  $J_f = \int_0^S \frac{\dot{m}_f(P_{eng}(s))}{v(s)} ds$ ,

419 (ii) Total NOx emission:  $J_N = \int_0^S \frac{\dot{m}_N(P_{eng}(s))}{v(s)} ds$ , and

420 (iii) Total travel time:  $J_T = \int_0^S \frac{1}{v(s)} ds$ .

421 Our goal is to minimise the three objectives while taking various preferences into account:

$$\text{minimize } \{J_f, J_N, J_T\}. \quad (9)$$

422 As per convention, necessary normalisation is needed for the three objectives in Eq (9) in an multiobjec-  
 423 tive optimization context. In our MO-SPO framework, we adopt the weighted sum method, one of the most  
 424 widely used techniques (Ehrgott, 2005). This approach assigns a weight to each objective and combines  
 425 them into a single objective function. By systematically varying the weights, different regions of the Pareto  
 426 frontier can be explored as comprehensively as possible. Specifically, the objective function is formulated  
 427 as,

$$J = w_f J_f + w_N J_N + w_T J_T, \quad w_f + w_N + w_T = 1 \quad (10)$$

428 where  $w_f, w_N$  and  $w_T$  are the weights associated with fuel, NOx and time objectives respectively. In addi-  
 429 tion to the objectives, the following constraints are included into our model to guarantee practical driving  
 430 scenarios in real-world.

431 The speed is restricted within the range of minimum speed limit  $v_{\min}$  to maximum speed limit  $v_{\max}$  for  
 432 all velocities  $v(s)$ . This range ensures adherence to legal speed limits on the motorway. Additionally, a lower  
 433 bound may be included if specified by the local traffic authority. The vehicle’s acceleration is confined within  
 434 the range of maximum acceleration limit  $-a_{\max}$  to  $a_{\max}$  for all velocities  $v(s)$ . This limitation is implemented  
 435 to prioritise the safety and comfort of the driver and passengers (Table 1). The initial and final states of the  
 436 journey entail the vehicle being stationary, indicated by the conditions  $v(0) = v(S) = 0$ . Standing condition  
 437  $\frac{dv}{dt} \neq 0, \forall v = 0$  is imposed such that when the speed reaches zero, the acceleration must not be zero to prevent  
 438 the vehicle from remaining stationary indefinitely. When a vehicle navigates through traffic, its movement  
 439 is influenced by the presence and behaviour of other vehicles nearby. These neighbouring vehicles create  
 440 constraints that impact how the vehicle can manoeuvre or accelerate, making it essential to consider these  
 441 limitations when planning or controlling its movement.

442 We denote the above constraints as a constraint set  $\mathcal{D}$ . Depending on the specific requirements, more  
 443 constraints apart from the above ones can be included into  $\mathcal{D}$ . Note that our driving model focuses on mo-  
 444 torway conditions and does not account for signal stop points. Nevertheless, these can be readily integrated  
 445 into the model depending on the chosen settings.

#### 446 4.2.2 Discretized optimal control problem based on road position

447 Similar to Ozatay et al. (2014) and Jia et al. (2022), the total distance  $S$  is discretised into  $Q$  equal intervals  
 448  $\Delta s = S/Q$ . This allows a variety of approaches, such as shortest path, MPC and DRL to be applied in prac-  
 449 tically solving the original optimal control problem. We further make the assumption that the acceleration  
 450 remains unchanged within each interval  $i = 1, \dots, Q$ , and denote it as  $a_i$ . Then the speed profile can be  
 451 derived by determining the start and end speed of each interval  $i$  (denoted as  $v_{1i}$  and  $v_{2i}$ ), or equivalently, by  
 452 determining the acceleration  $a_i = \frac{v_{2i}^2 - v_{1i}^2}{2\Delta s}$  of interval  $i$  if  $v_{1i}$  is given. Note that the time needed within interval

453  $i$  is  $\Delta t_i = \frac{2\Delta s}{v_{1i}+v_{2i}}$ . Therefore the fuel consumption and NOx emission incurred at interval  $i$  can be calculated  
 454 by  $\dot{m}_f(P_{eng}(i))\Delta t_i = \frac{2\dot{m}_f(P_{eng}(i))}{v_{1i}+v_{2i}}\Delta s$  and  $\dot{m}_N(P_{eng}(i))\Delta s = \frac{2\dot{m}_N(P_{eng}(i))}{v_{1i}+v_{2i}}\Delta s$  respectively, where  $P_{eng}(i)$  is the engine  
 455 power at interval  $i$  by applying Eq (1)–(5).

456 Three discretised objective terms on the distance domain can be further defined, corresponding to the  
 457 original objectives in (9):

458 (i) Total fuel consumption:  $J'_f = \sum_{i=1}^Q \frac{2\dot{m}_f(P_{eng}(i))}{v_{1i}+v_{2i}}\Delta s$ ,

459 (ii) Total NOx emission:  $J'_N = \sum_{i=1}^Q \frac{2\dot{m}_N(P_{eng}(i))}{v_{1i}+v_{2i}}\Delta s$ , and

460 (iii) Total travel time:  $J'_T = \sum_{i=1}^Q \frac{2}{v_{1i}+v_{2i}}\Delta s$ .

461 In a multiobjective optimisation framework, we aim to minimise the three objectives considering differ-  
 462 ent preferences:

$$\text{minimize } \{J'_f, J'_N, J'_T\}. \quad (11a)$$

$$\text{subject to } \mathcal{D}. \quad (11b)$$

463 The final objective after adopting weighted sum remains in the same form as in Eq (10).

464 We propose two alternative solution approaches to deal with the above multiobjective optimal control  
 465 problem in Sections 4.3 and 4.4 respectively.

### 466 **4.3 A two-phase approach using shortest path and MPC**

467 As our objective is to generate a speed profile based on real-time traffic conditions, it becomes imperative  
 468 to consider the influence of surrounding traffic, which sets it apart from traffic-free scenarios. MPC has  
 469 traditionally been an effective tool for addressing such real-time problems. However, when combined with  
 470 multiobjective optimisation, MPC encounters significant challenges, and despite considerable efforts made  
 471 in the past few decades, there is no satisfactory generic method to obtain exact or high-quality solutions  
 472 (Gambier and Badreddin, 2007; Bemporad and Muñoz de la Peña, 2009). Due to the successive computa-  
 473 tional nature of MPC, the results are often not Pareto optimal (Grüne and Stieler, 2017).

474 Considering the above challenges mentioned, we propose an approximate two-phase approach, striking  
 475 a balance between the “desirable” Pareto-efficient speeds obtained from the traffic-free condition (Phase-1)  
 476 and the adjusted speeds due to surrounding traffic, computed using an MPC model (Phase-2). In Phase-1,  
 477 in the absence of surrounding traffic, the speed profiles are ideally designed to minimise fuel consumption,  
 478 NOx emissions, and travel time, based on vehicle specifications and road geometry information. However,  
 479 these profiles may not be practical or entirely feasible due to the lack of surrounding traffic considerations.  
 480 In Phase-2, realistic solutions are generated by a conventional MPC model, accounting for other vehicles’  
 481 presence, while endeavouring to maintain speeds as close to those obtained in Phase-1 as possible. The  
 482 subsequent sections provide a comprehensive elaboration of both phases.

483 **4.3.1 Phase-1: traffic-free shortest path problem formulation**

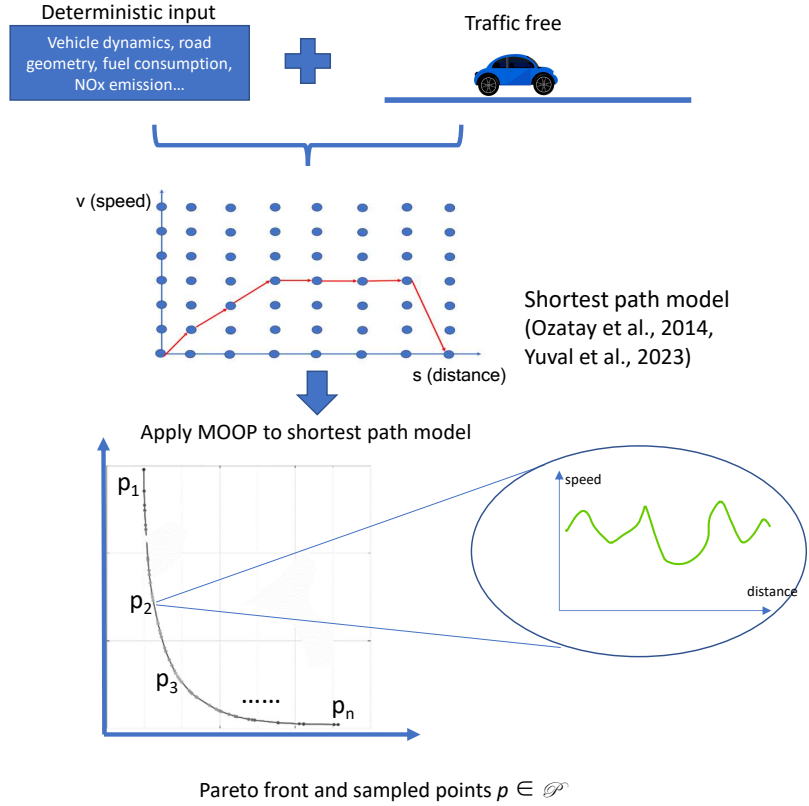


Figure 2: An illustration of Phase-1 where the traffic-free scenario is modelled as a shortest path problem and applied to a multiobjective optimization framework. Sampled points  $p_1, p_2, \dots, p_n \in \mathcal{P}$  correspond to different efficient speed profiles with respect to their own preferences.

484 In Phase-1, given the absence of surrounding traffic, the discretised multiobjective optimal control prob-  
 485 lem represented by (11) can be further reformulated as a deterministic shortest path problem (Ozatay et al.,  
 486 2014; Yuval et al., 2023), if the speed horizon is also discretised into  $[0, \Delta v, 2\Delta v, \dots, v_{max}]$ . This yields a short-  
 487 est path network defined over  $[0, \Delta s, 2\Delta s, \dots, S] \times [0, \Delta v, 2\Delta v, \dots, v_{max}]$ , where each node  $(s, v)$  in the network  
 488 represents a chosen speed  $v$  at a distance  $s$ , and an arc represents the costs (NOx, fuel and time) from one  
 489 node to another, i.e., how speed changes from one distance point to the next. This shortest path problem is  
 490 solvable using standard mathematical programming. The outcome of Phase-1 yields a Pareto front, illustrat-  
 491 ing various trade-offs among the preferred weight settings, where each point on the Pareto front corresponds  
 492 to a complete speed profile. A set of sampled points  $p \in \mathcal{P}$  will be collected from the Pareto front and be  
 493 used as reference points for Phase-2. For details in how to formulate the shortest path problem in the context  
 494 of generating speed profiles, see examples from Ozatay et al. (2014) and Yuval et al. (2023).



### 495 4.3.2 Phase-2: MPC problem considering surrounding traffic

496 In Jia et al. (2022), an MPC model is proposed to generate speed profiles that only minimise fuel consump-  
 497 tion considering surrounding traffic. Its objective function for an interval  $i$  and total prediction horizon  $n$   
 498 reads,

$$J(i) = \lambda_e \sum_{j=i}^{i+n-1} E_e(j)^2 + \lambda_k \sum_{j=i}^{i+n-1} (E_k(j) - \frac{1}{2} M_e v_d^2(j))^2 + \lambda_s \sum_{j=i}^{i+n-1} (E_e(j) - E_e(j-1))^2. \quad (12)$$

499 where the first term minimises the engine energy  $E_e$  (fuel), the second term minimised the deviation between  
 500 the actual speed (represented by kinetic energy  $E_k$ ) and the desired speed  $v_d$  and the third term minimises jerk  
 501 (represented by energy increment) to ensure driver’s comfort.  $\lambda_e$ ,  $\lambda_k$  and  $\lambda_s$  are the corresponding weights.

502 We have developed an MPC model based on Jia et al. (2022) to account for the surrounding traffic while  
 503 aiming to keep the speed profile as close as possible to the sampled Pareto solutions from Phase-1. A detailed  
 504 description of this MPC algorithm can be found in Appendix A3. Figure 3 provides an illustration of how our  
 505 Phase-2 operates: the MPC model is employed for generating vehicle speed profiles considering surrounding  
 506 traffic for each sampled points  $p \in \mathcal{P}$  from Phase-1. The vehicle’s dynamics accounts for various constraints  
 507  $\mathcal{D}$  including surrounding traffic (headway) and speed/acceleration limits. The MPC indirectly optimises the  
 508 three objectives (fuel, NOx and time) by minimising the deviation between  $v_d$  and the reference Pareto point  
 509  $p$ . The entire process is conducted over a finite distance, which is divided into discrete steps. The controller  
 510 predicts the vehicle’s future behaviour within the horizon, subject to the constraints  $\mathcal{D}$ . At each time step,  
 511 MPC solves an optimisation problem to find the optimal control input sequence. Then, the controller shifts  
 512 the horizon by one step and updates the information with new measurements.

513 It should be noted that we adopted a data-driven traffic predictive model for speed prediction which  
 514 applies the CNN-based deep learning method to capture spatio-temporal dependencies in traffic data (Jia  
 515 et al., 2022). The multi-view CNN processes multiple factors (e.g., traffic flow, speed) separately through  
 516 convolutional layers, fuses their outputs, and predicts traffic speed via fully connected layers. The model  
 517 uses a weighted loss function to balance contributions from different traffic factors. Predicted speeds are  
 518 transformed from the time domain to the space domain for use in predictive control systems, enabling real-  
 519 time speed optimization.

520 To realise the above, for each sampled Pareto point  $p \in \mathcal{P}$ , we set the desirable speed  $v_d$  in the MPC’s  
 521 objective function (see Jia et al. (2022)) dynamically depending on the speed of the front vehicle  $v_f$  and the  
 522 Pareto speed  $v_P(p)$  derived from Phase-1. Two strategies are designed to address the problem from different  
 523 aspects: a conservative MPC strategy (“MPC1”) and a balanced MPC strategy (“MPC2”).

524 **Conservative MPC strategy (MPC1):** Under this strategy, the new desirable speed  $v_d$  is calculated as  
 525 follows:

$$v_d = \begin{cases} v_P(p), & \text{if } v_P(p) \leq v_f, \\ v_f, & \text{if } v_P(p) > v_f. \end{cases} \quad (13)$$

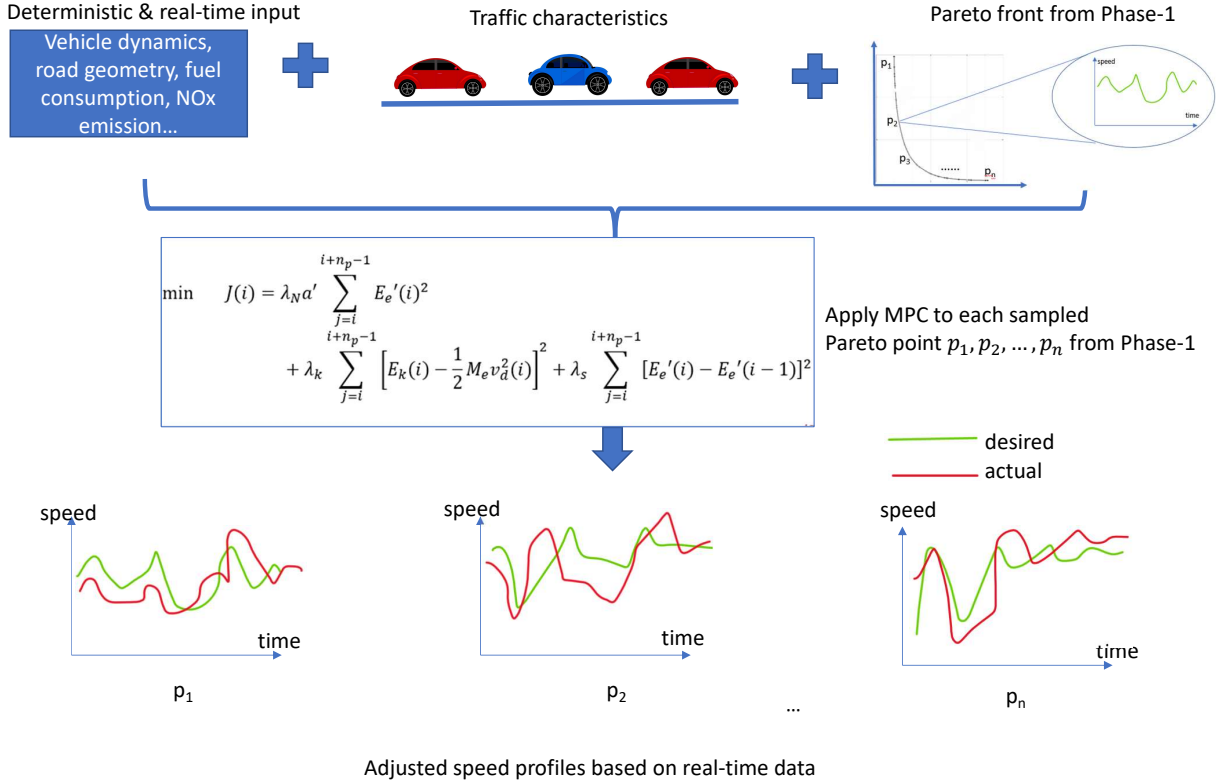


Figure 3: An illustration of Phase-2 where based on the sampled Pareto points  $p_1, p_2, \dots, p_n \in \mathcal{P}$  from Phase-1, the surrounding traffic is taken into account in an MPC model.

526 The justification for the conservative MPC tactic, as described in Eq (13), is that in order to maintain maximum safety, the speed of the targeted vehicle must not surpass that of the front vehicle at any given time.  
 527  
 528 Furthermore, the vehicle following the targeted one will regulate its speed in tandem with the targeted vehicle, and the whole set of traffic behind them will do likewise. Note that this strategy cannot guarantee that  
 529 the speed of the current vehicle will never exceed that of the preceding vehicle, as  $v_d$  can only be approached as much as possible in objective. However, this approach has the advantage that whenever the Pareto speed  
 530  $v_P(p)$  is less than the speed of the preceding vehicle  $v_f$ , the MPC will attempt to achieve  $v_P(p)$ , resulting in  
 531 solutions with higher quality in terms of the three objectives.  
 532  
 533

534 **Balanced MPC strategy (MPC2):** Since safety headway constraints are included in the MPC model (Jia et al., 2022), it is considered safe to occasionally allow the desired speed to be higher than the speed of the  
 535 front car. Therefore, in the balanced strategy, the desired speed is calculated as the average value of the  
 536 Pareto and front car speeds, i.e.,  
 537

$$v_d = \frac{v_P(p) + v_f}{2}. \quad (14)$$

538 This approach increases the likelihood of the current vehicle surpassing the front vehicle's speed when  
 539 prioritising minimisation of travel time. It provides more realistic speed profiles, but may result in lower

540 solution quality than “MPC1”, since the desired speed will only match the Pareto speed if  $v_P(p) = v_f$ .

#### 541 4.4 A deep reinforcement learning approach

542 Reinforcement learning (RL) enables agents to learn decision-making strategies for maximising cumulative  
 543 rewards in sequential processes (Sutton and Barto, 2018). Deep reinforcement learning (DRL) employs  
 544 multi-layer Artificial Neural Networks (ANNs) for training in simulated environments. Here, the agent  
 545 interacts with the environment, receives feedback on actions, and improves decision-making through trial  
 546 and error. This study focuses on continuously controlling the starting point’s acceleration in each section  
 547 to achieve a speed profile that addresses multiple diverse objectives. To address complex control tasks with  
 548 continuous state and action spaces, we use an actor-critic framework with the deep deterministic policy  
 549 gradient (DDPG) algorithm (Sutton and Barto, 2018). The actor-critic architecture, resembling a Generative  
 550 Adversarial Network, consists of two ANNs: the “critic” estimates state transition values, guiding decisions,  
 551 and the “actor” selects optimal actions based on critic feedback. The actor uses a Policy-based method for  
 552 high-dimensional and continuous action spaces, and the critic employs a Value-based method for efficiency  
 553 and stability. The iterative interaction in the actor-critic framework is depicted in Figure 4. The black lines  
 554 represent the predicting loop, while the red lines represent the training loop. The squares depict the agents  
 555 and the environment, and the ellipses represent the information flow. The red circle represents to update the  
 556 weights of ANNs for a given state-action pair.

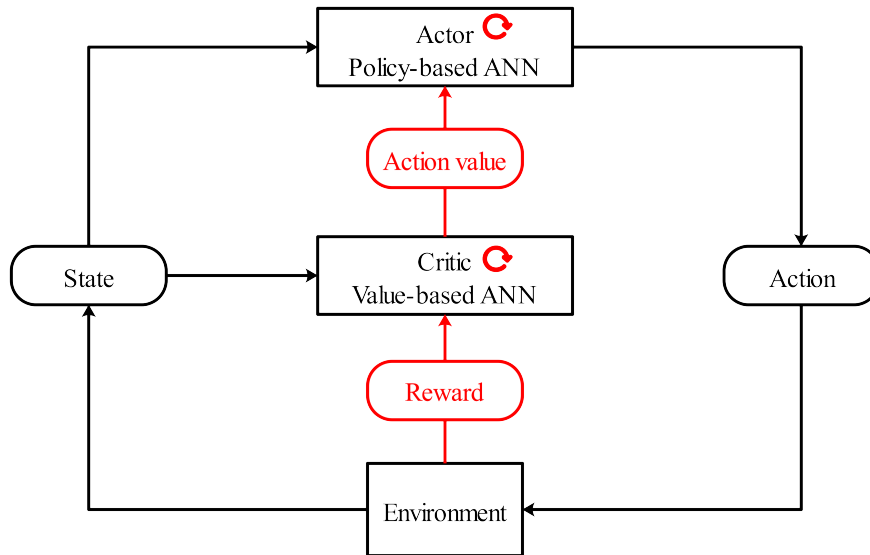


Figure 4: Actor-critic training framework

557 The DRL approach is shown in Figure 5. The state is formulated by traffic speed  $v_f$ , driving speed  $v$ ,  
 558 headway distance  $\delta$ , and gradient  $\theta$ . The action determines the speed variance  $a$ , which is a continuous  
 559 value, at the upcoming road section. Negative values indicate deceleration, while positive values indicate  
 560 acceleration. The action is constrained by the limits specified in Table 1, ensuring the agent’s acceleration or  
 561 deceleration stays within acceptable bounds during the control process. Consequently, the agent can adjust

562 its speed within the speed limit and efficiently navigate through the road section. The agent updates the  
 563 state at the beginning of each road section and receives the reward after traversing the section with the given  
 564 speed. The reward is formulated by combining the three objectives of the optimisation in Eq (11), namely  
 565 fuel consumption, NOx emissions, and travel time. These values are normalised and combined into the same  
 566 weighted objective. Due to the nature of minimisation, the reward is inversely proportional to the values of  
 567 fuel, NOx, and travel time.

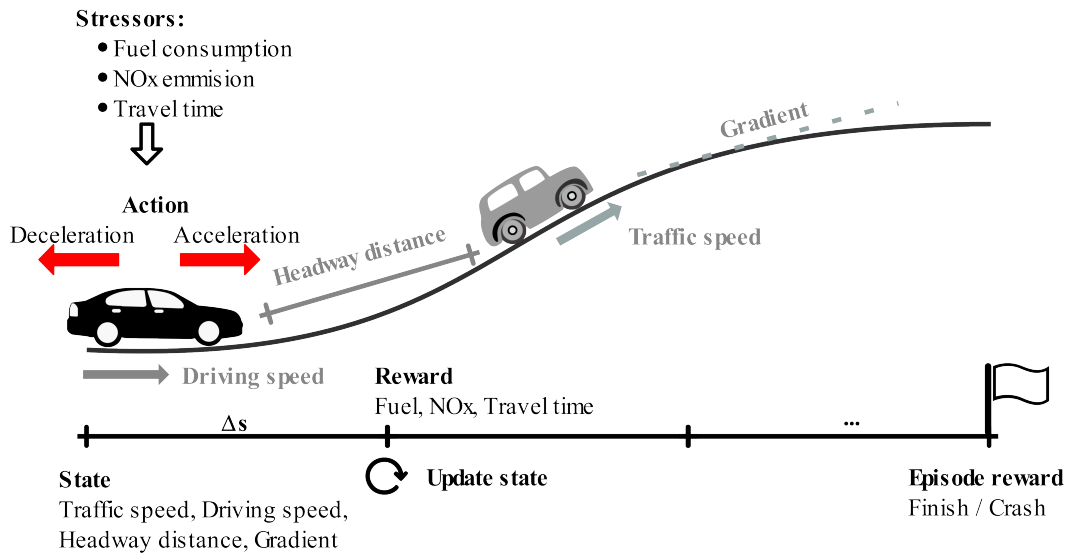


Figure 5: DRL framework for eco-driving with traffic flow

568 In this study, success is defined as the vehicle safely traversing the road without a crash, and failure  
 569 occurs when a crash happens. The step reward is provided after each action, but they don't distinguish  
 570 between success and failure. Increasing control accuracy results in more decision points, potentially leading  
 571 to sparse rewards before task completion. Too few penalties may reduce the agent's cautiousness, resulting  
 572 in numerous crashes in the initial stages of learning, hindering the ability to successfully complete the task.  
 573 Conversely, too large penalties may lead the agent to adopt overly conservative actions, such as driving  
 574 slowly to maintain a safe distance from the front car, which is not desired. Experiencing excessive failures  
 575 during training can lead the agent to adopt a conservative behaviour, often referred to as the *coward effect*  
 576 in reinforcement learning (Bakos and Davoudi, 2022). This is primarily attributed to the agent's exploration  
 577 of the environment resulting in infrequent successes. Over time, the agent begins to perceive the game  
 578 as consistently ending in failure. Consequently, its strategy shifts towards surviving longer rather than  
 579 optimising reward acquisition.

580 To prevent the agent from being stuck in local optimal solutions and to mitigate the coward effect, an  
 581 episode reward is designed each time the agent completes an episode, whether it is a failure or success.  
 582 The termination condition is determined by two standard criteria: (i) either the agent crashes the front  
 583 vehicle during the experiment (indicating failure) or (ii) the agent completes the entire journey through the  
 584 road (indicating success). When the agent fails, it receives a penalty, which is discounted by the length it

585 travelled. This means that the longer the agent travels before failure, the less severe the penalty. When  
586 the agent completes the task, it receives a reward, but the reward is discounted based on how the objective  
587 values achieved by the agent compare to the values derived from the ideal condition (representing traffic-  
588 free solution). This means that the agent receives a higher reward for achieving objectives closer to the ideal  
589 values. Accordingly, the agent receives an evaluation after termination based on its ending state, which is  
590 calculated by Eq (15).  $\gamma_+$  and  $\gamma_-$  are coefficients to balance the value of episode reward and step reward,  
591 which avoids the gradient vanishing during training.  $\beta_1$  is a parameter to control the discounting rate.  $Obj_I$  is  
592 the weighted sum of objectives derived from traffic-free solution, and  $Obj_E$  is that derived from this episode.  
593 The tendency of the episode reward is shown in Figure 6. The penalty curve (blue) follows an exponential  
594 shape, which penalises the agent more when the agent fails early, but imposes only a slight penalty if it fails  
595 near the end of the road. On the other hand, the reward curve (green) follows a linear shape, which uniformly  
596 increases as the objective becomes better. A linear-shaped function imparts a consistent and gradual reward  
597 as the agent performs better, thereby reducing the intricacy of stimulation and preventing the agent from  
598 getting trapped in local performance optima.

$$\text{Episode reward} = \begin{cases} \gamma_+ \times \frac{Obj_I}{Obj_E}, & \text{Finish} \\ \gamma_- \times \left( e^{\beta_1(\Sigma \Delta s - S)} - 1 \right), & \text{Failure} \end{cases} \quad (15)$$

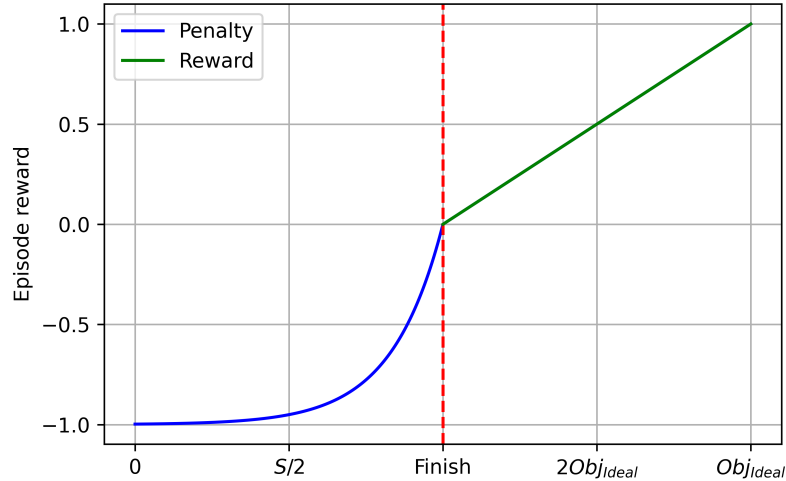


Figure 6: Episode reward under different termination states

599 The training process of ANN can be viewed as solving a parametric optimisation problem through  
600 stochastic gradient descent, which iteratively updates the parameters of ANN to minimise the loss function.  
601 The training process by DDPG algorithm follows the pseudo code in Algorithm 3 in Appendix A4.

602 The policy gradient method with time-difference error can be summarised with the following equations.  
603 A tuple  $(s_i, a_i, r_i, s_{i+1})$  represents the state, action, reward, and next state, respectively. First, compute the

604 target value  $y_i$  by the target critic-network  $Q_{target}$  with weight set  $\theta^{target\_critic}$  and target actor-network  $\mu$  with  
 605 weight set  $\theta^{target\_actor}$  by Eq (16).

$$y_i = r_i + \gamma Q_{target}(s_{i+1}, \mu(s_{i+1} | \theta^{target\_actor}) | \theta^{target\_critic}) \quad (16)$$

606 Here,  $\gamma$  is the discount factor, which represents how much importance is given to future rewards.

607 Then, calculate the loss function of critic network using the memory set containing  $N$  samples. This  
 608 is done by employing the mean square error as shown in Eq (17). Subsequently, the weights of the critic  
 609 network are updated using the gradient descent method with the gradient  $\nabla \mathcal{L}(\theta^{critic})$ .

$$\mathcal{L}(\theta^{critic}) = \frac{1}{N} \sum_i^N (Q(s_i, a_i | \theta^{critic}) - y_i)^2 \quad (17)$$

610 The loss function of actor network is defined as the negative mean of the expected Q-values for the  
 611 state-action pairs in the batch in Eq (18). This means that the actor seeks to minimise the negative Q-values,  
 612 effectively maximising the Q-values. Then, the gradient decent  $\nabla \mathcal{L}(\theta^{actor})$  is performed to update the  
 613 weight of actor network.

$$\mathcal{L}(\theta^{actor}) = -\frac{1}{N} \sum_i^N Q(s_i, \mu(s_i | \theta^{actor}) | \theta^{critic}) \quad (18)$$

614 After each training round, the target critic network is updated using a decay rate  $\tau$ . This update is  
 615 performed to prevent rapid changes in target Q-values, which can lead to unstable learning.

616 The action is selected following the  $\epsilon$ -greedy method where  $\epsilon$  is the explorative parameter. Before each  
 617 action is selected, a random number is generated according to a uniform distribution between 0 and 1. If the  
 618 random number is greater than  $\epsilon$ , the action with the highest probability is selected. Otherwise, an action  
 619 is selected randomly. For sufficient exploration at the initial process of the simulation,  $\epsilon$  is annealed in a  
 620 sigmoid shape as

$$\epsilon = \epsilon_{max} - \frac{\epsilon_{max} - \epsilon_{min}}{1 + e^{-\beta_2[(E-\beta_3)-\beta_4]}} \quad (19)$$

621 where  $\epsilon_{max}$  and  $\epsilon_{min}$  are the lower and upper bounds, respectively.  $\beta_2$ ,  $\beta_3$  and  $\beta_4$  are the parameters to control  
 622 the shape of annealing.  $E$  stands for the number of experienced episodes. The value of  $\epsilon$  decays with the  
 623 increasing of episode number.

624 The learning rate of the actor and critic ANNs is also decayed during iteration, following an exponen-  
 625 tial shape. The decaying learning rate ensures that the networks adapt to changing dynamics and avoids  
 626 overshooting or getting stuck in local minima during the learning process.

## 627 **5 Computational experiments**

### 628 **5.1 Experiment environment and dataset**

629 In this section, we present the experimental results obtained by applying both the two-phase approach  
630 (shortest-path + MPC) and the novel DRL-based approach to generate optimised speed profiles for our  
631 focused passenger car. The surrounding traffic was simulated using SUMO (Lopez et al., 2018), an open-  
632 source traffic simulation software that allows modelling and analysing the movement of vehicles, pedestri-  
633 ans, and other road users in urban areas. To validate the ability of the traffic simulator SUMO to replicate  
634 real-world traffic scenarios, we utilized loop data collected from April 1, 2015, to December 31, 2015, on  
635 a segment of the M25 highway. This segment includes approximately 30 evenly distributed detector points,  
636 which recorded average traffic speed and flow at 15-minute intervals. The same dataset was employed in  
637 Jia et al. (2022). Traffic demand was initially generated using DFROUTER based on historical loop data  
638 from entrance point A, as illustrated in Fig. 7a, and subsequently implemented in SUMO with the Intelligent  
639 Driver Model (IDM) for car-following behaviour. A validation point C was randomly selected midway along  
640 the highway segment to collect simulated traffic flow and average speed data, which were then compared  
641 against real-world records. Vehicles in the real dataset were classified into two categories: passenger cars  
642 and freight cars. Their parameters, such as speed and acceleration, were configured using default values in  
643 the simulation.

644 We applied our approaches to the same 12km segment on the M25 motorway in the UK as in Jia et al.  
645 (2022) and Yuval et al. (2023) (see Figure 7a), including the elevation data for this road segment from the  
646 Shuttle Radar Topography Mission (SRTM) Far (2007). In both the two-phase and MPC approaches, three  
647 objectives (fuel, NOx and travel time) were considered to fully explore the potential of these methods.

### 648 **5.2 Experiments on the two-phase approach**

#### 649 **5.2.1 Parameter settings**

650 The experiments for the two-phase approach were conducted using MATLAB 2022a (MathWorks). The  
651 phase-1 multiobjective shortest path problem was solved using the default linear programming solver of  
652 MATLAB. For the Phase-2 MPC problem, our MPC model was developed based on the OptiTruck model in  
653 Jia et al. (2022) by updating its objective terms and speed generating logic, and replacing the original heavy  
654 duty truck with our simulated car vehicle in Table 1.

#### 655 **5.2.2 Results from Phase 1 shortest path multiobjective optimization**

656 The experiment road section of 12 km is divided into 120 segment of 100 m and thus the available road  
657 positions form a finite set  $D = \{0, 100, \dots, 12000\}$ . The speed range from 0 to 120km/h (33.33 m/s) is divided  
658 into 33 levels with a 1m/s resolution and thus the available speed values form a finite set  $V = \{0, 1, 2, \dots, 33\}$ .  
659 The discrete road positions and speed values form the feasible region of the shortest path problem.

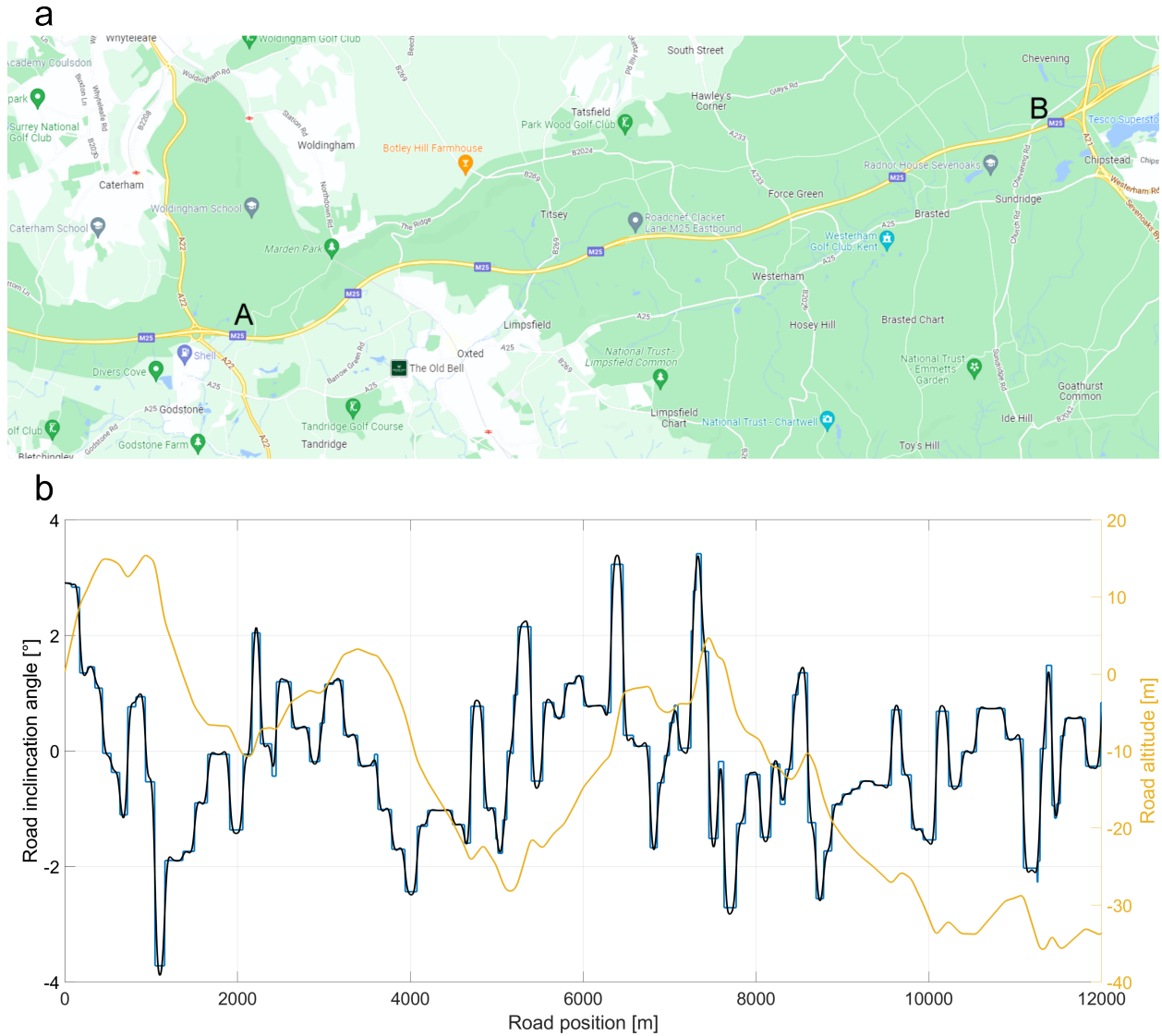


Figure 7: Road segment for experiments.  
a: A 12km road segment on the M25 motorway (marked from A to B) used in the experiments (Source: Google Maps).  
b: The plot illustrates the relationship between road position along a 12km segment of the M25 motorway and both the road slope angle.

660 Based on the relationships established in Eq (7) and (6) and the multiobjective optimization shortest  
661 path computations, we have obtained the corresponding Pareto front as shown in Figures 8 and 9. It can be  
662 concluded that generally the travel time is conflicting with both NO<sub>x</sub> and fuel but with different rates and  
663 patterns under free-flow. The relationship between NO<sub>x</sub> and fuel is positively correlated but is linear.

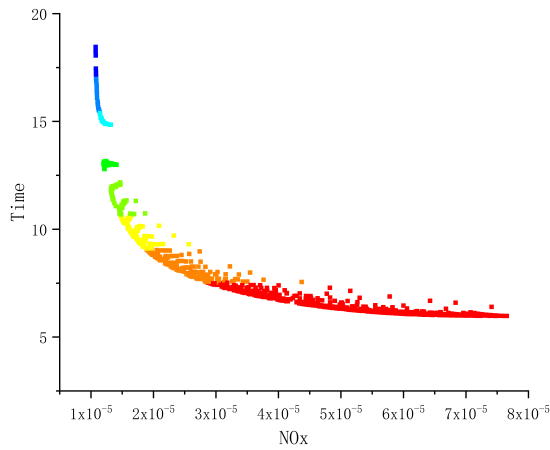
### 664 5.2.3 Knee point and sample points

665 In the two-phase approach, the Phase-1 Pareto front provides valuable guidance points for Phase-2. To  
666 ensure the sampled points adequately represent the Pareto front, we consider various types of points.

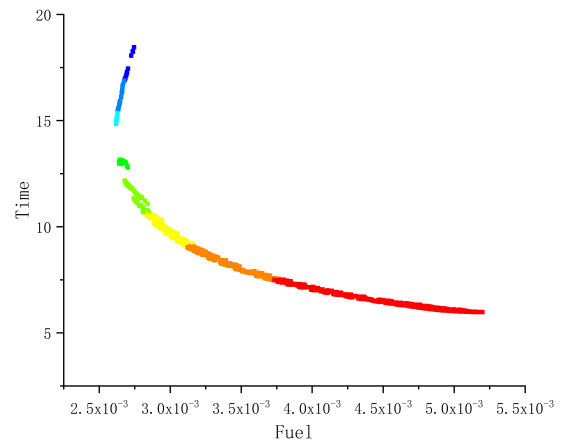


Symbol	Value [unit]	Description	Remarks
$g$	9.81 [m/s <sup>2</sup> ]	gravitational acceleration	
$A_f$	2 [m <sup>2</sup> ]	vehicle frontal area	
$M_v$	1505 [kg]	vehicle mass	
$N_w$	4	number of wheels	
$J_w$	15 [kg·m <sup>2</sup> ]	tire inertia	
$R_w$	0.6 [m]	tire radius	
$C_r$	0.012	tire rolling resistance coefficient	Wargula et al. (2019)
$C_d$	0.31	aerodynamic drag coefficient	Windsor (2014)
$g$	9.81 [m/s <sup>2</sup> ]	gravitational acceleration	
$\rho$	0.51 [kg/m <sup>3</sup> ]	air density	
$a_{\max}$	1.47 [m/s <sup>2</sup> ]	maximum acceleration/deceleration	Bae et al. (2019)
$v_{\max}$	120 [km/h]	maximum speed	Jia et al. (2022)
$S$	12 [km]	total travel distance	a segment of the M25 motorway

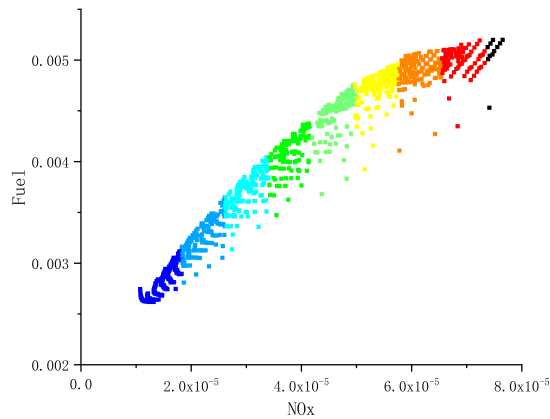
Table 1: Parameters settings



(a) 2D projection in space of NOx and time.



(b) 2D projection in space of fuel and time.



(c) 2D projection in space of NOx and fuel.

Figure 8: 2D projections of the 3D Pareto front.

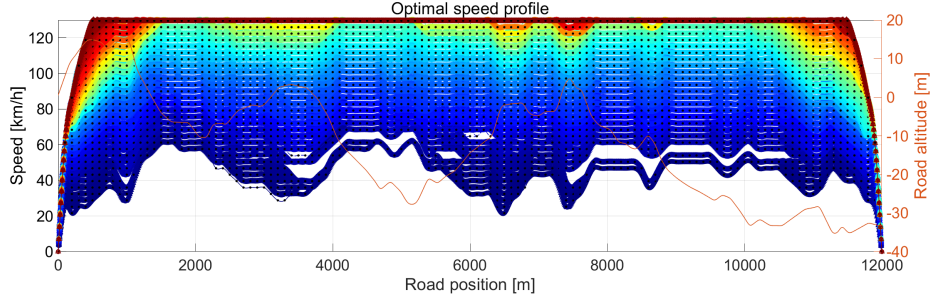


Figure 9: Speed profiles of three objective Pareto front (with the same colour legend as in Figure 8)

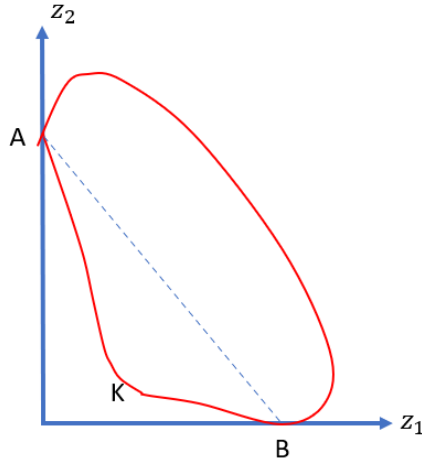


Figure 10: An illustrative example of the knee point ( $K$ ) and boundary points ( $A, B$ ) on the Pareto front in a minimisation problem with two objectives.

667 Firstly, we include the *knee point* (Das, 1999), where an enhancement in one objective would result in a  
 668 significantly adequate decline in at least one other objective. These solutions are often referred to as “knees”  
 669 due to their distinctive characteristics and are often found in the “middle” area of the Pareto front. A knee  
 670 point is arguably the most “balanced” point on the front (Branke et al., 2004). Additionally, we incorporate  
 671 the boundary points obtained by minimising only one individual objective. These points represent extreme  
 672 solutions along each objective axis and contribute to a comprehensive understanding of the Pareto front.  
 673 Furthermore, we include the points between the knee and boundary points by averaging the weights. These  
 674 intermediate points capture the gradual transition in the trade-off relationship and provide a more nuanced  
 675 representation of the Pareto front. Figure 10 gives an illustrative example of the knee and boundary points.

676 Algorithm 1 in Appendix A2 shows a classical approach in calculating the knee point that is used in  
 677 our experiments. Note that since the shortest path problem in Phase-1 is convex (Ahuja et al., 1993), this  
 678 standard approach suffices in finding the knee point.

679 By considering these different types of points, we ensure that the sampled points in Phase-2 are repre-  
 680 sentative enough to guide the MPC and DRL process effectively. The weight sets and Pareto-optimal values  
 681 of sample points can be found in Table 2 and Figure 11.

Sample	Fuel weight	NOx weight	Time weight	Fuel	NOx	Time (sec)
$p_1$	0	1	0	0.00536	$2.42 \times 10^{-5}$	1094
$p_2$	1	0	0	0.00529	$2.97 \times 10^{-5}$	866
$p_3$	0.68	0.16	0.16	0.00573	$3.44 \times 10^{-5}$	626
$p_4$	0.18	0.66	0.16	0.00541	$3.48 \times 10^{-5}$	716
$p_5$ (knee)	0.37	0.32	0.31	0.00822	$9.26 \times 10^{-5}$	419
$p_6$	0.18	0.16	0.66	0.00824	$1.07 \times 10^{-4}$	417
$p_7$	0	0	1	0.00835	$1.19 \times 10^{-4}$	415

Table 2: Sampled Pareto points from Phase-1 result (traffic-free)

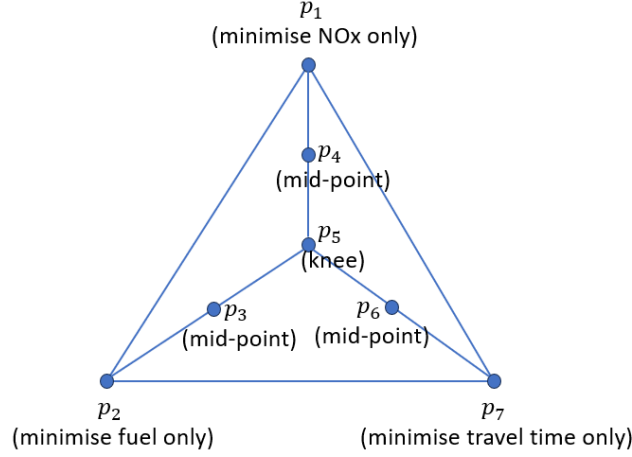


Figure 11: Illustration of sampled knee, boundary and middle points from the Pareto front with three objectives.

#### 682 5.2.4 Results from Phase-2 MPC approach

683 In these Phase-2 experiments, MPC was utilised to account for the surrounding traffic at each of the sampled  
684 points. The speed profiles of the seven points sampled from the Pareto front (see Figure 8 and Table 2) are  
685 designated as the Pareto speed  $v_p$ . The front car speed  $v_f$  is determined using the same simulated traffic  
686 as in Jia et al. (2022). The parameter settings in the MPC model remained the same as in Jia et al. (2022)  
687 except that the series of desired speed  $v_d$  was set in accordance with either Eq. (13) (MPC1) or Eq. (14)  
688 (MPC2). Both the conservative strategy (MPC1) and the balanced strategy (MPC2) were employed and  
689 their outcomes compared.

Sample	Fuel	NOx	Time (sec)
$p_1$	0.00562	$2.83 \times 10^{-5}$	1028
$p_2$	0.00564	$3.06 \times 10^{-5}$	854
$p_3$	0.00653	$4.28 \times 10^{-5}$	629
$p_4$	0.00599	$3.56 \times 10^{-5}$	715
$p_5$ (knee)	0.00919	$9.20 \times 10^{-5}$	495
$p_6$	0.00907	$8.80 \times 10^{-5}$	496
$p_7$	0.00959	$1.00 \times 10^{-4}$	493

Table 3: Phase-2 results given by MPC1 based on seven sampled points.

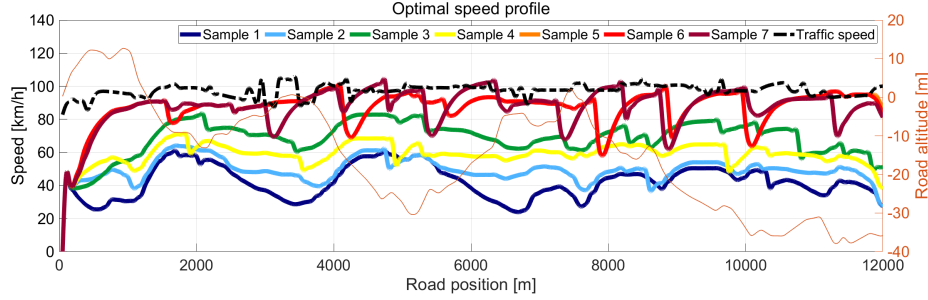


Figure 12: Phase-2 speed profiles given by MPC1 based on seven sampled Pareto points.

690 **Results from conservative strategy (MPC1)** Results in terms of the objective values of the three criteria  
691 from applying MPC1 are reported in Table 3 and the seven resulting speed profiles are depicted in Figure 12.  
692 In the figure, the dark blue line represents the speed profile of sample point  $p_1$ , the light blue line represents  
693  $p_2$ , the green point represents  $p_3$ , the yellow point represents  $p_4$ , the orange point represents  $p_5$ , the light  
694 red point represents  $p_6$ , and the dark red point represents  $p_7$ . The speed of the traffic flow is indicated by  
695 the black dashed line. The speed profiles correspond to the left y-axis, while the road altitude, represented  
696 by the light brown line, corresponds to the right y-axis. The influence of minimising travel time gradually  
697 becomes more significant from sampled point  $p_1$  to  $p_7$ , leading to higher speeds. The pattern depicted  
698 in Figure 12 remains consistent with the observation that maintaining a low speed approximately between  
699 40 and 60 km/h frequently leads to reduced fuel consumption and NOx emissions (see Figure 1). As the  
700 travel time is further prioritised, both the fuel and NOx get worse values. Note that due to the design of the  
701 strategy in Eq. (13), even  $p_6$  or  $p_7$  is set as the reference Pareto speed, MPC1 rarely gives solutions with  
702 speeds surpassing the traffic when travel time is more prioritised.

Sample	Fuel	NOx	Time (sec)
$p_1$	0.00670	$4.30 \times 10^{-5}$	657
$p_2$	0.00700	$4.90 \times 10^{-5}$	614
$p_3$	0.00796	$6.48 \times 10^{-5}$	548
$p_4$	0.00745	$5.74 \times 10^{-5}$	578
$p_5$ (knee)	0.00774	$7.10 \times 10^{-5}$	483
$p_6$	0.00757	$6.93 \times 10^{-5}$	482
$p_7$	0.00834	$8.81 \times 10^{-5}$	441

Table 4: Phase-2 results given by MPC2 based on seven sampled points

703 **Results from balanced strategy (MPC2)** Results regarding the objective values of the three criteria ob-  
704 tained by applying MPC2 are outlined in Table 4, along with the depiction of the seven resulting speed  
705 profiles in Figure 13. Similar to results given by MPC1, the impact of minimising travel time increases  
706 gradually from sampled point  $p_1$  to  $p_7$ , resulting in higher speeds. On the other hand, since MPC2 uses the  
707 average speed between the Pareto and front car speeds, when travel time is more of a priority, the speed of  
708 the vehicle can exceed that of the traffic, making the speed profiles more realistic and flexible. In addition,  
709 the speed profiles from MPC2 are more centred around the traffic, as opposite to the case in MPC1's result.

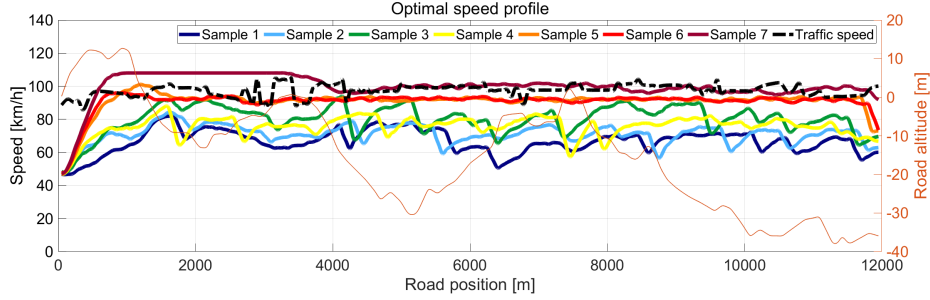


Figure 13: Phase-2 speed profiles given by MPC2 based on seven sampled Pareto points

710 However, as previously stated, this compromise comes at the expense of lower solution quality since the  
 711 profiles deviate further from the Pareto samples due to averaging the Pareto and front car speeds.

712 Overall, in either the solutions from MPC1 or MPC2, given the set of varied results, users have the  
 713 flexibility to select a speed profile from this collection based on their specific requirements while taking into  
 714 account of surrounding traffic. For instance, if a driver prioritises reaching their destination earlier and is  
 715 less concerned about fuel efficiency or NOx emissions, they can opt for  $p_6$  or  $p_7$  as their preferred speed  
 716 profile. By considering these options, users can tailor their driving experience to align with their individual  
 717 preferences and priorities.

## 718 5.3 Experiments using DRL-based approach

### 719 5.3.1 Parameter settings

720 With the same settings for section division, vehicle parameters, and traffic flow as Phase-2 MPC conditions,  
 721 we utilised the DRL method to simultaneously generate a speed profile considering both the three objective  
 722 terms and the traffic flow. The actor and critic networks were formulated using deep neural networks in  
 723 Python 3.9 with TensorFlow. The actor network consists of two hidden layers with 100 and 50 nodes,  
 724 utilising ReLU activation functions. The output layer uses tanh activation to ensure the output acceleration  
 725 remains within the specified accelerate/decelerate limits. On the other hand, the critic network has two  
 726 hidden layers with 300 and 200 nodes, using SELU activation to maintain the value of the penalty (negative  
 727 value). For learning rate decay, we employed the exponential decay function from TensorFlow with the  
 728 initial value of  $10^{-6}$  for the actor network and  $10^{-3}$  for the critic network. The decay step occurs every  
 729 1000 episodes, and the decay rate is set to 0.1. For epsilon decay, the parameters are set as follows:  $\epsilon_{min} =$   
 730  $0.1$ ,  $\epsilon_{max} = 1$ ,  $\beta_2 = 10^{-3}$ ,  $\beta_3 = 5000$ ,  $\beta_4 = 0.5$ . The total number of episodes in the training process is  
 731 set to 10,000. During each episode, the parameters used in the episode reward calculation are specified as  
 732 follows:  $\gamma_+ = 10$ ,  $\gamma_- = 50$ ,  $\beta_1 = 0.01$ .

733 In the three-objective settings of the two-phase method, we have selected 7 points from the Pareto front,  
 734  $p_1, p_2, \dots, p_7$ . These weighting sets are then utilised in the step reward of the DRL method to generate the  
 735 multi-objective solutions. Each of these 7 solutions corresponds to a specific combination of weights for the  
 736 three objectives. In the DRL method, the step reward is computed by normalising and weighting the three

737 objectives, and then summing them up. By leveraging these 7 different sets of weights, the DRL method  
738 produces 7 distinct solutions, each offering a unique trade-off among the three objectives. These solutions  
739 effectively provide a diverse set of optimised outcomes that cater to different decision-making requirements.

740 The settings were chosen with specific values to balance stability, convergence speed, and computa-  
741 tional efficiency. For example, the actor network’s two hidden layers use 100 and 50 nodes with ReLU,  
742 a choice that helps achieve quick convergence, while the tanh activation in the output layer ensures the  
743 acceleration stays within defined limits. Meanwhile, the critic network’s larger layers (300 and 200 nodes)  
744 with SELU activation are tailored to accurately capture the negative penalty values. The learning rate decay  
745 settings—starting at  $10^{-6}$  for the actor and  $10^{-3}$  for the critic, with a decay step every 1,000 episodes and a  
746 decay rate of 0.1—are specifically set to gradually reduce the learning rate as training progresses, prevent-  
747 ing overshooting and ensuring fine adjustments in later stages. Additionally, the epsilon decay parameters  
748 ( $\epsilon_{min} = 0.1$ ,  $\epsilon_{max} = 1$ ,  $\beta_2 = 10^{-3}$ ,  $\beta_3 = 5000$ ,  $\beta_4 = 0.5$ ) are precisely tuned to balance exploration and ex-  
749 ploitation over the 10,000 episodes of training. Finally, selecting 7 points from the Pareto front allows the  
750 method to cover a range of trade-offs among the three objectives by assigning distinct weight combinations  
751 in the step reward calculation, leading to a diverse set of optimized outcomes. Each of these specific settings  
752 plays a crucial role in ensuring the DRL method not only trains effectively but also maintains real-time  
753 responsiveness in deployment.

754 The DRL methodology was executed using Python on a high-performance computing system with In-  
755 tel Xeon Gold 6138 CPUs operating at 2.0GHz. Each training episode consumed approximately 7 sec-  
756 onds of computational time, resulting in an overall training duration of approximately 19 hours for 10,000  
757 episodes. It is worth noting that while the training process exhibited substantial duration, the application  
758 of a pre-trained agent demonstrated prompt responsiveness, effectively responding to a given state within a  
759 millisecond timeframe. This responsiveness aligns well with real-time response requisites.

### 760 5.3.2 Convergence analysis

761 Due to space limitations, we present the convergence progress of the DDPG training with epsilon decay for  
762 weighting set of the knee point. The convergence patterns for other weighting combinations are similar.  
763 The epsilon decay follows the shape depicted in Fig.14d. The convergence of the three objectives, namely  
764 fuel, NOx, and travel time, is shown in Fig.14a-Fig.14c, respectively. The moving average of 50 solutions  
765 is shown in the coloured lines, and the standard deviation is shown in the black dashed line. Based on  
766 the convergence figures, the grey lines represent the objective values obtained in each episode, while the  
767 coloured lines (red, blue, and yellow) show the moving averages of the 100 nearest values. At the exploration  
768 stage (episode 0-5,000), the relatively high epsilon indicates that the agent’s actions heavily rely on random  
769 selection. Consequently, the objective values show significant deviations, and the solutions fluctuate widely  
770 as the agent explores different actions to gather rewards in varying states. As the epsilon decays (episode  
771 3,000-6,000), the agent starts to depend more on its experience rather than random actions. This leads to  
772 a better understanding of the environment and rewards, resulting in less deviation among the solutions and  
773 more cost-saving solutions. At the exploitation stage (episode 6,000-10,000), both epsilon and learning

774 rate are low, indicating that the agent predominantly relies on the trained actor ANN. Consequently, it can  
 775 consistently provide cost-saving solutions and effectively drive the vehicle on the experiment road, striking  
 776 a balance among the three objectives.

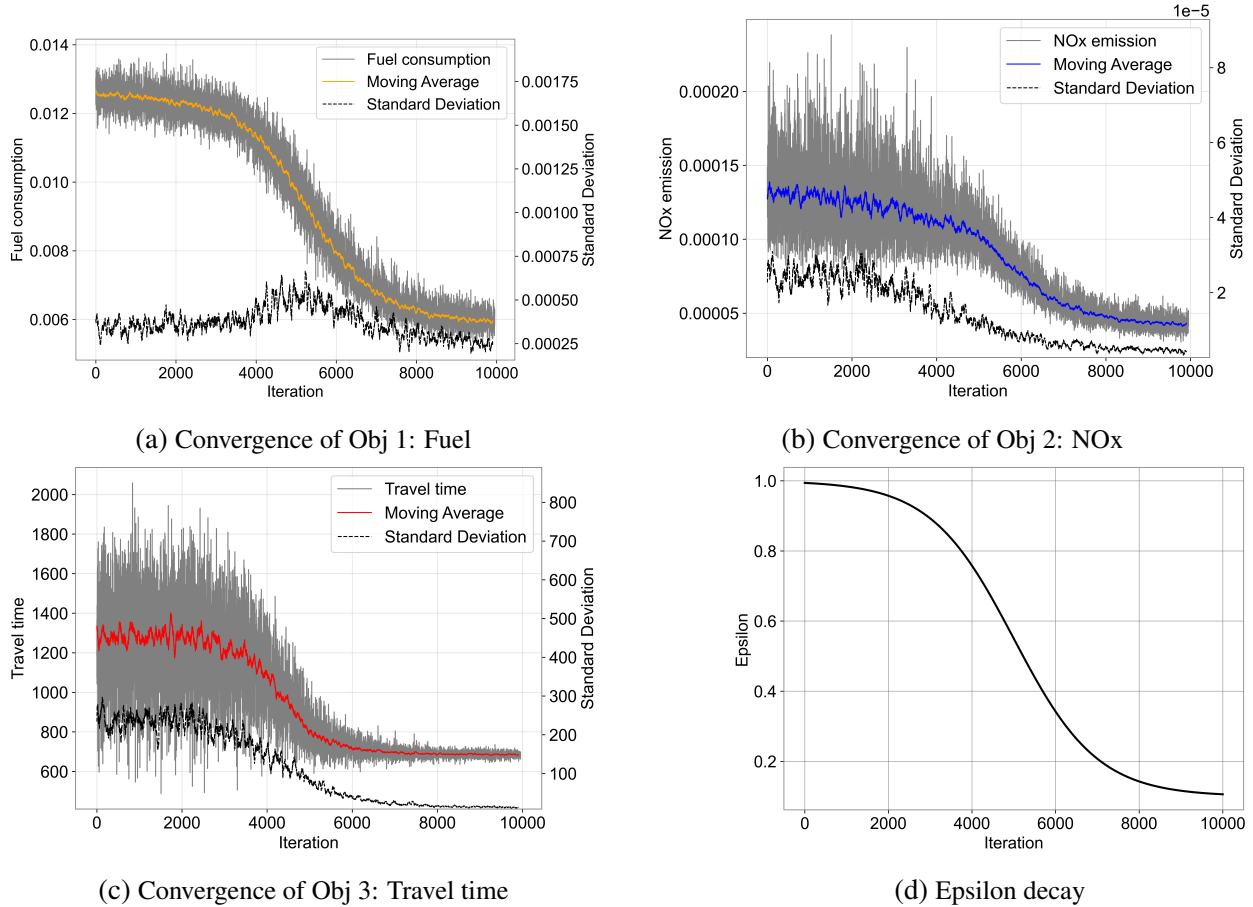


Figure 14: Convergence of DRL method using weighting set of the knee point

### 777 5.3.3 Application of the energy management system with DRL

778 Table 5 presents the objective values associated with the same sampled seven points as shown in Table 2,  
 779 which were obtained using the DRL method. A comparison among the Pareto-optimal solutions and solu-  
 780 tions derived from two-phase and DRL approaches is illustrated in Fig. 15, and the projections are shown  
 781 in Fig. 16. The proximity of a scatter point to the bottom-left corner indicates its superior performance.  
 782 Notably, the Pareto solutions reflect the best outcomes within a traffic-free context, representing the optimal  
 783 solutions for given weights. In actual scenarios, the speed profile is controlled by MPC or DRL approaches  
 784 amidst surrounding traffic flow. Upon comparison, it is evident that the DRL solutions are situated closer  
 785 to the Pareto front in contrast to the MPC solutions. Across all weight sets, the DRL solutions consistently  
 786 outperform the two-phase solutions under traffic flow conditions. The integrated DRL approach excels in  
 787 identifying solutions that yield reduced fuel consumption, NOx emissions, and time savings compared to

788 the two-phase approach.

Sample	Fuel	NOx	Time (sec)
$p_1$	0.0538	$2.49 \times 10^{-5}$	1104
$p_2$	0.00506	$2.38 \times 10^{-5}$	976
$p_3$	0.00577	$3.32 \times 10^{-5}$	760
$p_4$	0.00537	$3.08 \times 10^{-5}$	726
$p_5$ (knee)	0.00555	$3.73 \times 10^{-5}$	667
$p_6$	0.00808	$8.13 \times 10^{-5}$	456
$p_7$	0.00878	$1.13 \times 10^{-4}$	433

Table 5: Results given by DRL based on seven sampled points

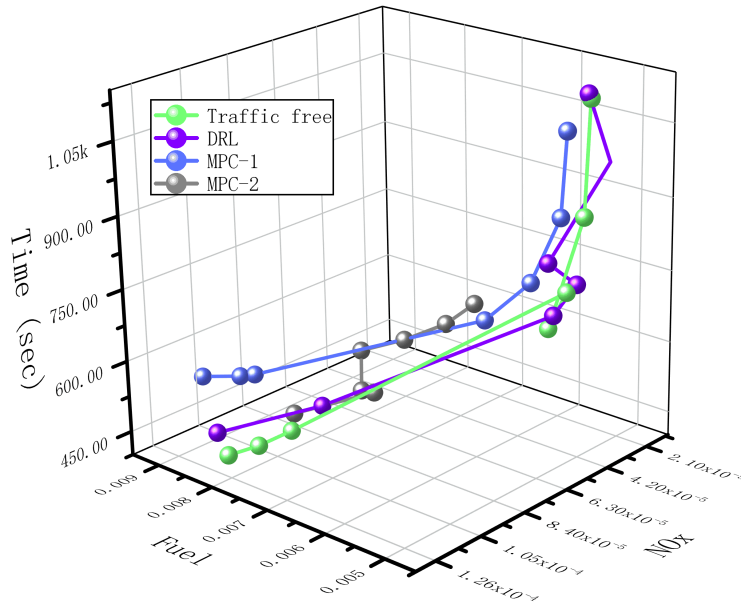
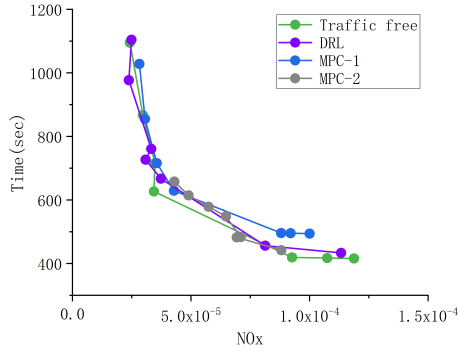


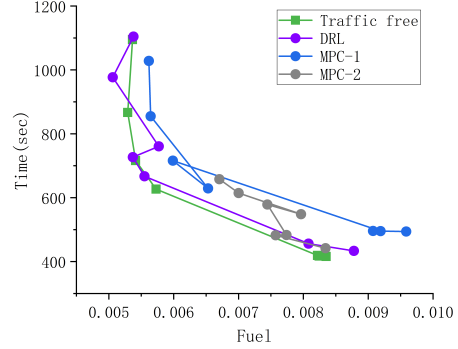
Figure 15: Comparison of the three objective values derived from Phase-1 Pareto (traffic-free), Phase-2 (MPC-1 and MPC-2) and DRL

789 The speed profiles resulting from the DRL approach, as depicted in Fig. 17, exhibit distinct qualities  
 790 when contrasted with the optimisation-based method. Notably, the DRL outcomes showcase several no-  
 791 table features. Firstly, the DRL approach offers enhanced flexibility in speed adjustments, a characteris-  
 792 tic that stems from its heightened sensitivity to variances in gradient, speed, and acceleration. This height-  
 793 ened adaptability enables it to more effectively address the three objectives, reacting dynamically to their fluctua-  
 794 tions. Importantly, boundary samples (1, 2, and 7) indicate DRL’s superiority over MPC1 and MPC2. These  
 795 boundary cases highlight the DRL agent’s ability to adeptly navigate the complex interaction between driv-  
 796 ing speed and emissions within the dynamic context of traffic flow. This showcases the DRL’s capacity to

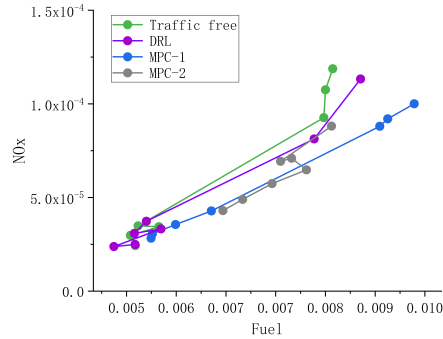




(a) 2D projection in space of NOx and time.



(b) 2D projection in space of fuel and time.



(c) 2D projection in space of NOx and fuel.

Figure 16: 2D projections of the 3D objective values.

797 capture nuanced relationships and deliver enhanced performance, setting it apart as a powerful optimisation  
 798 approach. Another notable attribute is the incorporation of gradient profiles. In scenarios favouring emis-  
 799 sion reduction over travel time, the DRL agent showcases a strategic behaviour: maintaining a consistent  
 800 speed on uphill sections while accelerating on downhill stretches. This smart strategy serves to optimise  
 801 both emission levels and travel time efficiency.

802 Moreover, the DRL method integrates the concept of headway gap, a safety parameter. In situations  
 803 where the gap remains within safe limits, the vehicle is allowed to accelerate, leading to instances where  
 804 driving speed outpaces traffic speed. This approach takes into consideration not only objective optimisation  
 805 but also road safety. The headway gap of the DRL, MPC1 and MPC2 are compared in Fig 18 where the  
 806 solutions with optimal travel time ( $p_7$ ) are selected. Because, when objectives focus on the NOx and fuel  
 807 consumption, the driving speed is always smaller than the flow speed, following the eco-driving require-  
 808 ments. It is obviously that the MPC methods will induce large headway with the front vehicle. Because  
 809 the MPC methods control the speed by referring to the traffic speed rather, while headway indicator is not  
 810 incorporated in such controlling algorithms. The vehicle cannot accelerate even though the headway is safe  
 811 enough.

812 The DRL approach outperforms the two-phase strategy due to its methodological advantages. Unlike  
 813 MPC, which lacks the capability to adjust acceleration based on headway distance, DRL provides a more  
 814 flexible strategy. MPC's conservative approach, prioritising collision avoidance based on the lead vehicle's

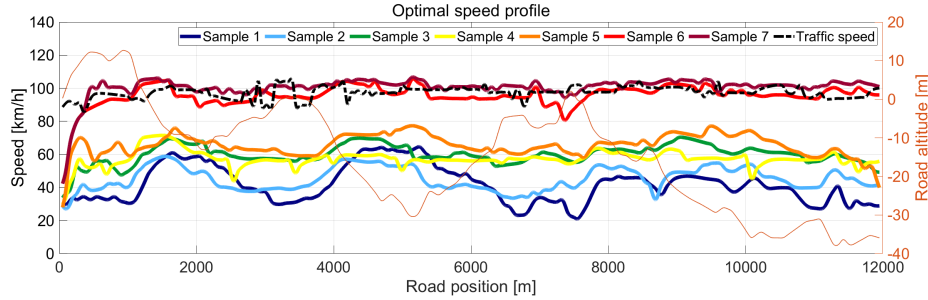


Figure 17: Speed profile of the seven sample Pareto points by DRL (three objectives case)

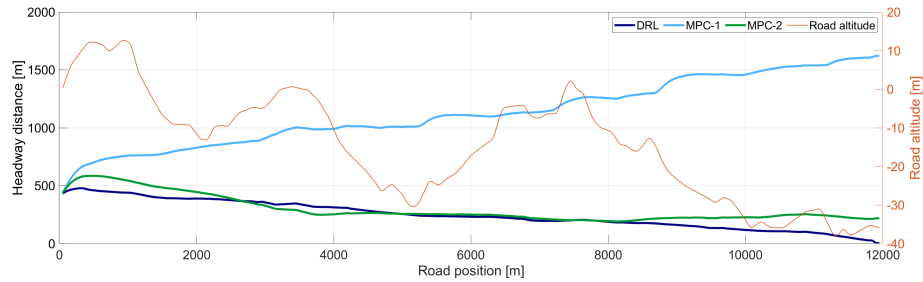


Figure 18: Comparison of headway between the three methods

815 speed, becomes inefficient when headway distance is safe. In such cases, if the lead vehicle slows down,  
 816 MPC responds by decreasing speed, impacting overall efficiency.

817 Unlike MPC, the DRL approach adapts dynamically, updating headway distance and traffic speed in  
 818 real-time. Trained to optimise acceleration and deceleration based on accumulated experience, it offers  
 819 enhanced flexibility, enabling more nuanced movement strategies aligned with optimisation goals.

820 Additionally, the issue of transferability is crucial. While the two-phase strategy generates optimal  
 821 solutions in traffic-free conditions and incorporates it into an MPC for real-world scenarios, the dynamic  
 822 nature of traffic and variable speeds can undermine the effectiveness of this idealised profile. If traffic speed  
 823 consistently falls below the set of Pareto-optimal solutions, the MPC may predominantly mimic traffic  
 824 speed, potentially sidelining essential optimisation objectives. In contrast, the DRL approach consistently  
 825 makes optimal decisions for each state variable, systematically addressing optimisation objectives at each  
 826 time step.

827 The experiment currently assumes that the following vehicle never surpasses our own, which is some-  
 828 what unrealistic. However, the DRL approach excels, especially in scenarios involving “vehicle insertion”.  
 829 Strategies focused on conserving fuel or reducing NOx emissions often entail maintaining a larger headway  
 830 distance, leading to situations where vehicles insert themselves between the subject vehicle and the lead  
 831 vehicle. In contrast, the MPC strategy may struggle to handle such insertions accurately, highlighting the  
 832 DRL agent’s strength in promptly recalibrating the headway distance and implementing suitable braking  
 833 measures.

834 Despite its advantages, the DRL approach has a drawback. It requires training for each specific weight

835 set, leading to a time-intensive process before convergence. This slower solving efficiency, compared to  
836 the two-phase approach, may limit its suitability for entirely new situations lacking training data. This  
837 highlights the trade-off between DRL’s enhanced decision-making and the computational time needed for  
838 optimal convergence.

839 Furthermore, the profiles of fuel consumption, NOx emissions, travel time, and headway are compared  
840 and analysed in Appendix A5 to comprehensively demonstrate the different eco-planning strategies resulting  
841 from various weight combinations.

#### 842 **5.4 Incorporation of the jerk cost**

843 As highlighted by several studies on eco-driving behaviour (Chen et al., 2018; Li et al., 2024a), the jerk  
844 cost significantly impacts driver comfort during acceleration and deceleration. To further account for driver  
845 comfort, this section evaluates the performance of our approaches by incorporating the jerk cost into the  
846 objectives. Methodologically, the jerk cost is calculated as the absolute difference between the previous and  
847 current speed across all road segments (Jia et al., 2022).

848 To generate speed profiles after incorporating the jerk cost, the weights of the objectives are uniformly  
849 set to 1/4 for fuel consumption, NOx emissions, travel time, and jerk cost. To assess the influence of the  
850 jerk cost, the knee point weight solution ( $p_5$ ) from Section 5.3.3 (which does not include the jerk cost in the  
851 objectives) is used as a benchmark for both the two-phase approaches and the DRL approach.

852 The speed profiles with and without the jerk cost in the objective function are illustrated in Fig. 19.  
853 The dark and light blue lines represent the DRL solutions, the dark and light green lines represent the  
854 MPC1 solutions, and the dark and light red lines represent the MPC2 solutions. As shown in the figure, the  
855 speed profiles produced by considering the jerk cost become smoother for the DRL and MPC1 approaches  
856 compared to those without the jerk cost. However, since the speed profile for the MPC2 solution is already  
857 sufficiently smooth even without considering the jerk cost, the difference is less pronounced. Incorporating  
858 the jerk cost effectively reduces severe acceleration and deceleration, thereby enhancing driving comfort.

859 The objective values for each term are presented in Table 6. For the DRL approach, while fuel consump-  
860 tion, NOx emissions, and jerk cost are reduced when the jerk cost is incorporated, the travel time increases  
861 from 658.7 to 718.05. Consequently, no dominated solution is found in the multiobjective optimization  
862 problem, demonstrating the capability of DRL to handle multiobjective optimization problems effectively.  
863 In contrast, for both the MPC1 and MPC2 approaches, incorporating the jerk cost results in a reduction of  
864 all four objective values, dominating the solutions that do not consider the jerk cost. This indicates that the  
865 two-phase approach is less robust in ensuring solution quality.

#### 866 **5.5 Online application with real-world traffic**

867 MO-SPO face significant challenges in real-time applications due to their high computational complexity,  
868 which arises from solving multiple conflicting objectives like fuel consumption, NOx emissions, and travel  
869 time simultaneously. These problems are further compounded by the dynamic and unpredictable nature

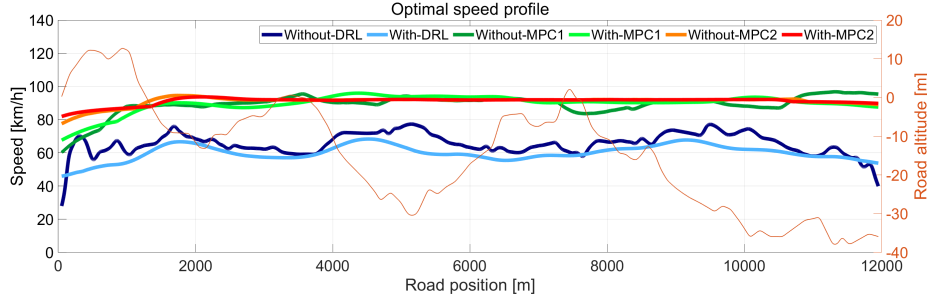


Figure 19: Comparison of speed profiles with and without jerk cost

	Without jerk cost			With jerk cost		
	DRL	MPC1	MPC2	DRL	MPC1	MPC2
Fuel consumption	0.00555	0.00919	0.00774	0.0052	0.0069	0.0068
NOx emission	3.73E-05	9.20E-05	7.10E-05	2.80E-05	5.35E-05	5.41E-05
Travel time	667	495	483	718.05	481.98	474.86
Jerk cost	88.48	159.83	90.70	28.55	43.76	29.14

Table 6: Objectives of the speed profiles with and without jerk cost

870 of real-world traffic conditions, such as fluctuating traffic speeds and driver behaviour, which MO-SPOs  
 871 struggle to adapt to efficiently. Additionally, as the number of objectives and constraints increases, the  
 872 complexity grows exponentially, making it difficult to scale MO-SPOs for large-scale or complex scenarios.  
 873 Finally, the lack of real-time feedback mechanisms means that solutions based on static data may become  
 874 suboptimal or infeasible in dynamic environments, limiting their practicality for online applications.

875 An advantage of our two-phase and DRL approach is their suitability for online applications, which  
 876 enable the generation of eco-driving speed profiles using real-time information. To demonstrate the online  
 877 applicability of our approaches, we applied our pretrained models to a novel real-world traffic scenario.  
 878 Specifically, we utilized evening peak-hour traffic speed data (19:00–21:00) collected from January 1–7,  
 879 2022, on a segment of the M25 highway. This segment includes 12 detector points, approximately evenly  
 880 distributed, where traffic speed was recorded at 1-minute intervals. The average speed of each segment was  
 881 used to represent the real-world traffic speed.

882 The comparison between the simulated traffic speed (using SUMO) and the real-world traffic speed is  
 883 illustrated in Fig. 20. In the figure, the blue line represents the simulated traffic speed, while the red line  
 884 represents the average real-world traffic speed. This comparison highlights the ability of our approaches  
 885 to adapt to real-world conditions, ensuring that the generated eco-driving speed profiles are both practical  
 886 and effective in dynamic traffic environments. By leveraging real-time data, our methods provide a robust  
 887 solution for optimizing speed profiles in real-world applications, particularly during peak traffic hours when  
 888 efficiency and responsiveness are critical.

889 By comparison, the real-world traffic speed is slightly higher than the simulated traffic speed. Since the  
 890 traffic speed serves as the upper bound for speed limitations and influences the headway to the front vehicle,  
 891 a higher traffic speed does not significantly impact the solutions for  $p_1$  to  $p_5$ . This is because the speed

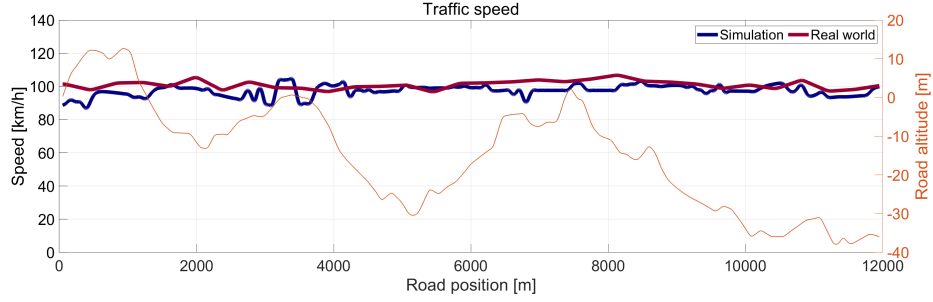


Figure 20: Comparison of traffic speed of simulating and real-world condition

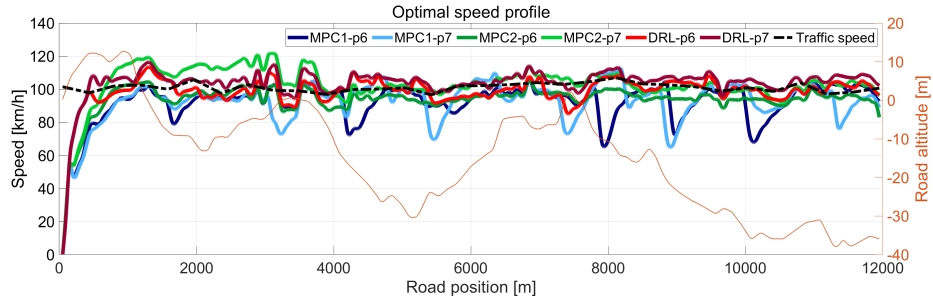


Figure 21: Speed profiles of  $p_6, p_7$  by different approaches

892 profiles for these points are consistently lower than the traffic speed to optimize fuel consumption and NOx  
 893 emissions. Therefore, to test the online application under real-world traffic conditions, the weights of  $p_6$   
 894 and  $p_7$  are applied. These points represent scenarios where the speed profiles are closer to the traffic speed,  
 895 making them more sensitive to real-world variations and thus better suited for evaluating the performance of  
 896 our approaches in dynamic environments. This ensures that the solutions remain robust and effective even  
 897 when applied to real-world traffic data with higher average speeds.

898 The speed profile of MPC1, MPC2 and DRL approaches are shown in Fig 21. The blue lines repre-  
 899 sent the speed profiles of MPC1 approach, the green lines represent the speed profiles of the MPC2, the  
 900 red lines represent the speed profiles of DRL. The light lines represent the sample  $p_6$ , and the dark lines  
 901 represent the sample  $p_7$ . Among the methods, DRL speed profiles demonstrate exceptional smoothness and  
 902 adaptability, closely aligning with the real-world traffic speed. For  $p_6$ , the DRL profile is smoother than  
 903 MPC1 and slightly more adaptive than MPC2, showcasing its ability to balance smoothness and real-world  
 904 responsiveness. For  $p_7$ , the DRL profile almost perfectly follows the real-world traffic speed, highlighting  
 905 its superior capability to handle dynamic conditions. This adaptability makes DRL particularly well-suited  
 906 for unpredictable environments.

907 Table 7 compares the performance of three approaches, namely MPC1, MPC2, and DRL, for two sam-  
 908 ple points,  $p_6$  and  $p_7$ , across three objectives: fuel consumption, NOx emissions, and travel time. Among  
 909 these, DRL stands out as the best-performing approach, particularly when travel time is prioritized as the  
 910 most important factor. DRL achieves the shortest travel times for both  $p_6$  (440.66) and  $p_7$  (418.68), making  
 911 it the fastest and most time-efficient method. This exceptional performance in reducing travel time is partic-

ularly critical for online applications, where speed and responsiveness are paramount, especially when user preferences prioritize time efficiency. While MPC2 and MPC1 excel in fuel efficiency and environmental performance, they cannot match DRL’s speed and responsiveness.

	MPC1		MPC2		DRL	
	p6	p7	p6	p7	p6	p7
Fuel consumption	0.0031	0.0037	0.0028	0.0034	0.0033	0.0041
Nox emission	3.43E-05	5.62E-05	3.38E-05	7.06E-05	5.57E-05	8.02E-05
Travel time	476.69	475.09	464.11	425.04	440.66	418.68

Table 7: Objectives of in online application

914

## 915 **6 Conclusions and future work**

916 Using multiobjective optimisation, this paper addresses the eco-driving problem by generating vehicle speed  
 917 profiles that consider up to three objectives: fuel consumption, NOx emission, and total travel time in real-  
 918 world scenarios with surrounding traffic. Unlike traditional approaches that generate a single solution, multi-  
 919 objective optimisation provides a collection of solutions, each representing unique preferences in weighting  
 920 different objectives. This approach is particularly suitable for problems with incomparable objectives, as is  
 921 the case in our study. Simulated data from GT-SUITE are used to derive the relationships between engine  
 922 power and the rates of fuel consumption and NOx emission, which can be determined analytically by vehicle  
 923 dynamics.

924 Two solution approaches are presented and compared. The first involves a two-phase process: Phase-1  
 925 solves a traffic-free problem analytically, providing “ideal” Pareto points for Phase-2. In Phase-2, an ex-  
 926 isting model predictive control approach generates compromised results considering both Pareto points and  
 927 surrounding traffic. The second approach, designed by the authors from scratch, employs deep reinforce-  
 928 ment learning (DRL) to generate speed profiles, considering multiple objectives and surrounding traffic  
 929 simultaneously. Both approaches use the weighted sum method to generate Pareto fronts, marking the first  
 930 application of multiobjective optimisation to simultaneously consider fuel consumption and NOx emissions  
 931 in generating optimised speed profiles.

932 The DRL approach outperforms the two-phase method in modeling flexibility and solution quality on  
 933 a real-world highway in southern England. It explicitly considers vehicle headway, leading to more so-  
 934 phisticated eco-driving strategies and optimised objective values across all three criteria. For instance, at  
 935 one representative Pareto point, results indicate that the DRL approach achieves up to 10% lower fuel con-  
 936 sumption and 16% lower NOx emissions compared to MPC-based methods while reducing travel time by  
 937 approximately 5%. In addition, the DRL method maintained safer headway distances, offering more robust  
 938 eco-driving strategies in dynamic traffic environments. However, it requires prior training, making it less  
 939 suitable for entirely new scenarios with limited or no training data.

940 Building on these promising results, future work could extend the MO-SPO framework to other ve-

941 hicle classes, such as heavy-duty trucks, electric vehicles, and hybrid models, by re-calibrating vehicle  
942 parameters and integrating appropriate powertrain and emission models to better reflect distinct dynamic  
943 characteristics. Moreover, adapting the framework to diverse traffic environments—including urban set-  
944 tings, mixed-traffic conditions, or multi-lane roads with varying densities—will enhance its applicability,  
945 while integrating richer traffic data, such as real-time signal timings or pedestrian interactions, could further  
946 improve its robustness. As the complexity of these extended scenarios may increase computational de-  
947 mands, future research should focus on improving training efficiency through methods like transfer learning  
948 or advanced parallel computing strategies to maintain real-time responsiveness. Additionally, incorporating  
949 further environmental metrics such as particulate matter (PM) and CO<sub>x</sub>, and integrating robust or stochas-  
950 tic optimization techniques to manage uncertainties in traffic flow, weather, and driver behavior, represent  
951 promising avenues for further refinement. Overall, these research directions aim to advance the MO-SPO  
952 framework towards a more comprehensive, adaptable, and environmentally conscious solution for modern  
953 traffic management.

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# 1172 **Appendices**

## 1173 **A1 Simulation environment and vehicle modules**

1174 Simulations were carried out using GT-SUITE simulation software, as detailed in (Gamma Technologies),  
1175 employing identical vehicle specifications outlined in Gao et al. (2021). The vehicle under study was a  
1176 Euro 6 compliant diesel passenger car equipped with a four-cylinder, four-stroke turbocharged diesel en-  
1177 gine. It weighed 1505 kg and boasted a maximum power output of 103 kW, correlating to an engine speed  
1178 of 4000 rpm. The diesel engine featured a compression ratio of 16.5:1. This vehicle model comprised  
1179 three main modules: vehicle powertrains, emission sources, and after-treatment systems. The powertrain  
1180 system encompassed an engine model, a transmission model, and a control model. The engine model was  
1181 constructed based on experimental tests, incorporating maps for brake-specific fuel consumption and brake  
1182 mean effective pressure. Additionally, the emission model integrated maps for exhaust temperature, emis-  
1183 sion factors, and exhaust flow rates to consider the impact of cold starts on emissions. The after-treatment  
1184 system encompassed a diesel oxidation catalyst and a diesel particulate filter, as discussed in (Gao et al.,  
1185 2021).

## A2 Algorithm for calculating the knee point

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### Algorithm 1: Calculate Knee Point on Pareto Front

---

**Require:** Non-dominated solution set on the Pareto front,  $S$   
**Ensure:** Knee point solution,  $K$

- 1: Initialize weights for distance and angle,  $w_d, w_a$
- 2: **for all** Non-dominated solution  $s_i = (x_i, y_i, z_i)$  in  $S$  **do**
- 3:     Initialize the utility (weighted sum of distance and angle) of  $s_i$ , i.e.,  $u_i := w_d \cdot d(s_i) + w_a \cdot \theta(s_i)$
- 4:     **for all** Other non-dominated solutions  $s_j$  in  $S$  where  $s_j \neq s_i$  **do**
- 5:         Calculate Euclidean distance  $d_{ij}$  between  $s_i$  and  $s_j$ :  

$$d_{ij} = \sqrt{(x_i - x_j)^2 + (y_i - y_j)^2 + (z_i - z_j)^2}$$
- 6:         Calculate angle  $\theta_{ij}$  between  $s_i$  and  $s_j$ :  

$$\theta_{ij} = \arccos\left(\frac{\mathbf{v}_i \cdot \mathbf{v}_j}{\|\mathbf{v}_i\| \cdot \|\mathbf{v}_j\|}\right)$$
, where  $\mathbf{v}_i$  and  $\mathbf{v}_j$  are vectors from origin to  $s_i$  and  $s_j$ , respectively.
- 7:         Update  $u_i := u_i + w_d \cdot d_{ij} + w_a \cdot \theta_{ij}$
- 8:     **end for**
- 9:     **if**  $u_i$  is the current minimum **then**
- 10:         Update knee point solution  $K = s_i$
- 11:     **end if**
- 12: **end for**
- 13: **return** Knee point solution  $K$

---

Here the weights on distance and angel ( $w_d$  and  $w_a$ ) are set as  $5 \times 10^{-9}$  and 0.5 respectively, and a

discount of  $10^{-8}$  is applied to eliminate the magnitude of distance.

## A3 Algorithm for the MPC method

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### Algorithm 2: Time-Varying Adaptive MPC for Speed Profile Generation

---

**Input:** Longitudinal model parameters (e.g.  $A(i)$ ,  $B(i)$ ,  $D(i)$ ), cost weights  $\lambda_e$ ,  $\lambda_k$ ,  $\lambda_s$ , prediction horizon  $n_p$ , initial state  $E_k(0)$ , vehicle and safety constraints, traffic context data, and desired speed profile  $v_d$

**Output:** Optimal engine energy sequence  $E_e^*(i)$  over the prediction horizon and corresponding speed profile

**Initialization:** Set current index  $i \leftarrow 0$ , obtain initial kinetic state  $E_k(i)$ , and retrieve initial traffic and road condition information.

**while** *vehicle has not reached the destination* **do**

**1. Update Measurements:**

Obtain current state  $E_k(i)$ , vehicle speed  $v(i)$ , and updated traffic context (including real-time local and predicted future traffic data).

**2. Update Prediction Parameters:**

Adapt the spatial step  $\Delta s$  based on the current vehicle speed  $v(i)$

Determine the desired speed profile  $v_d$  over the horizon using the traffic predictive model.

**3. Update Longitudinal Model:**

Compute the time-varying matrices  $A(i)$ ,  $B(i)$ , and offset  $D(i)$  from the linearized vehicle dynamics:

$$E_k(i+1) = A(i)E_k(i) + B(i)U(i) - D(i)$$

where the control input is  $U(i) = \begin{bmatrix} E_e(i) \\ E_b(i) \end{bmatrix}$ .

**4. Solve the MPC Optimization:**

Formulate the quadratic cost function over the prediction horizon:

$$J(i) = \sum_{j=i}^{i+n_p-1} \left( \lambda_e E_e(j)^2 + \lambda_k \left( E_k(j) - \frac{1}{2} M_e v_d(j)^2 \right)^2 + \lambda_s (E_e(j) - E_e(j-1))^2 \right)$$

subject to constraints  $\mathcal{D}$  and safety headway requirements.

Compute the optimal control sequence:

$$\{U^*(i), U^*(i+1), \dots, U^*(i+n_p-1)\} = \arg \min_U J(i)$$

**5. Implement Control Action:**

Apply the first control input  $U^*(i)$  (i.e., use  $E_e^*(i)$  and  $E_b^*(i)$ ) to update the vehicle state.

**6. Shift Horizon:**

Set  $i \leftarrow i+1$  and update the prediction horizon accordingly.

**return** Sequence  $\{U^*(0), U^*(1), \dots, U^*(N-1)\}$  representing the optimal engine energy inputs and resulting speed profile.

---



## A4 Pseudocode for DDPG

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### Algorithm 3: Deep Deterministic Policy Gradient (DDPG)

---

**Data:** Initialize actor network  $\theta^{\text{actor}}$  and critic network  $\theta^{\text{critic}}$  with random weights

**Data:** Initialize target actor network  $\theta^{\text{target\_actor}} \leftarrow \theta^{\text{actor}}$  and target critic network  $\theta^{\text{target\_critic}} \leftarrow \theta^{\text{critic}}$

**Data:** Initialize memory  $B$

**while**  $e \leq E$  **do**

- Receive initial state  $s_1$ ;
- for**  $t = 0$  to  $S/\Delta s - 1$  **do**
  - if**  $\text{random} \leq \varepsilon$  **then**
    - Choose action  $a_t = \mu(s_t | \theta^{\text{actor}})$ ;
    - else**
      - Random choose an action within the limit;
  - end**
  - Execute action  $a_t$  and calculate the driving speed;
  - Observe step reward  $r_t$  and new state  $s_{t+1}$ ;
  - Store transition  $(s_t, a_t, r_t, s_{t+1})$  in  $B$ ;
- end**
- Give the episode reward  $r_e$ ;
- Store the terminal tuple  $(s_e, a_e, r_e, \_)$  in  $B$ ;
- for**  $(s_t, a_t, r_t, s_{t+1})$  in  $B$  **do**
  - Pick a transition  $(s_i, a_i, r_i, s_{i+1})$  from  $B$ ;
  - Compute target value  $y_i$ ;
  - Calculate the loss function of critic network  $\mathcal{L}(\theta^{\text{critic}})$ ;
  - Update weights of critic network by gradient descent  $\nabla \mathcal{L}(\theta^{\text{critic}})$ ;
  - Calculate the loss function of actor network  $\mathcal{L}(\theta^{\text{actor}})$ ;
  - Update weights of actor network by gradient descent  $\nabla \mathcal{L}(\theta^{\text{actor}})$
- end**
- Update target networks:
  - $\theta^{\text{target\_critic}} \leftarrow \tau \theta^{\text{critic}} + (1 - \tau) \theta^{\text{target\_critic}}$ ;
- Decay exploration rate  $\varepsilon$  and learning rates;

**end**

---

## A5 Performance comparison between different weights of preference

Figure 22, 23, 24, and 25 display the profiles of NOx emission, fuel consumption, travel time, and headway distance resulting from the three approaches under various traffic conditions. Each subfigure presents the profile of a specific approach. The comparative analysis among different points obtained from the same approach reveals their sensitivity to weight proportions. Greater deviation signifies heightened sensitivity of an approach. A substantial similarity in profiles under diverse weight sets may fail to cater to different trade-off requirements.

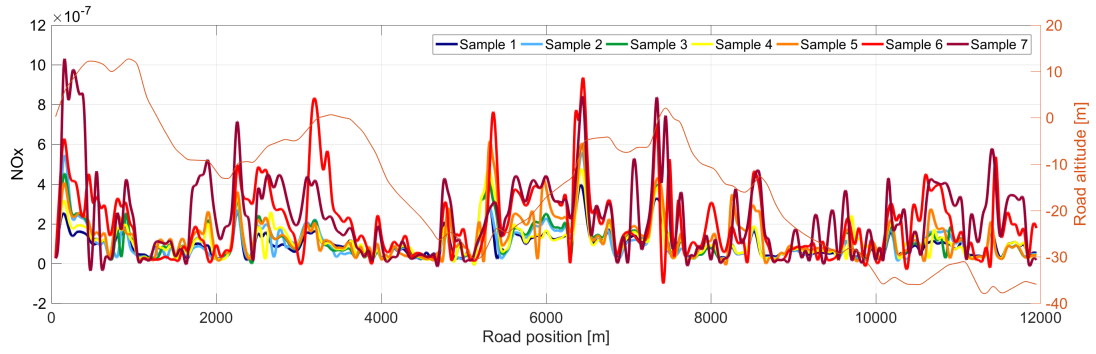
As observed in Fig. 22 and 23, the DRL approach exhibits more pronounced deviations in NOx emission and fuel consumption profiles, while the profiles of MPC-1 and MPC-2 remain similar across different samples. The objective value visualization in Fig. 16 illustrates that heightened sensitivity to weight proportions corresponds to larger differences between objectives on the Pareto front, allowing for more flexible choices. Significantly, the divergence in the time profile is substantial across all three approaches. Intriguingly, in  $p_1$  and  $p_2$ , where NOx and fuel are minimized, the time profile mirrors the road altitude. This similarity suggests that adopting a slower pace uphill and accelerating downhill can effectively conserve fuel and minimize emissions. Referring to Fig. 25, it's evident that the headway distance to the lead vehicle increases notably with higher weights assigned to NOx and fuel. Opting for strategies that minimize NOx or fuel eventually results in a headway gap surpassing 6,000 meters.

Figure 26, 27, 29, and 28 provide a comparative analysis of objectives and headway distance among the three approaches with different weight configurations. These samples encompass scenarios, including  $p_1$  (minimum NOx),  $p_2$  (minimum fuel),  $p_7$  (minimum time), and  $p_5$  (knee point). Each subfigure presents profiles of NOx emission, fuel consumption, travel time, and headway distance.

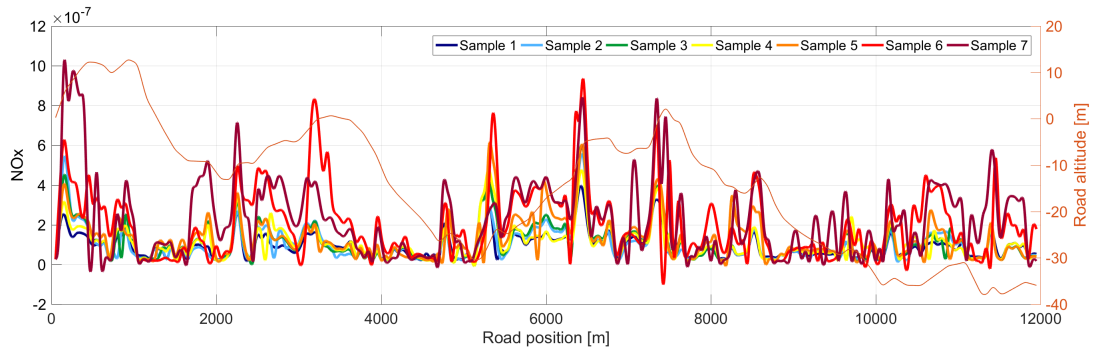
In the cases of the first two samples ( $p_1$  with minimum NOx and  $p_2$  with minimum fuel), MPC-2 exhibits the least favorable performance due to its higher driving speed. The strategy employed by MPC-2 struggles to address scenarios of minimum NOx and fuel, primarily because the driving speed is heavily influenced by the traffic speed. This limitation prevents MPC-2 from ensuring optimal speeds in scenarios where only a single objective is considered. Conversely, MPC-1 and DRL showcase similar performance. However, DRL adopts a more conservative driving approach compared to both MPC methods, prioritizing fuel and NOx reduction over higher speeds, irrespective of the traffic conditions.

In Sample 7, we delve into the scenario of minimizing travel time, where all three methods are focused on completing the drive as quickly as possible. Starting with the same initial headway distance, the two MPC approaches and the DRL approach adopt distinct strategies. MPC-1 consistently maintains its driving speed at the same pace as the traffic speed, resulting in a stable headway that hovers around its initial value. In contrast, MPC-2 employs a more uniform acceleration strategy, causing the headway to gradually decrease over time. Lastly, DRL opts for an initial speed increase, actively tailing the front vehicle. As the headway narrows, DRL slows down, ensuring that the vehicle maintains a reasonable distance from the vehicle in front. This strategy results in the headway fluctuating between approximately 50 to 300 meters.

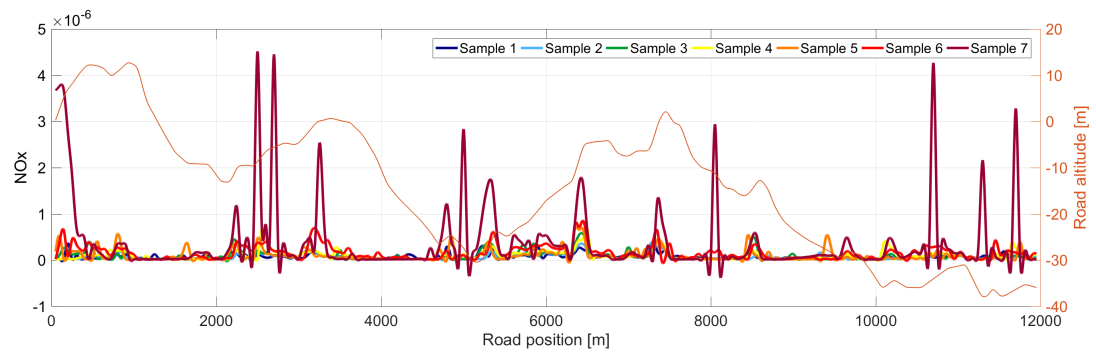
Examining the outcomes of the knee point ( $p_5$ ), the fuel consumption and NOx emission exhibit striking



(a) NOx emission of MPC-1 samples.

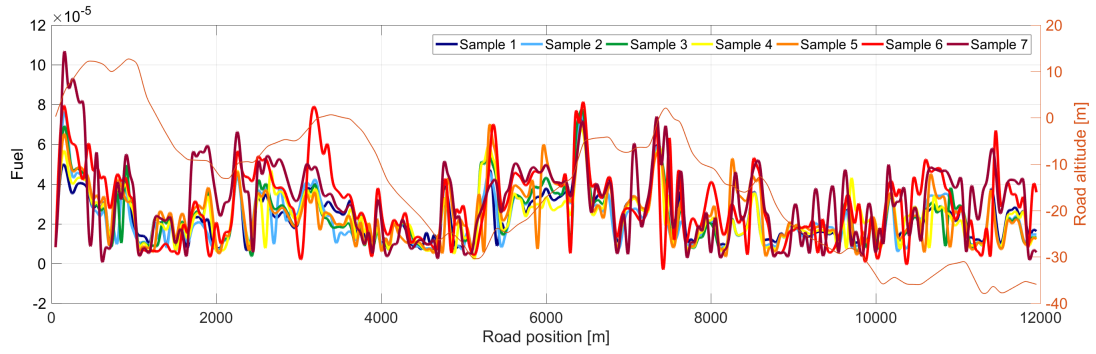


(b) NOx emission of MPC-2 samples.

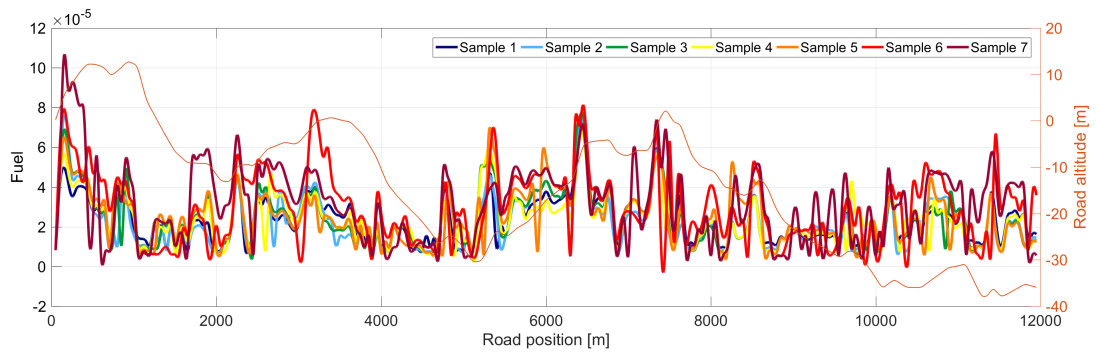


(c) NOx emission of DRL samples.

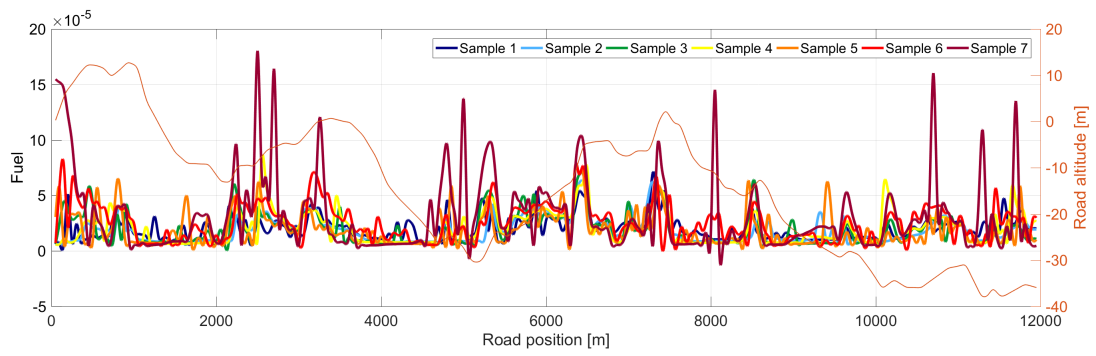
Figure 22: Comparison of NOx emission



(a) Fuel consumption of MPC-1 samples.

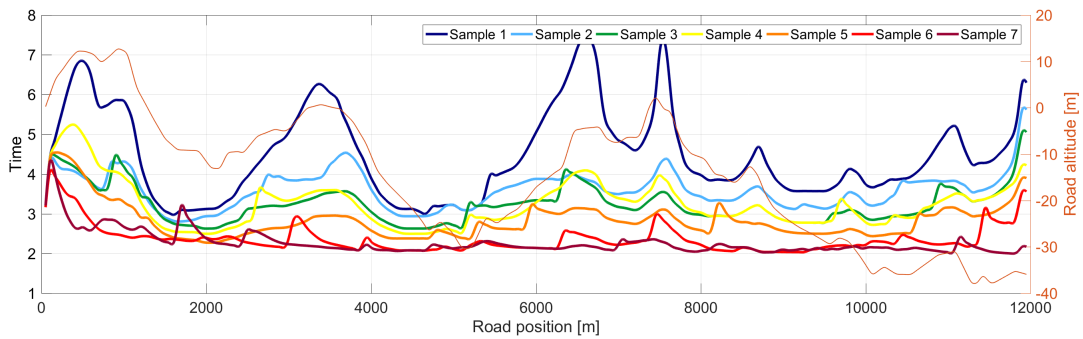


(b) Fuel consumption of MPC-2 samples.

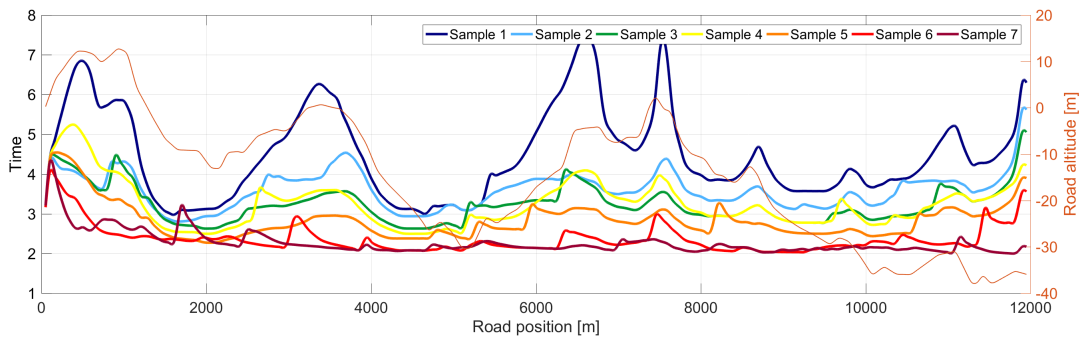


(c) Fuel consumption of DRL samples.

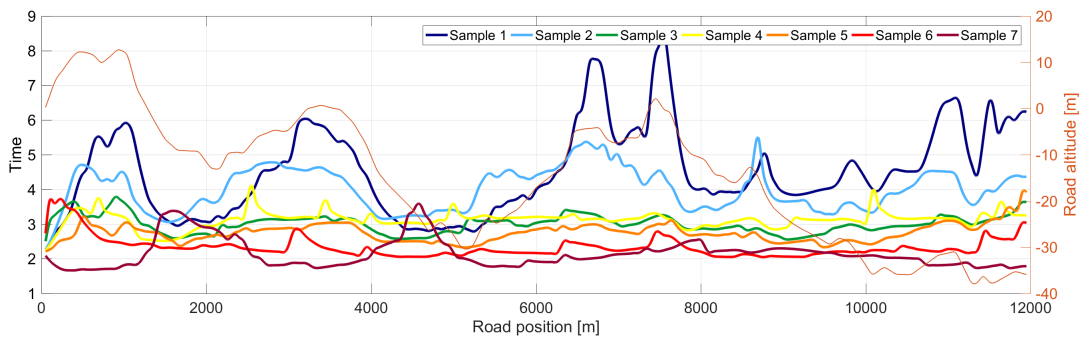
Figure 23: Comparison of fuel consumption



(a) Travel time of MPC-1 samples.

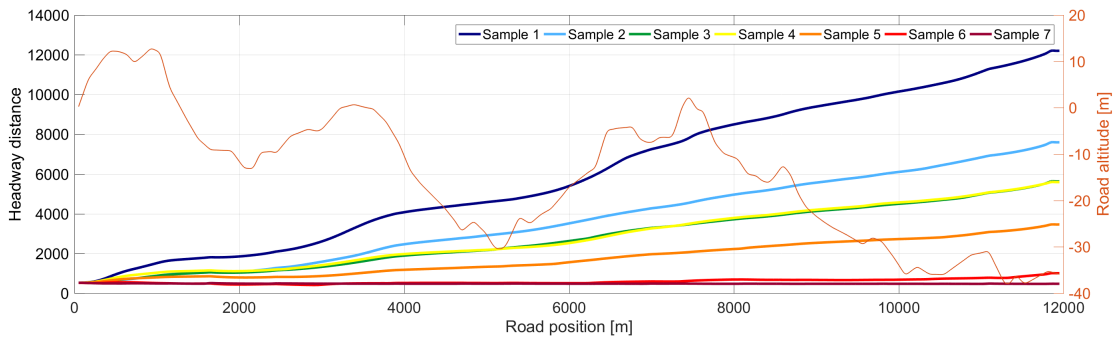


(b) Travel time of MPC-2 samples.

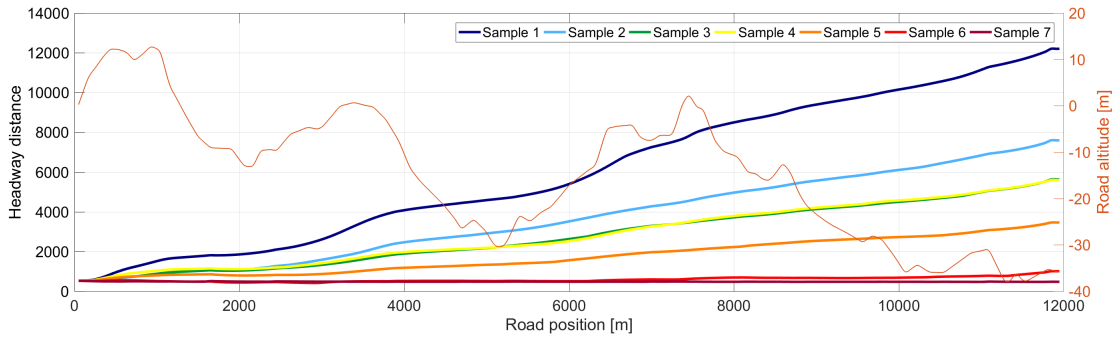


(c) Travel time of DRL samples.

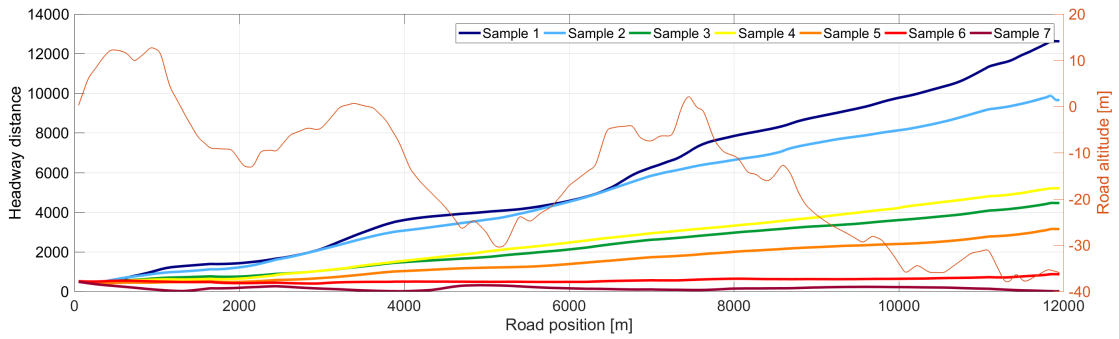
Figure 24: Comparison of Travel time



(a) Headway distance of MPC-1 samples.



(b) Headway distance of MPC-2 samples.



(c) Headway distance of DRL samples.

Figure 25: Comparison of Headway distance

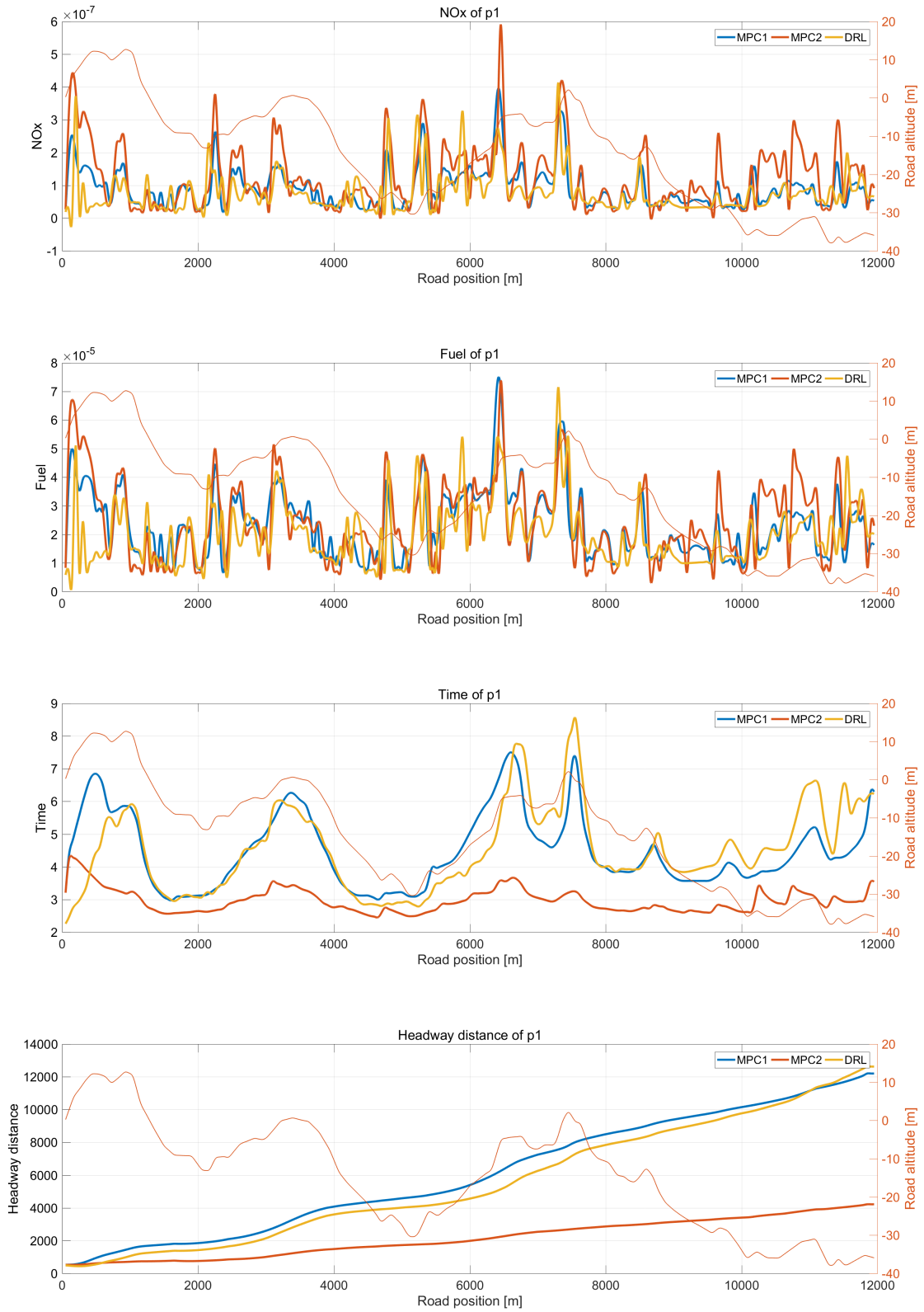


Figure 26: Comparison of results of  $p_1$  (minimum NOx)

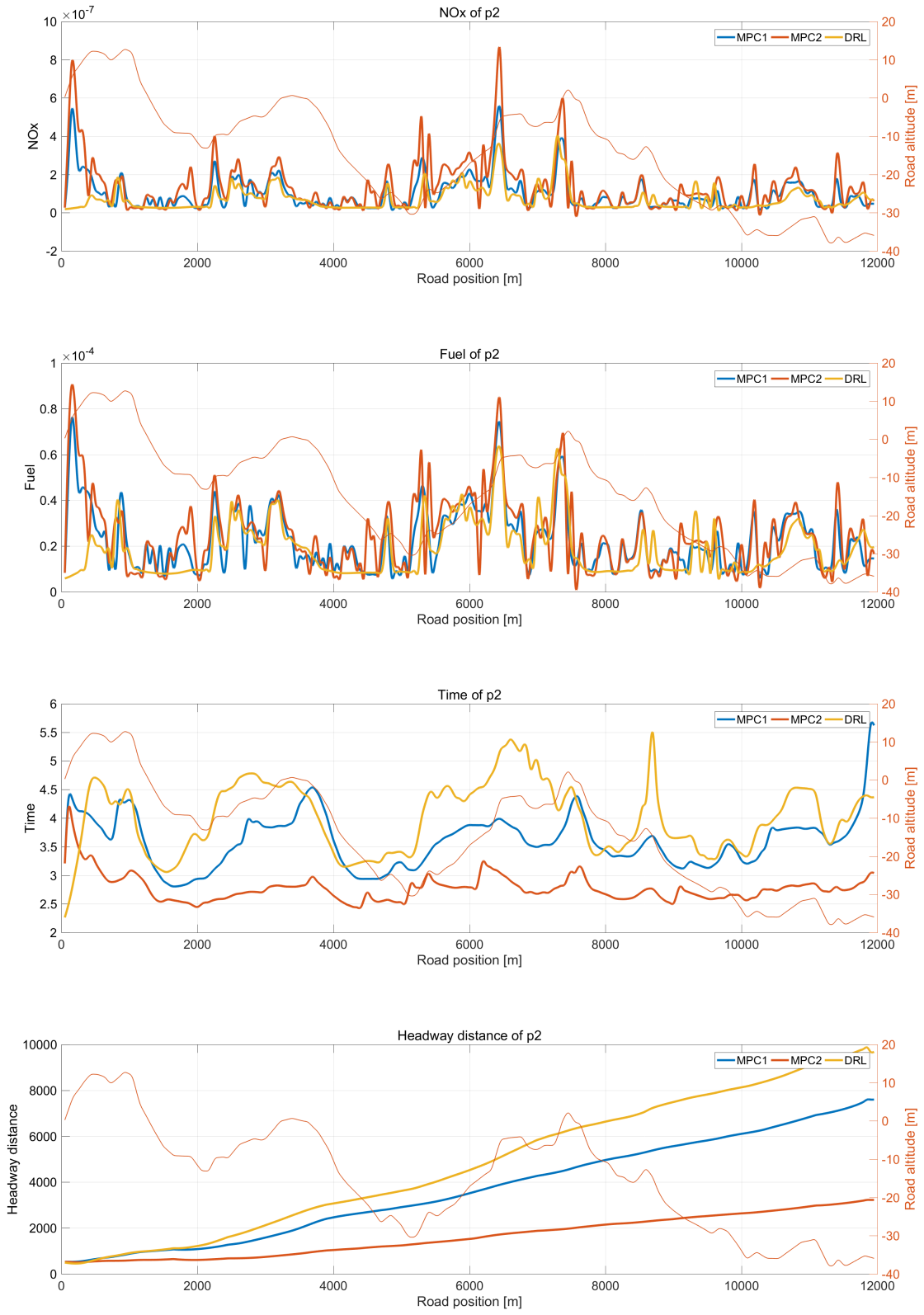


Figure 27: Comparison of results of  $p_2$  (minimum fuel)



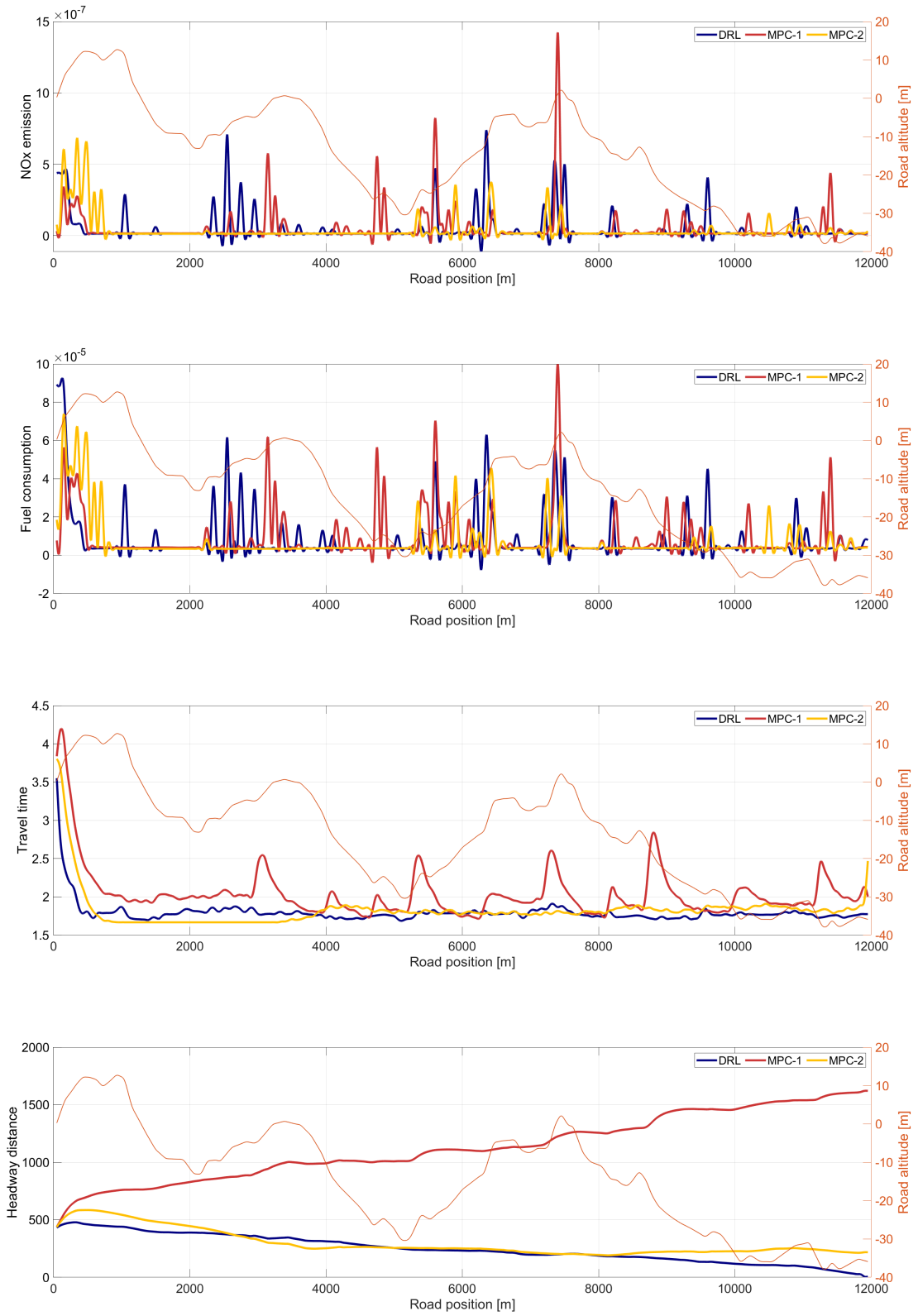


Figure 28: Comparison of results of  $p_7$  (minimum time)

1229 similarity across all three approaches. In terms of speed, the DRL approach positions itself between MPC-  
1230 1 and MPC-2, strategically finding a balance that minimizes the combined fuel and NOx values. This  
1231 measured approach to speed is complemented by the travel time and headway, both of which also fall within  
1232 the midpoint between the two MPC strategies.

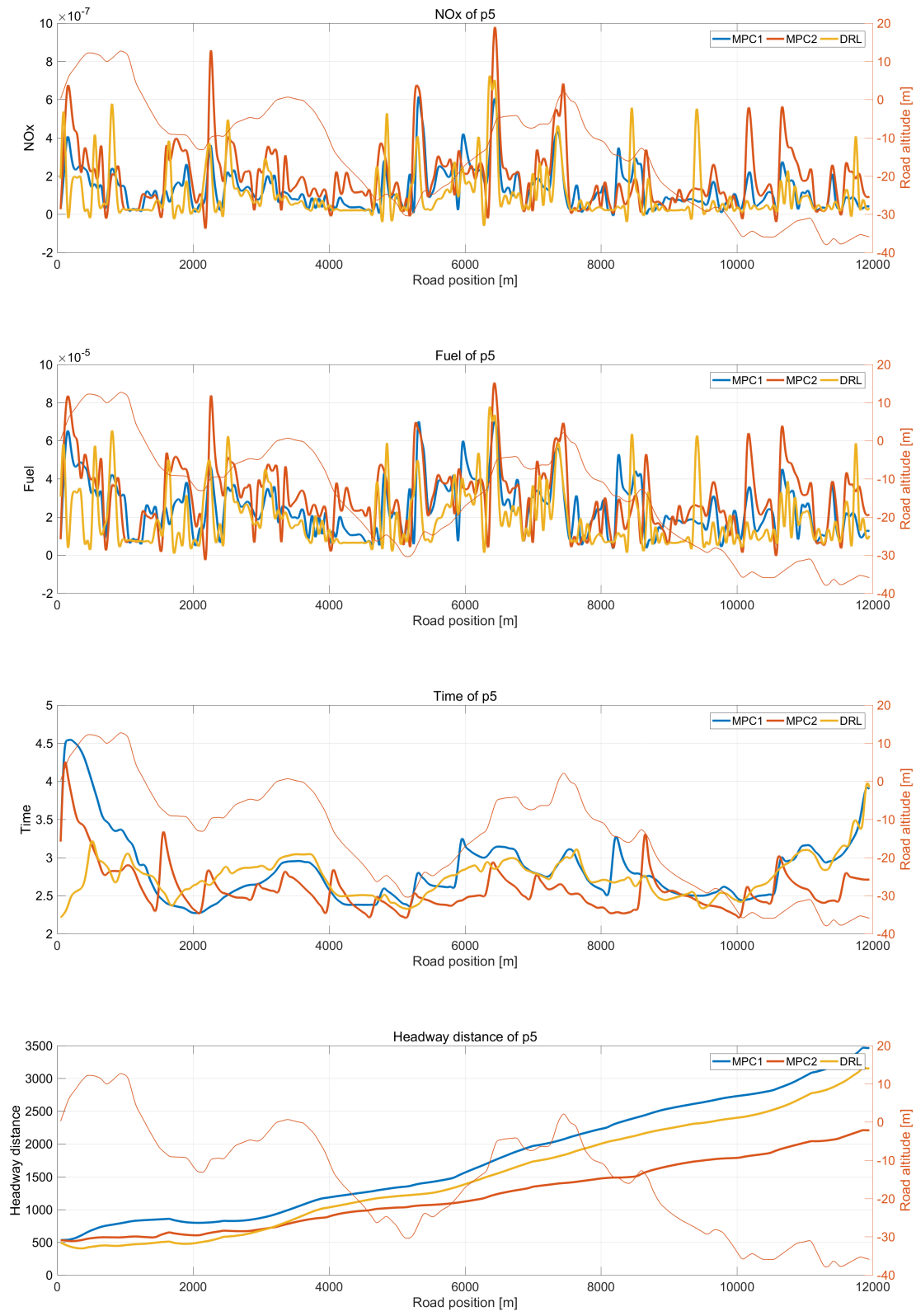


Figure 29: Comparison of results of  $p_5$  (knee point)