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1	A full-process, fine-grained, and quantitative rehabilitation assessment platform
2	enabled by on-skin sensors and multi-task gait transformer model
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28	Keywords: on-skin sensors, MG-former model, full-process rehabilitation assessments
29	lower limb movement disorders

Abstract

Rehabilitation of patients with lower limb movement disorders is a gradual process,
which requires full-process assessments to guide the implementation of rehabilitation
plans. However, the current methods can only complete the assessment in one stage and
lack objective and quantitative assessment strategies. Here, we develop a full-process,
fine-grained, and quantitative rehabilitation assessments platform (RAP) supported by
on-skin sensors and a multi-task gait transformer (MG-former) model for patients with
lower limb movement disorders. The signal quality and sensitivity of on-skin sensor is
improved by the synthesis of high-performance triboelectric material and structure
design. The MG-former model can simultaneously perform multiple tasks including
binary classification, multiclassification, and regression, corresponding to assessment
of fall risk, walking ability, and rehabilitation progress, covering the whole
rehabilitation cycle. The RAP can assess the walking ability of 23 hemiplegic patients,
which has highly consistent results with the scores by the experienced physician.
Furthermore, the MG-former model outputs fine-grained assessment results when
performing regression task to track slight progress of patients that cannot be captured
by conventional scales, facilitating adjustment of rehabilitation plans. This work
provides an objective and quantitative platform, which is instructive for physicians and
patients to implement effective strategy throughout the whole rehabilitation process.

1. Introduction

Many diseases such as stroke, Parkinson's disease, hemophiliac arthritis, etc., affect
the human body in the form of abnormal gait, resulting in the rising prevalence of lower
limb movement disorders, which cause great inconvenience or even life-threat to the
large number of patients ^[1] . For instance, there are about 10 million new cases of stroke
alone every year in the world, of which more than 70% of patients suffer from
movement disorders. Modern medical theory and clinical medicine have proved that
apart from early surgical and pharmacological treatment, scientific rehabilitation
training is equally important for patients with lower limb movement disorders ^[2] . In
particular, gait analysis and walking ability assessment are critical components in
rehabilitation medicine that allow physicians to assess ambulatory ability, diagnose
diseases, and formulate personalized rehabilitation programs ^[3] . However, conventional
gait analysis and walking ability assessment depend on the observation of physicians
regarding patients' movement, resulting in subjective results, while assessments based
on conventional scales lack fine-grained results ^[4] . For example, the conventional
Brunnstrom scale consists of only six levels, and the Tinetti gait assessment scale can
only give integer values within 0-12 points, which is difficult to capture the slight
progress made by patients in rehabilitation ^[5] . Besides, the assessment process is usually
carried out manually by physicians, which is difficult to meet the growing needs of
rehabilitation due to the workload burden ^[6] .
The rapid development of sensing technology has rendered gait analysis and
rehabilitation assessments more convincing with the support of quantitative data, which
provides a new assessment approach for clinicians to formulate more refined training
programs ^[7] . Among them, vision-based motion capture systems acquire spatial-
temporal parameters during walking, which can provide comprehensive information

about human movement ^[8] . Nonetheless, the motion capture systems are usually
complex and expensive, requiring skilled operators, and the recognition results can be
significantly affected by camera position and ambient light intensity ^[5a] . In terms of
wearable devices, inertial measurement units (IMUs) or pressure sensors are widely
adopted solutions to obtain information of human gait ^[9] . However, the gait monitoring
devices equipped with IMUs are bulky and inflexible, causing not only discomfort but
also errors in velocity and position data due to noise and signal drifting, while utilizing
plantar pressure distribution information alone is inadequate for those who require more
detailed gait information ^[10] . Besides, the surface electromyography (sEMG) combined
with kinematic and kinetic data is an effective approach to further assess muscle activity
levels and gait coordination ^[11] . Nevertheless, the weak sEMG signal strength (in
microvolts) and low signal-to-noise ratio affect the accuracy of assessment ^[12] . A
potential solution to address the above challenges lies in triboelectric sensors, which
are widely used to sense human motion and physiological activities by the high-quality
electric signals ^[11b, 13] . Fundamentally, the surface charge density induced by the
difference in electron affinity between two triboelectric materials greatly determines
the performance of triboelectric sensors ^[14] . Therefore, synthesis and optimization of
triboelectric materials are essential to achieve high electron affinity differences to
enhance the output performance of triboelectric sensors ^[15] .
Artificial intelligence technology has been widely adopted for disease diagnosis and
rehabilitation assessments, which has greatly promoted major progress in the field and
provided more reliable yet simpler solutions to complicated tasks. Previous studies have
utilized multi-feature fusion methods or support vector machines (SVM) by integrating
dynamic and physiological data to distinguish different walking patterns in stroke
natients. However, the multi-feature fusion and SVM require prior feature selection and

99	extraction, which may be suboptimal for time-series data, such as complex gait
100	signals ^[16] . Although deep learning approaches including convolutional neural networks
101	(CNN) and long short-term memory (LSTM) can automatically learn gait features, the
102	quantitative assessment of patients' walking ability cannot be achieved [17]. Besides, the
103	current algorithmic models can only perform a single-task in one stage of rehabilitation,
104	which hardly meets the needs of full-process rehabilitation assessments ^[18] . Hence, a
105	full-process and fine-grained rehabilitation assessments platform to quantitatively
106	assess the walking ability of patients is still highly desired.
107	In this work, we develop cost-effective on-skin sensors and an MG-former model to
108	build a full-process, fine-grained, and quantitative RAP for patients with lower limb
109	movement disorders. The on-skin sensors based on the coupling effect of contact
110	electrification and electrostatic induction are attached on the surface of dominant
111	muscle/tendon groups in lower limb to detect the deformation of skin during dynamic
112	gait movements and generate a series of electric signals. In addition, the signal quality
113	of the on-skin sensor is improved by synthesized triboelectric material and structure
114	design, with an average peak amplitude approximately 470 times higher than that of
115	traditional biopotential electromyography methods, demonstrating a promising method
116	for diagnosis and rehabilitation assessments. Based on the tasks of binary classification,
117	multiclassification, and regression performed by the MG-former model, the RAP can
118	complete the fall risk assessment, walking ability assessment, and rehabilitation
119	progress assessment, which covers the whole rehabilitation cycle and realizes full-
120	process rehabilitation assessments (Stage 1-3 in Figure 1a). By means of continual
121	learning, the MG-former model achieves an iterative update that improves the
122	assessment accuracy of the RAP from 90.67% to 93.33%. Besides, the results of the
123	RAP-based assessment of 23 hemiplegic patients match the scores obtained by

experienced physician according to the conventional Tinetti gait assessment scale. Furthermore, the rehabilitation progress assessment of patients with lower limb movement disorders for three consecutive weeks is completed to capture the slight progress based on the regression prediction task of the MG-former model, which is instructive for enhancing the patients' motivation and adjusting the rehabilitation plans.

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2. Results

2.1 Overview of the RAP and working principle

Figure 1a serves as a proof-of-concept demonstration of the full-process, fine-grained, and quantitative RAP based on on-skin sensors for gait diagnosis and rehabilitation assessments of patients with lower limb movement disorders, including fall risk assessment (Stage 1), walking ability assessment (Stage 2), and rehabilitation progress assessment (Stage 3), respectively. The flexible on-skin sensors are positioned on key muscle groups in the lower limb, which monitor overall movement patterns and behaviors of the patients, providing valuable data for gait diagnosis and rehabilitation assessments. The RAP integrates time-frequency domain analysis and MG-former model to perform multiple tasks such as binary classification (Task 1), multiclassification (Task 2), and regression (Task 3), corresponding to fall risk assessment, walking ability assessment, and rehabilitation progress assessment, respectively (Figure 1d). Here, a pair of high-elasticity triboelectric materials (polydimethylsiloxane/CaCu₃Ti₄O₁₂ nanoparticles (PDMS/CCTO) composite film and electrically conductive composites (ECC)) were developed to ensure the sensor can be conformally attached to detect subtle deformation resulting from lower limb movement during gait monitoring and rehabilitation assessments. Figure 1b presents a schematic diagram of the on-skin sensor, which consists of upper and lower layers. The upper

layer is formed by a PDMS encapsulation layer, a PDMS/CCTO composite triboelectric
layer, and a silver nanowires (AgNWs)-based top electrode. The uppermost PDMS film
can be used as an encapsulation layer to protect AgNWs, which can reduce the
interference of charges carried on external objects and improve the sensing accuracy.
Figure S2a illustrates the scanning electron microscopy (SEM) image of AgNWs,
which clearly shows that the single AgNW with a diameter of about $60~\mu m$ and the
AgNWs are interspersed with each other to form a conductive network, improving the
ductility of electrodes. The lower layer of on-skin sensor consists of ECC as bottom
electrode and triboelectric layer, and a PDMS substrate with arc-shaped protrusions
arranged in a circumferential array ^[19] . Notably, the arc-shaped protrusions were utilized
as the support structure for better separation after contact between the two triboelectric
layers.
Figure S2b shows the cross-sectional diagram of the ECC, where the thicknesses of
PDMS substrate and ECC electrode are about 220 μm and 50 μm , respectively, which
facilitates the conformal adhesion of on-skin sensor to skin surface to effectively
perceive the deformation of muscle/tendon. Besides, the side contacted with
PDMS/CCTO composite film presents a rough surface (Figure S2c), which increases
the effective contact area of the triboelectric layers, improving the signal quality. Both
the materials of the triboelectric pair in our study are highly stretchable and flexible
(maximum tensile limit of about 100%), enabling the accurate monitoring of skin
deformation (Figure S2d and e). More importantly, the ECC can be prepared with the
same polymer as the substrate, such as PDMS, to ensure strong adhesion between
interconnects and the substrate. Figure 1c-i and c-ii display the front and side optical
images of the on-skin sensor, respectively, and the specific fabrication details are
displayed in Section 4 and Figure S1a and b. Figure S2f-h show the on-skin sensor

during various mechanical deformation such as stretching, twisting, and bending,
demonstrating its good flexibility. Notably, all of the materials for building the key
components of the on-skin sensor are low-cost and fabricated through inherently
scalable and cost-effective methods. The fabricated on-skin sensor can actively capture
somatosensory signals by muscle motion (flexion and extension) and convert them into
distinguishable electric signals based on the coupling of triboelectrification and
electrostatic induction effect. The detailed working principle is elaborated in Figure S3
and Note S1, Supporting Information.

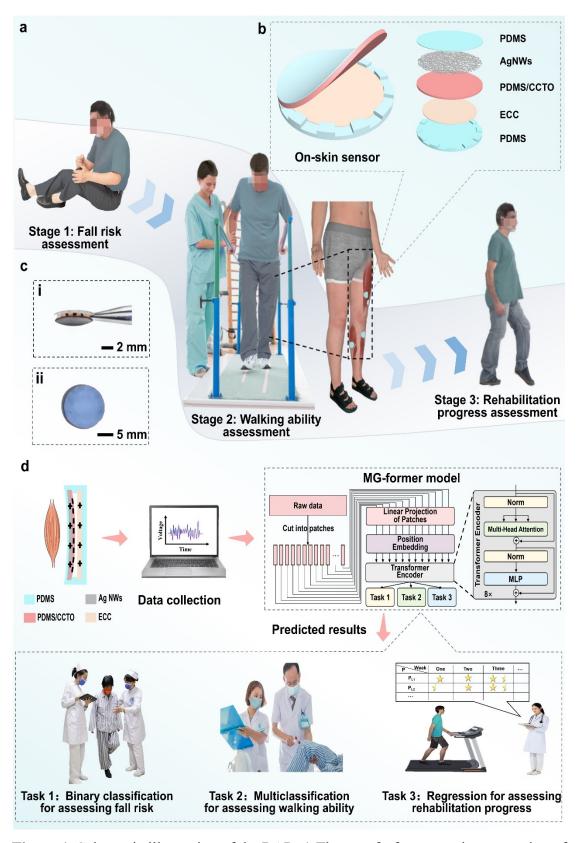


Figure 1. Schematic illustration of the RAP. a) The proof-of-concept demonstration of the full-process rehabilitation assessments platform. b) Schematic diagram of the onskin sensor. c-i and c-ii) The front and side optical images of the on-skin sensor. d) Schematic diagram of the full-process rehabilitation assessments for patients with lower limb movement disorders based on MG-former model.

2.2 Performance optimizations and characterizations of the on-skin sensor

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Typically, the output of the triboelectric sensor is inextricably related to the surface charge density of the triboelectric material^[15]. The maximum surface charge density (σ) is proportional to ε_r/d ($\sigma \propto \frac{\varepsilon_r}{d}$), where ε_r and d are the relative dielectric constant and effective dielectric thickness of the triboelectric layer^[20]. Based on literature review results (Table S10)^[15, 21], CCTO with a significantly higher dielectric constant ($\varepsilon_r =$ 7500) was selected as the dopant to improve the performance of the on-skin sensor. The CCTO is typical cubic-shape nanocrystal with an average particle size of ~300 nm, which are demonstrated by the SEM, transmission electron microscopy (TEM) and Xray Diffraction (XRD) results (Figure 2a-c)^[21e]. The inset of Figure 2a shows that elemental mapping was performed by energy dispersive spectroscopy (EDS) measurement to confirm the distribution of Ti, O, Cu, and Ca. Figure 2d shows the ε_r of composite films with different weight percentages (wt%) of CCTO. The results indicate that the addition of CCTO can significantly improve the ε_r of the PDMS/CCTO composite film. Specifically, compared to pure PDMS, the ε_r of PDMS/CCTO composite film is greatly enhanced from 4.7 (0wt% CCTO) to 8 (20wt% CCTO) at a frequency of 1k Hz. The incorporation of high dielectric constant materials, such as CCTO, into the base material (PDMS) enhances the dielectric constant by strengthening the polarization effect. This is attributed to the strong electric dipoles and high charge densities in the molecular structure of these materials, which facilitate charge redistribution and rearrangement under an external electric field^[15]. The formation of strong polarization interfaces between the high dielectric constant materials and PDMS further enhances the polarization effect, leading to an increase in the dielectric constant

of the composite films. Figure 2f displays the dependence of ε_r on temperatures ranging from 25 °C to 125 °C at frequency of 1 kHz, where ε_r decreases slightly with increasing temperature, which suggests that the PDMS/CCTO composite films exhibit excellent thermal stability. The surface roughness of the PDMS/CCTO composite films is shown in Figure 2g. It can be observed that the surface roughness of composite films increases with the increase of the content of CCTO. This can be attributed to the fact that as the doping concentration of CCTO increases, some CCTO particles tend to aggregate and cluster on the surface of the PDMS/CCTO composite film, leading to an increase in surface roughness^[21d]. The surface potential of the composite films was also examined by Kelvin probe force microscopy (KPFM) to further clarify the relationship between the doping content and the surface potential of the composite films. The contact potential difference (V_{CPD}) between the testing sample and platinum (Au) tip is determined by the equation:^[22]

$$V_{CPD} = \frac{\varphi_{tip} - \varphi_{sample}}{-e} \tag{1}$$

where φ_{tip} and φ_{sample} represent the work function of the tip and the sample, respectively, e is electronic charge (1.6 × 10⁻¹⁹ C). Since φ_{tip} is constant, the work function of the sample increases with the decrease of V_{CPD} value. The increase in work function renders the electron energy level lower, leading to easier reception of electrons on the PDMS/CCTO composite films during contact electrification. Figure 2h-i depicts that the V_{CPD} of pure PDMS is only -2.53 V, demonstrating the weak electron reception ability. By gradually adding CCTO powder into PDMS with gradient, the V_{CPD} value of the composite films was changed from -3.04 V (4%) to -5.51 V (20%), leading to a significant improvement in the charge-attracting property (Figure 2h-ii to Figure 2h-vi).

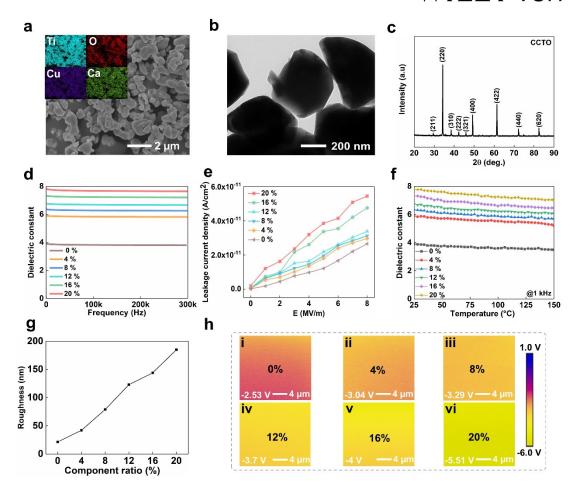


Figure 2. Characterizations and optimizations of the PDMS/CCTO composite films. The a) SEM, b) TEM, and c) XRD of CCTO nanoparticles. d) The ε_r and e) leakage current density of PDMS/CCTO composite films with the CCTO content from 0 to 20 wt%. f) The ε_r as a function of temperature at 1 kHz. g-h) The surface roughness and surface potential of the PDMS/CCTO composite films with different content of CCTO.

To evaluate the effect of CCTO content on the surface charge density of the composite film, the performance of the on-skin sensor made from composite films with different doping ratios were systematically characterized. As can be seen from **Figure 3a-c**, the open circuit voltage (V_{OC}), short circuit current (I_{SC}), and short circuit transfer charge (Q_{SC}) increase initially followed by an obvious decrease from wt% of 0% to 20%. The highest value of the V_{OC} , I_{SC} , and Q_{SC} is 11.4 V, 0.4 μ A, and 3.11 nC, respectively, at the doping ratio of 16%. Besides, when the content of CCTO is 0% (i.e., pure PDMS), the V_{OC} , I_{SC} , and Q_{SC} are only 6.99 V, 0.23 μ A, and 2.02 nC, which is increased by 64%, 73%, and 53%, respectively, when the wt% reaches 16%. This is due

to the increase of ε_r for composite film to capture charges, which improves the
performance of the on-skin sensor. In other words, the more negative the surface
potential value of PDMS/CCTO composite films, the more electron receiving ability
can be enhanced, which is consistent with the corresponding electrical output
characteristics of the electron (Figure 2h). Nevertheless, it is worth noting that the $V_{\rm OC}$,
$I_{\rm SC}$, and $Q_{\rm SC}$ decreased obviously at a CCTO content of 20%, which is due to the fact
that a high content of CCTO leads to a significant increase in the leakage current inside
the composite film (Figure 2e), thereby canceling out the triboelectric charges and
ultimately decreasing the output performance ^[20] . In addition, we also further
investigated the output performance of the on-skin sensor under different external
forces (Figure S5a-c), a linear motor (Figure S6) controlled by computer programming
was used to provide different loads and observed that output performance increased
gradually with increasing external force from 3.7 V, 0.14 $\mu A,$ and 1.41 nC at 5 N to 11.4
V, 0.4 μA , and 3.11 nC at 25 N. This is because the increase in the external force
increases the effective contact area between the two triboelectric layers, resulting in
more charge transfer to enhance the output performance.
Optimizing the performance of the on-skin sensor involves not only analyzing the
influence of triboelectric materials, but also considering the structure of the sensor. Here
the shape of the on-skin sensor was designed to be circular because the curvature of the
circular boundary is the same, which results in a small and uniform stress distribution ^[23]
The height of the arc-shaped protrusion (h) and the size of the central angle (α) were
chosen as key parameters to further investigate the subtle relationship between the on-
skin sensor structure and its performance. Figure 3d shows the stress distribution of on-
skin sensors with different α , which were analyzed by finite element analysis. Clearly,
the stress is relatively more uniform when α is decreasing at the same applied pressure

(1 N). However, a relatively smaller central angle (10°) results in a smaller area for each
arc-shaped protrusion, which leads to poor adhesion with the upper layer and affects
the durability of the on-skin sensor. Therefore, 15° is selected as the center angle in this
work. This carefully selected angle ensures that the stress distribution remains relatively
uniform while maintaining a sufficient area for each arc-shaped protrusion, thereby
promoting robust adhesion and durability. The height of the arc-shaped protrusion
determines the distance between the two triboelectric layers. Figure 3e describes the
influence of the height of the arc-shaped protrusions (0.4, 0.8, and 1.8 mm) on the
output signal of the on-skin sensor. Specifically, the on-skin sensor with h of 0.8 mm
achieved the best sensitivity, reaching 0.79 V/N, higher than the other two sensors in
the same force range (0.5-3 N). In addition, the signal obtained by the on-skin sensor
was compared with the commercial sEMG electrode to further demonstrate the
superiority of the on-skin sensor to retrieve muscle/tendon movement information.
Figure 3f shows the placement of an on-skin sensor (position 1) and the commercial
sEMG electrodes (position 1-3) on the right lower limb, which demonstrates the
convenience of the on-skin sensor. It is evident that the signal of the on-skin sensor
(1124 mV) displays more distinctive feature than sEMG signal (2.39 mV) during
dorsiflexion of foot movement, with an average peak amplitude approximately 470
times higher than sEMG (Figure 3g). Furthermore, the quality of the on-skin sensor
signal exhibits a significantly higher signal-to-noise ratio (SNR) of 34.07 dB in
comparison with the sEMG device's SNR of 18.34 dB (Figure 3h). The on-skin sensor's
higher sensitivity allows it to capture more subtle signals, but it may also amplify the
noise floor, resulting in a smaller difference in SNR compared to sEMG. Therefore,
although the average amplitude of the on-skin sensor is much larger than that of the
sEMG signal, the SNR of the on-skin sensor is not significantly increased compared

with the sEMG signal due to large signal noise. The more in-depth derivation and
calculation can be obtained from Note S2, Supporting Information. Figure 3i depicts
that the response and recovery time of on-skin sensor under the same pressure are only
53.6 ms and 64.2 ms, respectively, which further ensure the effective capture of human
gait-related triboelectric signals. The performance of the on-skin sensor remains almost
constant after about four months (Figure S7a) and 4, 000 cycles under different loading
forces (Figure 3j and Figure S7b-f, corresponding to 4 N, 5 N, 10 N, 15 N, 20 N, and
25 N, respectively.), which proves the great stability and reliability of the on-skin sensor
as a feasible method for long-term rehabilitation monitoring applications. Besides,
Figure S7b and g-i illustrate the relationship between the humidity and the output
performance of the on-skin sensor. It is worth noting that although the increase in
humidity inhibits the active ability of some of the electrons, resulting in a slight
decrease in performance, the output of the on-skin sensor remains relatively stable at
54% humidity.

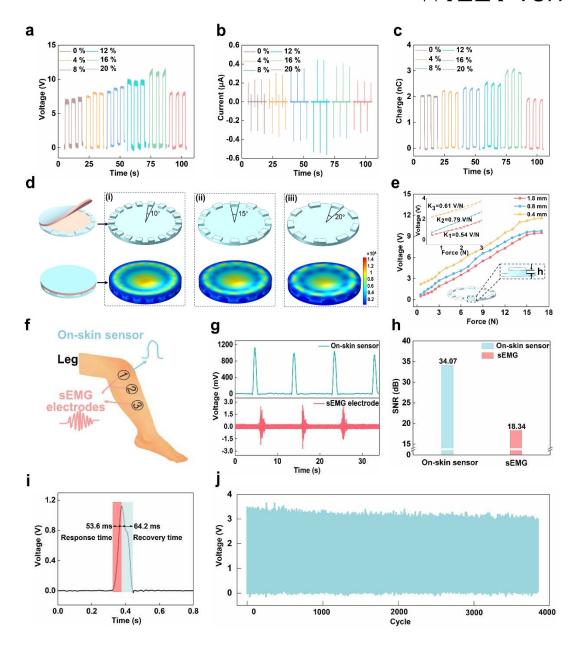


Figure 3. Characterizations and optimizations of the on-skin sensor. a-c) The $V_{\rm OC}$, $I_{\rm SC}$, and $Q_{\rm SC}$ of the on-skin sensor with different content of CCTO. d) The stress distribution of the on-skin sensor with different α were analyzed by finite element analysis. e) The influence of the height of the arc-shaped protrusions on the output signal of the on-skin sensor. f) The schematic illustration showing the placement of the on-skin sensor and the commercial sEMG electrodes on the right lower limb. g) The corresponding output voltage signals generated by the on-skin sensor and the sEMG electrodes, respectively. h) The SNR value of the on-skin sensor and sEMG electrodes. i) The response and recovery time of the on-skin sensor. j) The stability testing of the on-skin sensor.

2.3 Diagnosis and symptom analysis of abnormal gait

As one of the most common behavioral characteristics, gait is not only instinctively controlled by human joints, muscles, and nervous system, but also affected by key

information such as biomechanical and kinematic parameters ^[24] . According to the
muscle functions of each part in Table S1, the rectus femoris (RF), vastus lateralis (VL),
tibialis anterior (TA), and gastrocnemius (GM) were selected as signal source muscles
for diagnosis and rehabilitation assessments (Figure S8) ^[25] . Figure S9a and b illustrate
the optical images of the on-skin sensors on the lower limbs, respectively. The on-skin
sensor is firmly adhered to the skin surface by a medical waterproof polyurethane (PU)
film ^[26] . Besides, a pair of force sensing resistors (FSR) labeled FSR1 and FSR2 were
arranged on the front and back sides of a shoe to capture plantar pressure signals during
walking (Figure S9c).
As depicted in Figure 4a and b, the gait phase of one lower limb, which can be
divided into stance phase (Pre-stance, Mid-stance, and Ter-stance) and swing phase
(Pre-swing and Ter-swing) by plantar pressure signals, where the stance phase is
characterized by the stability of body's center of gravity, while the swing phase involves
the active forward swing of lower limb ^[27] . Figure 4b and Figure S10a illustrate the gait
signals generated by a healthy subject (H1) walking on a treadmill at regular speed. It
can be seen that most of the signals of on-skin sensors generated by muscle triggering
occur in swing phase, which is due to the fact that during the swing phase, the human
body needs to quickly adjust the posture and orientation as well as maintain the body
balance. Specifically, during the stance phase the muscles are in a contracted state
causing the two triboelectric layers to contact each other so that no charge transfer
occurs (Figure S3i). In contrast, the muscle relaxation during the swing phase causes
the two triboelectric layers to separate, generating a variable electric field that drives
the flow of free electrons in an external circuit to form a current (Figure S3ii). As can
be observed from Figure 4b, the time interval (T) between voltage signal peaks can
represent step frequency (1/T), while the signal amplitude reflects the strength of

contraction or propulsion force generated by the muscle. Meanwhile, the duration of
stance phase is about 60% of the whole gait cycle, which can also be demonstrated by
the experimental results of two other subjects (Figure S10b and c). We further
investigated the attachment of the on-skin sensor to the skin and evaluated its stability
and potential skin irritation or discomfort during long-term wear. It can be seen that
after 2 hours of continuous wear, there is no adverse reaction, irritation or discomfort
on the part of the human skin in contact with the sensor or PU film (Figure S10e and f).
Besides, the human skin in contact with the sensor can be recovered to the initial state
in about 8 minutes (Figure S10h-j), which again demonstrates that the on-skin sensor
does not cause irritation or discomfort to the skin even if worn for a long time. Moreover
the upper and lower layers of the on-skin sensor are connected tightly without any
delamination (Figure S10g). The stability of the on-skin sensor was demonstrated
through long-term testing of the subject wearing the on-skin sensor (e.g., tibialis
anterior (TA)), as shown in Figure S10d. The result shows that there is no obvious decay
or degradation of the output voltage during gait data collection, which validates good
stability and reliability of on-skin sensor.
In general, the impact of many diseases on the human body is exhibited in the form
of abnormal gait. For instance, the gait of the patient with post-stroke hemiplegia
(Figure 4c) is mostly characterized by instability, poor symmetry, abnormal rhythm,
and reduced balance and coordination ^[6] . Figure 4d and e present the gait signals of two
post-stroke hemiplegic patients (P1 and P2, as shown in Figure S11a and b,
corresponding to Movie S1 and Movie S2.) during walking at an adaptive speed on a
treadmill. As shown in Figure 4f and Movie S1, the peak-to-peak value of the on-skin
sensor signal generated by GM muscle deformation ($V_{\mathrm{PP-GM}}$) is the highest in a normal
person, followed by the unaffected side of P1, while the affected side of P1 is the lowest.

Notably, the power spectral densities of V_{PP-GM} also exhibit a similar trend, which can
give a key feature to assess the progress made by the patients during rehabilitation. This
difference is mainly due to the reduced or even loss of motor ability on the side of body
caused by the damage of central nervous system (CNS), while the muscle strength on
the unaffected side is relatively stronger, which renders the muscle deformation more
pronounced during walking and enhances the amplitude of the triboelectric signals ^[28] .
Besides, as presented in Figure 4d-i and d-ii, the duration of the stance phase on the
affected side is slightly shorter than that on the unaffected side ($t_{1U} > t_{1A}$), while the
swing phase shows the opposite trend ($t_{2U} < t_{2A}$). This is because hemiplegia has
reduced weight-bearing capacity on the affected side, which cannot provide adequate
support during walking. In order to maintain the stability of the body, it is necessary to
rely on the unaffected side to compensate for part of the weight ^[6, 29] . Therefore, patients
with post-stroke hemiplegic walk with a shorter duration of stance phase and a longer
duration of swing phase on the affected side compared to the unaffected side,
demonstrating an asymmetry in the spatiotemporal parameters of gait. For P2 (Movie
S2), the gait signal on the unaffected side presents the same irregular characteristics as
the affected side, which can be reflected by the low amplitude and chaotic oscillatory
signals from the sensors (Figure 4e-i and e-ii). This is because the P2 is more severely
than P1 and requires orthosis to maintain correct posture and provide stable support in
daily life. Clearly, long-term compensation for the loss of muscle function on the
affected side also affect the function of the unaffected side.

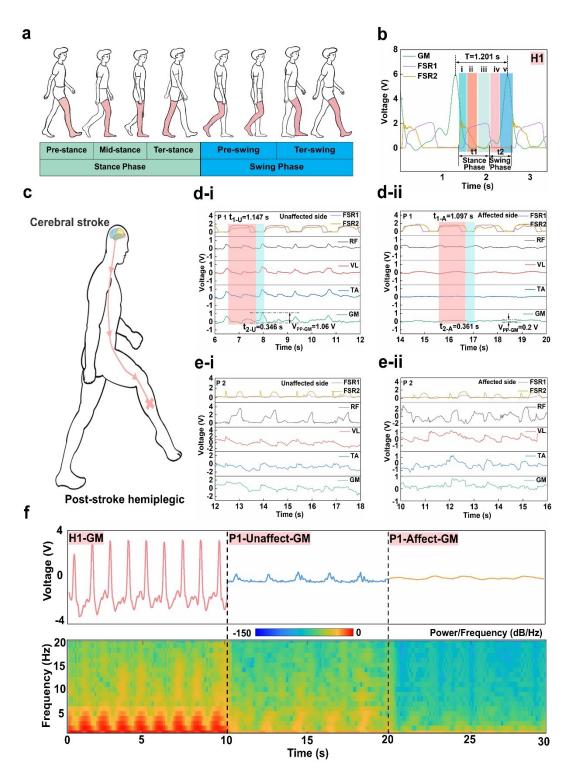


Figure 4. Diagnosis and symptom analysis of patients with post-stroke hemiplegia (P1 and P2). a) Schematics of a typical gait cycle and b) the corresponding signals of normal walking. c) Schematic diagram of walking for a stroke patient with hemiplegia. The gait signals on the unaffected side d-i) and affected side d-ii) of P1. The gait signals on the unaffected side e-i) and the affected side e-ii) of P2. f) The voltage signals (top) generated by the GM of H1, the unaffected side, and affected side of P1, respectively, and their power spectral densities (bottom).

2.4 The full-process rehabilitation assessments platform based on MG-former

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The full-process rehabilitation assessments (Stage 1-3: fall risk, walking ability, and rehabilitation progress assessment) are indispensable parts of the rehabilitation process for patients with lower limb movement disorders, which is of great importance in guiding rehabilitation programs and ensuring patients safety. Falls, as one of the common adverse events in the rehabilitation process of patients with lower limb movement disorders, have a serious impact on the subsequent rehabilitation of patients^[30]. Therefore, the fall risk assessment is the first part of the assessment, which is considered as the foundation of fall prevention. Besides, the quantitative and objective walking ability assessment is essential to accurately understand a patient's current level of rehabilitation, which is crucial for making personalized rehabilitation plans^[5a]. Furthermore, the fine-grained rehabilitation progress assessment can capture the slight progress made by patients, which is beneficial for enhancing the patient's motivation and adjusting the rehabilitation plans. Here, we proposed an MG-former model to take advantages of potential relationship between multiple tasks to improve performances on multiple interrelated tasks. Figure 5a demonstrates the schematic structure of the MG-former model, which can simultaneously perform multiple tasks including binary classification (Task 1), multiclassification (Task 2), and regression (Task 3). The MG-former model based on self-attention mechanism of transformer can provide rich and robust contextual information when processing sequential data, which is beneficial to accurately capture local or global features in the gait signal and adaptively learn the correlation between different parts^[31]. During the data collection process, we employed a 30 Hz low-pass filter using an NI data acquisition card to remove high-frequency noise and interference.

This filtering step is crucial in obtaining high-quality gait signals from the on-skin sensors. The signals with periodicity from on-skin sensors and FSR, which contain diversified information about a dynamic gait cycle, e.g., stride frequency and contacting force between feet and shoes, are cut into a sequence of patches. The size of the patch is closely related to the accuracy of the modelling algorithm, which is set to 100 samples (0.1 seconds × 1000 Hz). Then, the patch sequences are fed into the MG-former model, which consists sequentially of linear projection of patches, position embedding, stacks of transformer encoders, and multitask heads. Each transformer encoder encompasses layer normalization, multi-head self-attention, and multi-layer perceptron (MLP). Finally, the walking ability assessment results are generated from the corresponding task heads. To provide sufficient depth and modelling capability for gait data, the structure of the 8-layer transformer encoder stack was designed. Specifically, each encoder has an 8 attention heads, a forward propagation dimension size of 512, and an MLP with a single layer dimension size of 2048. In addition, the gaussian error linear unit (GELU) was used as the activation function as well as maintaining a dropout rate of 0.1. With each subject, the whole data was divided into the training set (60%) and testing set (40%). The detailed description of the MG-former model is presented in Note S3, Supporting Information.

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2.4.1 Task 1: The screening for abnormal gait for fall risk assessment (Stage 1)

Many diseases affect the human body in the form of abnormal gait, leading to increased risk of falls due to balance dysfunction in patients. Therefore, abnormal gait screening can be utilized for fall risk assessment, which is of great significance for physicians to implement early interventions to ensure patient safety. Here, an attending physician from the department of rehabilitation medicine with 10 years of clinical experience in rehabilitation assessment was invited to assess the fall risk of patients

according to the conventional Berg Balance Scale (BBS), which served as the golden
standard ^[32] . Specifically, the total score of the BBS is 56 points, with a lower score
indicating weaker balance function, and the score less than 40 points indicates the
greater risk of falling (Table S2). The results of fall risk assessment from the
experienced physician for 15 post-stroke hemiplegic patients (P1-P15, Table S3) in
Table S4. Based on the gold standard from the experienced physician, the patients were
categorized into two distinct groups: individuals with a lower risk of falling (The score
of BBS greater than 40 or equal to 40 points) and those with a higher risk (The score of
BBS less than 40 points). Through analyzing the gait data of the patients, the MG-
former model enables automated fall risk assessment through binary classification
(Task 1). This process identifies the high-risk population promptly, facilitating timely
interventions and preventive measures.
In order to visualize the overall clustering of the entire gait dataset, we introduced t-
distributed stochastic neighbor embedding (t-SNE) in the 2D feature space. The two
different colors represent subjects at lower fall risk (light blue) and higher fall risk (rosy
red) and each point refers to a sample of gait data projected from the high-dimensional
to two dimensions. Figure 5b and c illustrate the t-SNE distributions of subjects with
lower and higher fall risk in output layer of the MG-former model before and after
training when performing the binary classification task (Task 1). The results
demonstrate that there is an optimal feature clustering after training with the MG-former
model, in which subjects with higher and lower fall risk display less overlap and strong
interclass separability.
2.4.2 Task 2: The objective and quantitative walking ability assessment (Stage 2)
After performing the fall risk assessment, the experienced physician was invited to

assess the walking ability of the patient according to the conventional Tinetti scale

483 (Table S5)^[5a].

484	Firstly, the walking ability of the patients (P1-P15) was assessed by the experienced
485	physician based on the Tinetti scale (0-12 points) as the gold standard (Table S6) for
486	the assessment of the MG-former model. Each point on the Tinetti scale is considered
487	a category in 13 categories, where the higher score represents the better walking ability
488	of the subject. Then, the MG-former model combines the high-quality gait signals
489	captured by the on-skin sensors with the gold standard to achieve quantitative
490	assessment. Specifically, a 13-category classification task (Task 2: multiclassification)
491	based on the MG-former model was also implemented to quantitatively assess the
492	walking ability of 9 healthy subjects and 15 post-stroke hemiplegic patients by
493	supervised learning. Finally, the output category of the model is the prediction score of
494	the corresponding patients.
495	Since the gait signal is a periodic time-sequence signal, an appropriate sliding
496	window length is crucial for capturing the signal features of the complete gait cycle. At
497	the same time, it can effectively avoid the computational complexity caused by a large
498	sliding window length and the incomplete signal feature capture due to a short sliding
499	window length. Figure 5d demonstrates the effect of different sliding window lengths
500	on the accuracy of gait assessment, which corresponds to a maximum of 96.18%
501	accuracy when the sliding window length is 15 s. As presented in Figure 5e and Figure
502	S12, the results of walking ability assessment by means of the RAP are almost identical
503	to the scores given by the physician based on the conventional Tinetti gait assessment
504	scale, which demonstrates the validity of the RAP. It is worth noting that the results of
505	the walking ability assessment using RAP are presented in the form of mean and
506	standard deviation. This is because each subject's data is divided into multiple samples
507	using a sliding window, as mentioned earlier. Then, these samples are sequentially input

508	into the MG-former for assessment, and the average value and standard deviation of
509	each subject's assessment results are calculated. A smaller standard deviation indicates
510	lower variability in the assessment results, which implies more reliable outcomes.
511	Figure 5f illustrates the training process of MG-former model, highlighting the changes
512	in accuracy and overall loss function, as well as demonstrating that the neural network
513	can quickly obtain high recognition accuracy and exhibit good stability.
514	As shown in Figure S14a-e, different types of classification algorithms including
515	CNN, LSTM, fully connected networks (FCN), SVM, and random forest (RF) were
516	used to assess the walking ability of hemiplegic patients with stroke (P1-P15). By
517	comparing the different algorithms, it is found that the accuracy of MG-former model
518	is better than other models (Figure 5g), which indicates that MG-former model shows
519	clear advantages in processing sequential data. This is because the MG-former model
520	is attention mechanism-based and elucidates the nature of the input sequence,
521	dispensing with recurrence and convolutions entirely, thereby allowing input
522	dependencies modeling without regard to distance and enabling the assessment of
523	complex long-range correlations ^[31] . Meanwhile, the MG-former model enjoys
524	significant parallelizability and global receptive field thanks to self-attention. Therefore,
525	the MG-former model tends to achieve superior performance in large-scale and
526	complex sequential data tasks, especially gait signals. Clinically, hemiplegic gait
527	usually exhibits common characteristics such as decreased step length and gait velocity,
528	as well as increased bilateral asymmetry. However, there are also differences in age,
529	physical condition, and severity that inevitably lead to individual differences in gait of
530	hemiplegic patients. Therefore, it is difficult to build a comprehensive dataset for the
531	gait of hemiplegic patients at one time. Continual learning of the model is an optimum
532	strategy to solve the above problems. The detailed description of the iterative update of

533 the MG-former model is presented in Note S4, Supporting Information.

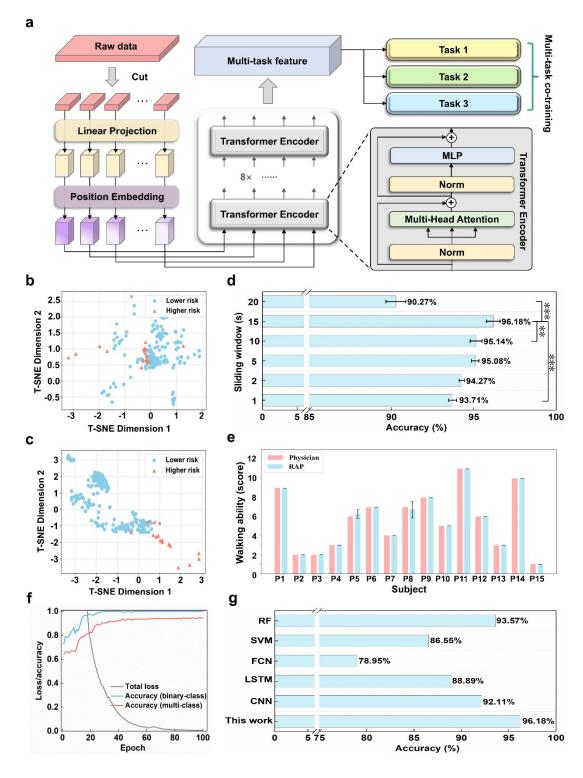


Figure 5. Rehabilitation assessments based on the MG-former model. a) The schematic structure of the MG-former model. b-c) The t-SNE distributions of subjects with higher and lower fall risk in output layer of the MG-former model before and after training when performing the binary classification task. d) The effect of different sliding window lengths on the accuracy of assessment. p-Values were calculated using a oneway ANOVA program with Tukey's multiple comparisons post hoc test. (*p < 0.05,

p < 0.01, *p < 0.001, and ns = no significant difference). Data in d) are presented as mean values \pm SD, n = 5. e) The comparison of the results of walking ability assessment by an experienced physician and RAP for 15 post-stroke hemiplegic patients (P1-P15). Data in e) are presented as mean values \pm SD, n = 3. f) Loss-accuracy curve during model training. g) The comparison of walking ability assessment results based on different types of machine learning model.

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2.4.3 Task 3: The fine-grained rehabilitation progress assessment (Stage 3)

Rehabilitation progress assessment (Figure 6a) plays an essential role in making rehabilitation plans, preventing complications, and assessing progress during the longterm rehabilitation process. However, conventional rehabilitation progress assessment methods struggle to capture these subtle advances, as they usually fall below the minimum precision discernible by such scales. Therefore, in order to further precisely and quantitatively track the progress made by the patients in rehabilitation process, the MG-former model performs the third task (Task 3), i.e. regression prediction (Figure 6b). As shown in Figure 6c-i and c-ii, two patients (P_{L1} and P_{L2}, Table S9) with lower limb movement disorders, were invited to perform monitoring for three consecutive weeks. As shown in Figure 6d-f and Movie S3-S5, the V_{PP-GM} of P_{L1} gradually increased from 0.6 V to 5.11 V after 3 weeks of rehabilitation and the average energy also gradually increased (Figure S18), which indicated that the muscle strength of patient was improved, as well as indirectly proved the effectiveness of the implemented rehabilitation strategy. As presented in Figure S19a, by observing the pressure signals of FSR (V_{FSR}) of P_{L2} , it was found that the patient exhibited an abnormal gait during the walking, characterized by simultaneous elevation and descent of the heel and the toe. Excitingly, the abnormal gait of P_{L2} was recovered after three weeks of rehabilitation training, and the value of FSR2 gradually increased to FSR1, indicating an even distribution of force between the heel and toes during walking (Figure S19a-c and Movie S6-S8). Furthermore, the comparisons of the V_{PP-GM} of P_{L2} over three weeks reveals a clear increase in the amplitude and the average energy of the triboelectric

570	signal (Figure S21), suggesting that the level of muscle strength of the patient has been
571	improved. The detailed descriptions of P _{L1} and P _{L2} is presented in Note S5, Supporting
572	Information.
573	As for the MG-former model, it allows each task to benefit from co-training with
574	other related tasks, which jointly improves the generalization of the model. Thus, the
575	Task 3 can utilize the gait information from Task 1 and Task 2, especially the gait data
576	from the previous 23 patients (P1-P23), to achieve efficient learning under inexact
577	supervision. Specifically, the regression task head of the MG-former model
578	incorporates an additional 8 decoder layers to further capture the slight progress of the
579	patient's rehabilitation process, which includes both time-domain information (Figure
580	6g and Figure S20) and frequency-domain information (Figure S18 and S21). At the
581	same time, the gait data excluding P_{L1} and P_{L2} were used as the training set and the
582	mean square error of minimizing the assessment scores was taken as the objective
583	function. After training, the MG-former model assessed the walking ability of P_{L1} and
584	P _{L2} based on their multiple sets of sliding window data over three weeks and output a
585	continual value (in the range of 0-12 points) as the result of the walking ability of the
586	patients. The mean of the patient's walking ability assessment results of each week was
587	used as the final result for that week to obtain a more objective assessment. Therefore,
588	the score indicates the walking ability of the patient, where higher score demonstrates
589	better physical recovery. In contrast to the discrete values (integer values in the range
590	of 0-12 points) output from performing the classification task (Task 2), the MG-former
591	model can output continual value (continuous values in the range of 0-12 points) when
592	performing the regression task (Task 3), which can assess the slight progress of patients

in the rehabilitation process that cannot be captured by conventional scales. Figure 6h

and i display the fine-grained rehabilitation progress assessment results based on MG-

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former model within 3 weeks for P _{L1} and P _{L2} , respectively. Clearly, the assessment
results of P _{L1} within three weeks were 7.94, 7.89, and 8.42 points respectively, which
showed that the rehabilitation progress was not obvious in the first and second weeks,
but there was a greater improvement in the third week. For P _{L2} , the walking ability of
the patient was steadily improving during the rehabilitation period, gradually increasing
from 7.9 to 8.1 points. By capturing the slight progress made by $P_{\rm L2}$ in the rehabilitation
process through the RAP, the P _{L2} are encouraged to actively participate in rehabilitation
and enhance his self-confidence. Specifically, the $V_{\rm FSR2}$ gradually increased from 0.46
V to 1.41 V close to the $V_{\rm FSR1}$ after 3 weeks of rehabilitation (Figure S19a-c). It is worth
noting that, compared with the coarse-grained assessment results of the conventional
Tinetti gait assessment scale (integer values in the range of 0-12 points, e.g., 7 or 8
points), the RAP based on the regression task of the MG-former model can capture the
slight progress of the patient's rehabilitation process with fine-grained assessment
results (continuous values in the range of 0-12 points, e.g., 7.9 or 8.1 points), which is
beneficial for adjusting the rehabilitation plans and improving the patient's motivation.
Moreover, the fine-grained assessment results provided by RAP can identify potential
issues in the rehabilitation process for early intervention and prevention of
complications. This is important for patients with lower limb movement disorders,
where small improvements can have a significant impact on their overall quality of life.
In addition, slight improvement shown by fine-grained assessment results can also
improve self-confidence and encourage the patients to be more active to participate in
rehabilitation.

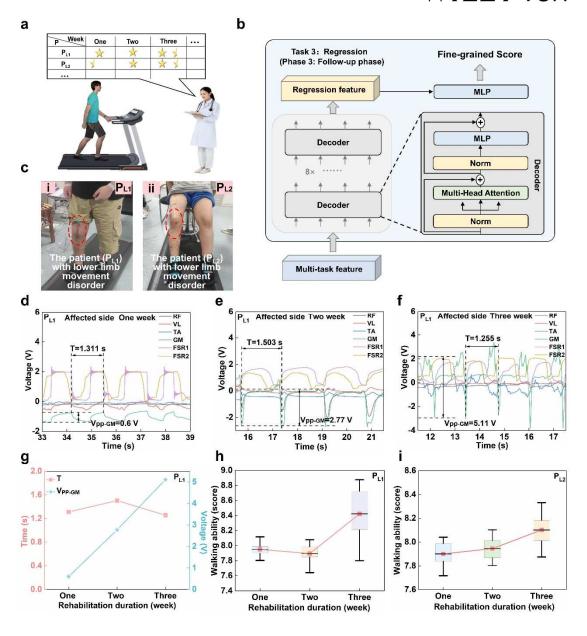


Figure 6. The fine-grained rehabilitation progress assessment based on the MG-former model. a) The diagram of rehabilitation tracking. b) The schematic structure of the MG-former model performs the regression prediction. c-i and c-ii) The photos of patients (P_{L1} and P_{L2}) with lower limb movement disorders. d-f) The complete gait signals on the affected side of P_{L1} for 3 weeks during rehabilitation. g) The evolution of the time intervals (T) and V_{PP-GM} for P_{L1} with the rehabilitation period. h-i) The rehabilitation progress assessment results of P_{L1} and P_{L2} for three consecutive weeks based on the MG-former model. Data in h) and i) are presented as mean values \pm SD, n = 3.

3. Discussion

In summary, we have reported a full-process, fine-grained, and quantitative RAP for patients with lower limb movement disorders, which covers the whole rehabilitation

cycle and realizes an objective and quantitative rehabilitation assessments. Compared
with existing methods that can only perform a single-task in one stage of rehabilitation
and hardly meet the needs of full-process rehabilitation assessments, this work provides
a quantitative and fine-grained approach, which can perform multiple tasks including
binary classification, multiclassification, and regression, corresponding to fall risk
assessment, walking ability assessment, and rehabilitation progress assessment,
respectively, which is beneficial for physicians and patients to implement effective and
timely plans throughout the whole rehabilitation process. The flexible and lightweight
on-skin sensors allow for direct contact with human skin to enhance the wearing
comfort, and the signal quality of on-skin sensor is improved by material and structure
design, resulting in a higher SNR compared with commercial sEMG electrodes. By
continual learning, the MG-former model achieves an iterative update that allows the
RAP to quantitatively assess the walking ability of 23 hemiplegic patients, and the
results agree with the scores given by the physician according to the conventional
Tinetti gait assessment scale, verifying the accuracy of the method. It is noteworthy that
the application of machine learning not only renders the results of rehabilitation
assessment more objective and precise, but also saves a considerable amount of labor
costs. Furthermore, the RAP based on the regression task of the MG-former model can
accurately assess the patient's slight progress in the rehabilitation process with fine-
grained assessment results, outperforming the coarse-grained assessment of
conventional walking ability assessment scales. The fine-grained rehabilitation
progress assessment of patients with the support of RAP was carried out for three weeks,
which provided timely feedback to the physicians for developing more effective next
step of rehabilitation program.

4. Methods

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Fabrication of the on-skin sensor

Firstly, the PDMS (Dow Corning 184) solution was prepared by pouring the curing agent to the base (with a 10:1 mixture of silicone prepolymer and curing agent). The PDMS mixture was supplemented with CCTO nanoparticles at varying weight percentages (0, 4, 8, 12, 16, and 20 wt%) and stirred uniformly for 20 minutes. Secondly, the PDMS/CCTO composite film was fabricated by spinning the coating solution onto an acrylic plate (diameter of 1cm) with a pattern at a spinning rate of 350 rpm for 45 s and then cured at 70 °C for 80 min. The composite film was stripped and the AgNWs solution (Nanjing XFNANO Materials Tech Co., Ltd) sprayed on the surface of the patterned side as the top electrode of the on-skin sensor. After curing the AgNWs, a layer of PDMS was spin-coated on the surface as an encapsulation layer. Then, the PDMS solution was dropped onto an acrylic mold (diameter of 1cm) with circular indentations, followed by placing it in a vacuum and allowing it to settle for 20 minutes to ensure complete filling of the PDMS. The width of the arc-shaped protrusion was fixed at 1 mm. Next, spin-coating was performed at a rate of 350 rpm to ensure a smooth surface of the PDMS and cured in an oven at 70 °C for 60 min. After curing, the prepared ECC was coated on its inner surface as the positive triboelectric layer and the bottom electrode. Finally, the upper and lower layer of the sensor were assembled using PDMS as an adhesive to form the on-skin sensor with a diameter of 1 cm.

Fabrication of the ECC

After being repeatedly washed with anhydrous ethanol, the silver powder was mixed with PDMS matrix in a grinding bowl at a mass ratio of 3:1 and homogenized by grinding for 10 minutes to achieve a uniform mixture.

Characterizations and electrical output measurements

- The programmable high-impedance electrometer (Keithley Instruments Model 6514) and a commercial force sensor (Xiamen Enlai Automatic Technology Co. Ltd.) were connected to the USB-6536 data acquisition card (National Instruments) to measure the 682 683 electrical outputs of the on-skin sensor. The force of 5-25 N was obtained by adjusting 684 the contact separation distance of the linear motor (LinMot, PS01-23 × 80-R). The surface and cross-section morphology of ECC, AgNWs, and CCTO powder were 685 686 obtained by SEM (Hitachi SU3900). The dielectric properties were measured via a LCR 687 meter (TZDM-RT-1000) over a frequency range of 1 kHz to 300 kHz. The crystallographic structure of the CCTO powder was tested using X-ray diffraction 688 689 (XRD, Bruker D8 Advance) with Cu Kα radiation (2θ range: 20°-90°). The surface 690 roughness and surface potential of composite film were characterized by KPFM (Park Systems, XE100).
- 692 The MG-former model with continual learning

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- 693 There were three tasks in the MG-former model, and each task had the same input
- space (input data), which can be expressed as $X = \{x_j\}_{j=1}^n$, where n represented the 694
- 695 number of samples. The output space (predicted values) for each task varies, denoted
- as $Y_i = \{y_{i,j}\}_{j=1}^n$, i = 1,2,3. The learning goal of MG-former model was to find the 696
- 697 optimal functions f_i to minimize the following cumulative multitask loss:

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$$\mathcal{L} = \sum_{i=1}^{3} \sum_{j=1}^{n} \alpha_i \mathcal{L}_i(f_i(\mathbf{x}_j), \mathbf{y}_{i,j})$$
 (2)

- where $\mathcal{L}_i(f_i(\mathbf{x}_i), y_{i,i}) \triangleq \mathcal{C}_i(f_i(\mathbf{x}_j), y_{i,j}) + \lambda_i ||f_i||^2$, \mathcal{C}_i was a cost function for task i, 699
- $||f_i||^2$ was the regularization term with parameter λ_i to control overfitting. The α_i were 700
- 701 the trade-off parameters among tasks.
- When new data $X' = \{x_j'\}_{j=1}^{n'}$, $Y_i' = \{y_{i,j'}\}_{j=1}^{n'}$ was collected, a knowledge 702
- 703 distillation method based on teacher-student framework was introduced into the MG-

- 704 former model.
- 705 The cumulative loss of the student model on the new data was as follows:

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$$\mathcal{L}' = \sum_{i=1}^{3} \sum_{i=1}^{n'} \alpha_i \mathcal{L}_i(f_i'(\mathbf{x}_i'), y_{i,i}')$$
 (3)

- However, direct minimization causes the student model to forget the old knowledge.
- 708 Therefore, the teacher model was still needed to guide the learning process by
- 709 minimizing the distillation loss:

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$$\mathcal{L}_{distillation} = \frac{1}{n'} \sum_{j=1}^{n'} d\left(\mathbf{z}_i'(\mathbf{x}_j'), \mathbf{z}_i(\mathbf{x}_j')\right) \tag{4}$$

- where $\mathbf{z}_i(\mathbf{x})$ and $\mathbf{z}_i'(\mathbf{x})$ donate the output layer representations of the teacher model
- and student model at input x, respectively. The function $d(\cdot, \cdot)$ computes the similarity
- between two representations, which was defined as the Euclidean distance in this paper.
- 714 Then, the overall loss of the student model was defined as:

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$$\mathcal{L}_{student} = \beta_1 \mathcal{L}' + \beta_2 \mathcal{L}_{distillation}$$
 (5)

- where β_1 and β_2 were trade-off parameters that control the balance between multi-task
- 717 cumulative loss and distillation loss. The detailed description was presented in Note S4,
- 718 supporting information.

719 Ethics Oversight

- All procedures in the tests in healthy individuals and patients were in accordance
- 721 with the experimental protocol approved by the Medical Ethics Committee, Union
- Hospital, Tongji Medical College, Huazhong University of Science and Technology
- 723 (UHCT-IEC-SOP-016-03-01). All subjects agreed with the study procedures and
- 724 provided signed consent forms.

725 Statistical Analysis

- All data were processed and analyzed in Microsoft Excel, MATLAB (MathWorks),
- and Origin. All data were presented as the mean \pm the standard deviation (SD) with at
- least 3 samples unless reported elsewise. Statistical significance of the variance was

- evaluated by the GraphPad prism (Version 7.0) using the one-way analysis of variance
- 730 (ANOVA) program with Tukey's multiple comparisons post hoc test. Values of *p<0.05,
- **p<0.01 and ***p<0.001 were considered statistically significant. And "ns" mean no
- 732 significant difference.

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734 Supplementary Materials

- 735 Note S1 to S5
- Figure S1 to S21
- Tables S1 to S10
- Movies S1 to S8

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Conflict of interest

The authors declare no conflict of interest.

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Author Contributions

Z.X.W. and X.R.H. contributed equally to this work. H.W., Z.P.Y., J.H., Z.X.W., and X.R.H. conceived the concept and designed the experiments. Z.X.W. conducted on-skin sensor fabrication and data analysis. X.L.X., Z.X.W., X.R.H., B.P., Z.Y.T., and W.G. implemented the tests on clinical cases. Z.X.W. and X.R.H. wrote the manuscript with contributions from all authors. H.W., J.H., Z.Q.Z., T.Z.B, and Z.P.Y. revised the original draft. All authors discussed the results and approved the final version of the paper.

Data availability

The data that support the findings of this study are available from the corresponding author upon reasonable request.

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Acknowledgments

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768 References

- a) T. Foltynie, Cell Stem Cell 2024, 31, 5; b) K. B. Baker, E. B. Plow, S. Nagel,
 A. B. Rosenfeldt, R. Gopalakrishnan, C. Clark, A. Wyant, M. Schroedel, J.
 Ozinga, S. Davidson, O. Hogue, D. Floden, J. Chen, P. J. Ford, L. Sankary, X.
 Huang, D. A. Cunningham, F. P. DiFilippo, B. Hu, S. E. Jones, F. Bethoux, S.
 L. Wolf, J. Chae, A. G. Machado, Nature Medicine 2023, 29, 2366.
- a) P. Boyne, S. A. Billinger, D. S. Reisman, O. O. Awosika, S. Buckley, J. Burson, D. Carl, M. DeLange, S. Doren, M. Earnest, M. Gerson, M. Henry, A. Horning, J. C. Khoury, B. Kissela, A. Laughlin, K. McCartney, T. McQuaid, A. Miller, A. Moores, J. A. Palmer, H. Sucharew, E. D. Thompson, E. Wagner, J. Ward, E. P. Wasik, A. A. Whitaker, H. Wright, K. Dunning, *Jama Neurology* 2023, 80, 342; b) L. Tang, Y. Yin, H. Liu, M. Zhu, Y. Cao, J. Feng, C. Fu, Z. Li, W. Shu, J. Gao, X. J. Liang, W. Wang, *Advanced Materials* 2024, 36, 2312897.
- 781 [3] P. Slade, M. J. Kochenderfer, S. L. Delp, S. H. Collins, *Nature* **2022**, 610, 277.
- 782 [4] C. Li, H. Yang, L. Cheng, F. Huang, S. Zhao, D. Li, R. Yan, *IEEE Transactions* 783 on Neural Systems and Rehabilitation Engineering **2022**, 30, 2032.
- a) Q. Yan, J. Huang, D. Wu, Z. Yang, Y. Wang, Y. Hasegawa, T. Fukuda, *IEEE Transactions on Neural Systems and Rehabilitation Engineering* 2022, 30, 2916;
 b) M. Penta, L. Tesio, C. Arnould, A. Zancan, J. L. Thonnard, *Stroke* 2001, 32, 1627.
- 788 [6] S. Zhang, L. Fan, J. Ye, G. Chen, C. Fu, Y. Leng, *IEEE Transactions on Neural Systems and Rehabilitation Engineering* **2023**, 31, 3106.
- 790 a) H. Wu, Z. Li, Z. Xu, X. Huang, W. Guo, J. Zhao, J. W. Zhang, S. Y. Liu, M. [7] 791 Tang, Y. Q. Qiu, G. G. Yang, J. T. Zhu, L. L. Liu, Y. J. Wu, W. Lei, P. Zhou, Z. 792 P. Yin, Z. B. Chen, Y. T. Liu, Science Translational Medicine 2023, 15, 793 eabq1634; b) G. Yang, Y. Hu, W. Guo, W. Lei, W. Liu, G. Guo, C. Geng, Y. Liu, 794 H. Wu, Advanced Materials 2023, 23, 2308831; c) Q. Yang, W. Jin, Q. Zhang, 795 Y. Wei, Z. Guo, X. Li, Y. Yang, Q. Luo, H. Tian, T.-L. Ren, Nature Machine 796 Intelligence 2023, 5, 169; d) D. Wei, J. Guo, Y. Qiu, S. Liu, J. Mao, Y. Liu, Z. 797 Chen, H. Wu, Z. Yin, National Science Review 2022, 9, nwac227; e) J. 798 Engelmann, A. D. McTrusty, I. J. C. MacCormick, E. Pead, A. Storkey, M. O. 799 Bernabeu, Nature Machine Intelligence 2022, 4, 1143; f) X. Huang, W. Guo, S. 800 Liu, Y. Li, Y. Qiu, H. Fang, G. Yang, K. Zhu, Z. Yin, Z. Li, H. Wu, Advanced Functional Materials 2022, 32, 2109109; g) S. Jin, H. Choi, D. Seong, C.-L. 801 You, J.-S. Kang, S. Rho, W. B. Lee, D. Son, M. Shin, *Nature* **2023**, 623, 58; h) 802 803 F. B. Wagner, J.-B. Mignardot, C. G. Le Goff-Mignardot, R. Demesmaeker, S. 804 Komi, M. Capogrosso, A. Rowald, I. Seáñez, M. Caban, E. Pirondini, M. Vat, L. A. McCracken, R. Heimgartner, I. Fodor, A. Watrin, P. Seguin, E. Paoles, K. 805 Van Den Keybus, G. Eberle, B. Schurch, E. Pralong, F. Becce, J. Prior, N. Buse, 806 807 R. Buschman, E. Neufeld, N. Kuster, S. Carda, J. von Zitzewitz, V. Delattre, T. 808 Denison, H. Lambert, K. Minassian, J. Bloch, G. Courtine, Nature 2018, 563, 809 65.
- 810 [8] T. v. Marcard, G. Pons-Moll, B. Rosenhahn, *IEEE Transactions on Pattern Analysis and Machine Intelligence* **2016**, 38, 1533.

- 812 [9] a) O. Dehzangi, M. Taherisadr, R. ChangalVala, Sensors 2017, 17, 2735; b) J.
- A. Ramirez-Bautista, J. A. Huerta-Ruelas, S. L. Chaparro-Cardenas, A.
- Hernandez-Zavala, *IEEE Reviews in Biomedical Engineering* **2017**, 10, 299.
- 815 [10] a) Q. Shi, Z. Zhang, T. He, Z. Sun, B. Wang, Y. Feng, X. Shan, B. Salam, C. Lee, *Nature Communications* **2020**, 11, 4609; b) J. L. Chen, Y. N. Dai, N. S. Grimaldi,
- J. J. Lin, B. Y. Hu, Y. F. Wu, S. Gao, *Advanced Materials Technologies* **2021**, 7,
 2100566.
- a) Y. Song, R. Y. Tay, J. Li, C. Xu, J. Min, E. S. Sani, G. Kim, W. Heng, I. Kim,
 W. Gao, *Science Advances* 2023, 13, eadi6492; b) J. P. Lee, H. Jang, Y. Jang, H.
 Song, S. Lee, P. S. Lee, J. Kim, *Nature Communications* 2024, 15, 530.
- [12] G. Yang, K. Zhu, W. Guo, D. Wu, X. Quan, X. Huang, S. Liu, Y. Li, H. Fang, Y.
 Qiu, Q. Zheng, M. Zhu, J. Huang, Z. Zeng, Z. Yin, H. Wu, *Advanced Functional Materials* 2022, 32, 2200457.
- 825 [13] H. Fang, L. Wang, Z. Fu, L. Xu, W. Guo, J. Huang, Z. L. Wang, H. Wu, *Advanced Science* **2023**, 10, 2205960.
- 827 [14] L. Shi, V. S. Kale, Z. Tian, X. Xu, Y. Lei, S. Kandambeth, Y. Wang, P. T. Parvatkar, O. Shekhah, M. Eddaoudi, H. N. Alshareef, *Advanced Functional Materials* **2023**, 33, 2212891.
- Y. Li, Y. Luo, H. Deng, S. Shi, S. Tian, H. Wu, J. Tang, C. Zhang, X. Zhang, J.
 W. Zha, S. Xiao, *Advanced Materials* 2024, 20, 2314380.
- 832 [16] C. Cui, G.-B. Bian, Z.-G. Hou, J. Zhao, G. Su, H. Zhou, L. Peng, W. Wang, 833 *IEEE Transactions on Neural Systems and Rehabilitation Engineering* **2018**, 26, 856.
- 835 [17] Z. Zhang, T. He, M. Zhu, Z. Sun, Q. Shi, J. Zhu, B. Dong, M. R. Yuce, C. Lee, 836 *npj Flexible Electronics* **2020**, 4, s41528.
- 837 [18] C. Estrada-Barranco, I. Sanz-Esteban, M. J. Giménez-Mestre, R. Cano-de-la-838 Cuerda, F. Molina-Rueda, *Journal of Clinical Medicine* **2022**, 11, 3771.
- W. Guo, P. Zheng, X. Huang, H. Zhuo, Y. Wu, Z. Yin, Z. Li, H. Wu, ACS Applied Materials & Interfaces 2019, 11, 8567.
- 841 [20] Y. Song, M. Liu, J. Bao, Y. Hu, M. Xu, Z. Yang, Q. Yang, H. Cai, C. Xiong, Z. Shi, *Carbohydrate Polymers* **2022**, 298, 120111.
- 843 [21] a) Y. Lu, Q. H. Qin, J. J. Meng, Y. J. Mi, X. Q. Wang, X. Cao, N. Wang, *Chemical Engineering Journal* **2023**, 468, 143802; b) J. Chen, H. Guo, X. He, G. Liu, Y.
- Xi, H. Shi, C. Hu, ACS Applied Materials & Interfaces 2015, 8, 736; c) J. Kim,
- H. Ryu, J. H. Lee, U. Khan, S. S. Kwak, H. J. Yoon, S. W. Kim, *Advanced*
- Energy Materials **2020**, 10, 1903524; d) C. Cai, T. Chen, X. Chen, Y. t. Zhang, X. h. Gong, C. g. Wu, T. Hu, Macromolecular Materials and Engineering **2021**,
- 306, 2100046; e) P. Manchi, S. A. Graham, M. V. Paranjape, A. Kurakula, V. S.
- Kavarthapu, J. S. Yu, Journal of Materials Science & Technology 2024, 190, 56.
- 851 [22] a) B. Xi, L. Wang, B. Yang, Y. Xia, D. Chen, X. Wang, *Nano Energy* **2023**, 110,
- 852 108385; b) H. Kang, H. T. Kim, H. J. Woo, H. Kim, D. H. Kim, S. Lee, S. Kim,
 853 Y. J. Song, S.-W. Kim, J. H. Cho, *Nano Energy* 2019, 58, 227.
- 854 [23] a) Z. Wang, Y. Wu, W. Jiang, Q. Liu, X. Wang, J. Zhang, Z. Zhou, H. Zheng, Z. Wang, Z. L. Wang, *Advanced Functional Materials* **2021**, 31, 2103081; b) X.

- Huang, T. Bu, Q. Zheng, S. Liu, Y. Li, H. Fang, Y. Qiu, B. Xie, Z. Yin, H. Wu, *National Science Review* **2024**, 11, nwae027.
- B58 [24] D. Liu, D. Zhang, Z. Sun, S. Zhou, W. Li, C. Li, W. Li, W. Tang, Z. L. Wang,
 Advanced Functional Materials 2022, 32, 2113008.
- 860 [25] X. Shi, P. Qin, J. Zhu, M. Zhai, W. Shi, *IEEE Access* **2020**, 8, 132882.
- a) L. Nguyen, L.-C. Xu, E. Yeager, W. J. Weiss, C. A. Siedlecki, *Journal of Biomaterials Applications* 2023, 38, 302; b) A. T. Stevenson, L. M. Reese, T. K.
 Hill, J. McGuire, A. M. Mohs, R. Shekhar, L. R. Bickford, A. R. Whittington, *Biomaterials* 2015, 54, 168.
- 865 [27] M. Ye, C. Yang, V. Stankovic, L. Stankovic, S. Cheng, *IEEE Transactions on Multimedia* **2020**, 22, 1113.
- 867 C. W. Tsao, A. W. Aday, Z. I. Almarzooq, A. Alonso, A. Z. Beaton, M. S. [28] 868 Bittencourt, A. K. Boehme, A. E. Buxton, A. P. Carson, Y. Commodore-Mensah, M. S. V. Elkind, K. R. Evenson, C. Eze-Nliam, J. F. Ferguson, G. Generoso, J. 869 870 E. Ho, R. Kalani, S. S. Khan, B. M. Kissela, K. L. Knutson, D. A. Levine, T. T. Lewis, J. Liu, M. S. Loop, J. Ma, M. E. Mussolino, S. D. Navaneethan, A. M. 871 872 Perak, R. Poudel, M. Rezk-Hanna, G. A. Roth, E. B. Schroeder, S. H. Shah, E. L. Thacker, L. B. VanWagner, S. S. Virani, J. H. Voecks, N.-Y. Wang, K. Yaffe, 873 874 S. S. Martin, Circulation 2022, 145, e153.
- 875 [29] G. Yavuzer, F. Eser, D. Karakus, B. Karaoglan, H. J. Stam, *Clinical Rehabilitation* **2016**, 20, 960.
- 877 [30] B.-B. Koo, P. Bergethon, W. Q. Qiu, T. Scott, M. Hussain, I. Rosenberg, L. R. Caplan, R. A. Bhadelia, *Archives of Neurology* **2012**, 69, 733.
- 879 [31] S. A. Khan, A. Maillo, V. Lagani, R. Lehmann, N. A. Kiani, D. Gomez-Cabrero, J. Tegner, *Nature Machine Intelligence* **2023**, 5, 1437.
- 881 [32] S. Downs, J. Marquez, P. Chiarelli, Journal of Physiotherapy 2014, 60, 85.