



**UNIVERSITY OF LEEDS**

This is a repository copy of *Characterising the dispersed phase hydrodynamics in Pulsed Sieve Plate Extraction Columns*.

White Rose Research Online URL for this paper:

<https://eprints.whiterose.ac.uk/195623/>

Version: Accepted Version

---

**Conference or Workshop Item:**

Fells, A [orcid.org/0000-0003-4392-3035](https://orcid.org/0000-0003-4392-3035), Muller, FL and Hanson, BC Characterising the dispersed phase hydrodynamics in Pulsed Sieve Plate Extraction Columns. In: World Conference on Multiphase Transportation, Conversion & Utilization of Energy, 27-31 Jul 2022, Xi'an, China and online.

---

**Reuse**

Items deposited in White Rose Research Online are protected by copyright, with all rights reserved unless indicated otherwise. They may be downloaded and/or printed for private study, or other acts as permitted by national copyright laws. The publisher or other rights holders may allow further reproduction and re-use of the full text version. This is indicated by the licence information on the White Rose Research Online record for the item.

**Takedown**

If you consider content in White Rose Research Online to be in breach of UK law, please notify us by emailing [eprints@whiterose.ac.uk](mailto:eprints@whiterose.ac.uk) including the URL of the record and the reason for the withdrawal request.



[eprints@whiterose.ac.uk](mailto:eprints@whiterose.ac.uk)  
<https://eprints.whiterose.ac.uk/>



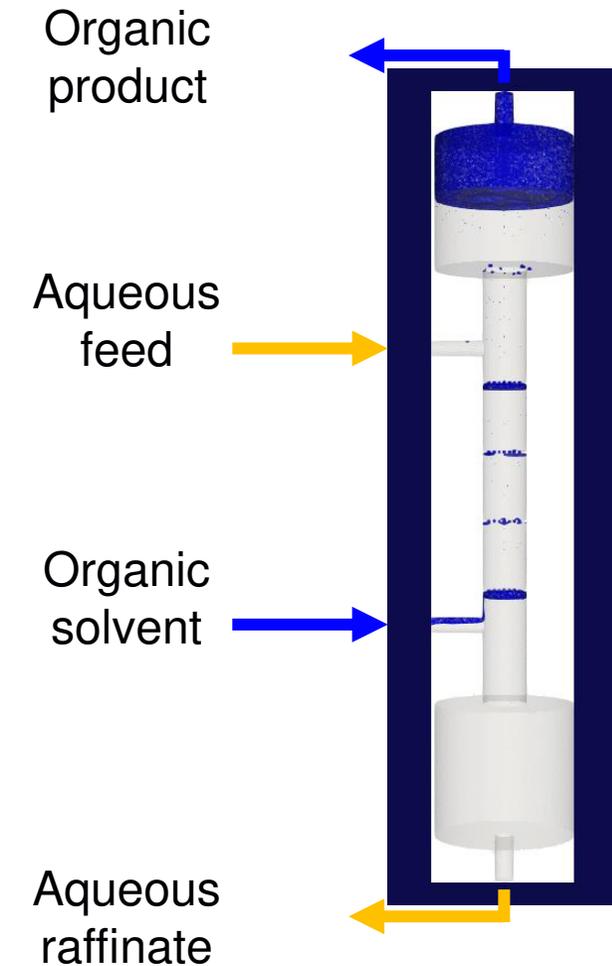
# Characterising the dispersed phase hydrodynamics in Pulsed Sieve Plate Extraction Columns

Multiphase Transportation, Conversion & Utilization of Energy Conference  
July 27<sup>th</sup> to 31<sup>st</sup> 2022

Alex Fells, F.L. Muller and B.C. Hanson, University of Leeds, UK

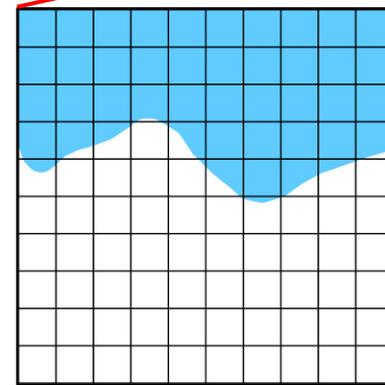
## PULSED SIEVE-PLATE EXTRACTION COLUMNS

- Counter-current liquid-liquid extraction unit operation.
- The good:
  - No moving parts
  - Can operate with solids
- The bad:
  - Empirical correlations are poor and not general.
  - Pilot plants and expensive.
- Can we develop a generalised approach to design?
- Need experimental data for validation.

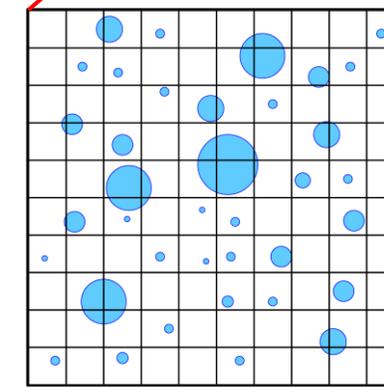
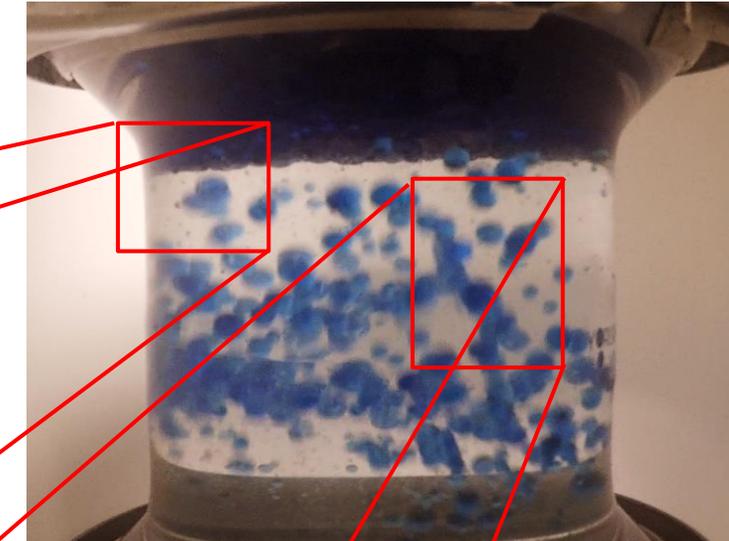


## MODELLING MULTIPHASE FLOWS

- Two traditional approaches to multiphase flows modelling:
  - Interface-scale averaging
    - Multifluid (Eulerian) models
    - Generally used for dispersed flows.
    - Droplets are smaller than cells
  - Interface-scale resolving
    - Interface capturing models
    - Segregated flows
    - Mesh is smaller than interface scales
- PSEC exhibits both small and large interfaces, so hybrid method necessary.



Interface capturing



Multifluid

## METHODOLOGY

- PSEC
  - 65 mm diameter, 3 stages, 4 plates (23% fractional free area)
  - 2:1 Solvent to aqueous flow ratio, 1 Hz pulse frequency
- Optical characterisation
  - 3 cameras, 30 fps, 1080p, 3 minutes.
  - Processing with Ilastic and OpenCV.

### 3 different plate designs used



$d = 1 \text{ mm}$

$d = 2 \text{ mm}$

$d = 4 \text{ mm}$

University of Leeds PSEC Pilot Plant

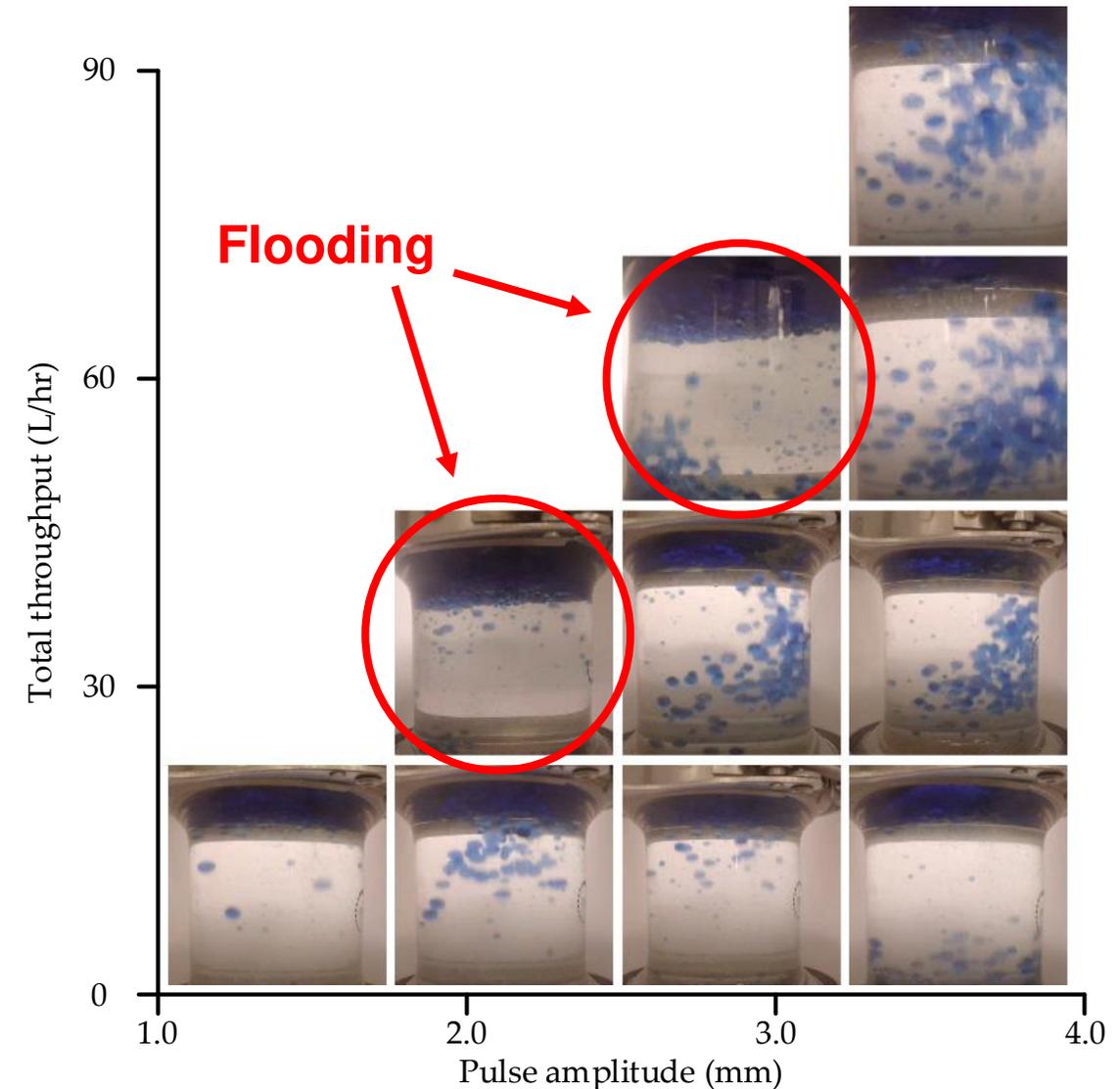


**Table 1:** Investigated experimental conditions

Parameter	Values
Total throughput $Q$ (L/hr)	15, 30, 45, 60, 75, 90, 105, 120
Pulse amplitude $A$ (mm)	1.48, 2.22, 2.96, 3.70
Plate hole diameter $d$ (mm)	1, 2, 4

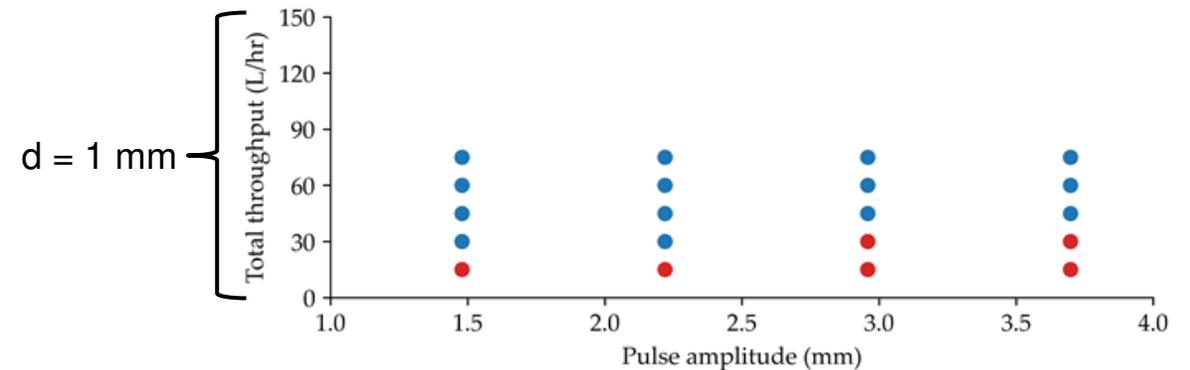
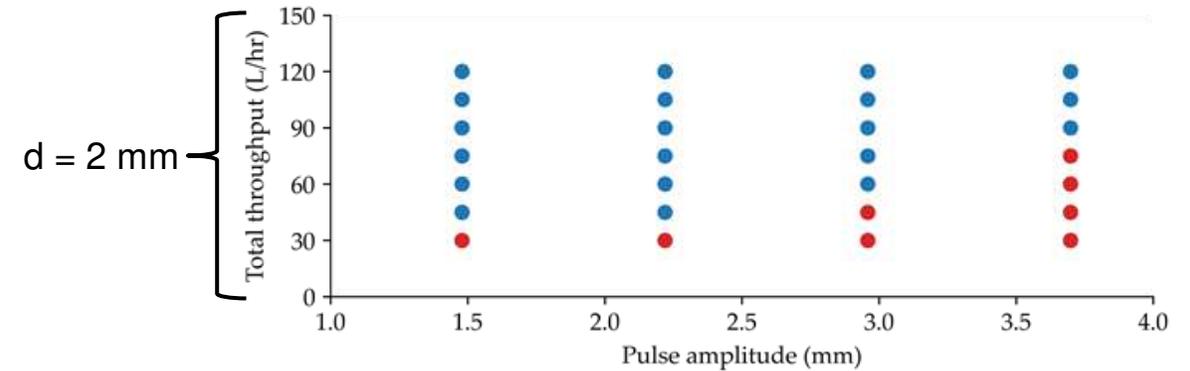
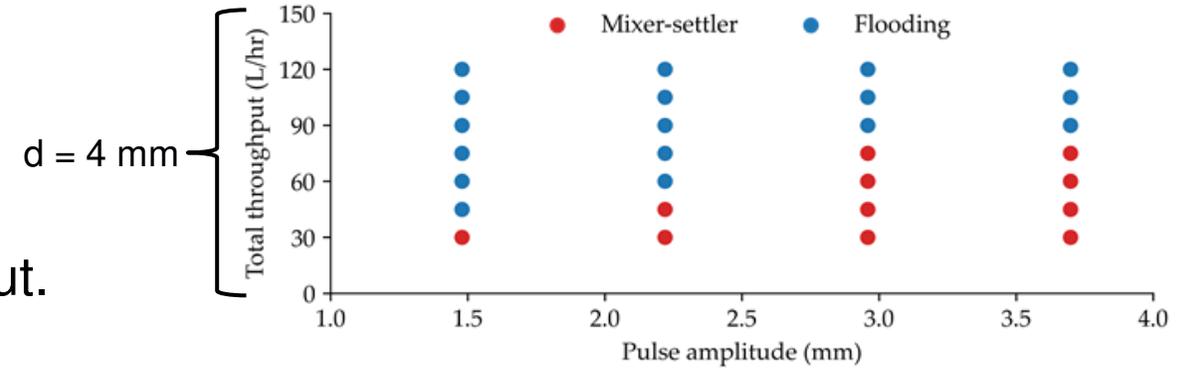
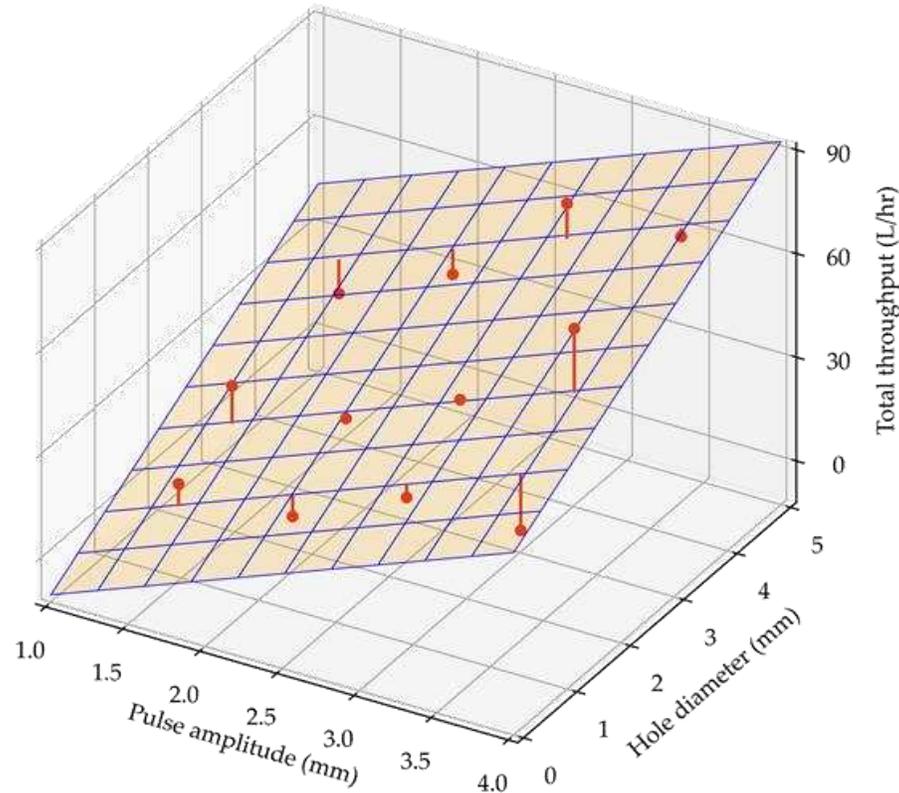
## RESULTS

- 1.8M droplets measured, 78 Gb of footage.
- Column operates in pseudo-steady-state mixer-settler (MS) regime.
  - Droplets formed by jetting.
  - Droplets rise and coalesce at plate.
- Insufficient pulsation results in flooding.
  - Accumulation of organic below plate.
  - Interface moves downwards overtime.
- Excessive throughput results in flooding.
  - Droplet rise velocity insufficient to overcome down coming fluid.
- Trends observed across all plate designs



## OPERATIONAL ENVELOPE

- Flooding caused by insufficient pulsation.
- Flooding caused by excessive column throughput.



## SAUTER MEAN DROPLET DIAMETER ( $d_{3,2}$ )

- Highly correlated to plate hole size.
- Unaffected by throughput or pulse amplitude.
- Hole size defines diameter.



$Q_{TOT} = 30$  L/hr,  $A = 3.70$  mm

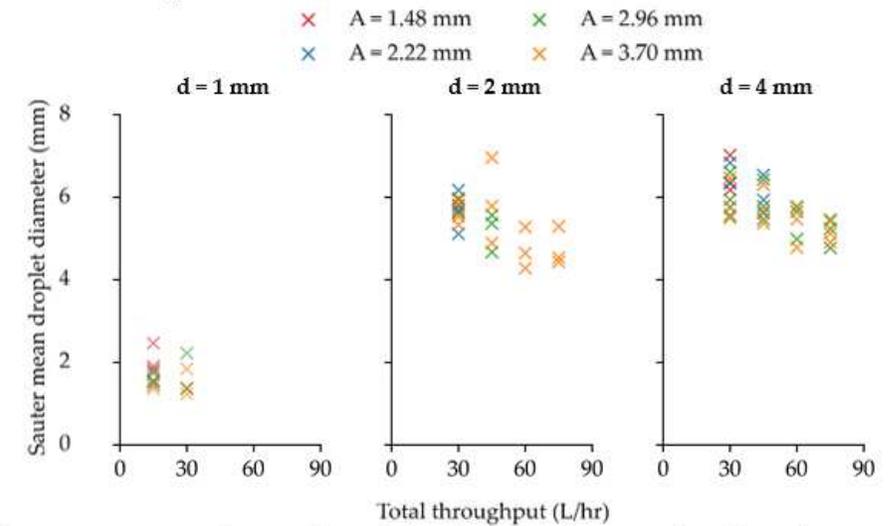


Figure X: Sauter mean diameter for each plate design as a function of total throughput ( $Q_{tot}$ ), grouped by pulse.

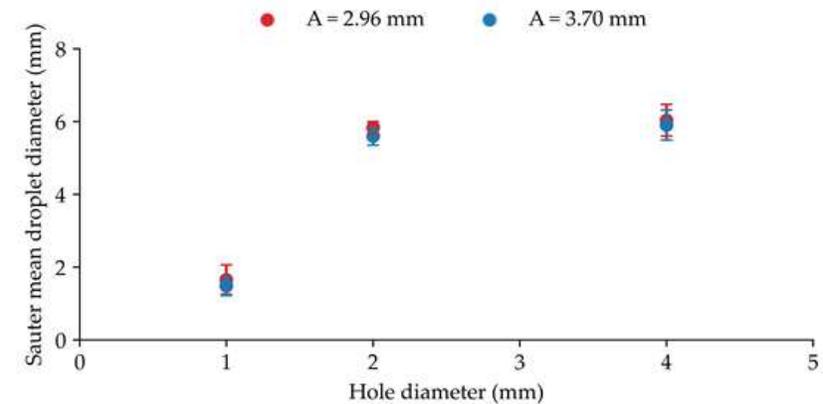


Figure X: Sauter mean droplet diameter for a total throughput ( $Q_{tot}$ ) of 30 L/hr for pulse amplitudes ( $A$ ) of 2.96 mm and 3.70 mm.

## DROPLET SIZE DISTRIBUTION (DSD)

- Behaviour consistent with operation in MS.
- Expect DSD to tighten for greater pulsation.
- Further work should consider PSEC operation in dispersion mode of operation.

$d = 1 \text{ mm}$

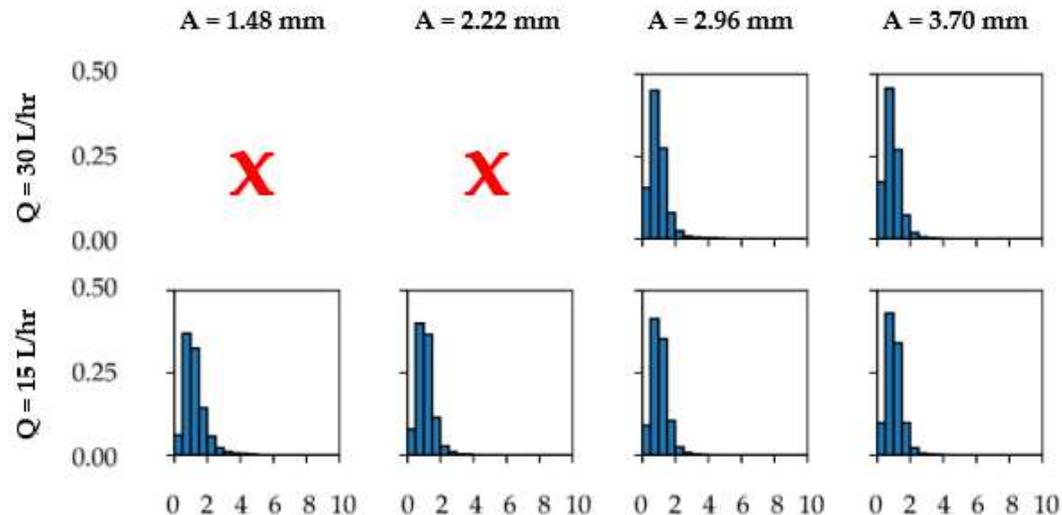


Figure X: Droplet size distribution as a function of total throughput ( $Q_{tot}$ ) and pulse amplitude ( $A$ ) for a plate hole diameter ( $d$ ) of 1 mm. A red x donates column flooding at the particular operating conditions.

$d = 2 \text{ mm}$

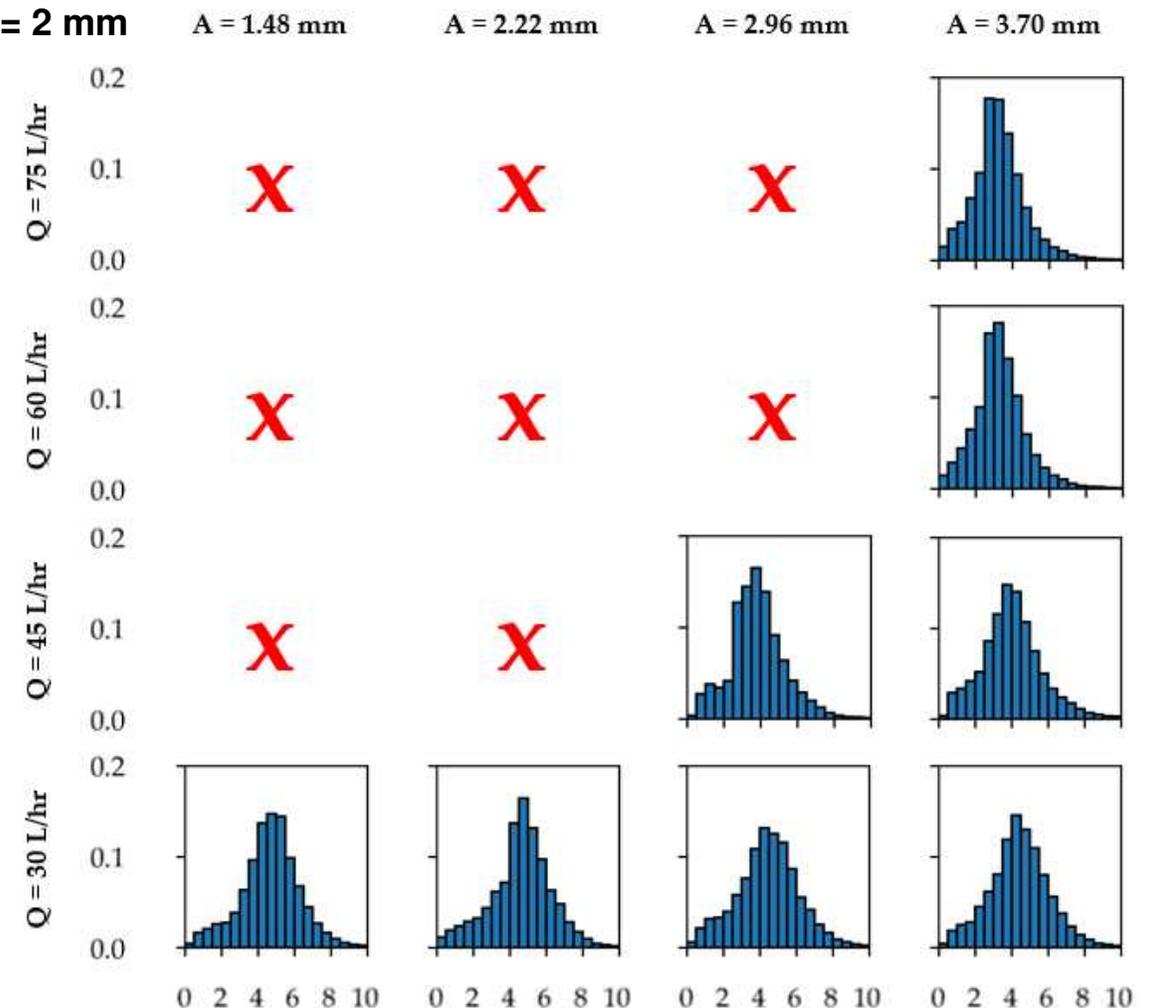


Figure X: Droplet size distribution as a function of total throughput ( $Q_{tot}$ ) and pulse amplitude ( $A$ ) for a plate hole diameter ( $d$ ) of 2 mm. A red x donates column flooding at the particular operating conditions.

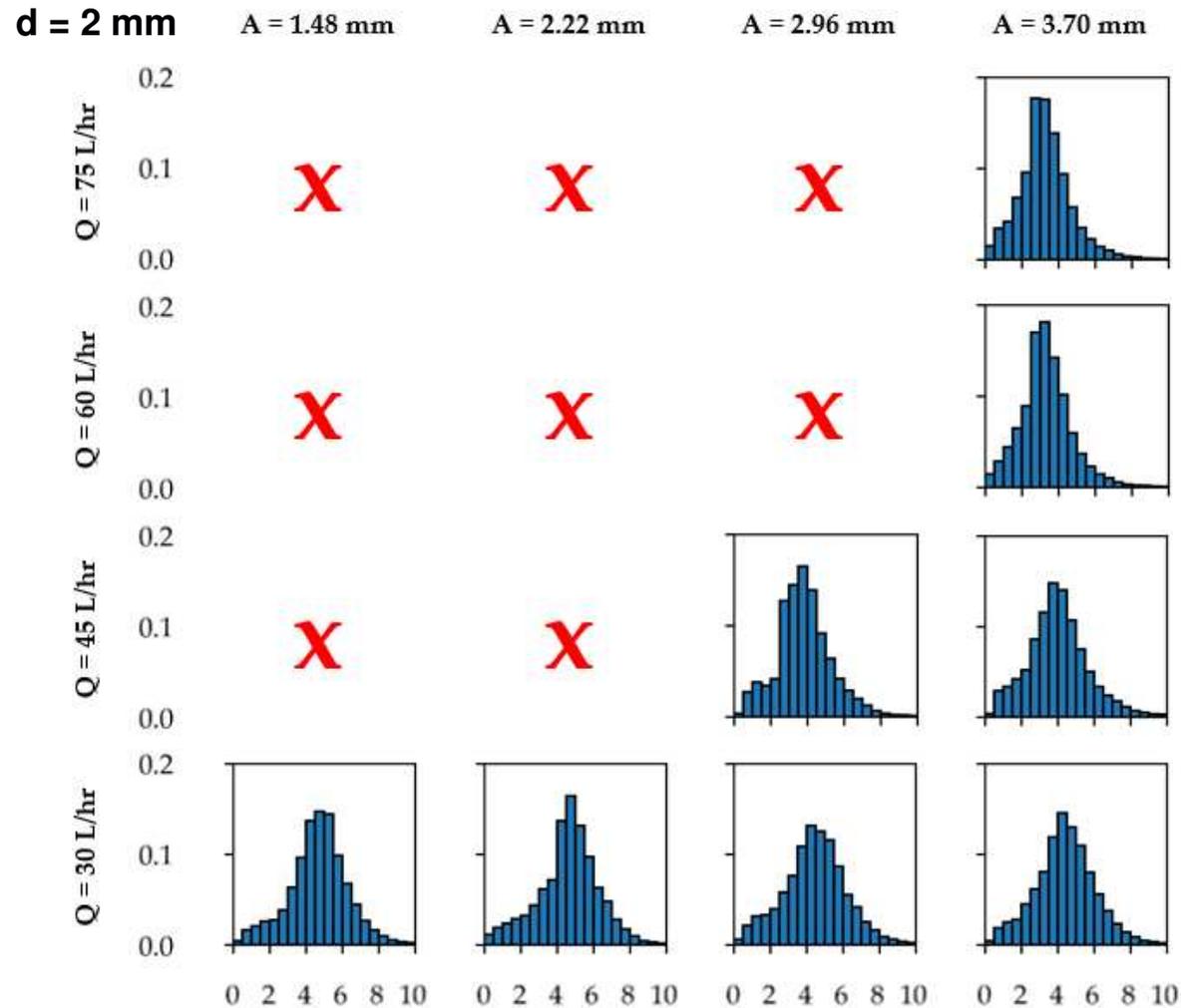


Figure X: Droplet size distribution as a function of total throughput ( $Q_{tot}$ ) and pulse amplitude ( $A$ ) for a plate hole diameter ( $d$ ) of 2 mm. A red x donates column flooding at the particular operating conditions.

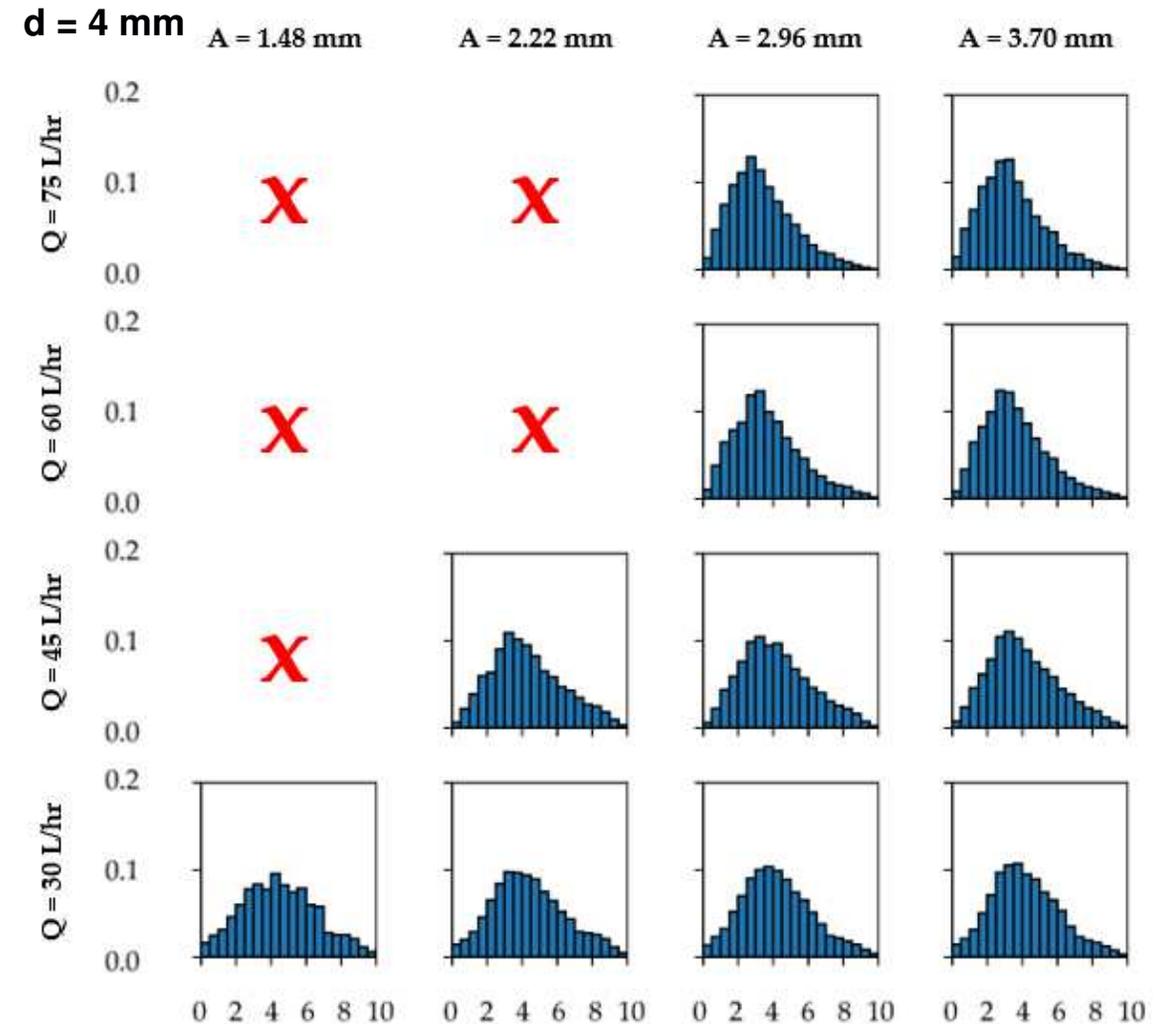


Figure X: Droplet size distribution as a function of total throughput ( $Q_{tot}$ ) and pulse amplitude ( $A$ ) for a plate hole diameter ( $d$ ) of 4 mm. A red x donates column flooding at the particular operating conditions.

## DROPLET RISE VELOCITY

- Highly correlated to plate hole size.
- Unaffected by throughput or pulse amplitude.
- Hole size defines diameter.
- Larger droplets result in a greater buoyancy force, resulting in increased rise velocity.



$Q_{TOT} = 30 \text{ L/hr}$ ,  $A = 3.70 \text{ mm}$

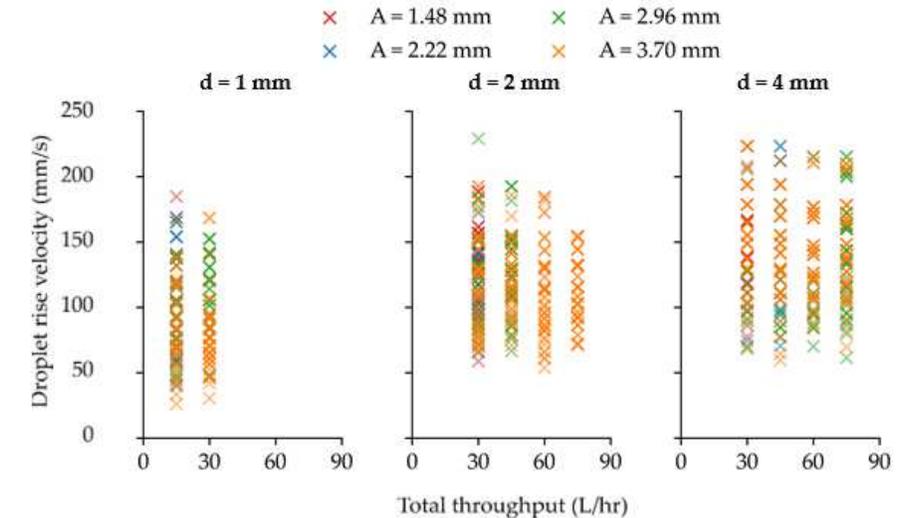


Figure X: Droplet rise velocities for each plate design as a function of total throughput ( $Q_{tot}$ ), grouped by pulse.

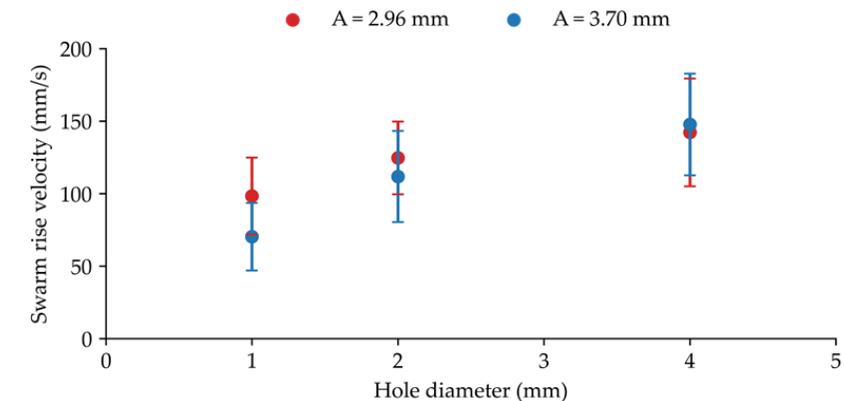


Figure X: Droplet swarm averaged rise velocities for a total throughput ( $Q_{tot}$ ) of 30 L/hr for pulse amplitudes (A) of 2.96 mm and 3.70 mm.



## ACKNOWLEDGEMENTS

- Supervision
  - Bruce Hanson
  - Frans Muller
- Funding
  - The University of Leeds
  - Engineering and Physical Sciences Research Council
  - Advanced Fuel Cycle Programme (AFCP)
  - The National Nuclear Laboratory (NNL)

## CONTACT DETAILS

- [pm11af@leeds.ac.uk](mailto:pm11af@leeds.ac.uk)



UNIVERSITY OF LEEDS



Department for  
Business, Energy  
& Industrial Strategy



NATIONAL NUCLEAR  
LABORATORY