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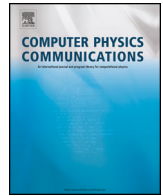
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Models of advanced recording systems: A multi-timescale micromagnetic code for granular thin film magnetic recording systems ^{☆,☆☆}

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ABSTRACT

Micromagnetic modelling provides the ability to simulate large magnetic systems reliably without the computational cost limitation imposed by atomistic modelling. Through micromagnetic modelling it is possible to simulate systems consisting of thousands of grains over a time range of nanoseconds to years, depending upon the solver used. Here we present the creation and release of an open-source multi-timescale micromagnetic code combining three key solvers: Landau-Lifshitz-Gilbert; Landau-Lifshitz-Bloch; Kinetic Monte Carlo. This code, called MARS (Models of Advanced Recording Systems), is capable of accurately simulating the magnetisation dynamics in large and structurally complex single- and multi-layered granular systems as is shown by comparison to established atomistic simulation results. The short timescale simulations are achieved for systems far from and close to the Curie point via the implemented Landau-Lifshitz-Gilbert and Landau-Lifshitz-Bloch solvers respectively. This enables read/write simulations for general perpendicular magnetic recording and also state of the art heat assisted magnetic recording (HAMR). The long timescale behaviour is simulated via the Kinetic Monte Carlo solver, enabling investigations into signal-to-noise ratio and data longevity. The combination of these solvers opens up the possibility of multi-timescale simulations within a single software package. For example the entire HAMR process from initial data writing and data read back to long term data storage is possible via a single simulation using MARS. The use of atomistic parameterisation for the material input of MARS enables highly accurate material descriptions which provide a bridge between atomistic simulation and real world experimentation. Thus MARS is capable of performing simulations for all aspects of recording media research and development. This ranges from material characterisation and optimisation to system design and implementation. The object orientated nature of MARS is structured to facilitate quick and simple development and easy implementation of user defined custom simulation types which can utilise either timescale or a combination of both timescales.

Program summary

Program title: MARS

CPC Library link to program files: <https://doi.org/10.17632/8mx7cndcdx.1>

Developer's repository link: <https://bitbucket.org/EwanRannala/mars/>

Code Ocean capsule: <https://codeocean.com/capsule/2549929>

Licensing provisions: MIT

Programming language: C++

Supplementary material: MARS testing methodology (PDF), HAMR simulation example video.

Nature of problem: A combined model that enables the complete modelling of magnetic recording processes at elevated temperatures covering all time scales from writing (nanoseconds) up to long term

[☆] The review of this paper was arranged by Prof. Blum Volker.

^{☆☆} This paper and its associated computer program are available via the Computer Physics Communications homepage on ScienceDirect (<http://www.sciencedirect.com/science/journal/00104655>).

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data storage (years). The model must also accurately describe the granular nature of the recording media as grain sizes are reduced to a few nanometres.

Solution method: Short timescale behaviours are captured via the Landau-Lifshitz-Gilbert and Landau-Lifshitz-Bloch solvers for low and high temperature systems respectively. The long time scale behaviours are captured via a kinetic Monte Carlo solver. To enable complex models which account for mixed timescale behaviours the solvers are implemented as a single class structure which allows for dynamic solver selection. The granular structure is generated via a Laguerre-Voronoi tessellation with a custom implemented packing algorithm to produce highly realistic grain size distributions. Complex thermal dependencies of materials can be incorporated via atomistic parameterisation forming a multi-timescale model of the material.

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1. Introduction

Magnetic recording using hard disk drives remains the dominant technology for cloud-based information storage. As data centres consume sufficient energy to represent a significant contribution to global warming there is an imperative to improve energy efficiency and minimise the required number of data centres by means of increasing storage density. A significant amount of cloud-based data is video, with content on demand services such as Netflix choosing to store approximately seventy different formats of each video in an effort to reduce energy consumption due to media transcoding [1]. This data is typically written once and then read back numerous times and as a result the energy required to both store and read back such data is significant. Hence, the reduction of the energy related to long term data storage and read back processes should also be considered to a similar degree as that of the data write processes. To achieve this, models which account for both short and long timescale behaviours of magnetic recording systems are required. In order to achieve the properties required for magnetic information storage, the storage medium must be granular in nature. The essential required property for the storage of binary information via granular media is the presence of a large magnetic anisotropy (K): the material property which provides an energy barrier to switching of the magnetisation and thereby creates a two-state magnetic system. The increase of areal density generally proceeds by a scaling of properties, particularly a reduction of the grain size to ensure adequate signal to noise ratio (SNR) given the reduction in bit size. This necessitates an increase in the value of K to ensure thermal stability, which makes the writing of individual bits more difficult due to an increase in write field: the magnetic 'trilemma' [2]. Current technology (perpendicular magnetic recording) is already running into write-field limitations and a step change of technology is required for future products. Based on the ASRC (Advanced Storage Research Consortium) road map, there are two future technologies: 1) heat assisted magnetic recording (HAMR) and 2) Bit patterned magnetic recording (BPMR), which combined can lead to Heated-Dot magnetic recording [3]. To facilitate the development and optimisation of the present-day and future magnetic recording technologies advanced models with greater levels of complexity are required. These models must capture the dynamics at both short and long timescales over a large number of bits/grains whilst accurately describing the variation of magnetic fields, temperatures and temperature dependent parameters. Models of granular thin films have a long history driven initially by the transition from particulate media for information storage to sputtered metallic thin films with in-plane anisotropy. The pioneering work of Gordon Hughes [4] was followed, for example by Zhu and Bertram [5] who demonstrated the important effect of intergranular exchange coupling on recorded transitions. This and most later models used a dynamic approach to the problem using the Landau-Lifshitz-Gilbert equation first introduced by Victora [6]. Models are generally based on grains

with single macrospins, with an underlying cubic discretisation used to approximate the magnetostatic field, although Finite Element Methods are also used [7,8]. Miles et al. [9] first combined a realistic dynamical thin film media with a kinetic Monte-Carlo solver to simulate long-timescale magnetisation decay and investigated parametric optimisation for terabit perpendicular recording as the transition from longitudinal to perpendicular technology was nearing completion. These and other developments to be described later, including models of the granular microstructure, the Landau-Lifshitz-Bloch dynamics and the calculation of magnetostatic fields, form the essential precursors from which MARS was developed.

HAMR is the current state of the art technology available, which is able to provide recording densities significantly greater than those achievable via standard perpendicular magnetic recording [10]. HAMR provides increased areal densities through the utilisation of high coercivity materials, potentially enabling up to 4 Tb/in² [11]. The initial difficulty with using high coercivity materials is the requirement of increased writing head field gradients. The solution to this is to temporarily reduce the coercivity of the medium, thus enabling writing with reduced field strengths. This process is achieved by applying a laser pulse to heat the material and cause a reduction in the material anisotropy. The physics of HAMR, involving heating up to or beyond the magnetic ordering (Curie) temperature T_c remains challenging and involves models with a thermodynamic basis beyond the scope of those used in the typical micromagnetic approach.

Atomistic models provide this level of detail and have been used to provide temperature dependent magnetic properties and reversal mechanisms in recording media [12–21]. Although atomistic simulations can provide exceptional detail of the underlying physical processes which govern their macroscopic properties these simulations carry a significant computational cost. This cost limits atomistic simulations of recording media to a lengthscale of a few grains and a timescale of nanoseconds. This significant computational cost limits the investigation of statistical variation in particle properties and inter-particle interaction or temperature/field profiles over a track of recording bits. However, to be able to design, test and optimise any present-day and future magnetic recording technology, it is vital to capture the recording of thousands of grains from the sub-nanosecond timescale to a data storage timescale (5–10 years).

Furthermore, experimental characterisations and tests are performed at the nanosecond timescale for FMR and millisecond timescale for standard measurements such as hysteresis loops, thermal decay, First Order Reversal Curves (FORC) and thermoremanence [22,23]. Over long timescales, thermally activated transitions over the energy barriers can lead to loss of recorded information. Transition times are governed by the Arrhenius-Néel law [24], which gives a characteristic time $\tau^{-1} = f_0 \exp(KV/kT)$, where V is the grain volume and K is the magnetic anisotropy constant. The pre-exponential factor is dependent on the value of

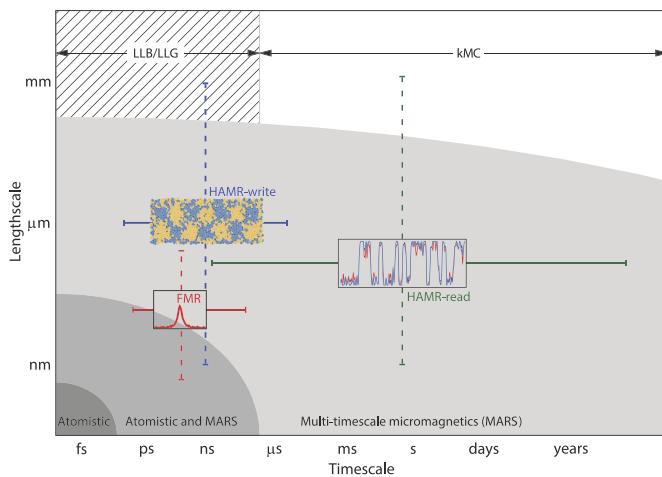


Fig. 1. Illustration of the time/length scales required by some common simulations.

K and is in the region of GHz to THz. Ensuring thermal stability of the written information for 5-10 years requires large energy barriers ($KV/kT > 80$) and good SNR. Typically short and long timescale investigations are performed separately, mainly due to the described fundamental difference between the simulation methodology. Nonetheless, there are numerous cases where both timescales are of interest, the simplest example of this is the effect of the writing process on nearby bits (nanosecond timescale) and data longevity (timescale of years).

Here we present the developed multi-timescale micromagnetic code, MARS (Models of Advanced Recording Systems), which has the functionality of utilising various solvers to best accommodate the required simulation time frames. MARS includes both short and long timescale solvers to make such investigations more simple and to open up the possibility to more easily access the effect of dynamic processes on the long timescale behaviour. MARS includes a stochastic-Landau-Lifshitz-Gilbert (sLLG) equation solver along with a stochastic-Landau-Lifshitz-Bloch solver, specifically the sLLB-II (which is shown to have greater accuracy at the Curie temperature [25]), to simulate short timescale dynamics of the magnetisation. A kinetic Monte-Carlo (kMC) solver is also included in order to simulate the long timescale behaviour. Fig. 1 illustrates the benefits of the multi-timescale micromagnetic approach over computationally expensive atomistic simulations. The addition of the kMC solver enables the simulation of timescales far beyond the standards set using dynamical micromagnetic solvers alone.

MARS has been designed to be used alongside atomistic simulations by utilising parameterisation obtained via atomistic simulation to describe material properties, this allows for highly accurate descriptions of simulated materials. There is no limit on the number of materials MARS can utilise in a single simulation. This enables multi-layered systems such as those used for exchange-coupled-composites to be simulated. Details of granular system generation and the numerical solvers are provided in section 2. MARS includes a set of commonly used simulation types for easy use, these include: HAMR writing, time evolution and data read back, thermoremanence, FORC and FMR. A selection of results obtained via these simulations is provided and discussed in section 3.

2. MARS: multiscale framework

2.1. Granular model

The micromagnetic approach consists of treating magnetic grains as macrospins with associated magnetisation, \mathbf{m} . The microstructure of the granular medium is a key component in the

simulation of their magnetic and recording properties. Early models, for example ref. [5], assumed an hexagonal lattices structure in order to simplify the magnetostatic field calculation. However, this exacerbated the correlations introduced by the intergranular magnetostatic and exchange interactions, especially along the symmetry axes. This had a detrimental effect on simulations of magnetic and recording properties. Miles and Middleton [26,27] first introduced realistic microstructures into the granular model, showing that the assumed microstructure could dominate magnetic features such as sawtooth transitions, flux closure and magnetisation ripple. One of the important factors in the structure is the grain size dispersion [28,29] which contributes to dispersion of the switching field and has also been shown [30] to introduce a dispersion of Curie temperature which could be a serious limitation to HAMR. Realistic modelling of physical microstructure of the medium in now a key factor in model development. The typical method for generating granular structures is via Voronoi tessellation [31–34]. The classical Voronoi algorithm starts with the creation of seed points throughout the system, cell walls are then created such that they lie halfway between two seed points. While the general process is the same there exist various methods to determine the initial locations of the seed points [35,36].

A major drawback with the classical Voronoi construction is evident when a distribution of grain sizes is required. When there is a local increase in seed density the construction can generate unrealistically angular cells. This occurs due to the only constraint on cell construction being the requirement that the cell wall must be equidistant between seed points.

To overcome this drawback, one can utilise centroidal Voronoi tessellation, this modified Voronoi process has been shown to be most effective when combined with Lloyd’s algorithm [37,38]. The process involves iterative relaxation of the constructed granular system by replacing the initial seed points with the centroids (typically known as the centre of mass) of the generated cells until convergence is achieved. Fig. 2 shows the system generated via MARS using centroidal Voronoi tessellation followed by the changes produced by applying Lloyd’s algorithm over three iterations.

A key limitation to all seed-based construction techniques is that they produce Gaussian cell size distributions [39,40]. In reality the grain size distribution has been shown to be described best by lognormal or Gamma distributions [41,11,42]. To enable the construction of systems following these distributions a method for performing a Voronoi construction using ‘hard discs’ instead of seeds is available, called the Laguerre-Voronoi method. The main challenge to the Laguerre-Voronoi method is the initial packing of the randomly sized hard discs. There are numerous methods for packing these hard discs, for MARS a custom “Drop and Roll” method has been implemented. This method provides a high level of contact between neighbouring discs resulting in a greater packing fraction while being more computationally efficient [43]. Using this algorithm MARS is capable of generating packing fractions of at least 80% for randomly distributed disc sizes. Once the system has been packed the cells are generated using the robust open source VORO++ package developed by Rycroft [44]. Fig. 3 shows the difference between the structures generated via the centroidal Voronoi tessellation and the Laguerre-Voronoi tessellation, the corresponding grain size distributions are shown in Fig. 4. The implementation of the Laguerre-Voronoi tessellation method within MARS enables the generation of realistic systems with a high level of control over the grain size distributions.

For micromagnetic simulations periodic boundary conditions are used for the Voronoi tessellation in order to remove edge effects, Fig. 5 shows a system created via a Laguerre-Voronoi tessellation with the periodic boundaries indicated by the dashed lines.

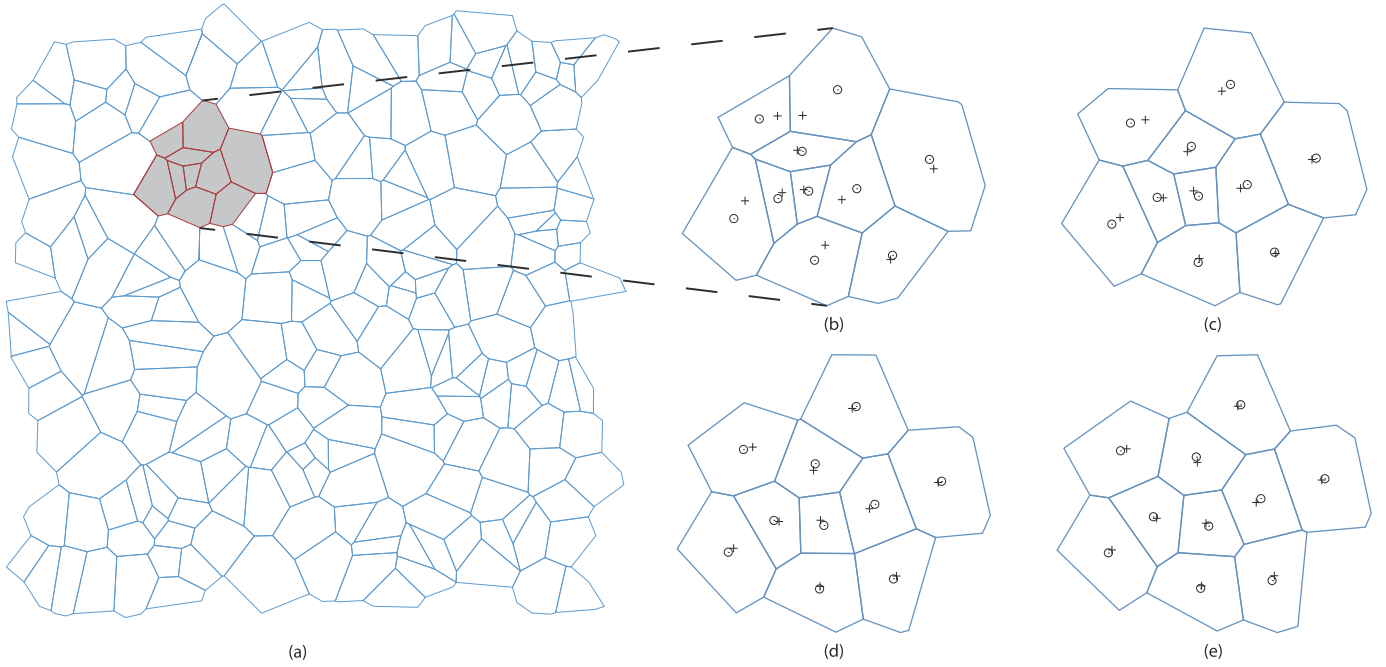


Fig. 2. Example of the granular structure obtained via the centroidal Voronoi tessellation (a). A subsection has been chosen to illustrate Lloyd's relaxation algorithm after: zero (b), one (c), two (d) and three (e) iterations. The seed points are indicated by the crosses with the centroids represented by the circles. As more iterations are performed the angular nature of the grains is reduced.

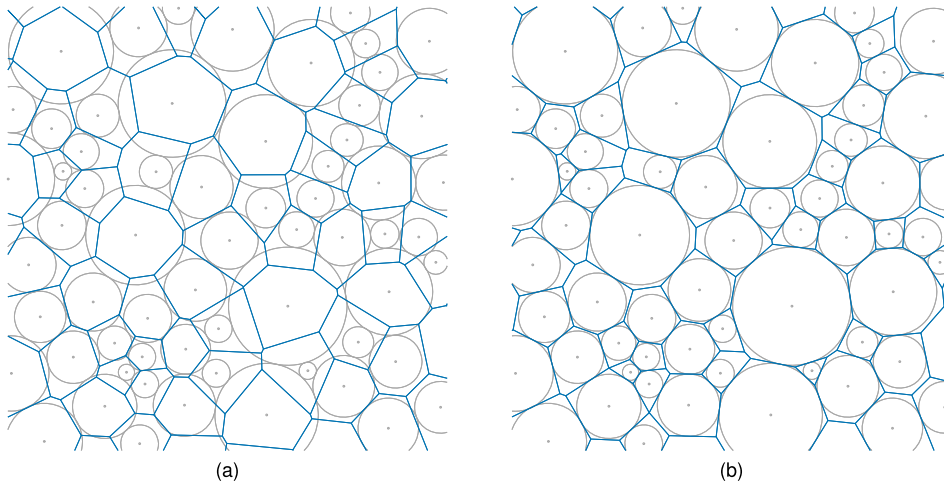


Fig. 3. Granular system generated from an single arrangement of hard discs via the centroidal Voronoi tessellation (a) and the Laguerre-Voronoi tessellation (b).

2.2. System energy and effective fields

For a magnetic film composed of N individual grains, which we can consider as macrospins, the energy of the system can be written as:

$$\begin{aligned}
 E = & - \sum_i V^i K^i (\mathbf{m}^i \cdot \hat{\mathbf{e}}^i)^2 - \mu_0 \sum_i M_s^i V^i \mathbf{m}^i \cdot \mathbf{H}_{\text{app}} \\
 & - \frac{1}{2} \sum_{m \neq j} (M_s^i V^i M_s^j V^j) J_{ij} \mathbf{m}^i \cdot \mathbf{m}^j \\
 & - \frac{1}{2} \sum_{i \neq j} \frac{\mu_0}{4\pi} (M_s^i V^i M_s^j V^j) \frac{3(\mathbf{m}^i \cdot \hat{\mathbf{r}}_{ij})(\mathbf{m}^j \cdot \hat{\mathbf{r}}_{ij}) - \mathbf{m}^i \cdot \mathbf{m}^j}{r_{ij}^3},
 \end{aligned} \quad (1)$$

where V^i is the volume of grain i with uniaxial anisotropy energy density K^i , easy axis direction $\hat{\mathbf{e}}^i$, bulk saturation magnetisation M_s^i and normalised magnetisation vector $\mathbf{m}^i = \mathbf{M}^i / M_s^i$. The anisotropy

energy density, saturation magnetisation and fractional exchange constant J_{ij} are all temperature dependent. The first term is the Zeeman energy which describes the interaction of the grains with an external applied field \mathbf{H}_{app} . The second term is the anisotropy contribution to the energy which describes the preferred alignment direction for the grains magnetisation. The third term describes the exchange interaction between nearest neighbour grains which can be expressed in terms of the local exchange field $\mathbf{H}_{\text{exch}}^i$. The fourth term is the long-range magnetostatic interaction, within the dipole approximation, which couples grains at sites \mathbf{r}_i and \mathbf{r}_j at a distance $\mathbf{r}_{ij} = \mathbf{r}_j - \mathbf{r}_i$ across the whole system. The effective field acting on each grain is obtained from the energy of the system (Eq. (1)) and is given by:

$$\mathbf{H}_{\text{eff}}^i = \mathbf{H}_{\text{app}} + \mathbf{H}_{\text{ani}}^i + \mathbf{H}_{\text{exch}}^i + \mathbf{H}_{\text{dmg}}^i. \quad (2)$$

The individual terms are described in the following.

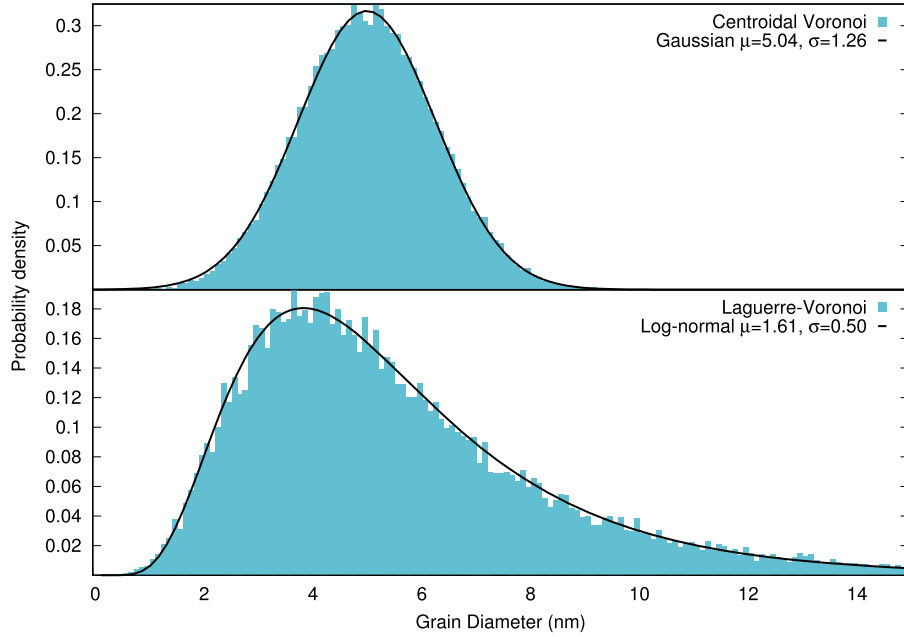


Fig. 4. Grain diameter distributions for centroidal Voronoi tessellation (top) and Laguerre-Voronoi tessellation (bottom). The input distribution was lognormal with $\mu = 1.65$ and $\sigma = 0.55$. The seed based Voronoi is unable to provide the desired distribution, instead providing a Gaussian. The Laguerre-Voronoi was able to produce the desired distribution type with only a small change of parameters, which is to be expected due to the random nature of the packing process.

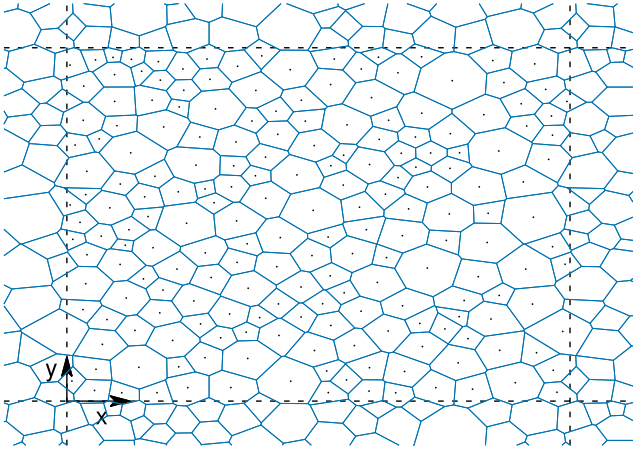


Fig. 5. Example of the periodic system generated via MARS using a Laguerre-Voronoi tessellation. The grains containing points are those generated, with the dashed lines indicating the periodic repetitions.

$\mathbf{H}_{\text{exch}}^i$ describes the coupling between different grains, belonging either to the same layer or to different layers as in the case of exchange-coupled composite (ECC) media. In the case of a granular medium the exchange results from the intergranular medium. Although this is engineered to ensure exchange decoupling, this is not necessarily complete: in fact in the case of media for perpendicular recording the exchange, which balances the effects of the magnetostatic field, is a part of the material design. Under the reasonable assumption that the intergranular exchange is proportional to the contact area between the grains, it has been shown that the exchange $\mathbf{H}_{\text{exch}}^i$ is given by [29,45]:

$$\mathbf{H}_{\text{exch}}^i = \sum_{j \in \text{neigh } i} H_{\text{sat}} J_{ij} \frac{\langle A \rangle}{A_i} \frac{L_{ij}}{\langle L \rangle} \mathbf{m}^j, \quad (3)$$

J_{ij} is the fractional exchange constant between the adjacent grains and L_{ij} is the contact length between grains i and j , A_i is the area of grain i , $\langle \rangle$ denotes the average value and H_{sat} is the exchange

field strength at saturation, which is generally derived from experiment. Sokalski et al. [46] investigated experimentally the exchange coupling between thin layers of *CoCrPt* separated by an oxide, finding an exchange strength which decayed experimentally with oxide layer thickness. Ellis et al. [47] found a similar relation using an atomistic model based on the presence of ferromagnetic impurities in the oxide layer. This study also showed the presence of higher order (biquadratic) exchange and importantly demonstrated that the intergranular exchange decayed to zero rapidly with increasing temperature, suggesting that intergranular exchange does not play a major role in the HAMR recording process. It is important to note, given the likely origin of intergranular exchange in the presence of impurity magnetic spins in the intergranular layer, that J_{ij} could vary significantly. According to refs. [29,45] this can lead to exchange weak links which act as pinning sites and reduce the sizes of clusters arising from magnetostatic interactions.

In the macrospin description there are a number of approaches for the calculation of the magnetostatic interaction. For N elements the time complexity of determining the magnetostatics via brute force is $O(N^2)$ as a result large simulations which account for magnetostatics via brute force become impractical as system sizes increase. However, there are numerous methods to more efficiently determine the magnetostatic field. The first and most simple is to truncate the number of neighbours used to determine the magnetostatic field acting on each grain. The region residing outside of the truncation range is accounted for using a mean field. The nature of this method reduces the complexity significantly to $O(N)$. While truncation can produce larger errors than more sophisticated methods [74], we have found that these errors are negligible as they produce field errors below the noise floor expected in modern recording media simulations. Fig. 6 shows the largest error as a function of the truncation radius. The percentage error is shown to fall rapidly as the truncation radius is increased. Due to the high thermal noise present in modern recording media systems truncation presents a highly efficient method for accounting for the magnetostatics.

For situations where the accuracy of the magnetostatics is highly important MARS provides two additional methods for de-

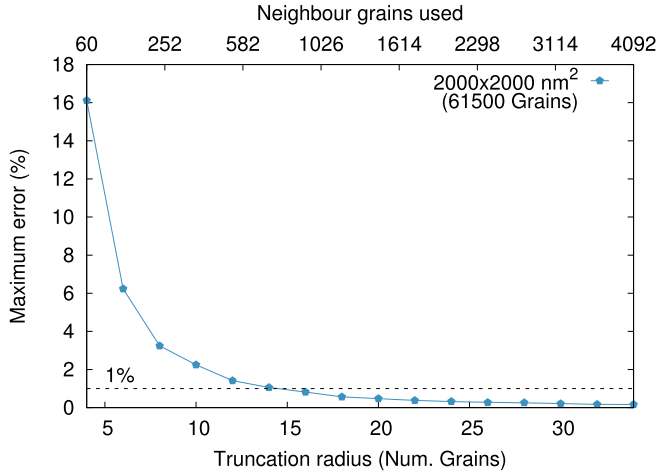


Fig. 6. Error in the determination of the magnetostatic field when using the truncation method as a function of the truncation radius.

termining the magnetostatic field, segmentation and hierarchical subdivision. The segmentation method provides a time complexity of $O(N)$. In segmentation the system is first divided into segments containing multiple grains which are then treated as a single element when determining the magnetostatic field. The field calculation is then split into two steps; the near-field, which is calculated exactly for the neighbouring grains and the far-field which is calculated using the segments for the remainder of the system. The hierarchical method increases the accuracy of the segmentation method by adding a mid-range step to the previously described two step field calculation [27]. The mid-range step involves dividing the nearest neighbour segments into sub-segments. The sub-segments are used to determine the mid-range magnetostatic field. The time complexity for the hierarchical approach is $O(N \log N)$.

Finally, there is also the option of utilising a Fast Fourier transform to perform fast calculations of the magnetostatic fields reducing the time complexity to $O(N \log N)$ as proposed by Mansuripur and Giles [48]. For continuous micromagnetic models which typically use a regular lattice of elements it is trivial to implement a fast Fourier transform (FFT) method. However, as MARS is a granular model where each grain is represented as a single macrospin there is a lack of uniformity thus the implementation of a non-uniform fast Fourier transform (NUFFT) is required [75]. For the initial release MARS does not contain a NUFFT method for determining the magnetostatics, however the addition of this feature is planned for a future release.

The magnetostatic field is calculated using the dipole approximation:

$$\mathbf{H}_{\text{dmg}}^i = \sum_{j \in \text{neigh } i} W_{ij} \mathbf{m}_j, \quad (4)$$

where W_{ij} is the demagnetisation tensor of the system:

$$W_{ij} = \frac{M_s V_j}{4\pi r_{ij}^3} \begin{bmatrix} \frac{3r_{ijx}^2}{r_{ij}^2} - 1 & \frac{3r_{ijx}r_{ijy}}{r_{ij}^2} & \frac{3r_{ijx}r_{ijz}}{r_{ij}^2} \\ \frac{3r_{ijy}r_{ijx}}{r_{ij}^2} & \frac{3r_{ijy}^2}{r_{ij}^2} - 1 & \frac{3r_{ijy}r_{ijz}}{r_{ij}^2} \\ \frac{3r_{ijz}r_{ijx}}{r_{ij}^2} & \frac{3r_{ijz}r_{ijy}}{r_{ij}^2} & \frac{3r_{ijz}^2}{r_{ij}^2} - 1 \end{bmatrix}, \quad (5)$$

V is the volume of the grain, $r_{ij\alpha}$ is the displacement between grains i and j , with the subscript $\alpha = x, y, z$ denoting the component of the displacement. The key benefit of using the tensorial form of the magnetostatic field is that the time complexity during integration is dependent upon the number of magnetostatic

neighbours and not on the method used to determine the demagnetisation tensor, as is evident from Eq. (4). This allows the method used to determine W_{ij} to be changed as required by the user without affecting the time required for simulation. Additionally as the W -matrix is dependent only on the positions and sizes of the grains it can be completely determined prior to the simulation. MARS is capable of accepting a pre-determined W -matrix supplied by the user. First MARS should be used to generate the granular structure. Next, using the output structure, a W -matrix can be determined using any method the user desires. The simulation can then be run with the W -matrix option set to import from an external file which will contain the data of the pre-determined W -matrix. The dipole approach is the simplest available to calculate the magnetostatic contribution and is the method currently implemented in MARS. There are numerous more complex and improved methods available to determine the magnetostatic field such as the surface-volume and surface-surface integral [49–51].

The temperature dependence of $\mathbf{H}_{\text{ani}}^i$ is described using the following expression:

$$\mathbf{H}_{\text{ani}}^i(T) = \frac{2K^i}{M_s^i} (m^i(T))^{\eta-1} (\mathbf{m}^i \cdot \hat{e}^i) \hat{e}^i, \quad (6)$$

where \hat{e}^i is the unit vector aligned along the easy axis, K^i is the anisotropy and M_s^i is the zero temperature saturation magnetisation of grain i . Here we exploit the fact that we can express the temperature dependence of K via the dependence on the magnetisation m described via Callen-Callen scaling [52], which allows $K(T)$ to be expressed as:

$$K^i(T) = K_0^i m^i(T)^\eta. \quad (7)$$

K_0 is the anisotropy energy density at 0 K and η is determined via experiment or atomistic parameterisation. Typically the exponent $\eta = 3$ for uniaxial anisotropy and $\eta = 2$ for 2-site anisotropy appropriate for FePt [53].

2.3. Dynamical and kinetic Monte-Carlo solvers

MARS utilises three separate solvers to describe the magnetisation, the Landau-Lifshitz-Gilbert, Landau-Lifshitz-Bloch and kinetic Monte Carlo. The LLG and LLB solvers require very short timesteps, in the region of picoseconds and femtoseconds respectively, to function and provide dynamic information about the magnetisation. The KMC is a probabilistic solver which sacrifices the dynamic information in order to enable much larger timesteps. This enables the simulation of long timescale phenomena, for example the long-term decay of written information arising from thermal activation. Each of the solvers presented in this work have been rigorously tested to ensure correct implementation and high accuracy. The details of these tests are provided in Supplementary Notes 1-3, with Supplementary Figs. 1-7 showing comparisons between produced and expected test results.

The LLG equation of motion for each grain i , including stochastic effects, is given by:

$$\frac{\partial \mathbf{m}^i}{\partial t} = -\frac{\gamma_e}{1 + \alpha^2} \left[\mathbf{m}^i \times (\mathbf{H}_{\text{eff}}^i + \mathbf{H}_{\text{th}}^i) \right] - \frac{\alpha \gamma_e}{1 + \alpha^2} \mathbf{m}^i \times \left[\mathbf{m}^i \times (\mathbf{H}_{\text{eff}}^i + \mathbf{H}_{\text{th}}^i) \right]. \quad (8)$$

The first term describes the quantum mechanical precessional motion of the magnetisation which in the presence of H_{th}^i becomes stochastic in nature, while the second term represents the phenomenological relaxation of the magnetisation towards an equilibrium position [54]. The Gilbert damping α couples the spin system

with the environment, considered to act as the thermal bath, and determines how fast the system relaxes towards equilibrium. \mathbf{H}_{th}^i is the thermal field, this stochastic field accounts for the thermally driven behaviour of the macrospin and is described by a non-correlated white noise Gaussian function.

$$\begin{aligned} \langle H_{\text{th}}^{i\alpha}(t) \rangle &= 0 \\ \langle H_{\text{th}}^{i\alpha}(t) H_{\text{th}}^{j\beta}(t') \rangle &= \frac{2\alpha k_B T}{\gamma_e M_s V} \delta_{ij} \delta_{\alpha\beta} \delta(t-t'), \end{aligned} \quad (9)$$

where: i, j label the magnetisation on the respective sites; $\alpha, \beta = x, y, z$; $k_B = 1.381 \cdot 10^{-16}$ ergK $^{-1}$ is the Boltzmann constant; T is the temperature; $\delta_{\mu\nu}$ is the Kronecker delta and $\delta(t-t')$ is the delta function. In this formulation the noise is considered to be spatially and temporally uncorrelated, i.e., white noise.

This approach works at relatively low temperatures where one can consider the grain to be fully magnetically saturated and to exhibit coherent rotation with all atomic spins remaining parallel. Under these circumstances the equation of motion need only model transverse dynamic processes and the LLG equation is valid. However, as temperature increases and approaches the Curie point this is no longer true and the Landau-Lifshitz-Bloch (LLB) equation must be used instead. The LLB introduces a longitudinal relaxation of the macrospin which accounts for the loss of magnetisation and divergence of the longitudinal susceptibility as the temperature approaches the Curie point. The LLB equation was first derived by Garanin [55,56]. The LLB equation is a single (macrospin) representation of the dynamical behaviour of a single grain and differs from the LLG equation in its inclusion of longitudinal relaxation of the magnetisation. Although the LLB equation parameters to be outlined below were originally derived from mean-field theory, these can be obtained from atomistic calculations. As shown by Chubykalo et al. [57], the LLB equation gives excellent agreement with atomistic model calculations, essentially validating its use in calculations of HAMR, which involve heating beyond the Curie temperature. The implementation of the stochastic LLB solver used by MARS follows the work of Evans et al. [25] (sLLB-II) and for each grain i reads:

$$\begin{aligned} \frac{\partial \mathbf{m}^i}{\partial t} &= -\gamma_e (\mathbf{m}^i \times \mathbf{H}_{\text{eff}}^i) + \frac{\gamma_e \alpha_{\parallel}}{m^i{}^2} (\mathbf{m}^i \cdot \mathbf{H}_{\text{eff}}^i) \mathbf{m}^i \\ &\quad - \frac{\gamma_e \alpha_{\perp}}{m^i{}^2} \left[\mathbf{m}^i \times (\mathbf{m}^i \times (\mathbf{H}_{\text{eff}}^i + \zeta_{\perp}^i)) \right] + \zeta_{ad}^i, \end{aligned} \quad (10)$$

where \mathbf{m}^i is the reduced magnetisation $\mathbf{M}^i/M(T=0)$, m^i is the length of \mathbf{m}^i and γ_e is the electron gyromagnetic ratio. The first and third terms are the precessional and damping terms for the transverse component of the magnetisation, as in Eq. (8), while the second and fourth terms are introduced to account for the longitudinal relaxation of the magnetisation with temperature. The stochastic LLG and LLB solvers both utilise the Heun integration scheme. The benefits of the Heun scheme are two-fold. First it provides second order accuracy in Δt for the deterministic part, with greater numerical stability than Euler type schemes due to the predictor-corrector method type. Second, it yields the required Stratonovich solution of stochastic differential equations. The damping of the magnetic moment is split into longitudinal α_{\parallel} and transverse α_{\perp} components given by:

$$\alpha_{\parallel} = \frac{2}{3} \frac{T}{T_c} \lambda \quad \text{and} \quad \begin{cases} \alpha_{\perp} = \lambda \left(1 - \frac{T}{3T_c} \right), & \text{if } T \leq T_c \\ \alpha_{\perp} = \alpha_{\parallel} = \frac{2}{3} \frac{T}{T_c} \lambda, & \text{otherwise.} \end{cases} \quad (11)$$

Where λ is the thermal bath coupling, a temperature independent phenomenological parameter, that is the same as that used in atomistic spin dynamics. The transverse damping is related to the Gilbert damping by the expression:

$$\alpha = \frac{\alpha_{\perp}}{m}, \quad (12)$$

ζ_{\perp} and ζ_{ad} are the diffusion coefficients that account for the thermal fluctuations. The thermal noise terms are described by Gaussian functions with zero average and a variance proportional to the strength of the fluctuations:

$$\begin{aligned} \langle \zeta_{ad}^{i\alpha}(t) \zeta_{ad}^{j\beta}(t') \rangle &= \frac{2|\gamma| k_B T \alpha_{\parallel}}{M_s V} \delta_{ij} \delta_{\alpha\beta} \delta(t-t') \\ \langle \zeta_{\perp}^{i\alpha}(t) \zeta_{\perp}^{j\beta}(t') \rangle &= \frac{2k_B T (\alpha_{\perp} - \alpha_{\parallel})}{|\gamma| M_s V \alpha_{\perp}^2} \delta_{ij} \delta_{\alpha\beta} \delta(t-t'). \end{aligned} \quad (13)$$

As temperatures approach and exceed the Curie point, Eq. (6) produces a fictitious longitudinal component of the anisotropy. This leads to a reduction in the longitudinal relaxation of the magnetisation as a function of temperature. To overcome this issue the anisotropy field can also be described as a function of the transverse susceptibility χ_{\perp} [56]:

$$\mathbf{H}_{\text{ani}}^i = \frac{-(m_x^i \hat{x} + m_y^i \hat{y})}{\chi_{\perp}}, \quad (14)$$

where m_x^i and m_y^i are the components of the reduced magnetisation vector and \hat{x} , \hat{y} are the unit vector along these directions, respectively. Unlike Eq. (6) this form of the anisotropy assumes that the easy axis lies along the z-axis however it is valid for all temperature ranges and is therefore the most suitable description for LLB applications. For soft materials the determination of χ_{\perp} is extremely challenging and thus both forms of the anisotropy are available for use with the LLB solver to enable the simulation of both hard and soft materials.

The LLB equation includes an additional field term, $\mathbf{H}_{\text{intragrain}}^i$ within the effective field. This term accounts for the exchange between the atoms within grain i , controls the length of the magnetisation and is given by

$$\mathbf{H}_{\text{intragrain}}^i = \begin{cases} \frac{1}{2\tilde{\chi}_{\parallel}} \left(1 - \frac{m^i{}^2}{m_e^2} \right) \mathbf{m}^i, & \text{if } T \leq T_c \\ -\frac{1}{\tilde{\chi}_{\parallel}} \left(1 + \frac{3}{5} \frac{T_c}{T - T_c} m^i{}^2 \right) \mathbf{m}^i, & \text{otherwise.} \end{cases} \quad (15)$$

Here m^i is length of the reduced magnetisation \mathbf{m}^i of grain i , and $m_e(T)$ is the equilibrium magnetisation. The term $\mathbf{H}_{\text{intragrain}}$ encapsulates the new physics introduced by the LLB equation. It incorporates the longitudinal fluctuations of the magnetisation while maintaining a mean value $m_e(T)$. It is important to note that the fluctuations diverge as $\tilde{\chi}_{\parallel}$ diverges close to T_c . This is responsible for the onset of the linear reversal model close to T_c . Clearly specification of the temperature dependence of the LLB parameters is of paramount importance: a factor complicated by the effects of finite size on the magnetic properties.

2.3.1. Atomistic parameterisation

The granular model requires characterisation of the temperature dependence of the magnetisation, anisotropy and susceptibilities. These quantities are obtained via fitting of atomistic data, obtained using the VAMPIRE package [58]. A key benefit of atomistic parameterisation is the improved accuracy of the modelled material's behaviours as well as the ability to simulate granular

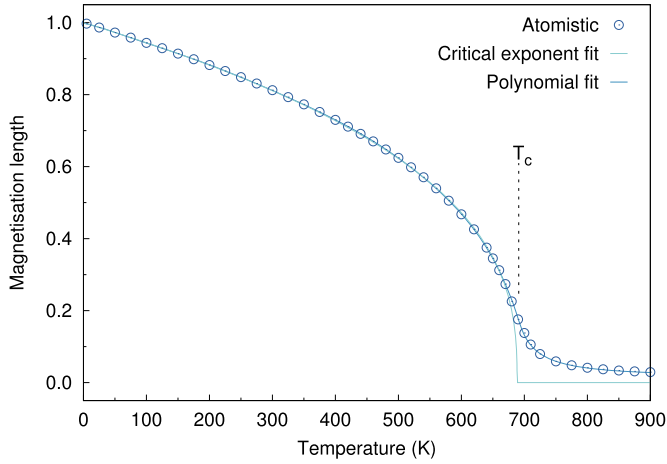


Fig. 7. Comparison of the fittings of the magnetisation achieved for a 5 nm grain via the two available methods implemented in MARS. The dots represent the atomistic data, while the lines show the fits.

systems which include a segregant between the grains as is typically the case in recording media. There are two available methods for fitting the magnetisation. The first is fitted according to $m(T) = M(T)/M_s = (1 - T/T_c)^\beta / M_s$, where M_s is the spontaneous magnetisation and β is the critical exponent. The second is fitted via a more complex polynomial in powers of $(T - T_c)/T_c$:

$$m(T) = \begin{cases} \sum_{i=0}^9 A_i \left(\frac{T_c - T}{T_c}\right)^i + A_{1/2} \left(\frac{T_c - T}{T_c}\right)^{\frac{1}{2}}, & \text{if } T < T_c \\ \left[\sum_{i=1}^2 B_i \left(\frac{T - T_c}{T_c}\right)^i + A_0^{-1} \right]^{-1}, & \text{otherwise.} \end{cases} \quad (16)$$

Both methods are capable of producing the characteristic behaviour of the temperature dependent magnetisation. A comparison of these two methods is given in Fig. 7. For bulk systems a strong criticality is expected and the critical exponent fit reproduces the sharp transition to zero magnetisation at the Curie point. However, as grain sizes decrease finite size effects become significant which cause a reduction in the criticality of the transition. The result of finite size effects is a small but non-zero magnetisation above the Curie point. The polynomial fit is capable of reproducing this behaviour and provides greater agreement with atomistic data for small grains (i.e. 5 nm) than the critical exponent fit.

The susceptibility χ is a measure of the strength of the fluctuations of the magnetisation. The components of the susceptibility, according to the spin fluctuation model, can be obtained by the fluctuations of the same magnetisation components as follows [59]:

$$\tilde{\chi}_\alpha = \frac{\mu_s N}{k_B T} \left(\langle m_\alpha^2 \rangle - \langle m_\alpha \rangle^2 \right). \quad (17)$$

Where $\tilde{\chi}_\alpha = \chi_\alpha / M_s V$ is the reduced susceptibility and is in units of field⁻¹. N is the number of spins in the system with magnetic moment μ_s . Here $\langle m_\alpha \rangle$ is the ensemble average of the reduced magnetisation component $\alpha = x, y, z$ and longitudinal. x, y, z are the spatial Cartesian components of the magnetisation, while longitudinal describes the length of the magnetisation. $\tilde{\chi}_\parallel$ describes the strength of the fluctuations of the magnetisation component along the easy-axis direction, which for our system is z . $\tilde{\chi}_\perp$ refers to the fluctuations orthogonal to the easy axis and thus on the x - y

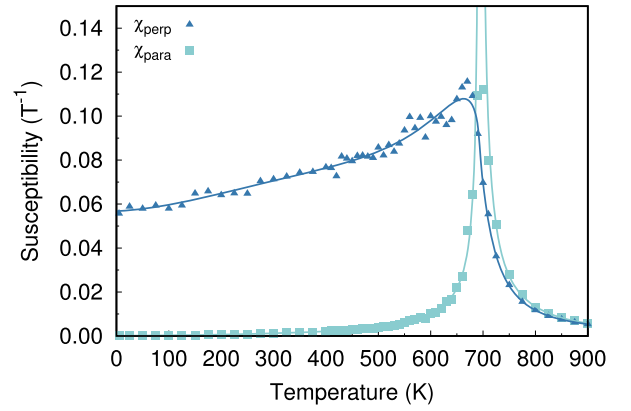


Fig. 8. Fit obtained for parallel and perpendicular susceptibility using the inverse method similar to that of Ellis [59]. The Curie point of this system is the temperature where the susceptibilities first intersect, which for this data is 685.14 K.

plane. For $\tilde{\chi}_\parallel$ and $\tilde{\chi}_\perp$, we use a similar approach to Ellis [59] and we fit the inverse of the susceptibility $1/\tilde{\chi}_{\parallel,\perp}$:

$$\frac{1}{\tilde{\chi}_{\parallel,\perp}} = \begin{cases} \sum_{i=0}^9 C_i \left(\frac{T_c - T}{T_c}\right)^i + C_{1/2} \left(\frac{T_c - T}{T_c}\right)^{\frac{1}{2}}, & \text{if } T < T_c \\ \sum_{i=0}^4 D_i \left(\frac{T - T_c}{T_c}\right)^i, & \text{otherwise.} \end{cases} \quad (18)$$

Where C_i and D_i are the fitting parameters and T_c is the Curie point, obtained by determining the temperature at which the susceptibilities intersect. Fig. 8 shows the susceptibilities and fits obtained from atomistically parameterised FePt, the Curie point of this system is 685.14 K.

Low anisotropy systems and systems of reduced dimensions cannot retain the alignment of the magnetisation along the easy axis up to T_c . In such cases $\tilde{\chi}_\parallel$ is a mix of the spatial components and becomes difficult to determine. A workaround is to avoid calculating $\tilde{\chi}_\parallel$ directly and to obtain $\tilde{\chi}_\parallel$ from the longitudinal susceptibility $\tilde{\chi}_l$, following the discussion presented in [60]. Unfortunately a similar method cannot be used for $\tilde{\chi}_\perp$ making it difficult to determine the anisotropy for soft systems when the anisotropy field is given by Eq. (14).

Alternatively, if the anisotropy field is described as in Eq. (6), the reduced anisotropy is given by $k(T) = K(T)/K_0 = m(T)^\gamma$, as discussed by Callen-Callen [52]. MARS implements both a standard Callen-Callen fitting and an extended version. The extended version utilises three temperature regions each with their own fit parameters such that there are no discontinuities. This extended fitting method enables greater accuracy in the reproduction of the anisotropy as a function of temperature. This approach should provide more useful results in the case of soft materials, where extracting $\tilde{\chi}_\perp$ can prove difficult. Fig. 9 is a comparison of the fits obtained using the standard and extended Callen-Callen fitting methods. Once all these parameters are determined, the granular model is fully parameterised regarding the material properties.

2.3.2. Kinetic Monte-Carlo solver

Finally we turn to the solver for long-timescale simulations: the kinetic Monte Carlo (kMC) solver. In the kMC approach as given in [61], the switching probability is dependent on the measuring time t_m as follows,

$$P_t = 1 - e^{-t_m/\tau}, \quad (19)$$

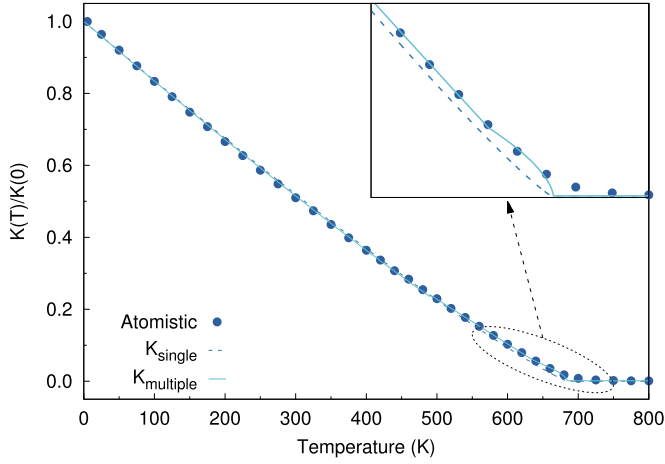


Fig. 9. Comparison of the fit achieved via the standard (single) and extended (multiple) Callen-Callen methods. The points represent the atomistic simulation data while the lines show the fits used in MARS. The extended Callen-Callen is able to provide an improved fit overall and especially near the Curie point as shown in the inset.

where the relaxation time τ is given by the Arrhenius-Néel law [24]

$$\tau^{-1} = f_0 \left(\exp \left[-\frac{\Delta E_{12}}{k_B T} \right] + \exp \left[-\frac{\Delta E_{21}}{k_B T} \right] \right), \quad (20)$$

where f_0 is the attempt frequency, usually assumed around 10^9 s^{-1} for these systems, and $\Delta E_{12,21}$ are the energy barriers for switching between states. Typically, large energy barriers of $> 60k_B T$ are required in order to ensure long-term thermal stability of written bits. τ^{-1} is given by $\tau^{-1} = \tau_{12}^{-1} + \tau_{21}^{-1}$. To model the physical effect of the easy axis dispersion, easy axes are chosen randomly within a Gaussian dispersion of angle about the normal. The total energy barrier including the effect of anisotropy dispersion can be written as

$$\Delta E(\mathbf{H}_T, \psi) = K_u V [1 - \mathbf{H}_T / g(\psi)]^{\kappa(\psi)}, \quad (21)$$

where \mathbf{H}_T the total effective field, $g(\psi) = [\cos^{2/3} \psi + \sin^{2/3} \psi]^{-3/2}$ and $\kappa(\psi) = 0.86 + 1.14g(\psi)$ are the numerical approximations given by Pfeiffer [62]. The kMC is capable of simulations on the timescale of years and is valid for systems where the energy barrier is much larger than the thermal energy. In order to function, the kMC requires calculation of the magnetisation states corresponding to the energy minima along with the energy barrier separating the two states. Stationary states are found by solution of the Stoner-Wohlfarth model of coherent rotation [63] for which the free energy is given by

$$E = K_u V (\hat{\mathbf{e}} \cdot \hat{\mathbf{m}})^2 - \mu \mathbf{H} \cdot \hat{\mathbf{m}}. \quad (22)$$

The final step [61] is to ensure that, after switching, the populations of the energy minima obey Boltzmann statistics. This approach leads to the condition that, if the reversal transition is allowed, the moment is then assigned to either energy minimum with a probability,

$$p = e^{-E_i} / (e^{-E_1} + e^{-E_2}), \quad (23)$$

where E_1 and E_2 are the energies of the two present minima and $i = 1, 2$ labels the respective minima, thereby ensuring that the population of the two states obeys the Boltzmann distribution in thermal equilibrium [61]. This is important in order to include the 'backswitching' mechanism which leads to dc or 'remanence' noise.

Taking account of both distributions the transition probability is determined using:

$$P_2 = \left(1 - \exp \left[-\frac{t_m}{\tau} \right] \right) \left(1 + \exp \left[-\frac{(E_2 - E_1)}{k_B T} \right] \right)^{-1}. \quad (24)$$

Where P_2 is the probability of the magnetic moment jumping to the second minima and $E_2 - E_1$ is the energy barrier separating the two minima. To determine if a switching event occurs a random number between zero and unity is generated and compared to P_2 . If it is less than P_2 the magnetic moment orientation is assigned corresponding to the second minimum otherwise it is assigned to the first minimum. t_m is the measurement time. During the measurement time the external properties such as magnetic field and temperature are assumed constant, such that Eq. (24) can be applied.

2.4. Curie temperature dispersion

The HAMR process involves heating through T_c which, as a result, becomes an important material parameter. More particularly, simulations by Li and Jhu [64,65] have shown that the dispersion of T_c is a serious limitation for the ultimate storage density achievable for HAMR. Here we consider an irreducible contribution to the dispersion of T_c which arises directly from the diameter dispersion. It is well known that finite size effects lead to a reduction of T_c , demonstrated experimentally for FePt by Rong et al. [66]. A theoretical investigation based on an atomistic model by Hovorka et al. [30] showed that the variation $M(T)$ was well described by the finite size scaling law

$$T_c(D) = T_c^\infty (1 - (d_0/D)^\lambda), \quad (25)$$

where D is the grain diameter, λ is the so-called phenomenological shift exponent and d_0 is the microscopic length scale close to the dimension of a unit cell of the lattice structure. The exponent λ is related to the correlation length universal critical exponent ν and it is expected that $\lambda = \nu^{-1}$. However, small grains can exhibit departure from universality so we prefer the form of Eq. (25) as a functional form to represent the diameter dependence of T_c . Clearly a dispersion of diameter maps onto the dispersion of T_c . Assuming a lognormal distribution of D , with logarithmic mean D_m and variance σ_D^2 it has been shown [30] that the dispersion of T_c is given by the distribution function

$$f_T(\Delta T_c) = \frac{1}{\sqrt{2\pi} \Delta T_c \sigma_T} \exp \left(-\frac{(\ln \Delta T_c - T)^2}{2\sigma_T^2} \right), \quad (26)$$

with $\Delta T_c = T_c^\infty - T_c$. Eq. (26) is a lognormal distribution function with logarithmic mean $T_m = \lambda (\ln(d_0(T_c^\infty)^{1/\lambda}) - D_m)$ and variance $\sigma_T^2 = \lambda^2 \sigma_D^2$. Through Eq. (25), with d_0 , λ and T_c^∞ determined either from experiment or atomistic model calculations, a T_c value can be assigned to an individual grain and Eq. (26) used to calculate the standard deviation of the T_c dispersion.

3. Simulations

This section presents a demonstration of some of the bundled simulation types available in MARS at release. These simulations serve to show the capability of MARS and provide some of the most common simulation types. The first example simulation is the writing of a pseudorandom bit sequence (PRBS) pattern for multiple HAMR systems. The second example is the determination of switching probabilities for characterising Curie point dispersion via comparison with experimental data. Finally an example of FMR simulations for use in determining system damping is provided.

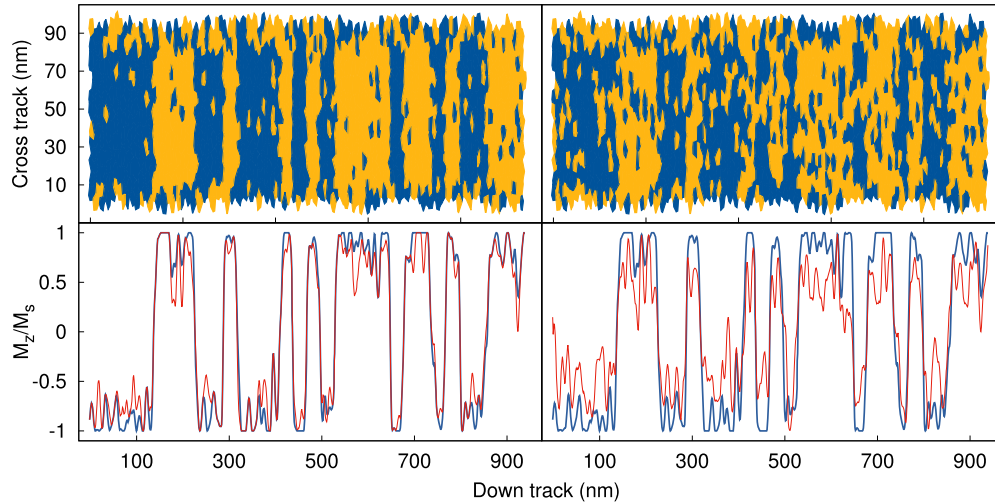


Fig. 10. HAMR writing and reading simulation for $KV/k_B T = 79$ on the left and $KV/k_B T = 62$ on the right. The top graph shows the magnetisation of the grains after the PRBS was written via the LLB solver. The bottom graph shows the signal obtained via read back immediately after writing (blue) and after a ten year time evolution (red) via the kMC solver.

3.1. Writing and reading processes for heat assisted magnetic recording

Development of improved heat assisted magnetic recording requires investigations into the thermal reversal of the grains along with the effect of bit spacing on data stability and writing performance. MARS contains three separate HAMR focused simulations. The first applies a temporally dependent laser and field profile onto a single bit, allowing investigations of thermal reversal properties of materials. The second simulation, consists of a bit within a surrounding system of grains, utilising a temporal and spatially dependent laser and field profile, allowing for investigation into the influence of the written bit on any surrounding grains. The third simulation models realistic data writing, via a square-wave or user specified binary sequence. This writing can occur for single or multiple tracks. Using this third simulation, comprehensive investigations into the entire HAMR writing process can be achieved. (Online only: An example of the simulation process is provided in Supplementary video 1: in this video the single tone is written to one track with multiple PRBS written on the adjacent track to investigate adjacent track erasure.)

Read back of a system can also be simulated in MARS. The read back simulation utilises a convolution of the read head sensitivity function with the system magnetisation as the read head is scanned along the track [73]. Two user configurable sensitivity functions are provided: a box shape, where any magnetisation outside of the box is ignored; and a Gaussian with a separate full-width at half-maximum (FWHM) for the down track and cross track dimensions. In order to investigate data decay over time the simulation utilises the kMC solver to simulate the system for years and performs read back at specified intervals.

Fig. 10 shows the output obtained via the realistic HAMR writing and reading simulation available in MARS. For this simulation two systems with energy barriers of $KV/k_B T = 79$ and 62 were used. Each system consisted of 1,300 grains with a lognormal grain size distribution with an average diameter of 8 nm. The material parameters used were $M_s = 1,051.65 \text{ emu/cm}^3$, $T_c = 693.5 \text{ K}$, $\lambda = 0.1$ and $K_u = 9.2 \cdot 10^7 \text{ erg/cm}^3$ and $K_u = 7.1 \cdot 10^7 \text{ erg/cm}^3$ respectively. A 31-bit PRBS was written to the systems. The sequence used was 1111100011011101010000100101100. Both systems were then evolved over time for ten years and read back to generate a second read back signal. The read head for this simulation was treated as ideal with the sensitivity function set as a 1 nm long box with a width equal to the track width. This simulation was performed 100 times with different random seeds,

the read back signal was then obtained for each simulation in order to obtain the spatial, i.e. of the medium, signal-to-noise ratio (SNR) as a function of time. There are two contributions to the spatial SNR: transition and remanence [34]. These SNRs describe the noise present at and away from the bit transitions respectively. The latter is caused by grains with $KV/k_B T$ such that switch back, whereas the former is a measure of how good a transition between bits is written. Transition noise is the noise expected to be dominant in high density media due to the reduce dimensions the bit size. The calculation of SNR is currently not included in the MARS software package, however, there are plans to do so in a future release.

The extraction of SNR is based on the ensemble wave form analysis developed by Seagate [67,68], a method that allows one to separate and extract the different noise components: transition and remanence. The approach proceeds as follows: a track is written multiple times, 100 times in the present case, with each track read back once only since reader noise is not included. The signals are first synchronised via cross-correlation and afterwards the average “noise-free” signal is obtained by averaging over the signal of the 100 written tracks. Then, the total spatial noise is calculated as the variance of the average “noise-free” signal. To extract the remanence and transition noise appropriate windowing functions are applied to the total spatial noise. Eventually, the SNRs are calculated as $10 \log_{10}$ of the ratio between the total signal power and the respective noise power. Fig. 11 shows the SNR components for the high energy barrier system ($KV/k_B T = 79$), and as expected the transition noise is the bottleneck.

For highly accurate determination of the SNR a large number of total bits is required. Fig. 12 shows the spatial SNR as a function of the total number of simulated bits. The results show that the SNR converges as the number of total bits is increased, with 5,000 bits and more showing a stable SNR with fluctuations of a maximum magnitude of 0.05 dB. In order to achieve these high total bit numbers one can simulate multiple systems in the same manner as described for the result shown in Fig. 10, however, the smaller the systems the greater the total number of required simulations. The systems presented previously were relatively small in order to enable a clear display of the obtained read back signals for the sake of explaining the implemented process. However, MARS is capable of simulated much larger systems. Fig. 13 shows the average magnetisation for an adjacent track interference simulation for a set of forty media realisations consisting of 135 bits with length 20 nm and three tracks with a width of 21 nm.

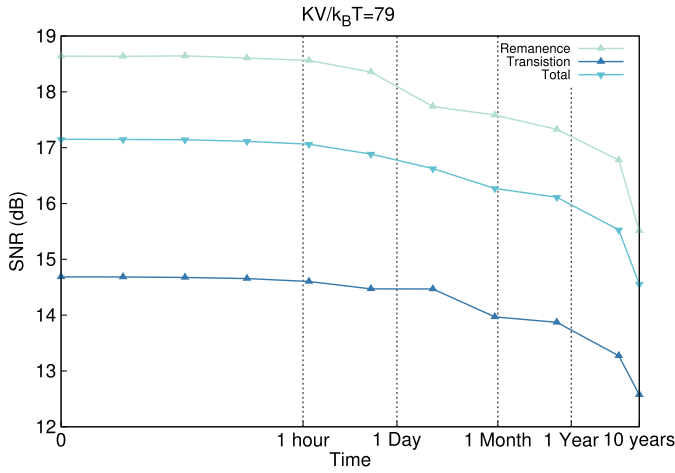


Fig. 11. SNR obtained from multiple read back simulations performed for a HAMR system with $KV/k_B T = 79$.

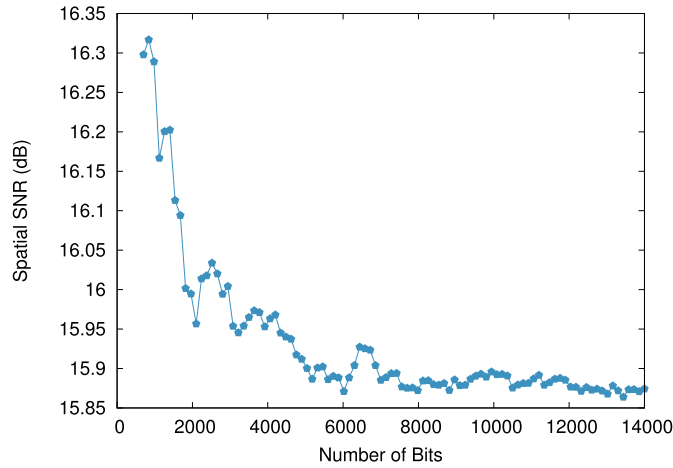


Fig. 12. Spatial SNR as a function of the total number of simulated bits.

3.2. HAMR switching probability

The heating in HAMR systems occurs in a narrow temperature region near T_c , thus the performance of HAMR is highly dependent on the T_c dispersion of the recording medium [31,64,65]. To determine the T_c dispersion experimentally the procedure requires measurement of the thermo-remanence magnetisation as a function of the applied laser pulse peak power [23]. The application of this laser pulse occurs over the long timescale thus LLB simulations are extremely computationally expensive, to the point of impracticability. MARS overcomes this problem by utilising the multi-timescale nature of the code. The solver used by the code is determined automatically based on the laser application time: if this time is of the order of microseconds or greater then the kMC is used otherwise the LLB is used. The heating and cooling phases require dynamic information to be modelled and hence are always performed via the LLB solver. The ability for MARS to automatically select the most suitable solver allows for the simulations to be run in batch jobs without specification of the solver or editing of the source code.

Fig. 14(c,d) are the results of thermoremanence simulations used to investigate the switching probability of single FePt grains as a function of peak temperature for HAMR-like heat pulses for various pulse lengths and under different applied fields. The considered pulse length falls within the few nanoseconds regime, thus the LLB solver has been employed in these simulations. These re-

Table 1

Bi-layer material parameters.

Parameter	FePt	Fe-like alloy
Anisotropy energy density (erg/cm ³)	$9.37 \cdot 10^7$	$0.70 \cdot 10^7$
Curie Temperature (K)	690	1040
Saturation magnetisation (emu/cm ³)	1067	700
Damping	0.1	0.5
Exchange field (Oe)	8000	26000

sults are compared with the switching probabilities obtained by performing atomistic simulations for the same system and setup, presented in panels (a,b). The agreement between the atomistic parameterised LLB and atomistic simulations, which have also been used for the parameterisation, proves the ability of MARS in describing such processes, as discussed in more detail in Ref. [20]. Fig. 15 presents an example of the average magnetisation dynamics for 100 FePt grains under the application of an external -1 T field along the z -axis, and a 1.8 ns heat pulse with peak temperature $T_{\text{peak}} = 600, 700$ K. The dashed brown line shows the Gaussian profile used to model the time dependence of the heat pulse:

$$T(t) = T_a + (T_{\text{peak}} - T_a) \exp[-(t - 3t_{\text{pulse}})^2 / t_{\text{pulse}}^2], \quad (27)$$

where t_{pulse} corresponds to 1/6 of the total pulse length and T_a is the ambient temperature, the temperature at which the grains are in absence of the heat pulse, 300 K in this case. For low T_{peak} and relatively fast pulses the magnetisation reversal of the grains cannot be achieved, however, despite this a partial reversal can be observed when the temperature approaches T_{peak} . However, as the grains cool down the magnetisation is restored along the initial direction. On the other hand, when T_{peak} approaches T_c of the grains, all grains are reversed.

Following the verification of the switching probabilities produced by the MARS code a bi-layer system consisting of a 5 nm Fe-like alloy layer on top of a 10 nm FePt layer has been simulated. Both materials were first parameterised using atomistic simulations, the key parameters are detailed in Table 1. Fig. 16 shows the switching probability as a function of both the peak temperature and pulse duration with an applied field strength of 8,000 Oe. As with the previous results the switching probability is shown to increase with longer pulse duration. Furthermore, the results show that the exchange-coupled composite media presents a switching probability of over 90% when using low peak temperatures and a short pulse duration. From these results it is clear that an ECC media will provide a significant improvement in the effectiveness of HAMR devices, with the possibility to not only reduce overall power draw but also to reduce the rate of failed switching events.

3.3. Ferromagnetic resonance

Ferromagnetic resonance (FMR) is an important technique used for the measurement of magnetic properties for bulk and thin-film magnetic media [69]. FMR simulations enable investigation into the dynamic properties of a material such as the damping [70] as well as the static properties such as saturation magnetisation and uniaxial anisotropy [71]. MARS provides a simple system to perform frequency and field swept FMR simulations over a range of temperatures via its LLG and LLB solvers. Fig. 17 shows the power spectrum obtained via FFT vs. the applied field frequency obtained via FMR simulations of a single system at various temperatures. The data have been fitted to a Lorentzian function:

$$L(x) = \frac{A}{\pi} \frac{0.5w}{(x - f_0)^2 + (0.5w)^2}, \quad \alpha = \frac{0.5w}{f_0}, \quad (28)$$

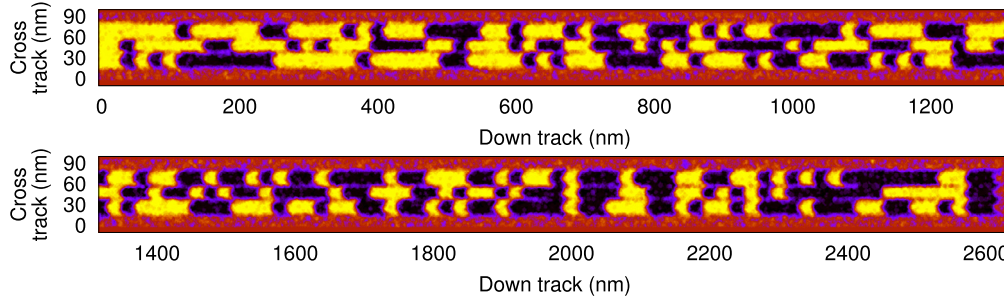


Fig. 13. Average magnetisation of forty 135 bit media realisations for use in an adjacent track interference simulation. The magnetisation is represented by yellow for parallel to the z-axis, purple for anti-parallel and red for zero magnetisation. The continuous track has been split in half for viewing.

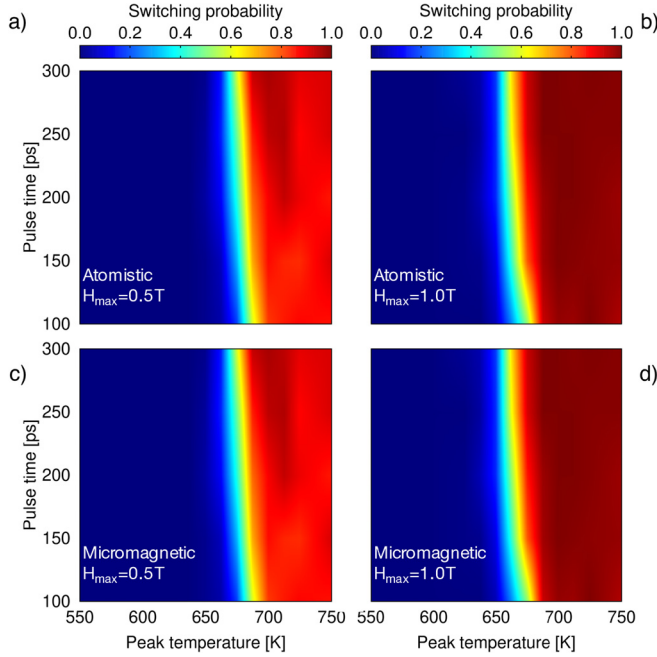


Fig. 14. Switching probability as a function of peak temperature for various pulse lengths for both micromagnetic and atomistic simulations. Adapted from Ref. [20].

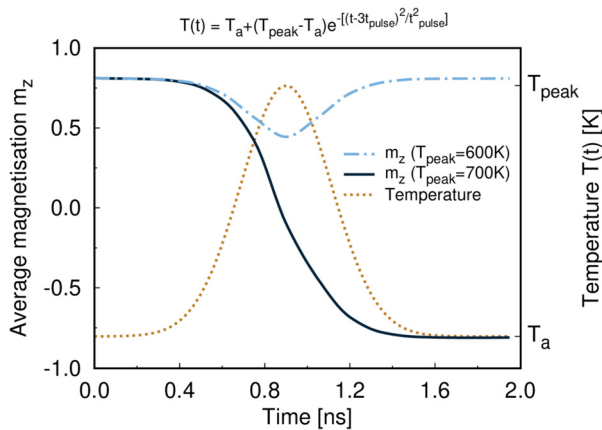


Fig. 15. Time dependence of the average magnetisation for 100 FePt grains, obtained with the LLB solver, for a heat pulse with $t_{\text{pulse}} = 300$ ps and $T_{\text{peak}} = 600$ K (dot-and-dash blue) and 700 K (solid black) under an applied field of -1 T along the z-direction. The brown dotted line shows the time dependence of the temperature pulse.

where A is the amplitude, w is the full width at half maximum, α is the damping parameter and f_0 is the resonant frequency. The resonance frequency can be determined via the Kittel formula [72].

$$f_0 = \frac{\gamma}{2\pi} (B + \mu_0 H_k), \quad (29)$$

where B is the in-plane FMR field amplitude. From this fitting the system's damping parameter and resonant frequency are extracted. Fig. 18 shows the damping and resonant frequency extracted as a function of system temperature. There is very good agreement between the extracted results and the analytical values, providing strong evidence for the ability of MARS to perform temperature dependent FMR simulations.

4. Conclusion

We have developed an open-source multi-timescale micromagnetic code (MARS) for simulating granular thin films. The primary focus of MARS is to enable detailed modelling and simulation of state of the art and future magnetic recording systems covering both the short timescale writing/reading processes and long timescale data storage. The functionality of MARS is provided via the development and inclusion of three micromagnetic solvers: the Landau-Lifshitz-Gilbert (LLG), Landau-Lifshitz-Bloch (LLB) and kinetic Monte Carlo (kMC). Short timescale simulations are possible via the LLG and LLB dynamic solvers. The LLB enables the simulation of systems up to and exceeding their Curie points, which is crucial for recording system such as HAMR. The long timescale simulations are performed via the kMC stochastic solver. The combination of these solvers allows for complex multi-timescale simulations to be developed and performed.

MARS has also been developed for use in material characterisation to aid research into the development and optimisation of recording media materials. The implementation of atomistic parameterisation enables highly accurate material descriptions within MARS and produces very good agreement between results obtained using MARS and those obtained atomistically. Thus MARS is highly useful for bridging the gap between atomistic simulation and real world experimentation. Furthermore to ensure an accurate description of granular media the numerous methods of Voronoi construction have been investigated and compared resulting in the Laguerre-Voronoi method being implemented in order to ensure realistic grain shapes as well as lognormal grain size distributions. Detailed descriptions of the models incorporated in MARS have been provided along with the various methods used to model temperature dependent material parameters.

Finally we have provided example results obtained via MARS for numerous published or on-going studies to show the versatility and capabilities of MARS. These studies cover the entire range of HAMR development starting from materials characterisation and optimisation through to HAMR writing and finally data storage and read back.

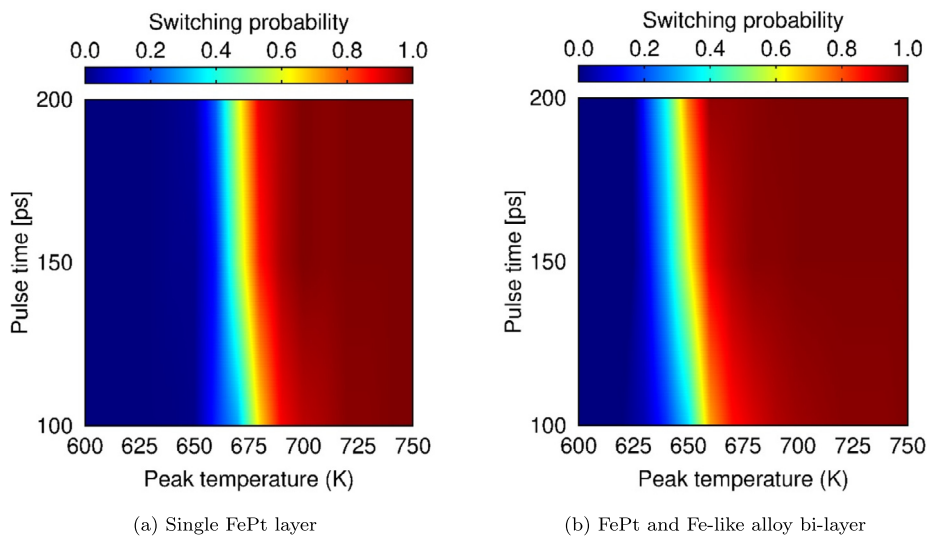


Fig. 16. Switching probability as a function of peak temperature and pulse duration for a single FePt recording medium and an ECC recording medium. The ECC system shows an increased switching probability for both shorter pulse duration and lower peak temperatures compared to the single layer FePt.

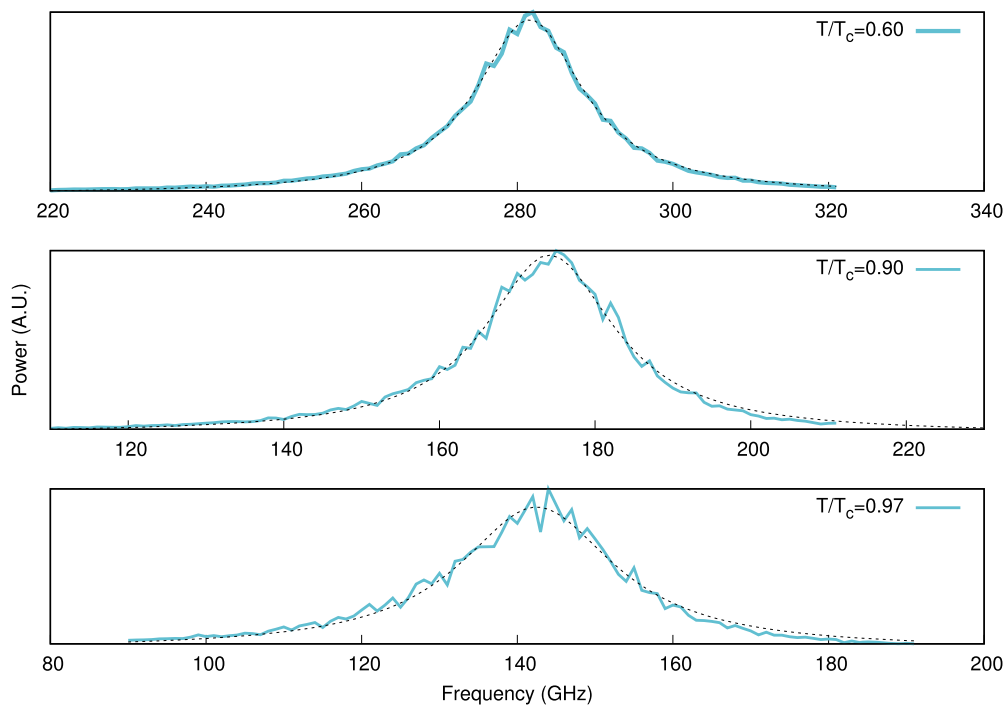


Fig. 17. Frequency swept FMR for FePt at various temperature values. The Power spectra have been fitted via a Lorentzian (dashed) to obtain the system resonant frequency and damping.

Declaration of competing interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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Appendix A. Supplementary material

Supplementary material related to this article can be found online at <https://doi.org/10.1016/j.cpc.2022.108462>.

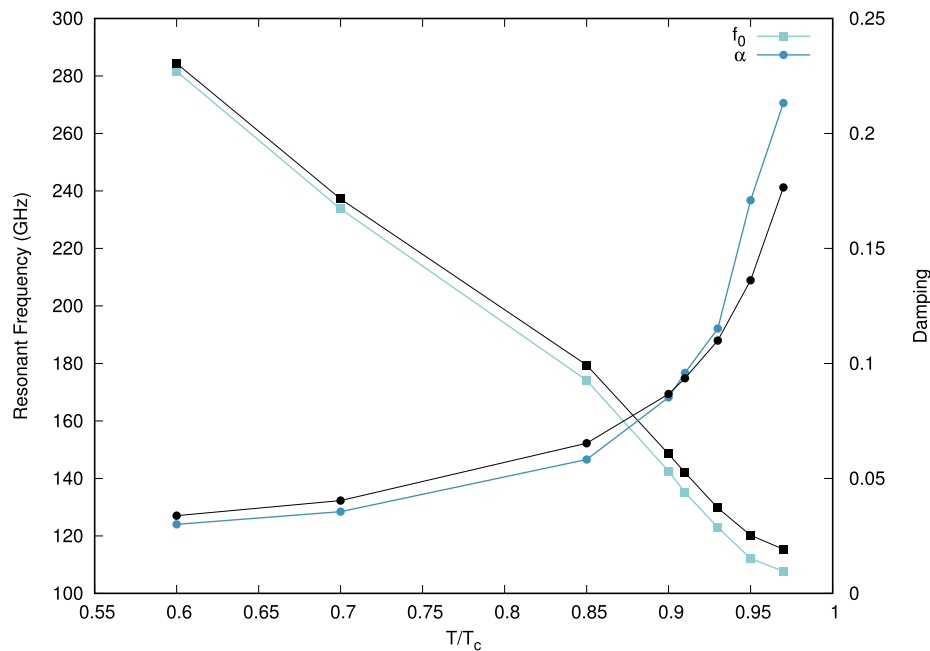


Fig. 18. Damping and resonant frequency as a function of temperature for a micromagnetic FePt system parameterised using 5nm × 5nm × 10nm FePt atomistic simulations compared to the expected analytical values (black lines).

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