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Dhimish, Mahmoud and Alrashidi, Abdullah (2020) Photovoltaic Degradation Rate Affected by Different Weather Conditions:A Case Study Based on PV Systems in the UK and Australia. *Electronics*. 650. ISSN 2079-9292

<https://doi.org/10.3390/electronics9040650>

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1 Article

# 2 Photovoltaic Degradation Rate Affected by Different 3 Weather Conditions: A Case Study Based on PV 4 Systems in the UK and Australia

5 Mahmoud Dhimish <sup>1,\*</sup> and Abdullah Alrashidi <sup>1</sup>

6 <sup>1</sup> Department of Computing and Engineering, University of Huddersfield, Huddersfield HD1 3DH;

7 [m.a.dhimish@hud.ac.uk](mailto:m.a.dhimish@hud.ac.uk)

8 \* Correspondence: [m.a.dhimish@hud.ac.uk](mailto:m.a.dhimish@hud.ac.uk)

9 Received: date; Accepted: date; Published: date

10 **Abstract:** This article presents the analysis of degradation rate over 10 years (2008 to 2017) for six  
11 different photovoltaic (PV) sites located in the United Kingdom (mainly affected by cold weather  
12 conditions) and Australia (PV affected by hot weather conditions). The analysis of the degradation  
13 rate was carried out using the year-on-year (YOY) degradation technique. It was found that the  
14 degradation rate in the UK systems varies from -1.05% and -1.16 %/year. Whereas a higher  
15 degradation ranging from -1.35% to -1.46%/year is observed for the PV systems installed in  
16 Australia. Additionally, it was found that in the Australian PV systems multiple faulty PV bypass  
17 diodes are present due to the rapid change in the ambient temperature and uneven solar irradiance  
18 levels influencing the PV modules. However, in cold weather conditions (such as in the Northern  
19 UK) none of the bypass diodes were damaged over the considered PV exposure period.  
20 Furthermore, the number of PV hot spots have also been observed, where it was found that in the  
21 UK-based PV systems the number of hot spotted PV modules are less than those found in the  
22 Australian systems. Finally, the analysis of the monthly performance ratio (PR) was calculated. It  
23 was found that the mean monthly PR is equal to 88.81% and 86.35% for PV systems installed in the  
24 UK and Australia, respectively.

25 **Keywords:** photovoltaic systems; degradation; hot-spots; performance analysis; performance ratio.  
26

## 27 1. Introduction

28 The ability to precisely predict the output power delivery over the course of time is of vital  
29 importance to the growth of the photovoltaic (PV) industry. Two key cost drivers are the efficiency  
30 with which sunlight is converted into actual energy and how this relationship fluctuates over time.  
31 An accurate quantification of power decay over time, also known as degradation rate [1], is critical  
32 to all stakeholders/utility companies, investors, integrators, and researchers alike.

33 Economically, PV modules degradation rates are equally important, because a higher  
34 degradation rate interprets directly into less output power produced by the system, thus reducing  
35 future cash flows [2]. Inaccuracies in determined degradation rates lead to amplified financial risks  
36 in the PV sector. Technically, degradation mechanisms are important to understand because they  
37 could lead to PV system failures [3]. Typically, a 10% decline is considered a failure, but there is no  
38 compromise on the definition of failure [4], because a high-efficiency module degraded by 50% may  
39 still have a higher efficiency than a non-degraded module from a less efficient technology.

40 The documentation of the degradation mechanisms through modeling and experiments in  
41 principle directly leads to lifetime improvements of PV modules as suggested by S. Kawai *et al.* [5].  
42 Outdoor field testing has played a significant role in measuring long-term lifetime and behavior for

43 at least two reasons: it is the typical functioning environment for PV installations, and it is the only  
44 way to correlate indoor testing apparatuses to outdoor results to forecast field performance.

45 There are various references in the literature that include the degradation rate of PV systems  
46 worldwide. However, there are a lack of references found in the literature describing the behavior  
47 and degradation analysis of an existing PV systems in the United Kingdom and Australia. Therefore,  
48 in this article, the degradation rate of six PV sites installed in three different locations in the UK and  
49 Australia are examined over a period of ten years (2008 to 2017). Before moving to the methodology,  
50 it is indeed important to have an overview of the degradation rate across multiple regions in the  
51 world, which will be summarized as follows:

- 52 • United States of America (USA): The USA is placed on the top five countries leading the PV  
53 technology worldwide [6]. In 1977, the Department of Energy established the Solar Energy  
54 Research Institute in Golden, Colorado. In 1991, it was renamed as the NREL. Outdoor testing  
55 of modules and sub-modules started at the Solar Energy Research Institute in 1982. When  
56 amorphous silicon (a-Si) modules first became commercially available, NREL began to report  
57 degradation rate that were considerably higher than -1.0%/year [7]. In [8] and [9], similar results  
58 of the PV degradation were found in small (<10 kWp) size PV installations, followed by a yearly  
59 degradation rate of approximate -0.8% to -1.25%/year.
- 60 • Europe: The terrestrial focus of PV industry in Europe can be traced to the oil crisis of the 1970s.  
61 The development and institution of PV sites can be divided into publicly and privately funded  
62 projects. The publicly funded portion in Europe can be additionally divided into the umbrella  
63 organization of the Commission of the European Communities and individual national  
64 programs. Never the less, various references indicate that the annual degradation rate in Spain  
65 and Italy is between -0.8% to -1.1%/year [10–12], in Germany between -0.5% to -0.7%/year [13,14],  
66 in Cyprus between -0.8% to -1.1%/year [15], in Greece between -0.9% to -1.13%/year [16], and  
67 finally in Poland is always greater than -0.9%/year [17].
- 68 • Asia: Chandel *et al.* [18] studied the degradation rate in India based on 28 year filed exposes  
69 mono crystalline PV modules, with the degradation rate found to be -1.4 %/year. Similar results  
70 were found by Thotakura *et al.* [19]. In this study, the degradation rate in southern India is  
71 observed at -1.3 %/year. Furthermore, in Thailand, the degradation rate was widely different,  
72 ranging between -0.5% to -4.9%/year [20]. However, C. Dechthummarong *et al.* [21] found that  
73 the degradation rate based on 15 years of PV exposure in northern Thailand is equal to -  
74 1.5%/year. The degradation rate of PV modules in many other countries such as Japan,  
75 Singapore, and Republic of Korea are reported in [22–24], the PV degradation rate is equal to -  
76 1.15%/year in Japan [22], -2.0%/year in Singapore [23], and -1.3%/year in Republic of Korea [24].  
77 It is worth noting that degradation rates in PV modules may differ too between lower and higher  
78 irradiance levels dependent on cause, for example:

- 79 1. Encapsulate browning - may be similar at low and high irradiance levels
- 80 2. Series resistance increase - will be worse at high irradiance conditions
- 81 3. Shunt resistance decrease - will be worse at low irradiance conditions
- 82 4. Random failures such as faulty bypass diodes - will give an even higher variability between PV  
83 installations

84 Worldwide point of view the PV degradation rate various between -0.4% to -2.0%/year.  
85 However, there is not enough evidence based on the annual degradation rate across the UK and  
86 Australia. Therefore, this article tries to fill-in this gap of knowledge by evaluating three different PV  
87 sites located in various locations in the United Kingdom (specifically in Scotland) and Australia. It  
88 was found that the average annual degradation rate of the PV installations varies between -1.05% to  
89 -1.16%/year in the UK, whereas the degradation rate in the PV systems installed in Australia ranges  
90 from -1.35% to -1.46%/year.

91 This paper is organized as follows: Section 2 presents the methodology including the description  
92 of the examined PV systems and the degradation rate analysis technique. In Section 3, the results of  
93 the degradation rate for all examined PV systems are described. Sections 4 and 5 present the overall  
94 discussion and conclusions of the article, respectively.

## 95 2. Methodology

### 96 3.1. Description of the examined PV systems

97 In this work, six different PV installations have been examined. The geographical distribution of  
 98 the PV sites is shown in Figure 1a,b) and summarized as follows: Group 1 – United Kingdom: PV site  
 99 A located in Glasgow; PV site B located in Edinburgh, and PV site C located in Aberdeen. Group 2 -  
 100 Australia: PV site D located in Albury; PV site E located in Sydney and PV site F located in Newcastle.

101 The PV sites have been categorized in two groups; the first group contains PV sites A, B and C  
 102 (located in the UK), whereas the second group consist of PV sites D, E and F (located in Australia). The  
 103 solar irradiance ( $G$ ) and ambient temperature ( $T$ ) play major role on the performance and annual energy  
 104 production for the PV panels. Since the examined PV sites are located in different locations, it is worthy  
 105 to address the locations weather and ambient temperature data.

106 The average values of the solar irradiance in all studied locations between the years 1981 – 2010 is  
 107 taken from [25] and reported in Figure 1a,b. As can be noticed, the irradiance in the UK and the  
 108 Australian sites are relatively equal to 850 kWh/m<sup>2</sup> and 2300 kWh/m<sup>2</sup>, respectively.

109 Additionally, the weighted temperature for all PV sites in the UK is equal to 11.2 °C, while it is  
 110 equal to 21.4 °C for the Australian PV sites. The weighted temperature is calculated using Equation (1)  
 111 [26]:

$$T_{\text{weighted}} = \frac{\sum T_{\text{PV}} \times G}{\sum G} \quad (1)$$

112 where  $T_{\text{weighted}}$  is the weighted temperature of the PV site,  $T_{\text{PV}}$  is the actual temperature measured in the  
 113 PV system in °C, and  $G$  is the solar irradiance affecting the PV system in W/m<sup>2</sup>.

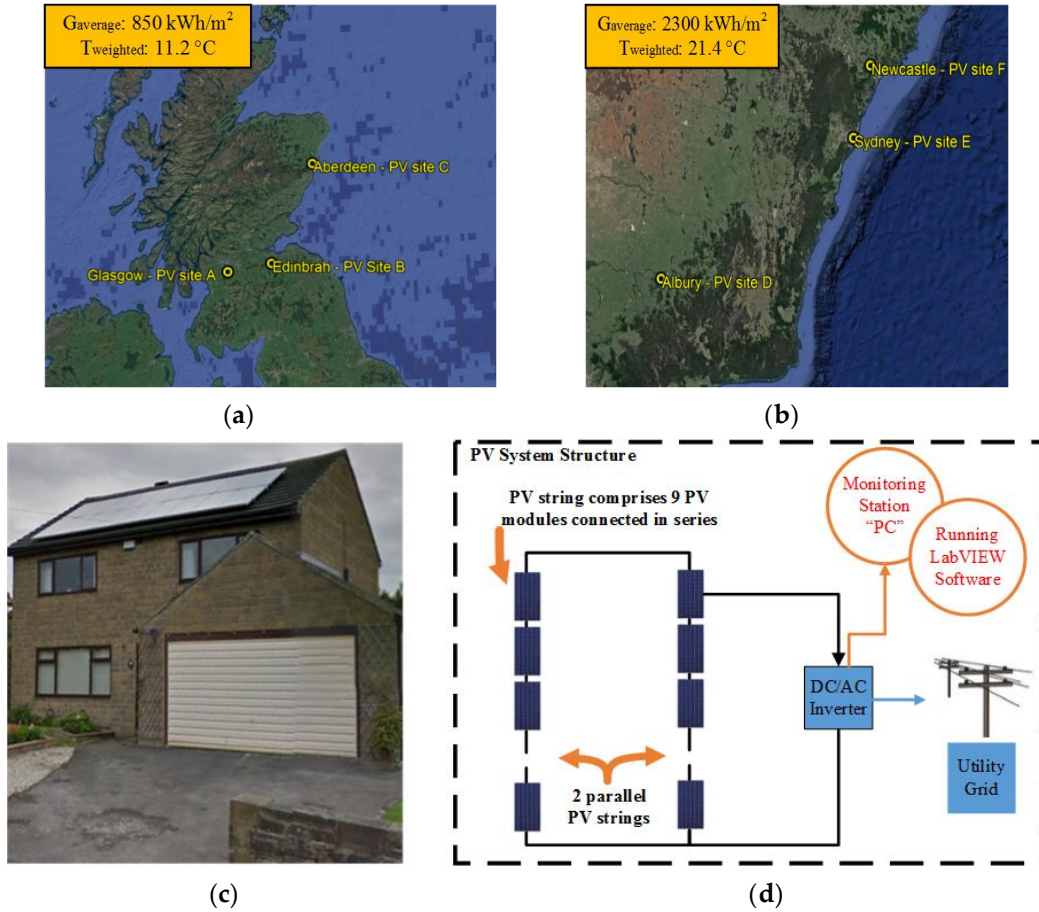
114 Figure 1c presents a real picture of the examined PV system located at Glasgow (PV site A). All  
 115 examined PV systems are residential rooftop systems and have an identical configuration which is  
 116 demonstrated in Figure 1d, as well as identical azimuth (-3° due to South) and tilt angle of (39°). The  
 117 PV installations are comprised of crystalline silicon PV modules with a peak power of 220 W, they are  
 118 configured in 2 PV strings connected in parallel, each comprised 9 PV modules connected in series. All  
 119 have the same PV capacity of 3960 W. The electrical characteristics at standard test conditions (STC)  
 120 including the peak power, voltage and current at maximum power point for the examined PV modules  
 121 are shown in Table 1.

122 Furthermore, all observed PV systems are fitted with an ICONICA maximum power point  
 123 tracking (MPPT) unit. This device has the capability of enhancing the output power during partial  
 124 shading conditions, with the MPPT efficiency ranging from 97.5% to 99.2%. The MPPT unit is  
 125 connected to a hybrid pure sine wave inverter linked to the grid, with the inverter efficiency is ranging  
 126 from 90% to 94%.

127 All examined PV sites have a weather station manufactured by the Davis Company. The weather  
 128 station measures the ambient temperature, wind speed, humidity, and solar irradiation. Onsite  
 129 measurements of DC voltage and current are recorded at the inverter input with a sampling rate of 5  
 130 min, thus the number of samples collected in each year was equal to 52,560 sample. The PV modules  
 131 are fitted in 2008, or at the end of 2007, therefore the comparison between degradation rates of the PV  
 132 sites will be studied starting from 2008 to 2017; 10 years of exposure.

**Table 1.** PV modules electrical parameters.

PV module parameter	Value
PV peak power	220 W
One PV cell peak power	3.6 W
Voltage at maximum power point ( $V_{\text{mpp}}$ )	28.7 V
Current at maximum power point ( $I_{\text{mpp}}$ )	7.67 A
Open Circuit Voltage ( $V_{\text{oc}}$ )	36.74 V
Short Circuit Current ( $I_{\text{sc}}$ )	8.24 A



**Figure 1.** Examined photovoltaic (PV) systems: (a) geographical distribution of the examined PV systems located in the United Kingdom including the average irradiance and weighted temperature over the last 30 years; (b) geographical distribution of the examined PV systems located in the Australia including the average irradiance and weighted temperature over the last 30 years; (c) real picture of the examined PV system installed in Glasgow site PV site A; (d) PV sites configurations, comprising two parallel PV strings each consisting of nine series connected PV modules.

133 3.2. Year-On-Year (YOY) Degradation Analysis Technique

134 In this article, we have used a new model called year-on-year (YOY) developed by the national  
 135 renewable energy laboratory (NREL). The open access software (RdTools) allows us to analyze the  
 136 degradation rate for PV installations [2]. The degradation calculations consist of several steps discussed  
 137 in the following processes:

- 138 • Import data and preliminary calculations: at this step, the time series of the energy yield, PV  
 139 temperature, and solar irradiance will be processed.
- 140 • Normalization: since PV data is randomly distributed, normalization process is required in order  
 141 to transform the data into a normal distribution mode. This step calculated a unitless performance  
 142 ratio (PR) metric with less variability than raw power production data. The PR is typically based  
 143 on the rated power of the PV system, measured PV power, and site irradiance (measured by  
 144 weather station). The normalization is done using the following Equation [27]:

$$PR = \frac{P}{P_{STC, rated} \times \frac{G_{poa}}{G_{ref}} \times (1 + \gamma (T_{PV} - T_{ref}))} \quad (2)$$

145 where P is the measured dc or ac power of the PV systems in watts,  $P_{STC, rated}$  is the rated dc or ac power  
 146 of the PV system in watts,  $G_{poa}$  is the plane-of-array irradiance,  $G_{ref}$  is the reference irradiance 1000  
 147 W/m<sup>2</sup>,  $\gamma$  is the maximum power temperature coefficient in relative %/°C,  $T_{PV}$  is the PV system  
 148 temperature in °C, and  $T_{ref}$  is the PV system reference temperature 25 °C.

- 149 • Data Filtering: PV data filtering is used to exclude data points that represents invalid data, create  
150 bias in the analysis, or introduce significant noise. Often, low irradiance conditions are associated  
151 with night-time data or with errors due to PV components startup such as the MPPT unit. An  
152 example of the data filtering output is shown in Figure 2a.
- 153 • Aggregation: PV data is aggregated with an irradiance and temperature weighted average. This  
154 step reduces the impact of high-error data points in the morning and evening time. The  
155 aggregation time-period was selected at one day period. Therefore, the final yield data has a  
156 resolution of 1 day. Example of output aggregation is shown in Figure 2b.
- 157 • Degradation analysis: the degradation analysis step processes the remaining data to compute a  
158 degradation rate based on year-on-year method. The rate of change is calculated between two  
159 points at the same time in subsequence years. Calculating such a rate of change for all data points  
160 and all years, results in a histogram (as shown in Figure 2c) of rates of change, the central tendency  
161 of which representing the overall system performance.

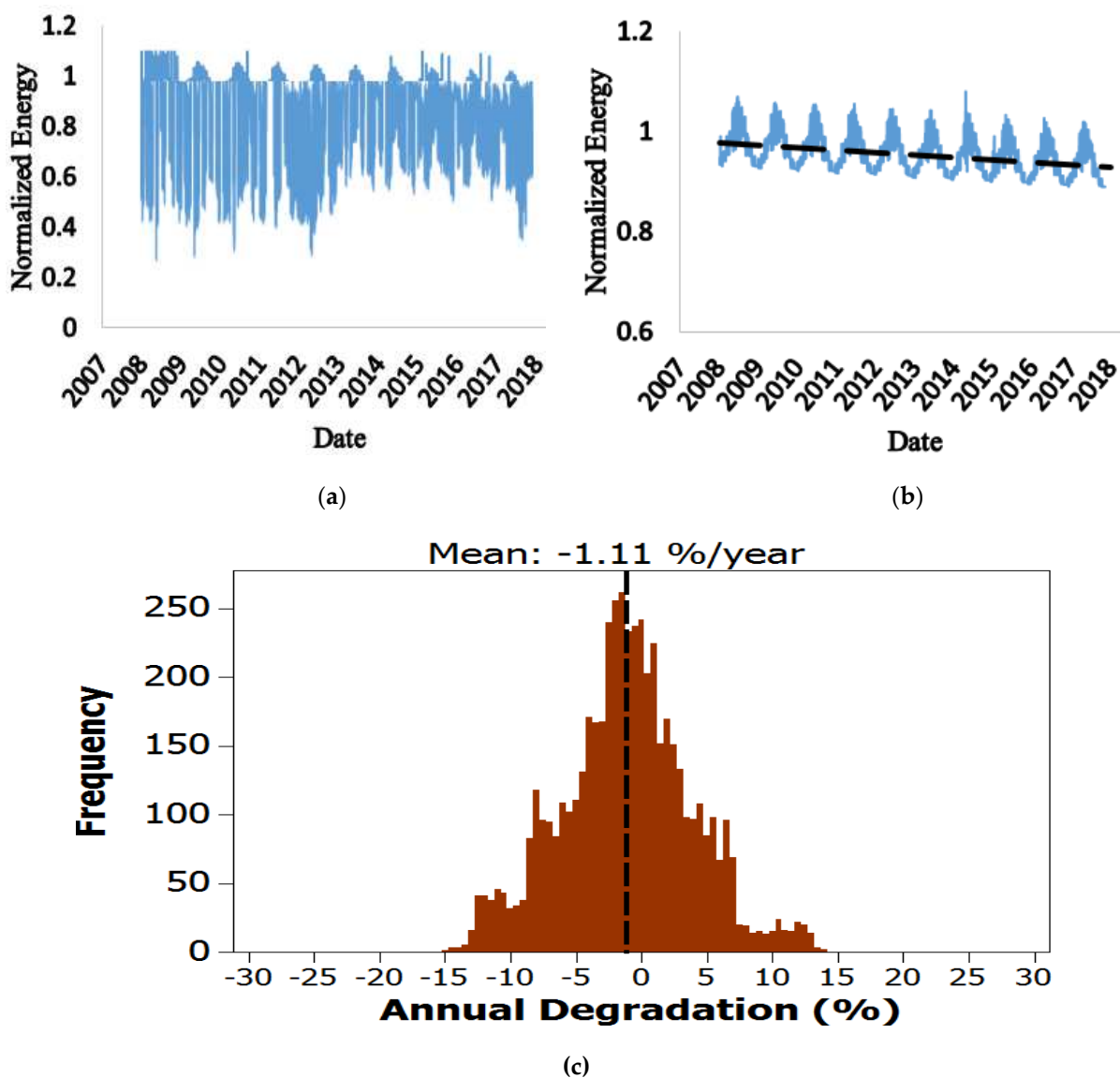


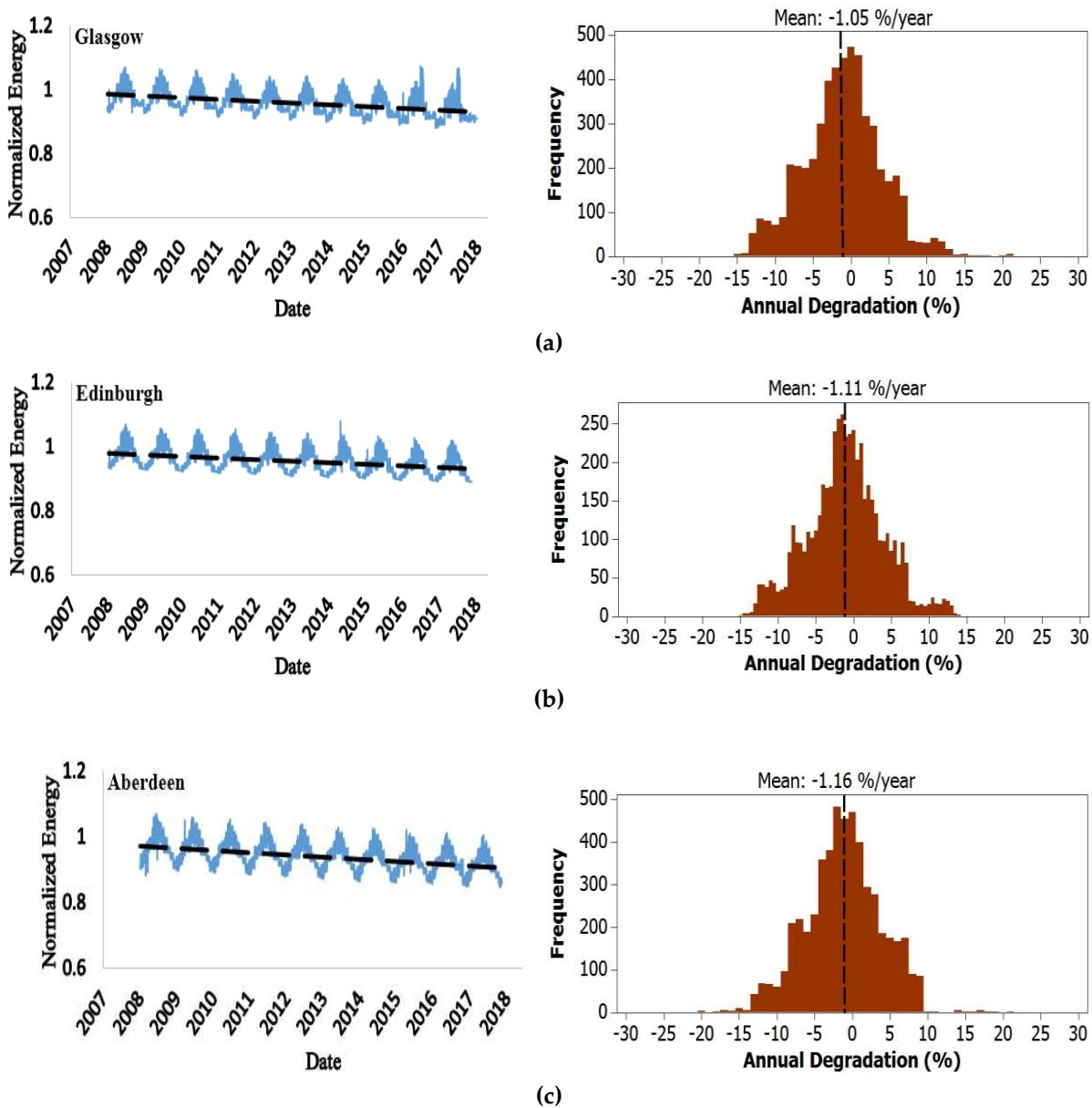
Figure 2. Example of the year-on-year (YOY) degradation process: (a) data filtration; (b) daily aggregation procedure; (c) the result of the degradation rate.



162 **3. Results**

163 *3.1. Degradation rates in the UK PV installations (A, B and C)*

164 The YOY degradation analysis technique was applied to calculate the degradation rate of the  
 165 examined PV systems based on their output dc power. Figure 3a-c shows the normalized output  
 166 energy and the histogram of the degradation rate analysis in sites A, B, and C. Accordingly, in the  
 167 Glasgow PV site, the mean degradation rate over the last 10 year is -1.05%/year. Grater degradation  
 168 mean of -1.11%/year is observed for PV system installed in Edinburgh. Furthermore, the highest  
 169 mean degradation rate is found in Aberdeen at -1.16%/year. Remarkably, this large degradation rate  
 170 in the PV systems is related to the fact that the PV sites (A, B, and C) are in cold areas. The heavy  
 171 snow, rain and high wind speed impact the surface of the PV modules, thus there is a higher risk for  
 172 PV hot spots, micro cracks, and damage in the surface of the PV modules due to hoarfrost, which  
 173 subsequently will increase the degradation rate of the PV modules.



**Figure 3.** Normalized energy and annual degradation of the examined PV systems in the UK: (a) PV site A - Glasgow; (b) PV site B - Edinburgh; (c) PV site C – Aberdeen.

174 Since the PV site C has the highest degradation rate (-1.16%/year) compared to PV site A and B,  
 175 this site has been inspected. Interestingly, a broken glass due to a hoarfrost was found in one of the  
 176 PV modules. In addition, three adjacent PV modules affected by hot spots were identified. Figure 4  
 177 shows the thermography image for the hot-spotted PV modules captured using FLIR E4 thermal  
 178 imaging camera. Fundamentally, hot spots reduce the output power production of the PV modules.  
 179 Thus, it will increase the degradation rate of this PV site.

180 In order to analyze the impact of these hot-spots affecting the PV system performance, we have  
 181 divided the dataset used for the degradation rate analysis into two main parts:

- 182 • First PV array: the PV array consists of 9 healthy PV modules; connected in series; all PV modules  
 183 are not affected by hot-spots, or any other types of faults.
- 184 • Second PV array: the PV array consists of 9 PV modules connected in series, of which three are  
 185 affected by hot-spots.

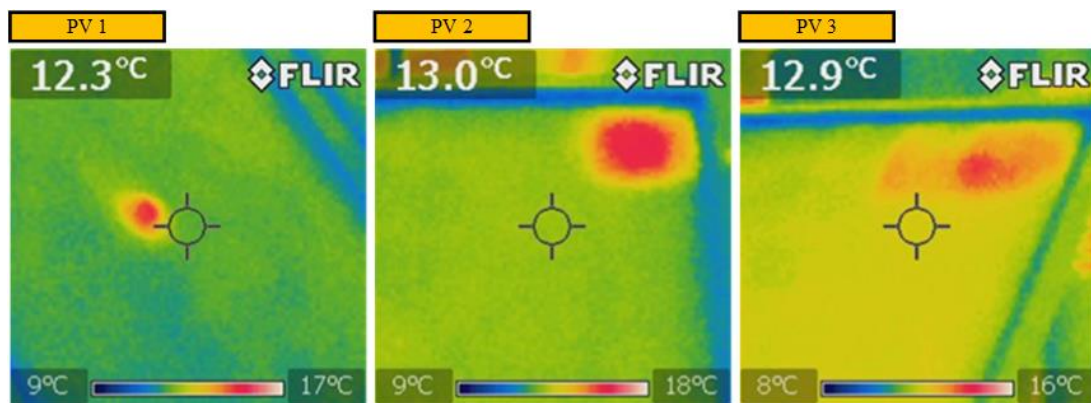


Figure 4. Hot spots captured in three different PV modules in the PV site C (Aberdeen PV site).

186 According to results shown in Figure 5a, the first PV array has an annual degradation rate of -  
 187 0.97%/year. Whereas, in Figure 5b, the PV second PV array affected by three hot-spotted PV modules  
 188 has an annual degradation rate of -1.35%/year. This result proves that Aberdeen site had the lowest  
 189 degradation rate compared to both Glasgow and Edinburg, due to the impact of the hot-spots found  
 190 in several PV modules.

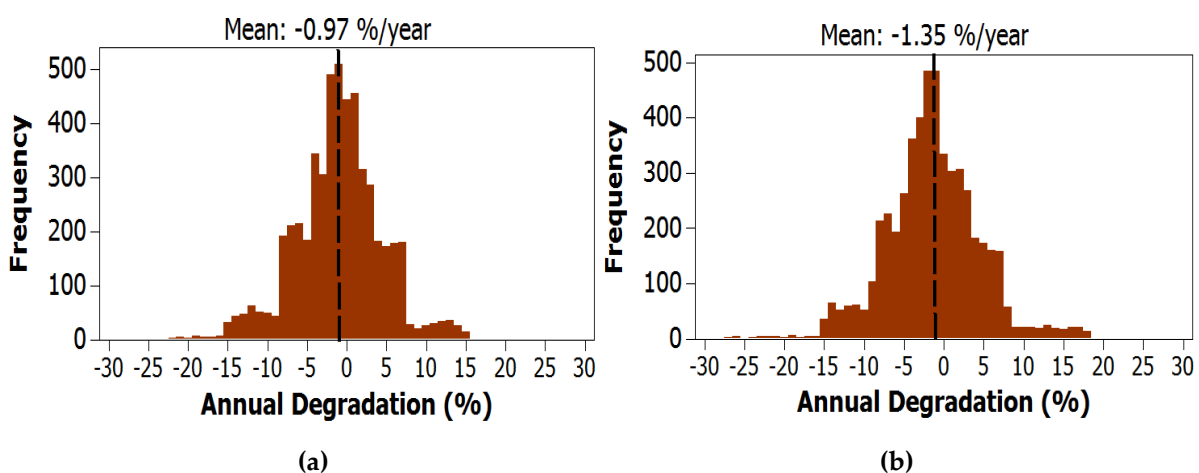


Figure 5. Degradation rate analysis per PV array for PV systems installed in Aberdeen: (a) first PV array annual degradation rate -0.97%/year; (b) second PV array “affected by three hot-spotted PV modules” annual degradation rate of -1.35%/year.



191 3.2. Degradation rates in the Australian PV installations (D, E and F)

192 Similar to the previous section, the analysis of the degradation rate for the Australian sites has  
 193 been conducted with the YOY degradation analysis technique. Figure 6a-c shows the normalized  
 194 output energy and the histogram of the degradation rate analysis in sites D, E, and F. Consequently,  
 195 in Albury PV site, the mean degradation rate over the last 10 year is -1.42%/year. A Lesser  
 196 degradation mean of -1.35%/year is observed for the PV system installed in Sydney. Furthermore, the  
 197 highest mean degradation rate is found in Newcastle at -1.46%/year.

198 Compared to the PV degradation rates obtained in the UK sites which are ranging from -1.05% to  
 199 -1.16%/year, the degradation in the Australian sites are always higher. This is due to various reasons  
 200 including (i) high levels of the ambient temperature affecting the PV modules, and (ii) the solar  
 201 irradiation affecting the PV modules is much higher than the UK-based PV systems. Interestingly, this  
 202 increase in the ambient and irradiance levels influence the PV modules by the following:

- 203 • PV modules bypass diodes failure: from the examined PV sites in Australia, it was found that  
 204 several PV modules had a faulty bypass diode. Two examples are shown in Figure 7a,b A faulty

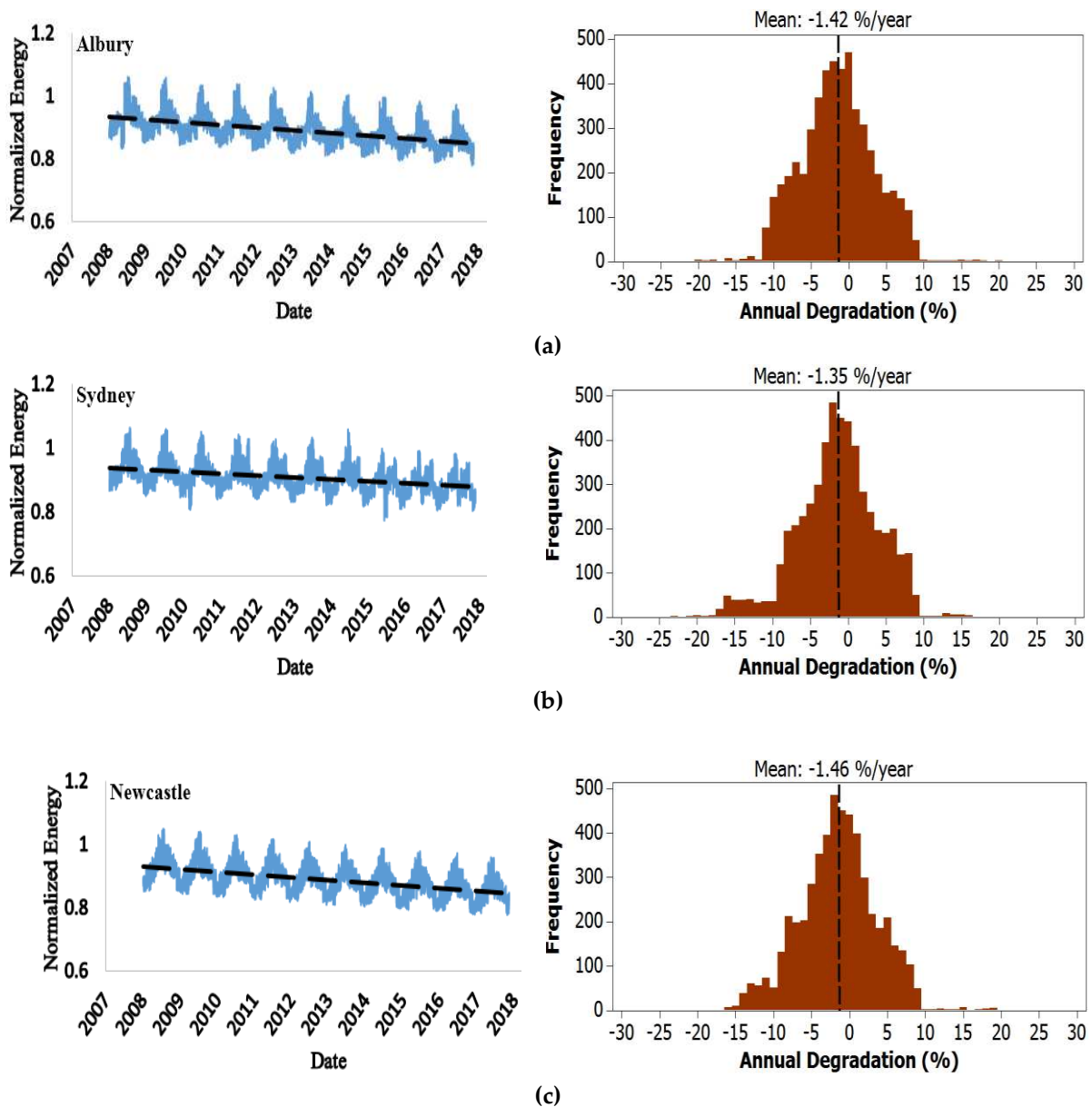
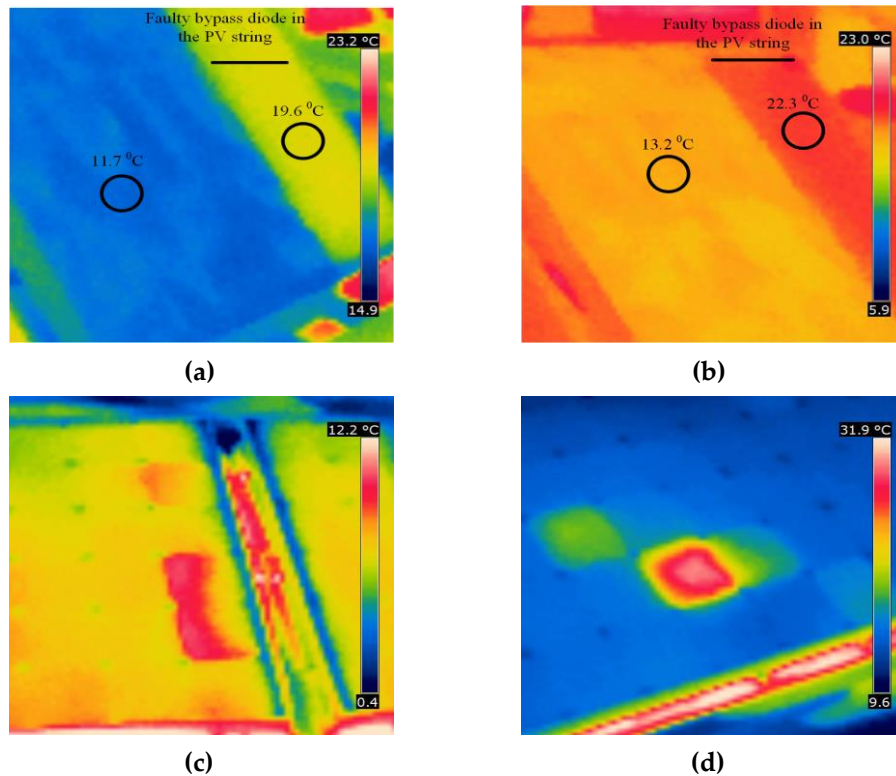


Figure 6. Normalized energy and annual degradation of the examined PV systems in Australia: (a) PV site D - Albury; (b) PV site E - Sydney; (c) PV site F – Newcastle.

205 bypass diode is found in a PV string, resulting an increase in the PV string temperature. In Figure  
 206 7a, the PV string has 7.9 °C increase in the temperature, whereas the PV string in Figure 7b has  
 207 9.1 °C increase in the PV string temperature due to the bypass diodes failure.

- 208 • Hot spots: as similar to the hot spots found in the PV site C (Aberdeen, UK) shown previously  
 209 in Figure 4b
- 210 • , after inspecting the PV site F (Newcastle, Australia), it was found that six PV modules were  
 211 affected by hot spots. Figures. 7c,d show two different PV modules affected by hot spots.

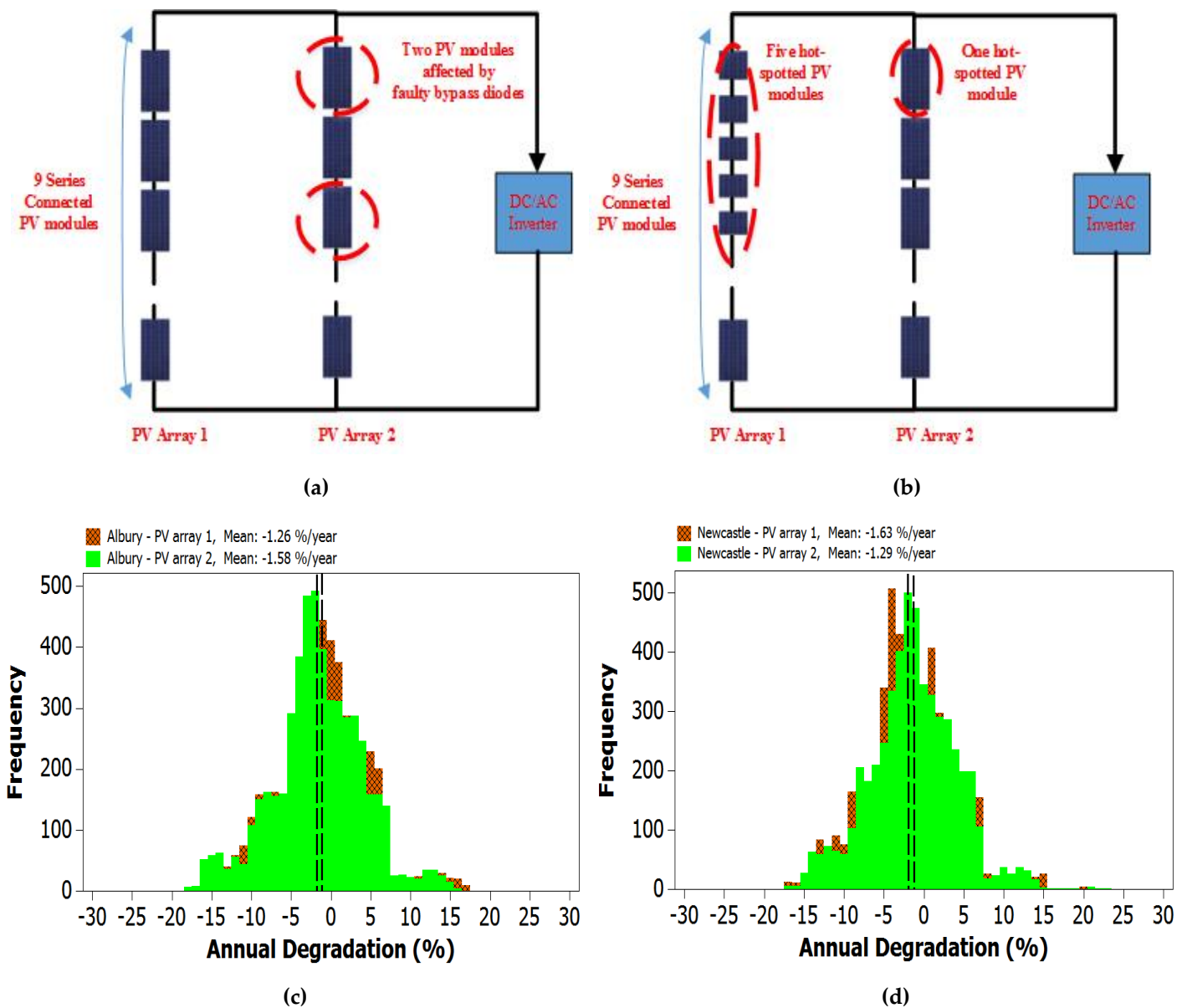
212 In order to visualize the impact of the failure in the bypass diodes, as well as the hot-spots in the  
 213 Australian PV sites, we have carried out the analysis of the sub-array of the affected PV installations.  
 214 Figure 8a shows the sub-array of the PV installation located in Albury, where two PV modules



**Figure 7.** Impact of high ambient temperature and solar radiation on the examined PV sites in Australia, images were taken using FLIR E4 thermal imaging camera: (a) faulty bypass diode in a PV string increasing the temperature of the PV string by 7.9 °C; (b) faulty bypass diode in a PV string increasing the temperature of the PV string by 9.1 °C; (c) PV hot spots found in a PV module in site F (Newcastle, Australia); (d) more PV hot spots found in a different PV modules in PV site F.

215 affected by faulty bypass diodes is observed in the PV array 2. According to Figure 8b, the Newcastle  
 216 PV system has five hot-spotted PV modules in the first PV array, while the second PV array is only  
 217 affected by one hot-spotted PV module.

218 Results shown in Figure 8c-d) present the annual degradation rate for the sub-array in both  
 219 Albury and Newcastle PV systems. According to Figure 8c, Albury PV site, the first PV array has an  
 220 annual degradation rate of -1.26%/year. Whereas, the PV second PV array affected by faulty bypass  
 221 diodes in two different PV modules has an annual degradation rate of -1.58%/year, resulting in a  
 222 higher annual degradation due to the existence of the faulty bypass diodes. Similarly, Figure 8d  
 223 shows the annual degradation rate in PV array 1 and 2 for PV systems located in Newcastle, Australia.  
 224 The First PV array has high annual degradation of -1.63%/year affected by various hot-spots.  
 225 However, less annual degradation is obtained for the second PV array of -1.29 %/year, while this PV  
 226 array is only affected by one hot-spotted PV module.



**Figure 8.** Analysis of the hot-spots and annual degradation rate in the Australian PV installations: (a) Two PV modules affected by faulty bypass diodes in the second PV array – found in Albury PV system; (b) PV array 1 is affected by five hot-spotted PV modules, while PV array 2 is affected by one hot-spotted PV module – found in Newcastle PV system; (c) Albury PV site annual degradation rate; (d) Newcastle PV site annual degradation rate.

227 **4. Discussion**

228 In this article, the degradation rate for two different PV sites were investigated. The first PV sites  
 229 are in the UK (affected by cold weather conditions), whereas the second PV sites are in Australia  
 230 (affected by hot weather conditions). From the findings discussed in above sections, this article claims  
 231 the following:

- 232 • In cold weather conditions the PV degradation rate is less than the degradation rate of PV  
 233 modules affected by hot weather conditions. Based on the analysis of three different PV sites, it  
 234 was found that PV degradation rate in the UK is between -1.05% to -1.16%/year, whereas the PV  
 235 degradation rate in Australia ranging from -1.35% to -1.46%/year.
- 236 • In cold weather conditions, there is high risk for glass broke due to hoarfrost, in addition, heavy  
 237 snow is expected to impact the PV modules by various hot spots, which will reduce the output  
 238 power generation of the PV modules.

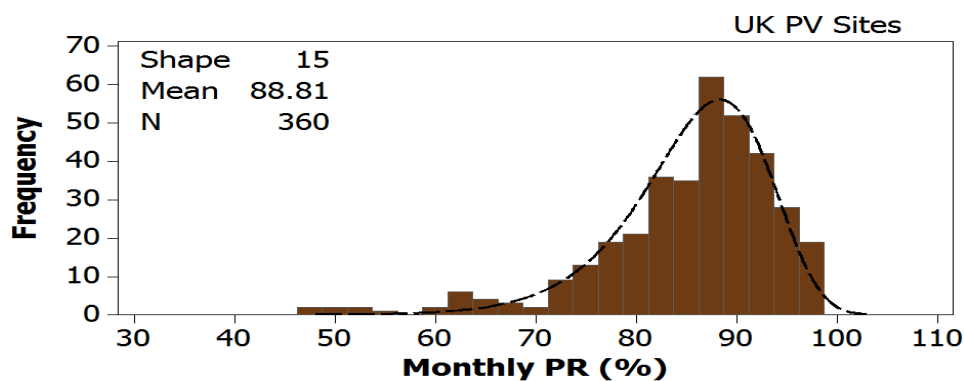
- 239 • In hot weather conditions, it was found that faulty PV bypass diodes are expected to occur due to
- 240 the high range of ambient temperature and uneven temperature and irradiance profiles affecting
- 241 the PV modules. However, in cold weather conditions, none of the bypass diodes were damaged
- 242 over the considered period; 10 years of operation.
- 243 • The number of PV hot spots found in UK PV sites are less than the number of hot spots found in
- 244 the Australasian PV sites.
- 245 • The observed failure of the bypass diodes in the Australian PV systems are a result of the sudden
- 246 drop in the output power of one of the three PV modules cell strings, this will activate the bypass
- 247 diode in the shaded PV string, while other bypass diodes in the un-shaded strings remains
- 248 switched-off. The repeated alternation in the switching (off/on) for the bypass diodes resulting in
- 249 a possible failure. This is also the case in many investigated studies such as [28]-[30].

250 The analysis of the monthly performance ratio for all examined PV sites in the UK and Australia  
 251 have been compared. A total number of 120 samples/site; resulting a total of 360 for all examined PV  
 252 sites in the UK as well as in Australia.

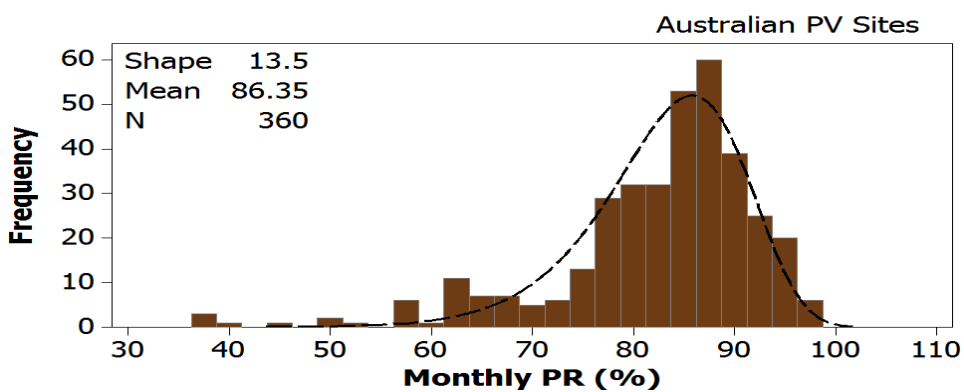
253 The performance ratio (PR) is a widely used metric for comparing relative performance of PV  
 254 installations whose design, technology, capacity, and location differ [31] and [32]. The PR is calculated  
 255 using Equation (3).

$$PR = \frac{Y_f}{Y_r} = \frac{E_{PV} \setminus P_{STC}}{GTI \setminus G_{STC}} \quad (3)$$

256 where  $Y_f$  is the final yield energy of the PV systems, while  $Y_r$  is the reference yield energy.  $E_{PV}$  is the  
 257 total energy produced by the PV system during a given period of time,  $P_{STC}$  is the rated power of the  
 258 PV system under STCs,  $GTI$  is the global solar irradiance received by the PV system, and  $G_{STC}$  is the  
 259 global solar irradiance under STC of 1000 W/m<sup>2</sup>. We have analyzed the monthly PR for all systems over  
 260 a period of 10 years. The monthly integrated PR obtained for the PV sites in the UK and Australia is  
 261 shown in Figure 9.



(a)



(b)

Figure 9. Monthly performance ratio analysis for all examined PV systems for a period of 10 years: (a) UK PV sites; (b) Australian PV sites.

262 The distribution does not follow a normal (or Gaussian) distribution, because an important fraction  
263 of the PV systems shows an overall performance lower than average, and others are clearly subject to  
264 faults, which skews the distributions towards the low PR values. The distribution is better explained  
265 with a Weibull distribution [33], which often arises when the range of variation of a population is  
266 physically limited at one extremity, but not at the other.

267 According to Figure 9a,b, the obtained mean monthly PR is equal to 88.81% and 86.35% for PV  
268 systems installed in the UK and Australia, respectively. Therefore, PV systems in the UK have an  
269 increase in the monthly PR of 2.46% compared to those installed in Australia. Interestingly, this result  
270 verifies that the PV annual degradation rate in the UK is lower than Australia, which was found in the  
271 previous section.

## 272 5. Conclusion

273 This article presents the analysis of degradation rate over 10 years (2008 to 2017) for six different  
274 PV sites located in the UK (mainly affected by cold weather conditions) and Australia (PV affected by  
275 hot weather conditions). The analysis of the degradation rate was carried out using the year-on-year  
276 (YOY) degradation technique. It was found that the degradation rate in the UK sites varies from -1.05%  
277 and -1.16%/year. Whereas a higher degradation ranging from -1.35% to -1.46%/year is observed for the  
278 PV sites installed in Australia.

279 Additionally, it was found that in the Australian PV installations, multiple faulty PV bypass diodes  
280 are present due to the rapid change in the ambient temperature and uneven solar irradiance levels  
281 influencing the PV modules. However, in cold weather conditions (such as northern UK), none of the  
282 bypass diodes were damaged over the considered PV exposure period. Furthermore, the number of PV  
283 hot spots have been also observed. It was found that in the UK-based PV sites the number of hot spotted  
284 PV modules are less than those found in the Australian PV systems.

285 On the other hand, the analysis of the monthly performance ratio was calculated in both observed  
286 counties. Remarkably, it was found that the mean monthly PR is equal to 88.81% and 86.35% for PV  
287 systems installed in the UK and Australia, respectively. This result verifies that the PV annual  
288 degradation rate in the UK is lower than Australia.

289  
290 **Author contributions:** Conceptualization M.D. and A. A.; methodology M.D. and A.A; software A.A.;  
291 validation M.D. and A.A; formal analysis A.A.; resources M.D.; data curation M.D.; writing-original  
292 draft preparation M.D.; writing-review and editing A.A.; supervision M.D. All authors have read and  
293 agreed to the published version of the manuscript.

294  
295 **Funding:** This research received no external funding.

296  
297 **Conflicts of Interest:** The authors declare no conflict of interest.

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