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1	Coring and Compaction: Best Practice in Blue Carbon Stock and					
2	<b>Burial Estimations</b>					
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11	Abstract					
12	A comparison of gouge and hammer coring techniques in intertidal wetland soils highlights a					
13	significant effect of soil compaction of up to 28% associated with the widely applied hammer					
14	coring method employed in Blue Carbon research. Hammer coring reduces the thickness of the					
15	soil profile and increases the dry bulk density, which results in an overestimation of the soil					
16	OC stock of up to 22%. In saltmarshes with multiple different soil units, we show that hammer					
17	coring is unsuitable for the calculation of OC stocks and should be avoided in favour of Russian					
18	or gouge cores. Compaction changes both soil dry bulk density and porosity and we show that					
19	resultant radiometric chronologies are compromised, almost doubling mass accumulation rates.					
20	While we show that the OC (%) content of these sediments is largely unchanged by coring					
21	method, the implication for OC burial rates are profound because of the significant effect of					
22	hammer coring on soil mass accumulation rates.					

# 23 Highlights

24	• Hammer coring causes soil compaction of up to 28% in saltmarsh soils.
25	• Hammer coring is unsuitable for the calculation of OC stocks in saltmarsh soils.
26	• Compaction due to hammer coring almost doubles calculated mass accumulation
27	rates.
28	• Hammer coring artificially elevates calculated OC burial rates.
29	
30	Keywords: Sediment, Coring; Compaction, Carbon; Intertidal; Saltmarsh;
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#### 44 **1. Introduction**

Carbon (C) buried and stored in costal ecosystems (saltmarsh, seagrass and mangroves) is 45 known as blue carbon (Nellemann et al., 2009). In the last decade blue carbon habitats have 46 47 risen in prominence and are increasingly recognised as potentially valuable nature-based solutions to help reduce atmospheric CO<sub>2</sub> and mitigate climate change (Duarte et al., 2013, 48 Mcleod et al., 2011, Pendelton et al., 2012, Rogers et al., 2019). Underpinning this 49 understanding is a wealth of research largely focused on calculating both the quantity of 50 organic carbon (OC) stored and the rate at which this OC is buried in coastal ecosystems. The 51 52 foundation of these estimates is the collection and measurement of soil samples, normally through sediment coring. Across the body of published blue carbon research different coring 53 approaches are adopted, generally falling into two categories: (i) palaeo-environmental 54 55 methods which often employ Russian and gouge corers (Frew, 2014; Glew et al., 2002), and (ii) low cost, often disposable hammer/impact/piston techniques, where plastic piping is 56 hammered into the soil (e.g. Howard et al., 2014). 57

Russian and gouge corers have long histories of use across a variety of applications including 58 peatland research, sea-level reconstructions, as well as blue carbon research (van Ardenne et 59 60 al, 2018, Wollenberg et al., 2018). The low-cost hammer approach is almost exclusively used for blue carbon research, but generally not used in palaeo-environmental research. Initially, the 61 hammer coring technique was used to sample seagrass soils; these soils are often submerged 62 and sandy in nature making them difficult to core using other sampling methods (Macreadie et 63 al., 2015, Serrano et al., 2018). However, in recent years the use of this approach has also been 64 gaining popularity in saltmarsh and mangrove ecosystems (Kelleway et al., 2016a, Macreadie 65 et al., 2013, Unger et al., 2016). 66

67 Gouge coring is minimally invasive and causes little disturbance to the soil; it largely avoids compacting the soil, where soil compaction is more widely recognised as a significant problem 68 in achieving successful paleo-environmental reconstructions (Brain, 2016, Brain et al., 2017, 69 70 Edwards, 2006). Within blue carbon research, a number of studies acknowledge that hammer coring causes compaction (Ewers Lewis et al., 2019, Kelleway et al., 2016a, b) but this 71 72 recognition is not universal. Where compaction is recognized during the coring procedure, a simple linear correction, where the length of the soil core is divided by the sampling depth is 73 often applied (Ewers Lewis et al., 2019, Kelleway et al., 2016a, b). Compaction of the soils 74 75 increases the bulk density, decreases the porosity and dewaters the soil (Archer and Smith, 1972, Håkansson and Lipiec, 2000). Additionally, the loss of water may potentially flush 76 77 soluble and porewater OC from the soil, all of which will have a bearing on the OC stock and 78 burial estimates; it is therefore unlikely that simple linear corrections address this complexity.

The widespread use of these different coring methods in saltmarshes raise questions about their direct impact on any subsequent calculation of OC stock and burial rate. In this study, we explore two of the most commonly employed coring techniques (gouge and hammer) to determine how each method influences the recovered soil (i.e. physical properties, compaction) and how, in turn, this alters the OC stock and burial estimates in a temperate saltmarsh.

# 84 2. Study Site

The Kyle of Tongue saltmarsh is one of the most northerly marshes found on the UK mainland (Fig.1). The marsh is situated at the head of the Kyle of Tongue (an infilled fjord), and as such is categorised as a loch-head marsh; a classification unique to Scotland in a UK context (Haynes, 2016). The marsh occupies an area of 9.31 ha with the majority of that being highmid marsh (9.08 ha) with only 0.23 ha considered low marsh (Fig.1) as characterised by vegetation communities and elevation (Haynes, 2016). The vegetation coverage of the marsh 91 is dominated by *Carex flacca, Filipendulo-Iridetum pseudacori, Puccinellia-turf fucoid* and
92 stunted forms of *Phragmites australis*. As with the loch-head marsh type, this vegetation
93 community is only found on the marshes of western and northern Scotland (Adam, 1978, Burd,
94 1989, Haynes, 2016).



#### 95

Figure.1 Location map detailing (a) the site in context of Scotland and (b) Ordnance Survey Map
detailing the location of the saltmarsh in relation to the Kyle of Tongue with the high (orange) and low
marsh (purple) highlighted (Haynes, 2016). (c) A regional overview. (d) Sampling locations across the
marsh environments (© Crown copyright and database rights [2019] Ordnance Survey (100025252).

100 **3. Methods** 

# 101 **3.1 Coring**

Dual coring (gouge and hammer) was undertaken at four sites on the Kyle of Tongue saltmarsh in November 2018. Three of the core sites were situated along a transect perpendicular to the shoreline, while a fourth site was located on a protruding raised platform to the west of the saltmarsh (Fig.1d). Gouge and hammer cores were collected at each site; the gouge cores were collected first to ensure minimal disturbance of the soils prior to collection of the hammer cores.

107 The gouge cores were collected using a 1m fixed length core barrel with a 3 cm diameter. The corer was manually pushed into the soil to the point of refusal, rotated and removed. Before 108 removal, the degree of compaction was assessed by measuring the soil surface within the core 109 110 tube relative to the height of the outer marsh surface; the difference between the measurements was used to calculate compaction (Kelleway et al., 2016b). On site, the core face was cleaned 111 with a sharp knife, photographed and the soil profile described using the Tröels-Smith, (1955) 112 classification scheme for unconsolidated sediments. Once described, fixed volume (4 cm<sup>3</sup>) 113 samples were collected every 10 cm along the length of the core. The location and elevation of 114 115 the core was recorded using DGPS.

Adjacent hammer cores were collected 25 cm from the gouge core locations; each new location 116 was recorded with DGPS. The core tube consisted of 150 cm lengths of polyvinyl chloride 117 118 (PVC) piping with a 6.16 cm inner-diameter and a wall thickness of 0.24 cm. The PVC pipe was enhanced with a sharpened bevelled edge to allow more efficient cutting of root material 119 during the insertion of the core tube into the soil. Core tubes were manually hammered into the 120 soil to a depth of 100 cm below the external soil surface. The top of the core was sealed to 121 create a vacuum and the core was pulled out of the soil using a tractor jack. Total compaction 122 123 was measured in the field by comparing the external and internal elevation of the marsh surface recorded from outside and inside the core tube. The top end of the core was plugged with foam, 124 125 while both ends were capped and sealed with tape to prevent disturbance during transport. 126 Cores were stored at 4°C in a cold room at the University of St Andrews until processing.

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- 3.2 Laboratory Analysis
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# **3.2.1 Physical Properties**

The hammer cores were cut lengthways and split into working and archive sections; the soils
were described using the Tröels-Smith (1955) classification scheme. The distance between the

core top within the liner was compared to the ground level marked on the linear in the field allowing the total compaction of the core to be determined and assure no additional compaction or expansion has taken place post collection. Fixed volumetric samples (4 cm<sup>3</sup>) were extracted at 10 cm intervals throughout the length of the core using a fixed volume sampler (syringe).

Sub-samples from both the gouge and hammer cores were weighed before and after drying at
50°C for 48 hrs. This data allowed wet bulk density (WBD), dry bulk density (DBD), porosity
and water content to be calculated following the standard methodologies (Athy, 1930, Appleby
and Oldfield, 1978, Dadey et al., 1992):

140 Wet Bulk Density 
$$(g \ cm^{-3}) = \frac{Wet \ Mass \ (g)}{Wet \ Sample \ Volume \ (cm^3)}$$
 (1)

141 
$$Dry Bulk Density (g \ cm^{-3}) = \frac{Dry \ Mass \ (g)}{Wet \ Sample \ Volume \ (cm^3)}$$
 (2)

142 
$$Water Content (\%) = \frac{Wet Mass (g) - Dry Mass(g)}{Wet Mass (g)} \times 100$$
(3)

143 
$$Porosity(\%) = \frac{Mass of Water in the Soil(g)}{Mass of Water in the Soil(g) + \left(\frac{Dry Mass(g)}{Dry Bulk Density(g cm^{-3})}\right)}$$
(4)

144 The degree of compaction of the soils collected by hammer coring was determined by 145 comparing the thickness of discrete soil horizons observed in the adjacent gouge cores.

146

#### 3.2.2 Elemental Analysis

Elemental analysis (EA) was used to quantify the OC content of the saltmarsh soils. The oven 147 148 dried samples were milled to a powder, and a 10 mg sub-sample was placed in a silver capsule. The soils within the silver capsules were treated with HCl through acid fumigation to remove 149 carbonate (Harris et al., 2001) and, after drying (24 hrs at 50°C), the samples were analysed 150 using an Elementar EL Vario following the methodology of Verardo et al. (1990). Analytical 151 precision was estimated from repeat analyses (n=18) of standard reference material B2178 152 (Medium Organic Content Standard; Elemental Microanalysis, UK); the analytical precision 153 for the OC measurements was  $\pm 0.09$  %. 154

#### 3.2.3 Assessing OC stocks and burial rates

To test the potential impacts of compaction associated with hammer coring on soil mass and 156 OC stock estimations; we undertook a simple test, where we calculated both soil mass (kg) and 157 OC stock (kg) for an area of  $1 \text{ m}^2$  using the thickness (m) of the different soil horizons 158 associated with each coring method. The saltmarsh soil mass and OC stocks were calculated 159 down to the depth were the basal silts are introduced in the stratigraphy (Fig.2) as these 160 represent the switch from saltmarsh to intertidal mudflat habitat which is currently not 161 considered a blue carbon environment (Nellemann, et al., 2009). The test assumed that each 162 core was representative of the surrounding  $1 \text{ m}^2$  of saltmarsh soil. Using the data collected from 163 the cores the mass of soil and the OC stock for the soil underlying the  $1 m^2$  was estimated. 164 These estimates were made following the standard methodology: 165

166

167 Soil Volume 
$$(m^3) = Area (m^2) \times Soil Unit Thickness (m)$$
 (5)

168 Soil Mass 
$$(kg) = Soil Volume (m^3) \times Dry Bulk Density (kg m^{-3})$$
 (6)

169 
$$OC Stock (kg) = Soil Mass (kg) \times OC Content (\%)$$
 (7)

170

This approach was used with the stratigraphic data collected from both the hammer and gouge cores, enabling the soil mass and OC stock estimates to be compared in order to assess any effect of coring-related compaction on the soils.

Sedimentation and mass accumulation rates of saltmarsh soils are commonly calculated using radiometric age control (<sup>210</sup>Pb and <sup>137</sup>Cs) (Krishnaswamy et al., 1971, Appleby and Oldfield, 1978). Dry bulk density and porosity are key to these calculations. In order to test the effect of soil compaction on calculated sedimentation and mass accumulation rates, we have used a previously published (Barlow et al., 2014) radiometric age model from a core collected using a wide dimeter gouge corer from the same location as core KT-18-03. The new DBD and porosity data from the gouge and hammer cores collected at site KT-18-03 were used, together
with the original radiometric age control data, to recalculate the most common age-depth
methods: simple linear interpolation, the constant rate of supply (CRS) model (Appleby and
Oldfield, 1978) and the constant initial concentration (CIC) model (Robbins and Edgington
1875).

- 185 **4. Results and Interpretation**
- 186

#### 4.1 Saltmarsh Soil Profiles

187 The soil profiles of the Kyle of Tongue saltmarsh have four main units, with a fibrous peat (Turfa herbacea) surficial layer overlying humified peat (Substantia humosa) and organic rich 188 silt, which sits upon a basal layer of marine mud (Fig.2), (and further summarised in Barlow et 189 190 al, 2014). Core KT18-05, the more seaward core of the main transect, however, differs from the others in that it lacks the surficial fibrous peat layer and has a thin layer of humified peat 191 capping the underlying silts. In places, iron (Fe) staining is observed in the silt layer, indicating 192 the presence of Fe oxides, most likely a consequence of increased oxygen penetration into the 193 soil layer (Luther III et al., 1992, Kostka, and Luther III, 1994) at this site. The soil units 194 themselves differ significantly in thickness between coring sites, with the fibrous peat ranging 195 from 4-9 cm, the humified peat ranging from 120-310 cm and the organic rich silts ranging 196 from 70-350 cm (Fig.2). The hammer core generally penetrated further into the basal silty mud 197 198 than the gouge core.





Figure 2. Comparison of the effects of the coring method on the soil profiles, OC content and
dry bulk density across the four sites. The grey lines represent the difference in cumulative
depth (cm) of the soil horizons in each core as described by the Tröels-Smith classification
scheme (1955). The thickness of the different soil units can be found in the supplementary table
204

#### 4.2 Compaction

By comparing the soil profiles obtained from the hammer cores (both in the field and the 209 laboratory) to those recorded from the gouge cores, where compaction observed in the field 210 211 was minimal (< 2 %), it is estimated that the soils from the hammer cores were compacted by between 22.9% and 27.8% (Fig.3). The laboratory-based compaction calculations compare 212 favourably to the field-measurements, confirming that the field-based estimates of total depth 213 compaction are robust (Fig.3). KT18-02 and 03 are the only cores where the field 214 measurements are exceeded by the laboratory-based estimates of compaction. This is 215 216 potentially due to the stretching (a piston effect) of certain soil horizons during extraction. For example, it was observed upon extraction of core KT18-03 that the degree of overall 217 compaction had reduced from the *in situ* measurements in the field. Indeed, when the soil 218 219 profile is examined in greater detail, the equivalent silt unit in the hammer core is thicker than that in the adjacent gouge core, further suggesting that stretching of the soil profile has taken 220 place whilst extracting the material from the ground (Fig.3). 221



Figure 3. Comparison of field- and laboratory-based measurements of total soil compaction
(%) in the four hammer cores.

These measurements are useful to quantify the total amount of compaction which has occurred during the coring process, but they don't provide the required insight into the degree of compaction of the individual soil units. However, by comparing the adjacent soil profiles recovered from the two coring techniques, the level of compaction for each of the soil units can be calculated (Table 1).

		Mean Dry BulkMean WaterDensity (g cm <sup>-3</sup> )Content (%)		Porosity (%)		Compaction (%)		
Site	Soil Unit	Gouge	Hammer	Gouge	Hammer	Gouge	Hammer	Hammer
KT18-02	Peat	0.39	0.36	70.09	25.14	51.69	45.67	53.85
	Humified Peat	0.45	0.67	58.90	36.11	53.94	41.68	21.4
	Silt with Organics	0.70	0.62	45.25	42.01	45.93	36.96	25
KT18-03	Peat	0.23	0.27	81.36	23.86	46.09	44.46	63.64
	Humified Peat	0.24	0.39	71.83	30.76	46.89	38.01	20.51
	Silt with Organics	0.40	0.90	58.76	49.94	46.13	39.51	-19.23
KT18-05	Humified Peat	0.61	0.59	58.42	42.78	44.24	33.28	50
	Silt with Organics (Fe)	0.60	0.81	43.22	54.73	40.23	34.05	53.85
	Silt with Organics	0.79	0.88	36.63	60.92	36.11	33.75	28.13
KT18-21	Peat	0.36	0.43	67.55	35.65	43.67	40.58	60.87
	Humified Peat	0.54	0.60	57.33	42.56	44.82	41.68	21.21
	Silt with Organics	1.02	0.98	36.82	61.05	38.49	37.13	61.11

232	<b>Table 1.</b> Comparison of the dry bulk density (g cm <sup>-3</sup> ) and water content (%) of the saltmarsh
233	soils across the four coring sites, using the two coring methods. Additionally, the degree of
234	compaction (%) for each soil unit calculated by comparing the thickness of each soil unit
235	(Fig.2) from the gouge and hammer cores (negative compaction values are indicative of
236	stretching).

237 The surficial layers of fibrous and humified peat experience the greatest compaction (Table 1). In core KT18-05, we observe above average compaction of the silt layer (Table 1), most likely 238 due to the thin overlying peat layers (Fig.2). The compaction of the soil profiles significantly 239 240 dewatered the upper peat units, which in turn increases soil DBD (Table 1). It was hypothesised that dewatering of the soils would flush the soluble OC from the compacted sediment and, in 241 turn, evacuate porewater dissolved organic carbon (DOC) and reduce the measured OC content. 242 243 However, a comparison of the down core OC content of the sediments obtained by both coring methods (Fig.2) indicates only minimal differences between OC content. These differences in 244 245 OC are well within the range of natural variability and we therefore conclude that coring compaction in itself does not directly impact the relative (%) OC content of saltmarsh soils. 246

247

#### 4.3 Consequences for OC stock and burial estimations

248 The alteration (generally reduction) in the thickness of the individual soil units, combined with increases in DBD associated with the hammer coring technique, are likely to alter soil mass 249 250 and OC stock estimates. However, the reduction in soil thickness and increase in DBD may act to offset one another, while still resulting in accurate estimates of soil mass and OC stock. 251 252 Saltmarsh soil mass and OC stock estimates differ between the hammer and gouge cores for all sites (Table 2). The hammer cores KT18-02, 05 and 21 all overestimate the normalized soil 253 mass by between 3.9 - 37 % in comparison to the gouge core estimates. The resulting OC stocks 254 255 derived from these cores are also overestimated by between 14.8 to 22%. KT18-03 differs from the other sites in that the hammer core estimates are slightly lower than the gouge 256 equivalents for both the soil mass and OC stock (Table 2). This difference is potentially a 257 consequence of the material stretching when the core was removed from the ground (Fig.2), 258 resulting in a soil profile similar to that observed in the gouge core. 259

		Soil N	fass (kg)	OC Stock (kg)		
Site	Soil Unit	Gouge	Hammer	Gouge	Hammer	
KT18-02	Peat	21.6	41.3	6.2	10.8	
	Humified Peat	120.3	117.1	19.8	16.7	
	Silt with Organics	237.1	235.0	5.7	9.6	
	Total	379	393.4	31.6	37.1	
	Difference (H-G)	+14.4 kg (3.9 %)		+5.5 kg (14.8 %)		
KT18-03	Peat	10.7	25.6	3.37	7.4	
	Humified Peat	129.5	124.7	32.74	31.1	
	Silt with Organics	233.4	163.1	24.34	19.5	
	Total	373.6	313.1	60.46	57.9	
	Difference (H-G)	-60.5 k	g (16.1%)	-2.56 kg (4.2 %)		
KT18-05	Humified Peat	23.7	56.1	2.06	5.0	
	Silt with Organics	437.5	447.8	15.47	17.5	
	Total	461.3	503.9	17.53	22.5	
	Difference (H-G)	+42.6 kg (8.5%)		+5.0 kg (22.1 %)		
KT18-21	Peat	38.6	92.8	4.4	13.7	
	Humified Peat	156.8	187.3	17.1	18.1	
	Silt with Organics	72.7	143.2	6.0	2.78	
	Total	268.12	423.2	27.5	34.0	
	Difference (H-G)	+155.2 k	kg (36.7 %)	+6.5 kg (19.2 %)		

262

**Table 2.** Soil mass and OC stock estimates for  $1 \text{ m}^2$  of saltmarsh using the thickness of each unit measured from each of the cores.

While the differences between the gouge and hammer core-derived OC stocks may seem relatively small (-2.56 to 6.51 kg) it is worth highlighting that these estimates are for an area 1 m<sup>2</sup>. When these estimates are scaled up to the total area of the Kyle of Tongue saltmarsh (9.31 ha), itself a relatively small saltmarsh by UK standards, the OC stock calculation could result in an underestimation of 238 tonnes OC all the way to an overestimation of 606 tonnes OC, if the hammer coring method was employed in deriving those soil OC stocks.

Furthermore, as bulk density and porosity are essential components required for the successful radiometric age-calculation of soil profiles (Appleby and Oldfield, 1978, Appleby, 2002) these coring-related compaction changes will directly impact the calculation of OC burial rates. By inputting the DBD and porosity value calculated for the gouge and hammer core from site KT- 276 18-03 into the Barlow et al. (2014) radiometric age model, the effect of compaction can be assessed. The outputs from the age model (Fig.4) show that the age profile and mass 277 accumulation rate calculated from the gouge core does differ from that of Barlow et al. (2014) 278 but this difference is minor. The age models (CRS, CIC and simple linear) developed for the 279 hammer core significantly diverge from both that of Barlow et al. (2014) and that calculated 280 for the gouge core. Furthermore, the increase in DBD significantly increases the mass 281 accumulation rate to almost double that of the gouge core; this artificially increased mass 282 accumulation rate will therefore propagate into significantly increased OC burial rate estimates 283 284 in hammer cores.





Figure 4. The effect of compaction on radiometric dating (based on original data from the Kyle 287 288 of Tongue reported by Barlow et al., 2014) of cores collected from site KT-18-03 using

different calculation approaches (a) constant rate of supply (CRS) model (Appleby and
Oldfield, 1978). (b) Constant initial concentration (CIC) model (Robbins and Edgington 1975).
(c) Simple linear model (d) Mass sedimentation rates calculated from the CRS model.

292

## 293 5. Discussion

The comparison of the two coring techniques clearly highlights that hammer coring can cause significant compaction and alter the physical properties of collected saltmarsh soils (Fig.2). While soil compaction using the hammer coring method has previously been observed in saltmarshes (Callaway et al., 2012, Ewers Lewis et al., 2019, Kelleway et al., 2016a, b, Unger et al., 2016), the consequences of compaction are rarely discussed in light of their impact on OC stock and burial estimates.

300

OC stock estimates are calculated using the thickness of a soil unit and DBD, yet both these 301 properties are shown to have been altered during hammer coring (Fig.2). By comparing the soil 302 profiles collected in the gouge compared to the hammer cores, we observe that hammer coring 303 304 has a significant impact, by both reducing the thickness of each soil unit and increasing the DBD, which generally leads to an overestimation of the saltmarsh soil OC stock (Table 2). Yet 305 the degree of this uncertainty in OC stock is highly variable because each unit within the soil 306 307 profile compresses by different amounts (Table 1). This highlights that the linear corrections used to compensate for coring-related compaction (Ewers Lewis et al., 2019, Kelleway et al., 308 2016a, b) would be unsuitable to deal with the stratigraphic complexity of the soils examined 309 310 here. In saltmarshes with complex soil profiles (i.e. multiple different soil units), we have shown that hammer coring is unsuitable for the calculation of OC stocks and should be avoided. 311 Callaway et al., (2012) suggested that where compaction was >3 cm in cores of 50 cm length, 312

that those cores should not be used for OC stock calculations; we consider this to be areasonable suggestion.

315

316 OC burial rates for the recent past (last 150 years) are often calculated from chronologies produced from <sup>210</sup>Pb and <sup>137</sup>Cs radiometric dating of soils, while long-term burial rates are often 317 estimated using radiocarbon (<sup>14</sup>C). DBD and porosity are key components to the measurement 318 and production of radiometric chronologies (Appleby and Oldfield, 1978, Appleby, 2002). As 319 compaction changes both of these soil properties, the resultant radiometric chronologies will 320 321 be compromised (Fig.4). Johannessen and Macdonald (2016), for example, have recently critically reviewed the misunderstanding and use of <sup>210</sup>Pb dating, arguing that this has resulted 322 in significant overestimation of OC burial in seagrass soils. However, soil compaction during 323 the coring process and resulting errors in the <sup>210</sup>Pb chronology were not considered by 324 Johannessen and Macdonald, (2016) nor in the response by Arias-Ortiz et al., (2018). For the 325 reason discussed, there are few studies which use hammer cores for dating in saltmarshes (Boyd 326 et al., 2017, Unger et al., 2016) and as there is no way to correct for the alteration to any 327 complex soil profile, OC burial rates derived from hammer cores should be treated with caution. 328

329

The advantages to hammer coring are its low cost, provision of large quantities of sample material and its application in settings and soils where other corers would struggle to recover sediments (i.e. submerged soils, sands). Indeed, this explains why the hammer coring method is so widely used for seagrass sampling, for example. However, in saltmarshes, other effective coring options are available and are therefore preferable.

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336

#### 338 **6. Recommendations**

By comparing gouge and hammer cores, we show that the hammer coring method is unsuitable 339 for the reliable estimation of OC stocks and burial rates in saltmarsh soils. We acknowledge 340 that in some environments and sediment types hammer coring is the only viable, practical 341 option. In these circumstances, some simple steps can be taken to improve research outcomes: 342 (i) report if compaction took place and the correction factor applied; (ii) provide a description 343 of the soil profile; (iii) set a threshold (e.g >3cm for 50cm cores, Callaway et al., 2012) for 344 compaction which, if exceeded, will preclude the cores being used for OC stock estimates; (iv) 345 avoid the dating of bulk soil samples collected by hammer cores. While the above steps will 346 not resolve all of the coring-related issues identified in this study, they will allow the 347 calculation of OC stocks with an appropriate reporting of potential errors due to compaction. 348 349 Where possible, we therefore strongly recommend the use of tried and tested coring methods, such as gouge and Russian corers, which provide a strong foundation to reliably estimate 350 saltmarsh blue carbon stocks and burial rates. 351

352

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357

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