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1 **Beam-induced oxidation of mixed-valent Fe (oxyhydr)oxides (green rust) monitored by STEM-** 2 **EELS**

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8 **Abstract**

9 Analytical transmission electron microscopy (TEM) is often used to investigate morphologies, crystal
10 structures, chemical compositions and oxidation states of highly reactive mixed-valent mineral
11 phases. Of prime interest, due to its potential role in toxic metal remediation, is green rust sulphate
12 (GR_{SO_4}) an $\text{Fe}^{\text{II}}\text{-Fe}^{\text{III}}$ layered double hydroxide. In this study, we quantified the effects that TEM
13 analysis has on GR_{SO_4} in order to ensure the measured material properties are a result of synthesis and
14 reaction kinetics, and not due to sample preparation and analysis technique. To do this, we compared
15 two sample preparation techniques (anoxic drop-cast with drying, and frozen-hydrated cryogenic) and
16 exposed samples to the electron beam for several minutes, acquiring fluence series between ca. 40 e^-
17 \AA^{-2} and $10,000 \text{ e}^- \text{\AA}^{-2}$. TEM imaging and electron diffraction showed that the hexagonal plate-like
18 morphology and crystal structure of GR_{SO_4} were largely unaffected by sample preparation and analysis
19 technique. However, quantitative analysis of a series of monochromated Fe $L_{3,2}$ -edge electron energy
20 loss spectra (EELS) showed that electron irradiation induces oxidation. We measured an Fe(II)/Fe(III)
21 ratio of 1.94 (as expected for GR_{SO_4}) at $50 \text{ e}^- \text{\AA}^{-2}$. However, above this fluence, the ratio
22 logarithmically decreased and dropped to ca. 0.5 after $1000 \text{ e}^- \text{\AA}^{-2}$. This trend was approximately the
23 same for both sample preparation techniques implying that it is the beam alone which causes valence
24 state changes, and not exposure to oxygen during transfer into the TEM or the vacuum of the TEM
25 column. Ultimately this work demonstrates that GR valence can be quantified by EELS provided that
26 the sample is not over exposed to electrons. This also opens the possibility of quantifying the effect

27 of redox-sensitive toxic metals (e.g., As, Cr, Se) on Fe oxidation state in GR phases (relevant to the
28 treatment of contaminated soils and water) with a higher spatial resolution than other techniques (e.g.,
29 Mössbauer spectroscopy).

30 KEYWORDS: monochromated EELS; Fe oxidation; green rust; cryo-TEM; low dose TEM.

31 HIGHLIGHTS:

- 32 • Energy-resolved STEM-EELS to quantify Fe oxidation states in green rust
- 33 • Demonstration of electron beam induced *in situ* oxidation
- 34 • Methodology for quantifying the redox interaction between green rust and toxic metals

35 1. Introduction

36 Green rust (GR) materials are redox-active, mixed-valent Fe(II)-Fe(III) layered double hydroxides
37 which exhibit high surfaces area and can intercalate inorganic or organic species into the plate-like
38 structure due to their anion exchange capacity (Goh et al., 2008; Newman and Jones, 1998; Usman et
39 al., 2018). GR phases can be easily engineered for a wide-range of applications such as catalysis,
40 electrochemistry, and environmental remediation (Bhave and Shejwalkar, 2018; Chen et al., 2018;
41 Huang et al., 2019; Zhang et al., 2018). In particular, they are promising reactants for ground water
42 remediation where they have been shown to remove toxic metal contaminants from water by adsorption
43 (Jönsson and Sherman, 2008; Mitsunobu et al., 2009; Perez et al., 2019), reduction (O'Loughlin et al.,
44 2003; Skovbjerg et al., 2006; Thomas et al., 2018), interlayer intercalation (Refait et al., 2000) and
45 substitution of structural Fe (Ahmed et al., 2008; Refait et al., 1990).

46 Green rust sulphate ($[\text{NaFe}^{\text{II}}_6\text{Fe}^{\text{III}}_3(\text{OH})_{18}(\text{SO}_4)_2 \cdot 12\text{H}_2\text{O}]$ hereafter referred to as GR_{SO_4}) is composed of
47 positively charged brucite-like iron hydroxide layers that alternate with interlayers containing sulphate
48 and water molecules (following Christiansen et al.). The structural Fe(II)/Fe(III) ratio of 2 has been
49 determined by Mössbauer spectroscopy, chemical analysis, and X-ray diffraction (Christiansen et al.,
50 2009; Génin et al., 1996; Hansen et al., 1994; Perez et al., 2019; Refait et al., 1999, 1990). When using
51 GR for groundwater remediation, it is important the mineral remains stable and does not transform to
52 other iron (oxyhydr)oxides, which can be less effective substrates for the sequestration of toxic metals.

53 For example, partial oxidation or transformation of GR phases to other iron (oxyhydr)oxides can lessen
54 its ability to reduce redox-sensitive metals (e.g. Cr, Se, U) or its adsorption uptake (e.g. As) (Jönsson
55 and Sherman, 2008; O’Loughlin et al., 2003; Perez et al., 2019; Skovbjerg et al., 2006; Thomas et al.,
56 2018). One way to check the stability of GR over time is to monitor the Fe(II)/Fe(III) ratio following
57 interaction with metals. As such, it is essential that applied characterisation techniques can
58 quantitatively evaluate any changes in oxidation state resulting from environmental reactions and are
59 not a result of the characterization technique itself. Analytical transmission electron microscopy (TEM)
60 provides information at high spatial resolution regarding the morphology, crystal structure, chemical
61 composition and oxidation state of a specimen. To date, many TEM studies of GR have used
62 conventional sample preparation techniques (drop-cast and dried) under anoxic conditions (Ahmed et
63 al., 2010; Bach et al., 2014; Géhin et al., 2002; Mann et al., 1989; Perez et al., 2019; Skovbjerg et al.,
64 2006; Thomas et al., 2018). Such methods involve aqueous sample dilution, drop casting onto a TEM
65 grid and drying with alcohol in an anaerobic chamber to minimise the risk of oxidation. The dried grid
66 thus contains a well dispersed sample that is subsequently exposed to air for rapid transfer into the
67 TEM. Much of the literature regarding TEM of GR has so far assumed that both sample preparation
68 and the TEM environment do not significantly affect the specimen. In some studies (particularly
69 Johnson et al. (2015)) these factors are taken into account, such as the short term air exposure during
70 sample transfer to the TEM and electron beam induced “nanoscale restructuring”, where low dose
71 operating conditions were used (Johnson et al., 2015). Here, we further explore these factors in relation
72 to the stability of the oxidation state by measuring electron energy loss spectra (EELS) at the valence
73 sensitive Fe $L_{3,2}$ -edge following both conventional (anoxic drop-cast and dried) and cryogenic (cryo;
74 frozen hydrated suspension) sample preparation for a range of controlled electron fluences.

75 Minimising exposure of GR to oxygen prior to TEM analysis and to vacuum dehydration during TEM
76 analysis can be achieved by retaining the mineral in a thin layer of vitreous ice; the grid must be wetted,
77 blotted and plunge frozen into liquid ethane for cryo transfer into the TEM. This method results in the
78 GR plates being dispersed in a thin layer of electron transparent, vitreous ice. Cryo-TEM has been
79 successfully used to investigate the formation of magnetite (Fe_3O_4) from a ferrihydrite precursor, which

80 can often proceed via GR as a transient phase, a process that had previously only been quantified by
81 time resolved X-ray diffraction (Dey et al., 2015; Michel et al., 2010; Sumoondur et al., 2008). The
82 cryo-TEM sample preparation used by Dey et al. (2015) was required to capture and monitor the
83 morphological changes of the gel-like ferrihydrite precursor phase at various points during the
84 transformation reaction.

85 Assessing a specimen's sensitivity to electron irradiation can be achieved by collecting an electron
86 fluence series whereby the same area is repeatedly analysed during exposure to the electron beam.
87 Knowledge of the beam current, size of the analysed area, and the time the specimen is exposed to the
88 beam allows for the number of electrons per unit area (i.e. fluence) to be determined. A critical fluence
89 can then be calculated when the property being measured changes by a characteristic value (e.g., 1/e).
90 Previous TEM studies of Fe-bearing minerals have used EELS to show that electron irradiation can
91 induce changes in the oxidation state of structural Fe (Garvie et al., 2004; Pan et al., 2010). In the work
92 of Garvie et al. (2004), a threshold fluence of $10^4 \text{ e}^- \text{ \AA}^{-2}$ (for a 100 kV beam) was determined for the iron
93 silicate mineral cronstedtite ($\text{Fe}^{\text{II}}_2\text{Fe}^{\text{III}}(\text{SiFe}^{\text{III}}\text{O}_5)(\text{OH})_4$). It was found that beyond this fluence, the
94 electron beam-induced loss of structural H in the specimen was likely to be significant enough to cause
95 oxidation, as measured by an increasing Fe(III) contribution to the EELS Fe $L_{3,2}$ -edge. It was also
96 demonstrated that thinner specimens ($< 400 \text{ \AA}$) were more susceptible to beam-induced alterations.
97 Conversely, 200 kV EELS analysis at the Fe L_3 -edge by Pan et al. (2010) showed a reduction in Fe(III)
98 content following electron irradiation of various Fe-bearing phases (iron phosphate dihydrate,
99 ferrihydrite, haemosiderin and ferritin). They proposed that the dominant damage mechanism was
100 radiolysis induced loss of structural O, OH and H_2O , resulting in both Fe coordination and oxidation
101 state changes. In addition, the hydrated samples were found to be more beam sensitive than cronstedtite
102 (reported by Garvie et al. 2004), potentially due to increased levels of H_2O associated with these
103 minerals increasing the efficiency of radiolysis.

104 The work reported here used analytical (S)TEM including imaging, selected area electron diffraction
105 (SAED) and monochromated EELS to monitor changes in morphology, crystal structure and
106 Fe(II)/Fe(III) ratio of GR_{SO_4} plates that were prepared through two different TEM sample preparation

107 techniques: (i) drop-cast onto TEM grids and dried (in anoxic atmosphere, with rapid air transfer to the
108 TEM) and (ii) frozen hydrated suspensions cryo-transferred and cryo-analysed. This allowed us to
109 isolate the factors which we hypothesised might contribute to a change in oxidation state: (i) exposure
110 to oxygen during TEM transfer of anoxic drop-cast and dried samples (potentially sufficient to oxidise
111 the sample); (ii) exposure to the vacuum in the microscope column (potentially sufficient to cause loss
112 of interlayer water molecules and associated sulphate groups in the A, B planes which may lead to a
113 change in the interlayer charge balance, increasing Fe(III) content (Simon et al., 2003)); and (iii)
114 exposure to electron irradiation (potentially sufficient to either induce a loss of structural H and oxidise
115 the specimen (Garvie et al., 2004), or induce radiolysis and reduce the specimen (Pan et al., 2010)).

116 In this work, we revisit similar Fe $L_{3,2}$ -edge analysis methods to those used by Pan et al. (2010), but
117 with the improved energy resolution of a monochromated electron source and additional, absolute edge
118 energy measurement by dual EELS acquisition (Gubbens et al., 2010). In addition, we demonstrate the
119 need for low fluence EELS in order to measure representative Fe(II)/Fe(III) ratios for GR_{SO4} at a higher
120 spatial and energy resolution than previously reported techniques (Génin et al., 1996; Hansen et al.,
121 1994; Perez et al., 2019; Refait et al., 1999, 1990).

122 **2. Materials and Methods**

123 GR with interlayer sulphate was synthesized in aqueous suspension in an anaerobic chamber (97% N₂,
124 3% H₂, Coy Laboratory Products, Inc.) at room temperature using a modified co-precipitation method
125 (Génin et al., 2002; Perez et al., 2019). We ensured the supernatant used in the sample preparation steps
126 did not contain excess Fe²⁺ from the initial synthesis, as this would have added to the EELS signal. To
127 achieve this, the fresh GR_{SO4} slurry was rinsed inside the anaerobic chamber with de-oxygenated
128 deionized water by centrifugation and re-dispersion until the Fe²⁺ concentration in the supernatant was
129 below 2 mM (as measured by inductively coupled plasma - optical emission spectrometry (ICP-OES)).
130 All drop-cast TEM sample preparation was performed in the anaerobic chamber using diluted
131 suspensions in de-oxygenated water. These diluted suspensions were drop cast onto holey amorphous
132 carbon Cu grids (Agar Scientific Ltd.), left to dry in the anaerobic chamber and further dehydrated with
133 a drop of ethanol. Samples were transferred to the TEM in a grid box wrapped in parafilm, loaded into

134 a double tilt FEI TEM holder and inserted into the TEM; the grid was exposed to air for approximately
135 60 s. In all cases, data was collected from clean GR plates; those that were considered free of
136 contamination and/or visible stray iron (oxyhydr)oxide minerals of different valence ratios.

137 Cryo TEM sample preparation used non-diluted suspensions. Approximately 3.5 μL was dispensed by
138 micro pipette onto a lacey amorphous carbon coated Cu grid which was blotted and plunge frozen into
139 liquid ethane by an FEI Vitrobot[®] markIV (at blot force 6). The undiluted suspension was exposed to
140 air at 100% humidity for less than 5 s before plunge freezing. The frozen sample was then cryo-
141 transferred into the TEM using a Gatan 914 holder with the temperature maintained below $-165\text{ }^{\circ}\text{C}$.

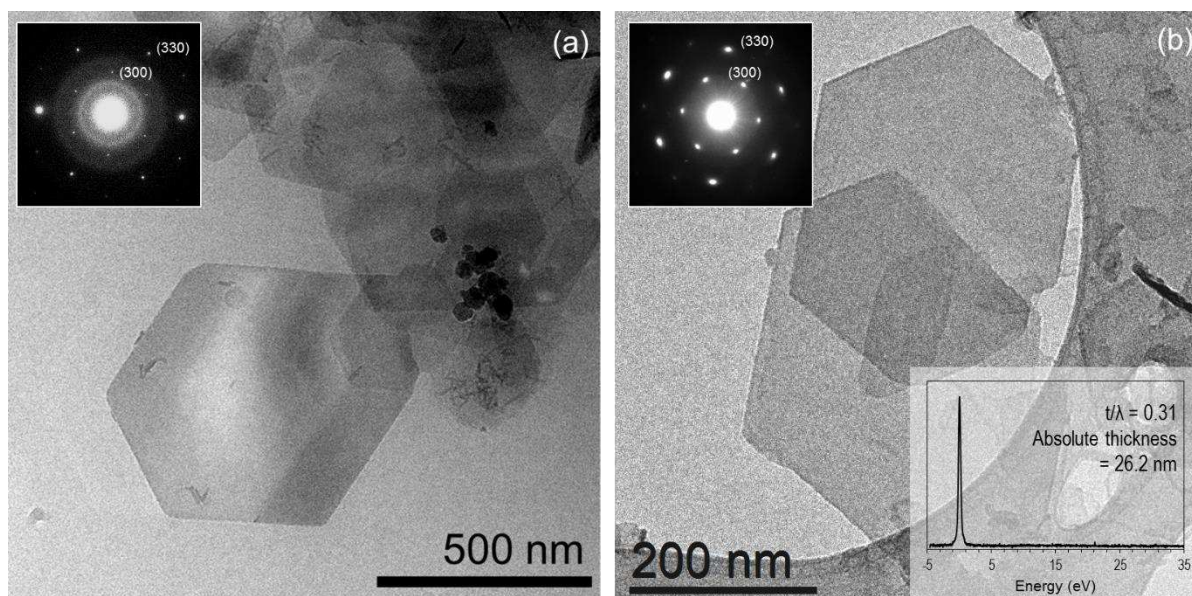
142 For both sample preparation techniques, an FEI Titan³ Themis G2 S/TEM operating at 300 kV was used
143 with an FEI Super-X energy dispersive X-ray (EDX) system, a monochromator with an energy spread
144 of ca. 0.35 eV, a Gatan Quantum 965 ER energy filter for dual EELS (which allows for core-loss edges
145 to be calibrated against the simultaneously acquired low loss spectrum) and a Gatan OneView CCD. A
146 ca. 1.4 \AA probe was formed for STEM with an estimated convergence semi-angle of ca. 10 mrad
147 (limited by the second smallest C3 aperture) and a probe current of up to 300 pA when the
148 monochromator is excited (as measured by the dose metre on the flu cam, calibrated using a Faraday
149 cup). Fluence was controlled in STEM by limiting the dwell time (to as low as 0.8 μs) and pixel size
150 and collecting EEL spectra while scanning (i.e. by continuously scanning at a magnification that
151 approximately matches the GR plate size to the field of view). In STEM-EELS mode, a 2.5 mm
152 entrance aperture provided a collection semi-angle of 21 mrad. Spectra were collected for 30 s and then
153 background subtracted (power law) in ‘Gatan Microscopy Suite’ software (version 3.0.1), with t/λ
154 values generally < 0.35 for anoxic drop-cast specimens. SAED patterns were obtained using an aperture
155 with an effective diameter of 200 nm at the imaging plane. The electron fluence per frame (F) was
156 calculated using equation 1:

$$157 \quad F(e^{-}\text{\AA}^{-2}) = \frac{I \times t}{e^{-} \times d_s^2} \quad \text{Eq. 1}$$

158 Where t is the dwell time, I is the probe current, e^{-} is the charge of an electron ($1.602 \times 10^{-19}\text{ C}$) and d_s
159 is the pixel size.

160 **3. Results**

161 TEM images showed hexagonal GR_{SO_4} plates between 0.1-1 μm in width, and ca. 20-50 nm thick (as
162 measured from the low loss EEL spectrum) (Figure 1). The general morphology of the GR plates did
163 not vary between sample preparation technique, and the SAED patterns provide evidence that the
164 hexagonal crystal structure was maintained. EDX spectroscopy (not shown) confirmed the presence of
165 Fe, S and O as expected. Diffraction patterns from both sample preparation techniques show reflections
166 for the $\{300\}$ and $\{330\}$ family of spots which are at 2.77 \AA and 1.60 \AA respectively and close in value
167 to those reported by powder XRD (2.75 \AA and 1.59 \AA) (Christiansen et al., 2009). Diffraction patterns
168 collected at higher fluences ($>10,000 \text{ e}^- \text{\AA}^{-2}$) showed slightly lower in-plane atomic spacing values for
169 the same type of pattern, of 2.59 \AA $\{300\}$ and 1.51 \AA $\{330\}$, a reduction of 6% for both planes.

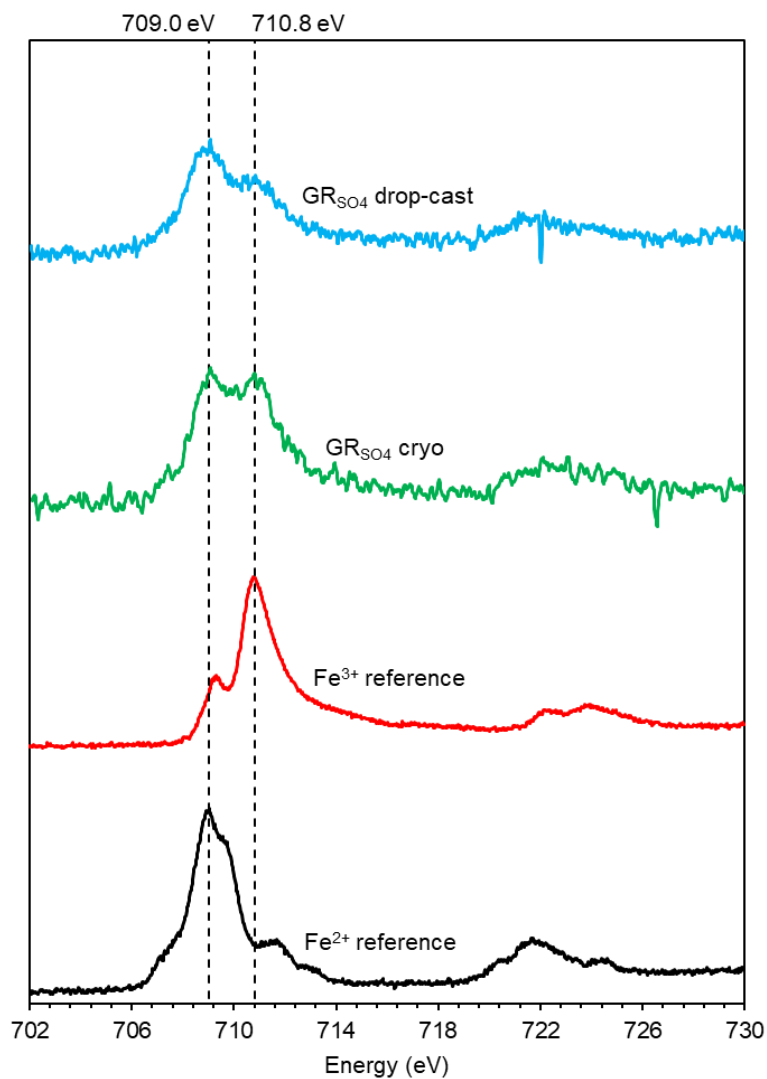


170

171 **Figure 1 TEM images and SAED pattern (inset) of GR_{SO_4} (a) cryo frozen-hydrated sample preparation (b) anoxic drop-**
172 **cast dry sample preparation. Note the additional amorphous ring in (a) from the scattering of electrons by ice. Dashed**
173 **lines represent areas associated with the SAED pattern, and the low loss EELS spectrum for calculating specimen**
174 **thickness is shown in (b).**

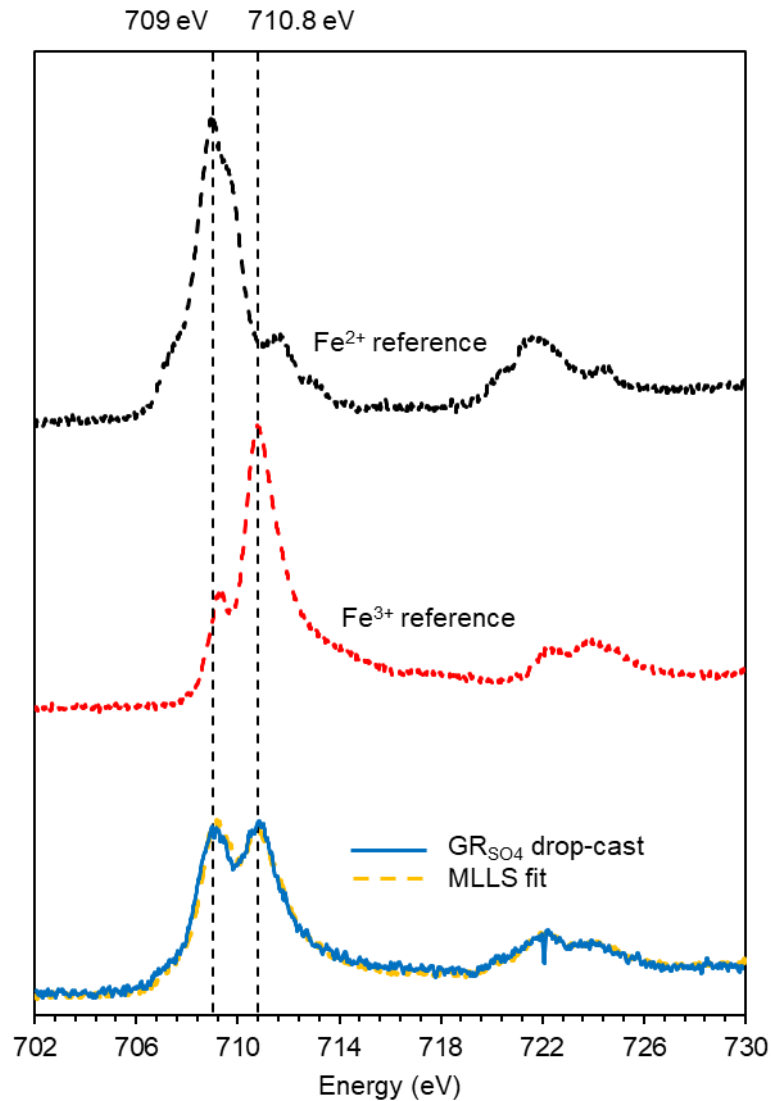
175 To measure the effect of electron irradiation on oxidation state, EELS Fe $L_{3,2}$ -edges were collected at
176 known fluences and compared to reference spectra; Figure 2 shows representative low fluence spectra
177 from both sample preparation techniques and the reference materials. To date, techniques to quantify
178 the Fe(II)/Fe(III) ratio in Fe bearing materials via EELS have used $L_{3,2}$ -edges for the white line intensity
179 ratio method (Cavé et al., 2006; Van Aken and Liebscher, 2002), have included the O-K edge (Brown
180 et al., 2001), or used reference spectra for non-linear least-squares (NLLS) fitting (Pan et al., 2009,

181 2006, 2010). With recent advances in EELS energy resolution via the addition of a monochromator or
182 the use of a cold FEG (Paterson and Krivanek, 1990), it is now possible to clearly resolve two sub-
183 peaks within the Fe L_3 edge; the lower energy sub-peak at ca. 709.0 eV can be attributed to a
184 predominant Fe^{2+} contribution and the higher energy sub-peak at ca. 710.8 eV to a Fe^{3+} contribution
185 (Brown et al., 2017). Being able to resolve these two sub-peaks enables a more accurate multiple linear
186 least-square (MLLS) fitting, and a ratio of Fe(II)/Fe(III) to be calculated. In this work, we fitted the
187 acquired Fe $L_{3,2}$ -edges against reference spectra of hedenbergite (100% octahedral Fe^{2+}) and haematite
188 (100% octahedral Fe^{3+}) using the ‘Gatan Microscopy Suite’ software (Figure 3). The higher energy sub-
189 peak of the core loss spectra were energy calibrated to 710.8 eV, background subtracted and area
190 normalised in the energy range 702-730 eV before being fitted. The spectra of the reference material
191 were collected with the same TEM and the same monochromator excitation but under the TEM
192 collection conditions described in Brown et al. (2017).



193

194 **Figure 2. Background subtracted Fe L_{3,2}-edge spectra for Fe²⁺ (black) and Fe³⁺ (red), plus lowest fluence GR_{SO4} Fe L_{3,2}-**
 195 **edge spectra from cryo (frozen hydrated suspension) sample preparation (green) at 255 e²Å⁻² and GR_{SO4} from anoxic**
 196 **drop-cast sample preparation (blue) at 50 e²Å⁻². Due to a low signal to noise ratio in the cryo spectrum (due to high levels**
 197 **of scattering in ice), a 5 point moving average has been applied to the data.**

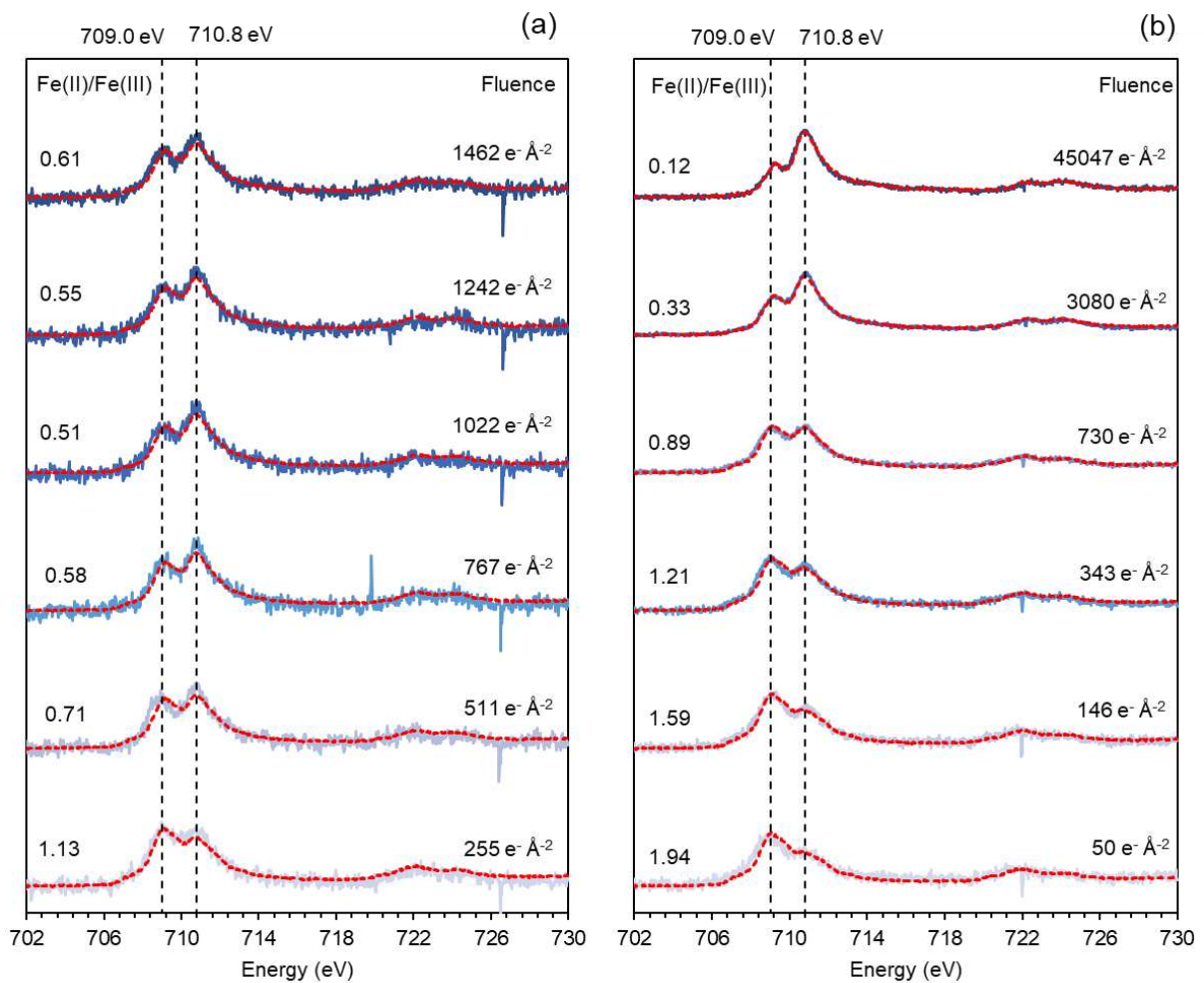


198

199 **Figure 3. Example MLLS fitting of a background subtracted and area normalised Fe $L_{3,2}$ -edge spectrum of anoxic drop-**
 200 **cast and dried GR_{SO_4} (blue) fitted against a reference spectrum MLLS fit (yellow) from haematite (Fe^{3+}) (red) and**
 201 **hedenbergite (Fe^{2+}) (black). The estimated Fe(II)/Fe(III) ratio is 0.89 ± 0.09 . Received fluence for GR_{SO_4} spectrum is 730**
 202 **$e^{-\text{\AA}^{-2}}$.**

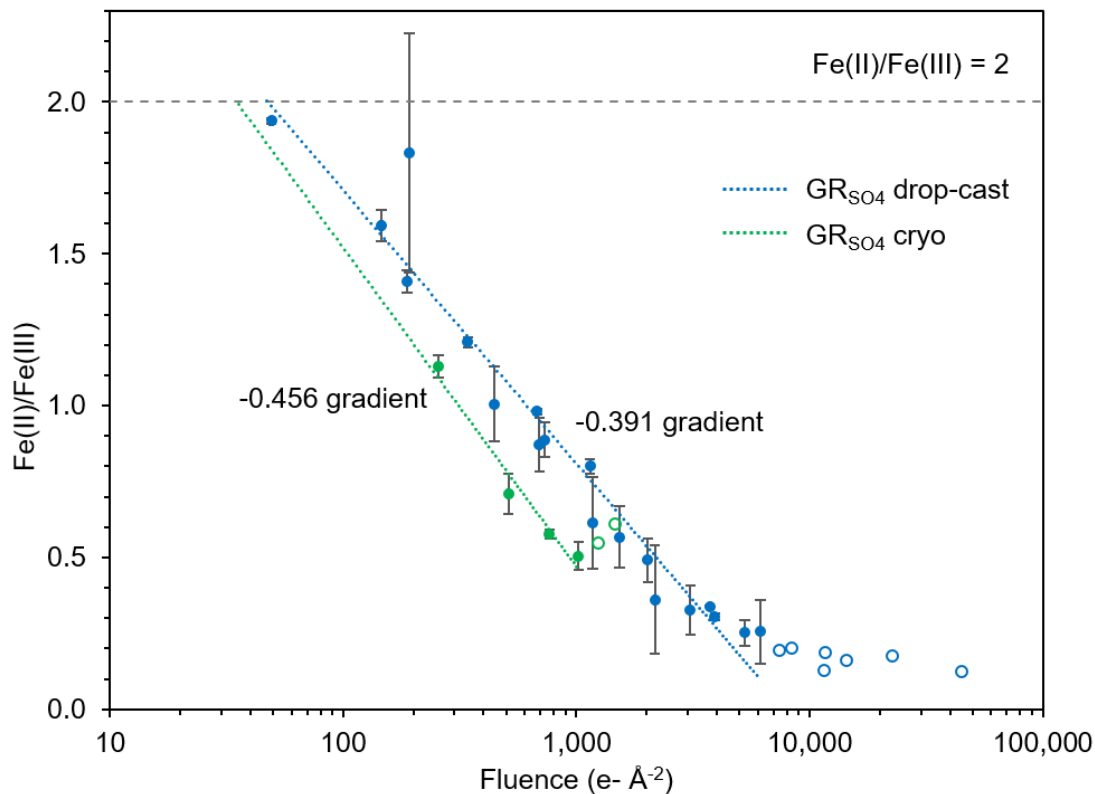
203 Applying this fitting procedure to spectral series from both sample preparation techniques provides
 204 quantitative evidence for the *in-situ* oxidation of GR_{SO_4} during exposure to the electron beam. Stacked
 205 spectral series (along with the MLLS fits) for both the cryo-frozen hydrated GR_{SO_4} and the anoxic drop-
 206 cast sample preparation methods are shown in Figure 4, and the measured change in Fe(II)/Fe(III) ratio
 207 with electron fluence is plotted in Figure 5 (for both sample preparation techniques). Figure 4 shows
 208 how the relative intensities of the two sub-peaks in the Fe- L_3 edge change with electron fluence; the
 209 intensity of the 709.0 eV peak quickly diminishes for both datasets. By ca. $1000 e^{-\text{\AA}^{-2}}$ the relative
 210 intensities of the two peaks tend not to change further for the cryo data whereas the 709.0 eV peak

211 continues to reduce for the drop-cast data. Following quantification of these peaks with the MLLS
 212 fitting procedure, it is possible to calculate that for the cryo data the Fe(II)/Fe(III) ratio stabilises at
 213 around 0.5 after ca. $1000 \text{ e}^- \text{ \AA}^{-2}$, and for the drop-cast data it stabilises at 0.15 after $6000 \text{ e}^- \text{ \AA}^{-2}$ (Figure
 214 5). The initial Fe(II)/Fe(III) ratio was higher for drop-cast samples (ca. 1.93) as it was possible to collect
 215 spectra with sufficient signal to noise ratios at a lower fluence due to the lack of vitreous-ice.
 216 Trendlines have been added to the data series in Figure 5 to measure the gradient (i.e., the rate of
 217 oxidation with electron fluence) and to extrapolate the data to the theoretical Fe(II)/Fe(III) ratio (2 for
 218 GR_{SO_4}). These extrapolated trendlines for both sample preparation techniques essentially meet at
 219 $\text{Fe(II)/Fe(III)} = 2$ as might be expected. This allowed us to determine a threshold fluence of $40 \pm 5 \text{ e}^- \text{ \AA}^{-2}$
 220 ², beyond which electron beam-induced oxidation occurred with either preparation method.



221

222 **Figure 4** Stacked core loss EEL spectra (blue) showing changing shape of the Fe L_3 edge during electron irradiation in
 223 cryo-TEM (a) and anoxic drop-cast (b) sample preparation methods. The MLLS fits are shown in red. The corresponding
 224 Fe(II)/Fe(III) ratios are shown on the left hand side, and the associated electron fluence shown on the right hand side.



225

226 **Figure 5** Change in Fe(II)/Fe(III) content with electron fluence for conventional (anoxic drop-cast) sample preparation
 227 (blue) and cryo (frozen-hydrated) sample preparation (green). Logarithmic (dashed) trendlines have been extrapolated to
 228 Fe(II)/Fe(III)=2, terminating where data points begin to plateau at higher fluences (non-filled data points). The error in
 229 fluence is not shown here however we estimated a maximum variation of 12% due to a change in probe current during
 230 in-situ measurements. The error in Fe(II)/Fe(III) ratio was based on deviation from the least-squares trendline. Note
 231 that the cryo data is from a single GR plate whereas the plotted anoxic drop-cast data is from three different GR plates;
 232 this is due to the fact that in cryo-TEM it is more challenging to find a suitable sample area (i.e. enough specimen in a
 233 thin region of vitreous ice).

234 4. Discussion

235 We can now address the key factors which we initially hypothesised might contribute to a change in
 236 oxidation state of GR when measured by (S)TEM-EELS. We have demonstrated that exposure to
 237 oxygen during TEM transfer of the anoxic drop-cast and dried samples was not sufficient to cause
 238 discernible oxidation because the measured Fe(II)/Fe(III) ratio (as high as 1.93 ± 0.09) was retained at
 239 low fluences. In addition, we can exclude the hypothesis that exposure to the vacuum in the electron
 240 column was sufficient to cause loss of interlayer water molecules and associated sulphate groups which
 241 may have led to a charge imbalance, as we have observed similar trends from both anoxic drop-cast
 242 samples and cryo frozen-hydrated samples, the latter of which is not directly exposed to the vacuum.
 243 The third hypothesis regarding electron irradiation induced valence changes has also been addressed
 244 and we showed that there is a threshold fluence of $40 \pm 5 \text{ e}^- \text{Å}^{-2}$ for the onset of GR oxidation for either

245 specimen preparation route. Unfortunately, collecting EELS spectra at such a low fluence is challenging
246 and we have compromised spatial resolution to approximately the size of an individual GR plate in
247 order to approach these values. Above this fluence threshold, we saw progressive oxidation of the GR
248 for anoxic drop-cast samples, where exposure to electron irradiation was sufficient to induce the
249 deprotonation of apical OH⁻ ions in the Fe octahedra (i.e. loss of structural H as reported by *Garvie et*
250 *al.* (2004) for mixed-valent Fe-bearing silicates). This charge imbalance within the Fe hydroxide layer
251 is compensated through the oxidation of structural Fe(II) to Fe(III). The *in situ* oxidation of GR phases
252 through deprotonation of the apical OH⁻ ions has been previously studied in GR carbonate by Mössbauer
253 spectroscopy and X-ray photoelectron spectroscopy (Ruby et al., 2006; Genin et al., 2006; Ruby et al.,
254 2008; Mullet et al., 2008). For cryo frozen-hydrated samples, this also seems to be the case for relatively
255 low fluences (i.e. <1000 e⁻Å⁻²), however beyond this point, the Fe(II)/Fe(III) content apparently
256 stabilises at 0.5. At fluence values above 1000 e⁻Å⁻² the vitreous ice (encasing the GR plates) has been
257 shown to melt and or sublime (Ilett et al., 2019) and certainly by this stage diffusion limited damage
258 due to the beam-induced radiolysis of the ice will become significant so that H₂O loss and reduction (as
259 reported by Pan et al. 2010) might operate alongside the ongoing beam-induced oxidation (as reported
260 by Garvie et al. (2004) and documented in this study). The fact that the Fe(II)/Fe(III) ratio plateaus at a
261 value of ca. 0.5 suggests that together, these mechanisms have a balanced effect which does not alter
262 the net oxidation state (Figure 5).

263 The subtle differences between in-plane atomic spacings measured by SAED for low (< 1000 e⁻Å⁻²) and
264 high (> 10,000 e⁻Å⁻²) fluences could also be evidence for beam-induced oxidation. Calculations by
265 Shannon (1976) showed that the ionic radius of Fe depends on its oxidation state; 0.780 Å in Fe(II) and
266 0.645 Å in Fe(III), which corresponds to a 17 % reduction in ionic radius following complete oxidation
267 (Shannon, 1976). While dehydration of the sample (in the TEM high vacuum column) would also
268 decrease d-spacing, this reduction would only occur between iron hydroxide layers and not in-plane.
269 The measured fluence dependent reduction of in-plane atomic spacings in this study might therefore be
270 attributed to the partial oxidation of Fe although further investigation, collecting a fluence series of

271 SAED patterns, would be needed to confirm this. If confirmed, this method could be used to monitor
272 GR oxidation on TEMs which do not have the ability to acquire high resolution monochromated EELS.
273 Ultimately, with this work we have demonstrated that only by using low fluences can one obtain truly
274 representative Fe(II)/Fe(III) ratios in GR when analysing these redox sensitive materials by STEM-
275 EELS. Spatial resolution has been compromised to achieve this however smart acquisition techniques
276 such as that reported by Sader et al. (2010) may be used to improve spatial resolution and assess
277 valence variation across an individual GR plate (Sader et al., 2010). This technique relies on
278 averaging spectra from the same position within multiple plates to increase EELS signal and improve
279 spatial resolution while minimising net fluence.

280 **5. Conclusion**

281 We have studied GR_{SO4} using analytical TEM, in particular monochromated STEM-EELS, to
282 demonstrate the sensitivity of Fe(II) content under electron irradiation. Using anoxic drop-casting and
283 cryogenic sample preparation techniques allowed us to isolate the cause of oxidation to structural H
284 loss induced by the electron beam, and not exposure to oxygen during sample transfer into the TEM
285 or to the vacuum within the TEM column. MLLS fitting to reference Fe L_3 -edge EEL spectra enabled
286 the Fe(II)/Fe(III) ratio to be determined which was plotted against electron fluence to identify the
287 beam induced oxidation rate. The lowest fluence Fe(II)/Fe(III) ratio was 1.93 ± 0.09 at $40 \text{ e}^- \text{ \AA}^{-2}$ and
288 compares favourably with the expected value of 2. Beam induced *in-situ* oxidation of GR_{SO4} was
289 quantified for both sample preparation techniques allowing us to calculate a threshold fluence at
290 which oxidation begins ($40 \text{ e}^- \text{ \AA}^{-2}$), and at which the Fe(II)/Fe(III) ratio stabilises at 0.15 for anoxic
291 drop-cast samples ($6000 \text{ e}^- \text{ \AA}^{-2}$) and 0.5 for cryo-samples (at ca. $1000 \text{ e}^- \text{ \AA}^{-2}$). Based on these results we
292 have developed a robust analytical TEM methodology for the investigation of highly redox sensitive
293 materials like GR. This low fluence approach can be applied to measure the spatial variation in Fe(II)
294 content across a single GR plate and to measure change in Fe(II) content of GR reacted with toxic
295 metals such as As, Cr and Se (relevant to the remediation of polluted water).

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