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High Energy Storage Density and Large Strain in Bi(Zn_{2/3}Nb_{1/3})O₃-Doped BiFeO₃-BaTiO₃ Ceramics

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ABSTRACT

High recoverable energy density ($W_{rec} \sim 2.1 \text{ J/cm}^3$) was obtained in (0.7-x)BiFeO₃-0.3BaTiO₃-xBi(Zn_{2/3}Nb_{1/3})O₃ + 0.1 wt% Mn₂O₃ (BF-BT-xBZN, x = 0.05) lead-free ceramics at < 200 kV/cm. Fast discharge speeds (< 0.5 μs), low leakage ($\sim 10^{-7} \text{ A/cm}^2$) and small temperature variation in W_{rec} ($\sim 25\%$ from 23 to 150 °C) confirmed the potential for these BiFeO₃ based compositions for use in high energy density capacitors. A core-shell microstructure composed of a BiFeO₃-rich core and BaTiO₃-rich shell was observed by scanning and transmission electron microscopy which may contribute to the high value of energy density. In addition, for x = 0.005, a large electromechanical strain was observed with $S_{pos} = 0.463\%$ and effective $d_{33}^* \sim 424 \text{ pm/V}$, suggesting that this family of ceramics may also have potential for high strain actuators.

Keywords: energy storage, bismuth ferrite, lead-free ceramics, piezoelectrics, dielectrics, capacitors

INTRODUCTION

The current research into new energy storage materials is mainly driven by concerns regarding the continued use of fossil fuels for automotive applications. Therefore, low cost, sustainable and environmentally-friendly energy storage materials with high energy densities are required.¹⁻³ Among current energy storage devices, ceramic capacitors are emerging as promising technological alternatives to fuel cells and batteries, because of their high power densities combined with fast charge-discharges rates, which are favoured in advanced pulse power applications.⁴⁻⁷ This drives the search for dielectrics exhibiting both high energy and power densities, to satisfy for power supply components incorporated into portable electronics, electric vehicles and other high power and energy storage applications.⁸⁻¹⁰

To attain high recoverable energy density (W_{rec}) and efficiency (η), a polarization maximum (P_{max}), a small remnance (P_r) and an optimised breakdown strength (BDS) are simultaneously required. Furthermore, the stability of devices in a range of temperature is also a critical parameter. For example, for hybrid electric vehicles these devices are expected to operate at temperatures ranging from $-40\text{ }^\circ\text{C}$ to $140\text{ }^\circ\text{C}$.^{1,11} Consequently, ferroelectrics (FE) and antiferroelectrics (AFE) are promising candidates due to their high P_{max} and Curie temperature (T_C). The total energy density (W), W_{rec} and η of FE and AFE ceramics is given by:

$$W = \int_0^{P_{max}} E dP, \quad (1)$$

$$W_{rec} = \int_{P_r}^{P_{max}} E dP, \quad (2)$$

$$\eta = W_{rec}/W \quad (3)$$

where P , P_{max} and P_r are the polarization, polarization maximum and remnance, respectively.

Although there are commercial energy storage devices based on La doped lead zirconate titanate, concerns over the toxicity of PbO have led to a large body of recent research on lead free replacements such as BaTiO_3 (BT), $(\text{K}_{0.5}\text{Na}_{0.5})\text{NbO}_3$ (KNN) and $(\text{Bi}_{0.5}\text{Na}_{0.5})\text{TiO}_3$ (BNT) based ceramics.¹²⁻²⁵ Oxide additives such as Al_2O_3 , SiO_2 , MgO enhance both W_{rec} and BDS in BT-based ceramics¹²⁻¹⁴ but BT- $\text{Bi}(\text{M},\text{N})\text{O}_3$ ($\text{M} = \text{Li}, \text{Mg}, \text{Zn}$, $\text{N} = \text{Nb}, \text{Ti}, \text{Zr}$) ceramics show greater promise, with W_{rec} up to 2.5 J/cm^3 .¹⁵⁻

²¹ In addition, $\text{Bi}_{0.5}\text{Na}_{0.5}\text{TiO}_3\text{-BaTiO}_3\text{-KNbO}_3$ (BNT-BT-KN) and $\text{Bi}_{0.5}\text{Na}_{0.5}\text{TiO}_3\text{-BaTiO}_3\text{-NaTaO}_3$ (BNT-BT-NT) also exhibit large W_{rec} of 1.72 and 1.2 J/cm³, respectively.^{22,23} In a recent study, Du et al. showed a commensurate improvement in W_{rec} to ~ 4 J/cm³ in KNN-ceramics due to an enhancement of BDS (300–400 kV/cm), which was achieved by a careful control of grain growth.^{24,25} $\text{BiFeO}_3\text{-BaTiO}_3$ (BF-BT) ceramics are characterised by high values of Curie maximum (T_C) and P_{max} (> 40 $\mu\text{C}/\text{cm}^2$)²⁶⁻³², but because their dielectric $\tan\delta$ and P_r are relatively large, their energy storage characteristics have been seldom studied. Recently, Nb_2O_5 , $\text{La}(\text{Mg}_{1/2}\text{Ti}_{1/2})\text{O}_3$, $\text{Ba}(\text{Mg}_{1/3}\text{Nb}_{2/3})\text{O}_3$ and Nd_2O_3 have been used as either dopants in, or in solid solution with, BF-BT with W_{rec} of 0.71, 1.66, 1.56, and 1.82 J/cm³, respectively, reported³³⁻³⁶ Nd doped BF-BT multilayers showed particular promise with both high W_{rec} ~ 6.74 J/cm³ and $\eta \sim 77\%$, from RT to 125 °C.³⁶

Wu et al. theoretically predicted that FE ceramics with core-shell microstructure could achieve enhanced energy density and reduced energy loss.³⁷ However, to our knowledge, up to now the energy storage characteristics of BF-based ceramics featuring a core-shell microstructure remain elusive, as no experimental evidence has been provided. Also $\text{Bi}(\text{Zn}_{2/3}\text{Nb}_{1/3})\text{O}_3$ (BZN) doped BF-BT materials were recently reported to have excellent piezoelectric properties²⁷ but their energy storage performance is yet to be determined, despite each effect relying on a large remanent/induced polarisation. In this work, a unique core-shell microstructure was induced by the substitution of BZN into BF-BT, its impact on the structure-property relationships, in particular on the energy storage characteristics, evaluated.

EXPERIMENTAL SECTION

Ceramic synthesis and characterisation: $(0.7-x)\text{BiFeO}_3\text{-}0.3\text{BaTiO}_3\text{-}x\text{Bi}(\text{Zn}_{2/3}\text{Nb}_{1/3})\text{O}_3 + 0.1\text{wt}\% \text{Mn}_2\text{O}_3$ (BF-BT-xBZN, $x = 0, 0.005, 0.01, 0.02, 0.05, 0.08$) ceramics were fabricated using solid state reaction.^{26,36} In order to increase the resistivity of ceramics, 0.1 wt% Mn_2O_3 was added into the calcined powder of BF-BT-xBZN.^{26,28,36} Mn-ions are considered to form defect dipoles with oxygen vacancies and decrease their mobility. Densities of ceramics were determined by the Archimedes immersion method and were typically $>95\%$. The phase structure of sintered ceramics was determined at RT by X-ray powder diffraction (XRD) using a Bruker D2 Phaser. Grain and sub-grain structures were

evaluated by scanning electron microscope (SEM) and transmission electron microscopy (TEM) using an FEI Inspect F50 equipped with a backscattered (BSE) detector and a Tecnai G2-F20, respectively. For SEM, ceramics were ground/polished to a mirror finish using wet abrasive paper and diamond paste (MetPrep Ltd.). For TEM, BF-BT-0.05BZN ceramics were ground to 120 μm , 3 mm disks ultrasonically cut and their centers dimpled down to 10 μm . Prior to Ar-ion milling to achieve electron transparency, samples were annealed at 650 $^{\circ}\text{C}/0.5$ h to ensure that residual stresses were removed.

Electrical properties: Fired-on gold paste electrodes were applied to both surfaces of the ceramics. 100-120 $^{\circ}\text{C}$ was used to pole the electroded ceramics at fields of 40 ~ 60 kV/cm. A ferroelectric tester (aixACCT TF 2000E) was employed to measure the polarization and the electric-field induced strain from -50 $^{\circ}\text{C}$ to 150 $^{\circ}\text{C}$ using a 1 Hz triangular signal at provided by a TREK power supply. Leakage current density was also measured using the aixACCT TF 2000E. The dielectric properties as a function of temperature were evaluated from RT to 650 $^{\circ}\text{C}$ using an LCR meter (Agilent 4184A). AC impedance spectroscopy was carried out at 400 $^{\circ}\text{C}$ using a second LCR Meter (Agilent E4980A). Charging-discharge characteristics were determined using a capacitor discharge circuit.^{16,36} A Tektronix DPO 4104 oscilloscope together with a Pearson 6585 coil were employed to obtain the discharge current waveforms. The discharge energy was then measured using ceramics connected in series with a load resistor (RL).

RESULTS AND DISCUSSION

Room temperature XRD data in the 20 $^{\circ}$ ~70 $^{\circ}$ 2θ range for BF-BT-xBZN ceramics are illustrated in Fig. 1(a). Reflections are ascribed to either a single-phase perovskite or a mixture of perovskite phases, without any detectable secondary impurity phases for $x < 0.08$. Secondary peaks however, were observed for $x = 0.08$, denoting the solid solubility limit for $\text{Zn}_{1/3}/\text{Nb}_{2/3}$ self-compensated doping in BF-BT. The average ionic radii, R , of $(\text{Zn}_{2/3}\text{Nb}_{1/3})^{3+}$ ions is given by $R = 2/3R(\text{Zn}^{2+}) + 1/3R(\text{Nb}^{5+}) = 0.707$ \AA (0.74 \AA and 0.64 \AA are the respective ionic radii of Zn^{2+} and Nb^{5+}),³⁸ which is larger than that of Fe^{3+} and Ti^{4+} (0.645 \AA and 0.605, respectively) and consistent with the diffraction peaks shifting to lower diffraction angle with increasing BZN concentration (Fig.1). The likely crystal symmetry is often

determined by (021)/(110) peak splitting at $\sim 2\theta = 32^\circ$. In the present case, expanded XRD patterns reveal an apparent coexistence of rhombohedral (*R*) and pseudocubic (*PC*) symmetries at room temperature in BF-BT-*x*BZN ceramics, as corroborated by broad multiple peaks. To confirm the phase assemblage, Rietveld refinement of BF-BT-0.05BZN was carried out using a two-phase refinement method ($R3c + Pm\bar{3}m$) in the GSAS+EXPGUI package.^{39,40} Observed and calculated patterns were in good agreement for BF-BT-0.05BZN as demonstrated in Fig. 1(b) ($R_p = 7.6\%$, $R_{wp} = 9.7\%$ and chi-squared (χ^2) = 2.3), corroborating the presence of *PC* ($Pm\bar{3}m$) and *R* ($R3c$) symmetries.

The relative permittivity (ϵ_r) and dielectric loss ($\tan \delta$) for BF-BT-*x*BZN ceramics from RT to 550 °C measured at 100 kHz are illustrated in Fig. 1(c). BF-BT and BF-BT-0.005BZN exhibit a relatively sharp peak in ϵ_r at 476 °C and 480 °C, respectively, associated with a ferroelectric to paraelectric transition (T_c) on heating but with increasing BZN concentration, two broad dielectric maxima are observed, each at lower temperatures. Furthermore, compared with BF-BT and BF-BT-0.005BZN, the maximum dielectric permittivity (ϵ_m) of BF-BT-*x*BZN ($x > 0.005$) decreases significantly and is accompanied by the emergence of broad frequency-dependent dielectric peaks (Fig. 1c). These two modifications are a manifestation of polar coupling disruption brought in by replacement of $(Zn_{2/3}Nb_{1/3})^{3+}$ for Fe^{3+} . Despite these changes, $\tan \delta$ remains < 0.15 at < 230 °C, and then increases greatly (Fig. 1c), presumably due to a rise in dc conductivity. To evaluate the electrical homogeneity, impedance spectroscopy (IS) analysis was performed at 400 °C, Fig. 1(d) and Fig. S1. Indeed, electrical homogeneity can be qualitatively assessed from Z'' and M'' spectroscopic plots constructed from IS data.^{41,42} It is evident that the peak positions of Z'' and M'' are almost coincident for BF-BT (Fig. S1a of ESI), however a frequency offset between the Z'' and M'' peak is observed for BF-BT-0.02BZN and BF-BT-0.05BZN (Fig. 1d and Fig. S1b of ESI). This shows the latter compositions to be electrically heterogeneous, which we interpret on balance of evidence as arising from compositional inhomogeneity.

The SEM images of as-sintered and polished surface for BF-BT-*x*BZN are illustrated in Fig. S2 and Fig. 2(a-c), respectively. All samples present a single modal grain size distribution around an average

of $\sim 4 \mu\text{m}$ (Fig. S2 of ESI). Except for BF-BT and BF-BT-0.005BZN ceramics, there is evidence of core shell microstructure for BF-BT-xBZN (Fig. 2a-c), with dark and light contrast relating to BaTiO_3 -rich and BiFeO_3 -rich regions according to energy dispersive X-ray spectroscopy (EDS) mapping (Fig. 2d-k). The EDS elemental maps of polished BF-BT-0.05BZN samples are shown in Fig. 2(d-k). The Ba and Ti signals are weaker in the brighter regions of the SEM image, associated with the grain cores (Fig. 2d and e). Conversely, Bi and Fe exhibit a slightly increased intensity in the brighter areas (Fig. 2f, g). These results indicate that the observed core-shell microstructure in BF-BT-xBZN are associated with the micro-segregation of Ba and Ti into the shell, while Bi and Fe are concentrated in the core regions.⁴¹⁻

^{47.} Murakami et al. investigated the role of composition and quenching on core-shell formation in $\text{BiMg}_{1/3}\text{Nb}_{2/3}\text{O}_3$ doped BF-BT ceramics.^{41,42} They concluded that the major influence was the onset of immiscibility on cooling from the sintering temperature, driven by the electronegativity difference of the dopant species. Effectively, the more covalent the dopants, the greater the tendency for immiscibility.

To examine the core-shell microstructure, TEM was conducted on BF-BT-0.05BZN ceramics. For further data on undoped systems the reader is referred to ref. 36. Fig. 3a is bright-field (BF) TEM image of a grain close to a $\langle 211 \rangle_{\text{pc}}$ zone axis. The dark spherical region in the grain center corresponds to the bright regions in the SEM images in Figure 2 and is thus BiFeO_3 rich. $\langle 211 \rangle_{\text{pc}}$ zone axis diffraction patterns (Fig. 2a) from the BiFeO_3 rich core have $\{1/2\ 1/2\ 1/2\}$ superstructure reflections arising from antiphase O-octahedral tilting consistent with an R3c phase.³⁶ These superstructure reflections are absent in the shell regions which are BaTiO_3 -rich, suggesting that they are PC. The weak aligned contrast in the shell region is consistent with relaxor-like phases in which there is nano- rather than micro- or meso-range correlation of dipoles, commensurate with the diffuse frequency dependent Curie maxima, Fig. 3(b). The core and shell structures shown in Fig 3(a) and in Fig. 2 have been tentatively assigned to the high (BiFeO_3 -rich) and low (BaTiO_3 -rich) temperature broad Curie maxima in Fig. 3(b).

Field-induced polarization (P-E), bipolar strain (S-E) and unipolar strain curves for BF-BT-xBZN ceramics measured at 100 kV/cm are illustrated in Fig. 4(a-c) (no field-induced strain for BF-BT-0.08BZN was detected). P_r , coercive field (E_c) and electric-field induced positive (S_{pos}) and negative

strain (S_{neg}) as a function of x are summarized in Fig. 4(d,e). The large signal piezoelectric strain coefficient (d_{33}^*) and hysteresis (SH) are calculated by

$$d_{33}^* = S_{\text{max}}/E_{\text{max}}, \quad (5)$$

$$\text{SH} = H_{E_{\text{max}/2}}/S_{\text{max}}, \quad (6)$$

where S_{max} , E_{max} and $H_{E_{\text{max}/2}}$ is the average electric field induced maximum strain obtained from the unipolar strain loops, the maximum electric field and the width of the loop at half the applied field, respectively.⁴⁸ BF-BT and BF-BT-0.005BZN ceramics exhibit saturated polarization loops and butterfly-shaped strain loops at 100 kV/cm (Fig. 4a,b), which also corroborate the high electrical resistivity of these ceramics. With increasing BZN content, the P-E and S-E loops become slimmer and are no longer saturated (Fig. 4a,b), along with P_r , E_C , d_{33} and S_{neg} continuously decreasing (Fig. 4d,e), suggestive of relaxor-like behavior, which is commensurate with both the broad ϵ_m (Fig. 1c) and nanodomain structure (Fig. 3). The largest $P_r \sim 24.6 \mu\text{C}/\text{cm}^2$, $E_C \sim 32.8 \text{ kV}/\text{cm}$, $d_{33} \sim 180 \text{ pC}/\text{N}$, $S_{\text{neg}} \sim 0.079\%$ values and smallest HS $\sim 18.4\%$ value are exhibited by BF-BT ceramics (Fig. 4d,e,f), due to coexistence of R3c and PC symmetries (Fig. 1).^{26,36} On the other hand, the largest $S_{\text{pos}} \sim 0.463\%$ and $d_{33}^* \sim 424 \text{ pm}/\text{V}$ values are exhibited by BF-BT-0.005BZN ceramics (Fig. 4e,f), which arises from a field-induced transition from short- to long-range dipolar order at the transition from a normal to a relaxor ferroelectric (Fig. 4a,b and Fig. 1c).^{26,36}

Because of their slim P-E loops (Fig. 4a), BF-BT-0.05BZN and BF-BT-0.08BZN exhibit a greater potential for energy storage and were selected for further characterization. Unipolar P-E loops are illustrated in Fig. 5(a,b), with corresponding values of P_{max} , P_r and ΔP ($P_{\text{max}} - P_r$) at different electric fields given in Fig. S3. As the increase of electric field, P_{max} and ΔP are found to increase linearly with a marginal improvement of P_r for both samples (Fig. S3). The highest values of P_{max} and ΔP are 36.7 and 32.8 $\mu\text{C}/\text{cm}^2$ for BF-BT-0.05BZN at 180 kV/cm, 26.4 and 24.5 $\mu\text{C}/\text{cm}^2$ for BF-BT-0.08BZN at 190 kV/cm, respectively. Equations 1-3 are employed to calculate W , W_{rec} and η , Fig. 5(c,d). As field increases, W and W_{rec} increase, reaching 3.7 and 2.06 J/cm^3 for BF-BT-0.05BZN at 180 kV/cm, and 2.9 and 1.98 J/cm^3 for BF-BT-0.08BZN at 190 kV/cm, respectively. The η values, however, decrease

for both compositions to 53% for BF-BT-0.05BZN at 180 kV/cm and 68% for BF-BT-0.08BZN at 190 kV/cm.

The discharge behaviour, leakage current and temperature stability are critical for high power capacitors. The discharge behaviour of BF-BT-0.05BZN and BF-BT-0.08BZN as a function of applied field is given in Fig. 6. The current increases as the electric field increases from 40 kV/cm to 70 kV/cm and all discharge processes occur within $\sim 0.5 \mu\text{s}$, as shown in Fig. 6(a,b). The time for the discharge energy in the load to achieve 90% of the final value ($\tau_{0.9}$), is obtained from the W_{rec} curves (Fig. 6c,d). $\tau_{0.9}$ of both composition under different electric fields is less than $0.1 \mu\text{s}$.

In-situ temperature dependence of leakage current density (J) and unipolar P-E loops at 120 kV/cm for BF-BT-0.05BZN are shown in Fig. 7(a,b). The corresponding values of J, P_{max} , P_r and ΔP are given in Fig. 7(c) and Fig. S4. W, W_{rec} and η are also calculated and plotted in Fig. 7(d). The value of J below 50°C is of the order of 10^{-7} A/cm^2 in the high field region (Fig. 7a,c), \sim one order magnitude less than reported for BF-based ceramics at RT.^{49,50} From -50°C to 150°C , J consistently increases (Fig. 7a,c), indicating increased conductivity at high temperatures. As temperature increases, saturated P-E loops are obtained at $\sim 150^\circ\text{C}$, giving increased values of P_{max} and P_r (Fig. S4), which is attributed to lower activation energy of the transition from relaxor to ferroelectric.^{26,36} W increases with temperature, while W_{rec} and η increase before decreasing from a maximum of 1 J/cm^3 and 59% at $75\text{-}100^\circ\text{C}$, Fig. 7(d). The variation in W_{rec} is $\sim 25\%$ between RT and 150°C , which is attractive for commercial applications.

A comparison of W_{rec} and strain for ceramics is plotted in Fig. 8.^{12-25, 26-36, 48-92} W_{rec} generally increases with electric field but lead-based ceramics still exhibit larger W_{rec} values compared to the lead-free ceramics (Fig. 8a). To our knowledge, BF-BT-0.05BZN has one of the highest value of $W_{\text{rec}} \sim 2.1 \text{ J/cm}^3$ among current lead-free FE ceramics with an electric field $< 220 \text{ kV/cm}$, which is ascribed to the high

BDS ~ 190 kV/cm, $P_{\max} \sim 36.7$ $\mu\text{C}/\text{cm}^2$ and $\Delta P \sim 32.8$ $\mu\text{C}/\text{cm}^2$. In Fig. 8(b), BF-BT-0.005BZN has one of the highest values of strain $\sim 0.463\%$ amongst ferroelectric ceramics, with a medium value of $d_{33}^* \sim 424$ pm/V and a low value of strain hysteresis $\sim 38\%$ (in comparison with BNT),⁸²⁻⁸⁹ which is attractive for actuator applications. Core-shell structures in FE ceramics are reported to alleviate inhomogeneity of local electric fields and weakens dielectric nonlinearity, resulting in slimmer hysteresis loops.³⁷ Although the work presented does not conclusively prove the arguments presented by the authors of ref. 37, enhanced energy storage is observed for core-shell BT-BF-xBZN compositions. Furthermore, we note that recent multilayering of Nd doped BF-BT ceramics improved W_{rec} from 1.82 to 6.74 J/cm³ and η from 50 to 77%.³⁶ Similar improvements for multilayers of BF-BT-xBZN whose bulk ceramics have superior energy storage properties would suggest that they have potential for commercialization should lead based systems fail to gain exemption from future environmental legislation. Moreover, BT-BF-xBZN compositions are rare-earth (RE)-free, lowering their cost and enhancing their potential for sustainable manufacturing.

CONCLUSIONS

Dense BF-BT-xBZN lead-free ceramics were fabricated using solid state reaction. *R* and *PC* phases coexisted in all studied BF-BT-xBZN compositions at RT. As BZN concentration increased, a core-shell microstructure was observed with a BaTiO₃-rich shell and BiFeO₃-rich core, confirmed by SEM, EDS, IS, TEM and LCR measurements. With the increase of BZN concentration, relaxor-like behaviour dominated with P_r , E_C , d_{33} and S_{neg} decreasing. The highest values of $P_r \sim 24.6$ $\mu\text{C}/\text{cm}^2$, $E_C \sim 32.8$ kV/cm, $d_{33} \sim 180$ pC/N, $S_{\text{neg}} \sim 0.079\%$ and $HS \sim 18.4\%$ were achieved for the undoped BF-BT. The highest value of $S_{\text{pos}} \sim 0.463\%$ and $d_{33}^* \sim 424$ pm/V was obtained for BF-BT-0.05BZN. For energy storage properties, with increasing electric field, W and W_{rec} increased from 3.7 and 2.06 J/cm³ for BF-BT-0.05BZN at 180 kV/cm, and 2.9 and 1.98 J/cm³ cm² for BF-BT-0.08BZN at 190 kV/cm, respectively. η decreased however, to 53% for BF-BT-0.05BZN at 180 kV/cm and 68% for BF-BT-0.08BZN at 190 kV/cm, respectively. A fast discharge speed (less than 0.5 ms), leakage current $\sim 10^{-7}$ A/cm² and a small temperature variation in W_{rec} ($\sim 25\%$ in a temperature range between RT and 150 °C) were also obtained, suggesting that the BF-BT-xBZN is a potential lead-free candidate for pulsed power capacitors and

electromechanical actuators.

ASSOCIATED CONTENT

Supporting Information.

This material is available free of charge via the Internet at <http://pubs.acs.org>.

Spectroscopic plots of Z'' and M'' for (a) BF-BT and (b) BF-BT-0.02BZN. SEM images of BF-BT- x BZN (a) $x = 0$, (b) $x = 0.005$, (c) $x = 0.01$, (d) $x = 0.02$, (e) $x = 0.05$ and (f) $x = 0.08$. P_{max} , P_r and ΔP for (a) BF-BT-0.05BZN and (b) BF-BT-0.08BZN. Temperature dependence of P_{max} , P_r and ΔP for BF-BT-0.05BZN at 120 kV/cm. The schematic diagram of the discharge circuit.

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Notes

The authors declare no competing financial interest.

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Figure Captions:

Fig. 1. a) Room temperature XRD patterns of BF-BT-xBZN from $20^\circ \sim 70^\circ 2\theta$. b) Rietveld refinement analysis of BF-BT-0.05BZN using the GSAS+EXPGUI package. c) Temperature dependence of ϵ_r and $\tan\delta$ for BF-BT-xBZN; (d) Spectroscopic plots of Z'' and M'' for BF-BT-0.05BZN.

Fig. 2. SEM images of polished surfaces for BF-BT-xBZN (a) BF-BT, (b) BF-BT-0.02BZN and (c) BF-BT-0.05BZN. EDS elemental mapping results of polished BF-BT-0.05BZN samples (d) Ba, (e) Ti, (f) Bi, (g) Fe, (h) O, (i) Zn, (j) Nb and (k) elemental layered image.

Fig. 3. a) Bright field TEM image of a grain in BF-BT-0.05BZN, illustrating a BiFeO_3 rich core and BaTiO_3 rich shell; $\langle 211 \rangle$ zone axis diffraction patterns reveal the absence of $\frac{1}{2}\{000\}$ superstructure reflections in the shell (up) compared with core regions (down). b) The BiFeO_3 and BaTiO_3 core-shell regions are tentatively ascribed to the high and low temperature dielectric anomalies.

Fig. 4. High electric field (a) bipolar P-E, (b) bipolar S-E and (c) unipolar S-E loops of BF-BT-xBZN samples at 100 kV/cm. (d) P_r and E_C as a function of BZN concentration. (e) S_{pos} and S_{neg} as a function of BZN concentration. (f) d_{33}^* and SH as a function of BZN concentration. d_{33} as a function of BZN concentration is in the inset of (d).

Fig. 5. Unipolar P-E loops under different electric fields for (a) BF-BT-0.05BZN and (b) BF-BT-0.08BZN. W , W_{rec} and η as a function of electric field for (c) BF-BT-0.05BZN and (d) BF-BT-0.08BZN.

Fig. 6. Time dependence of the pulsed discharge current for (a) BF-BT-0.05BZN and (b) BF-BT-0.08BZN. Time dependence of W_{rec} for (c) BF-BT-0.05BZN and (d) BF-BT-0.08BZN.

Fig. 7. In-situ temperature dependence of (a) J and (b) unipolar P-E loops for BF-BT-0.05BZN at an electric field of 120 kV/cm. (c) J as a function of temperature at different electric fields. (d) W , W_{rec} and η as a function of temperature.

Fig. 8. Comparison of (a) W_{rec} vs electric field and (b) strain vs d_{33}^* among lead-based and lead-free ceramics.^{12-25, 26-36, 48-92}

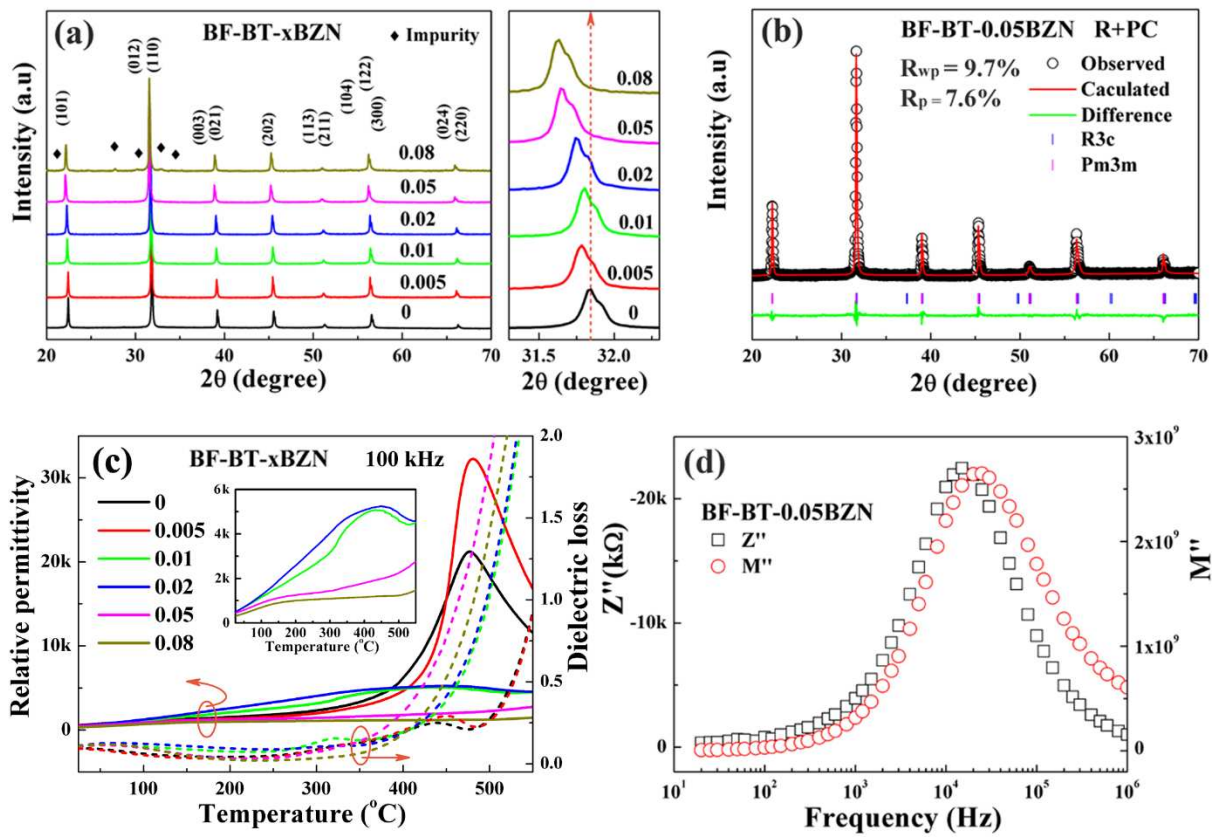


Fig. 1

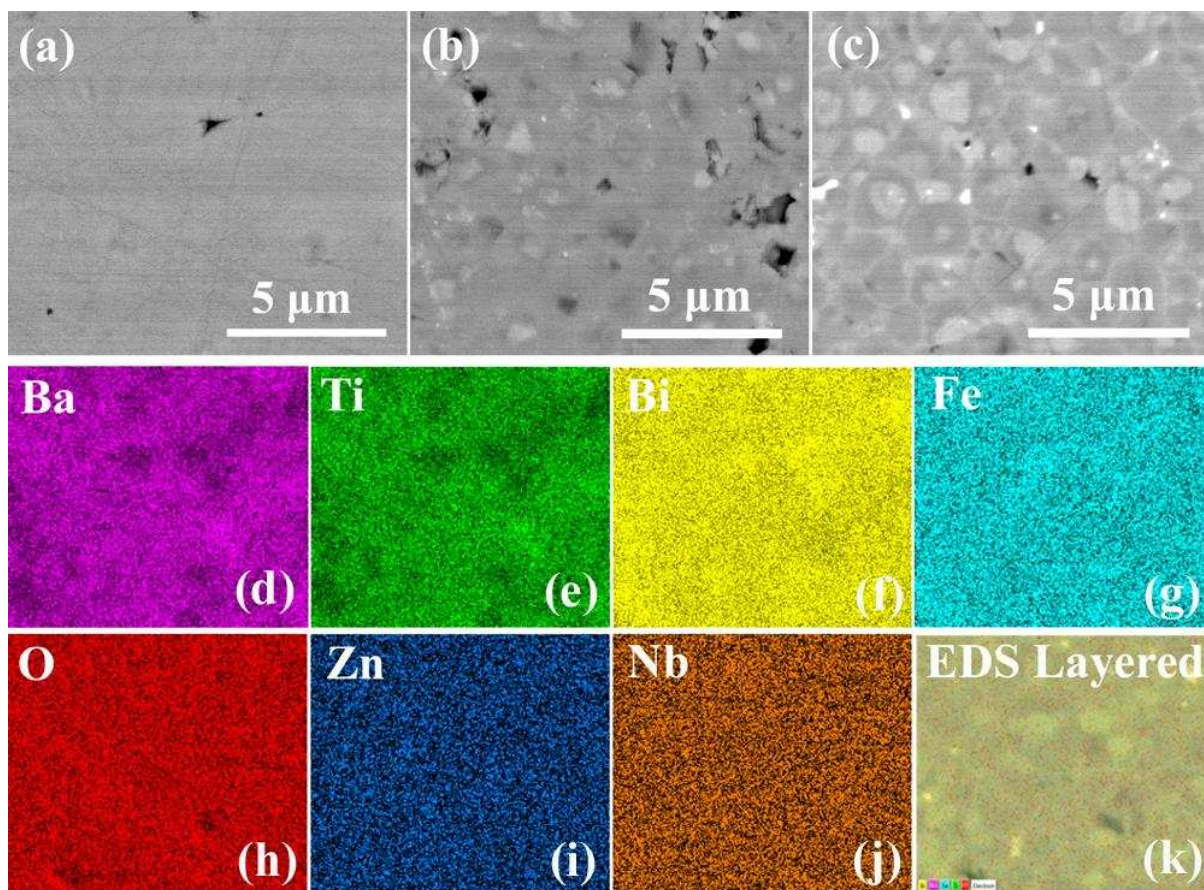


Fig. 2

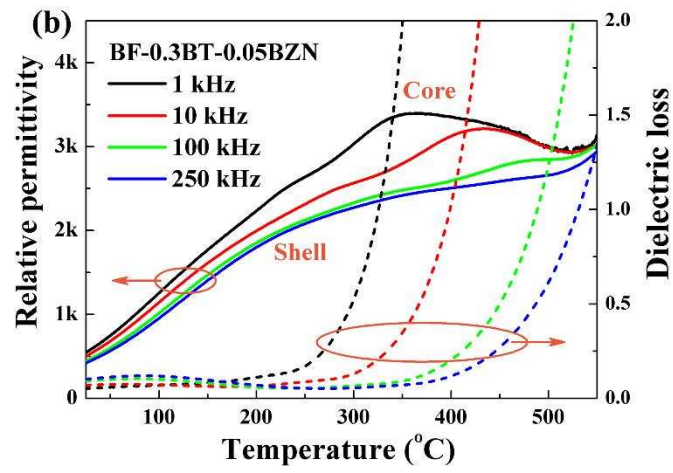
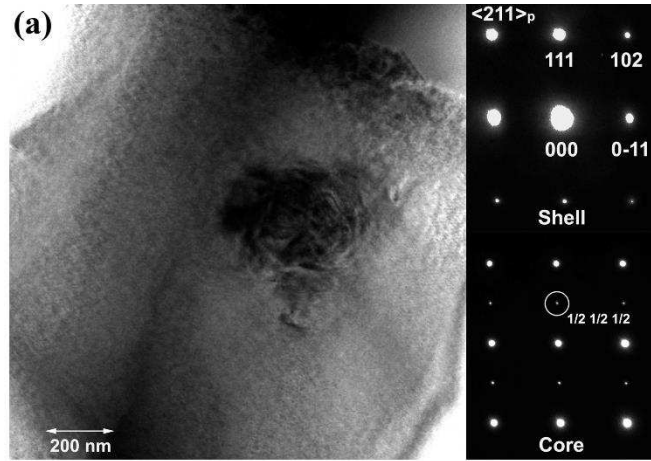


Fig 3

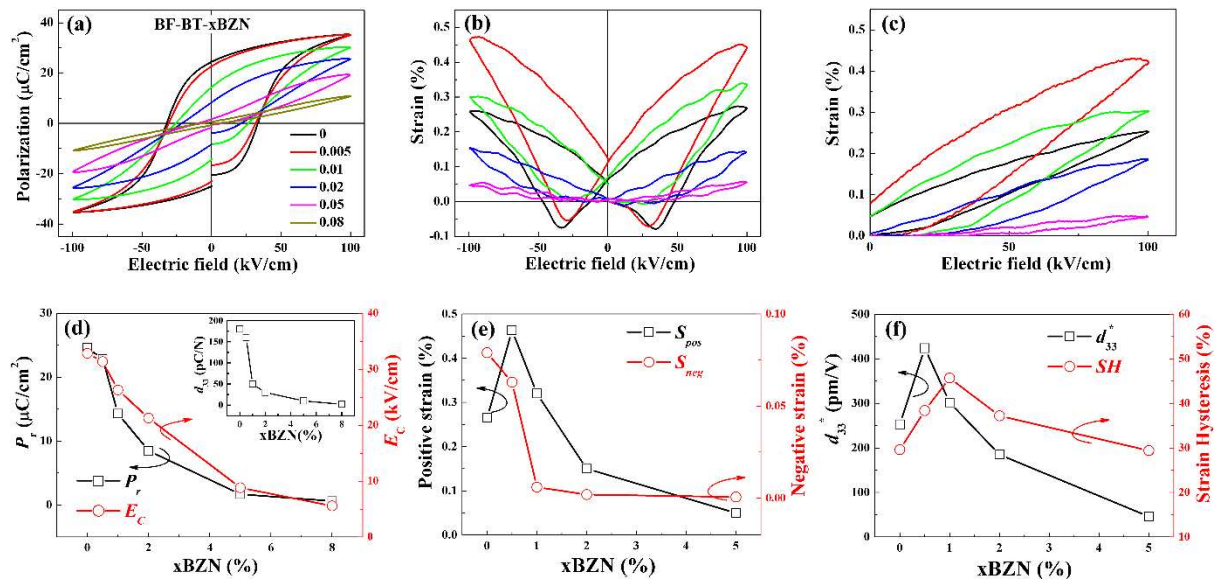


Fig. 4

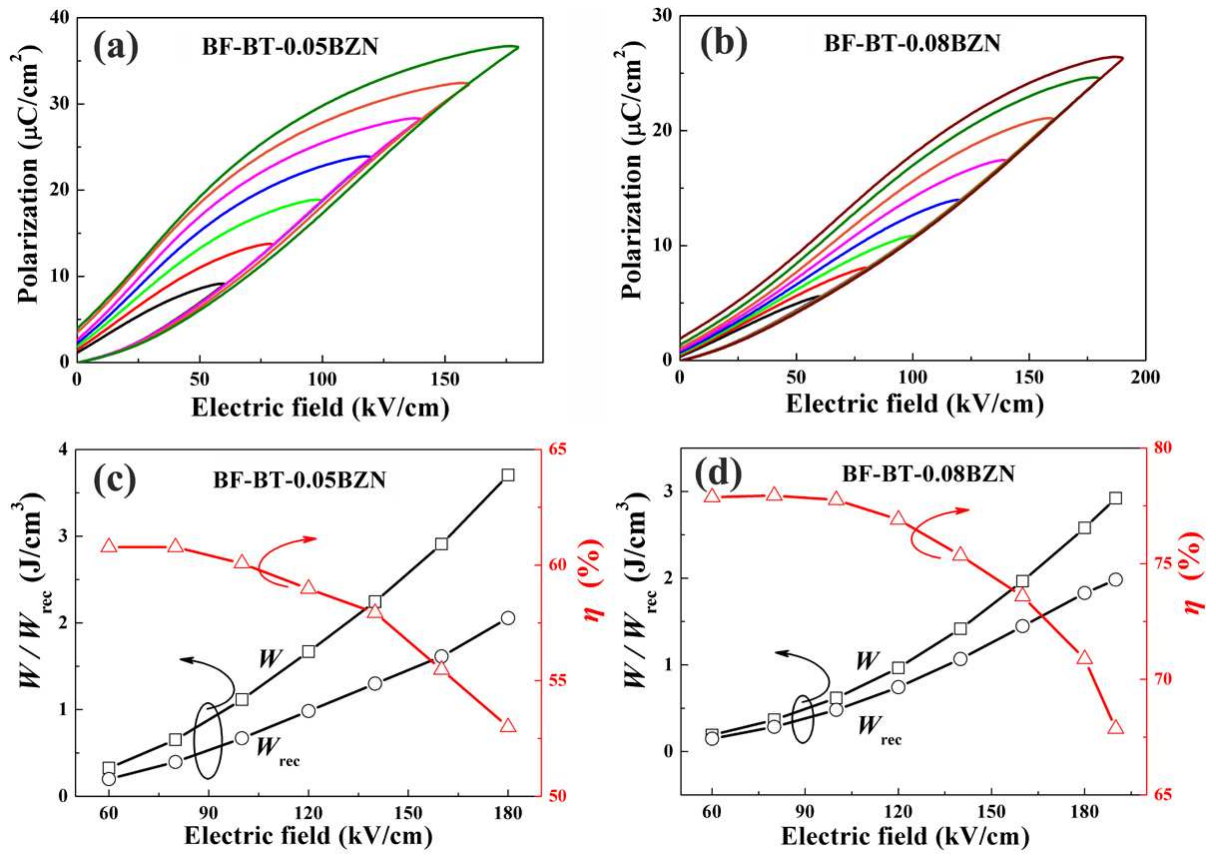


Fig. 5

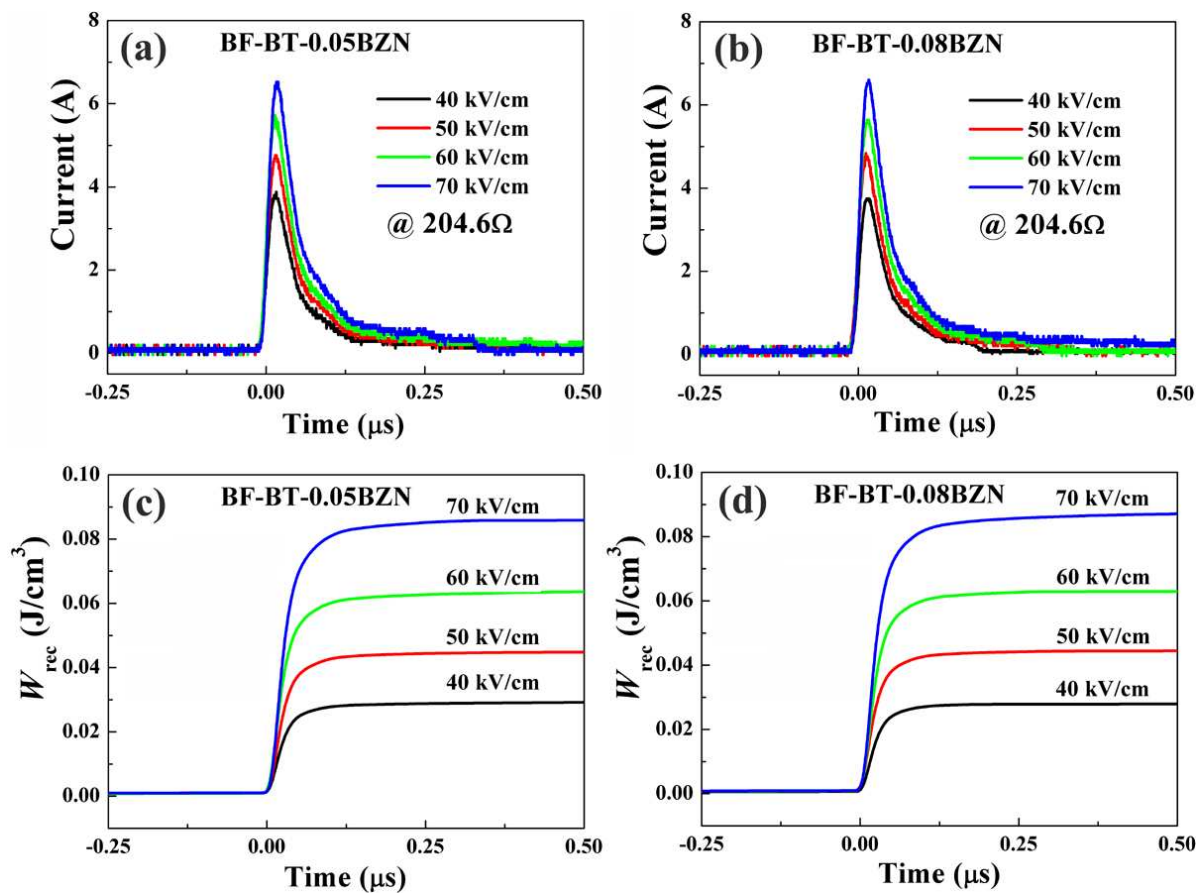


Fig. 6

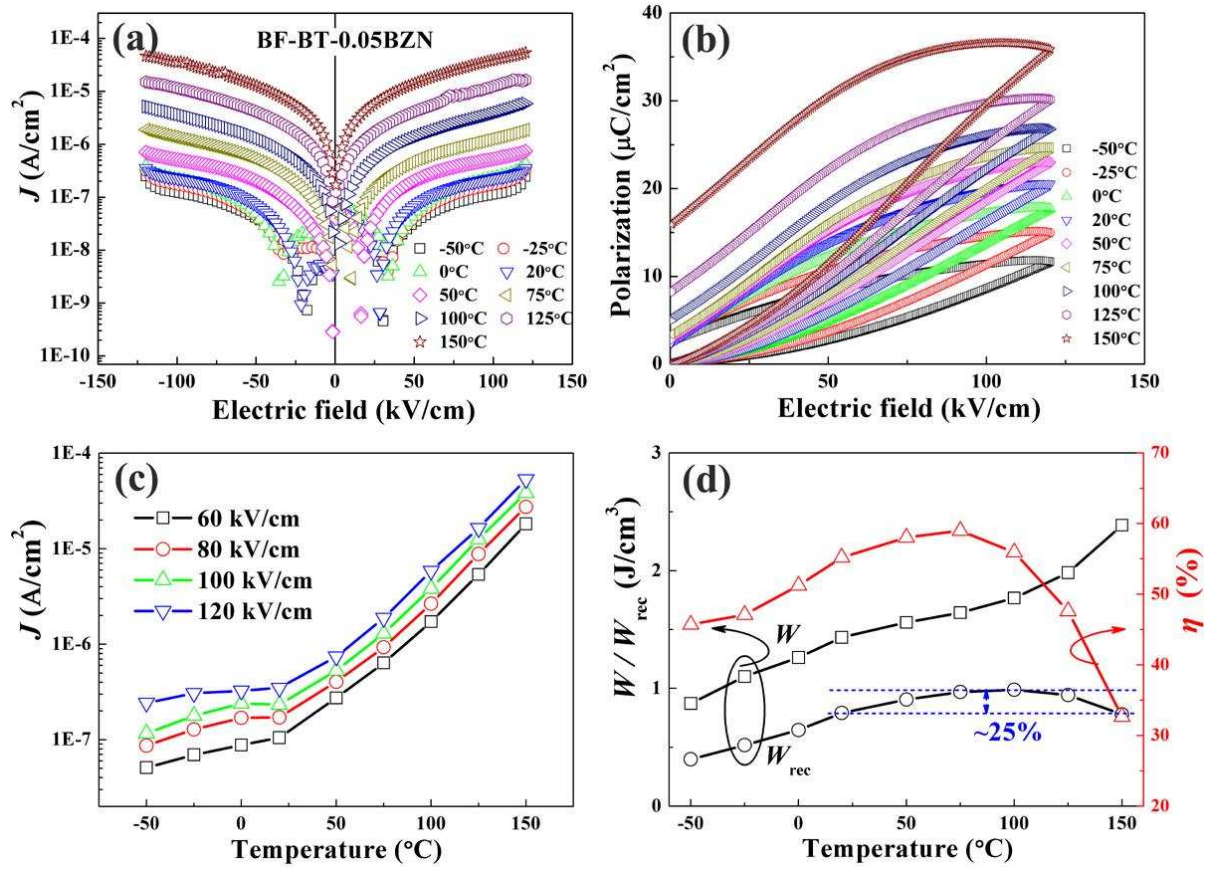


Fig. 7

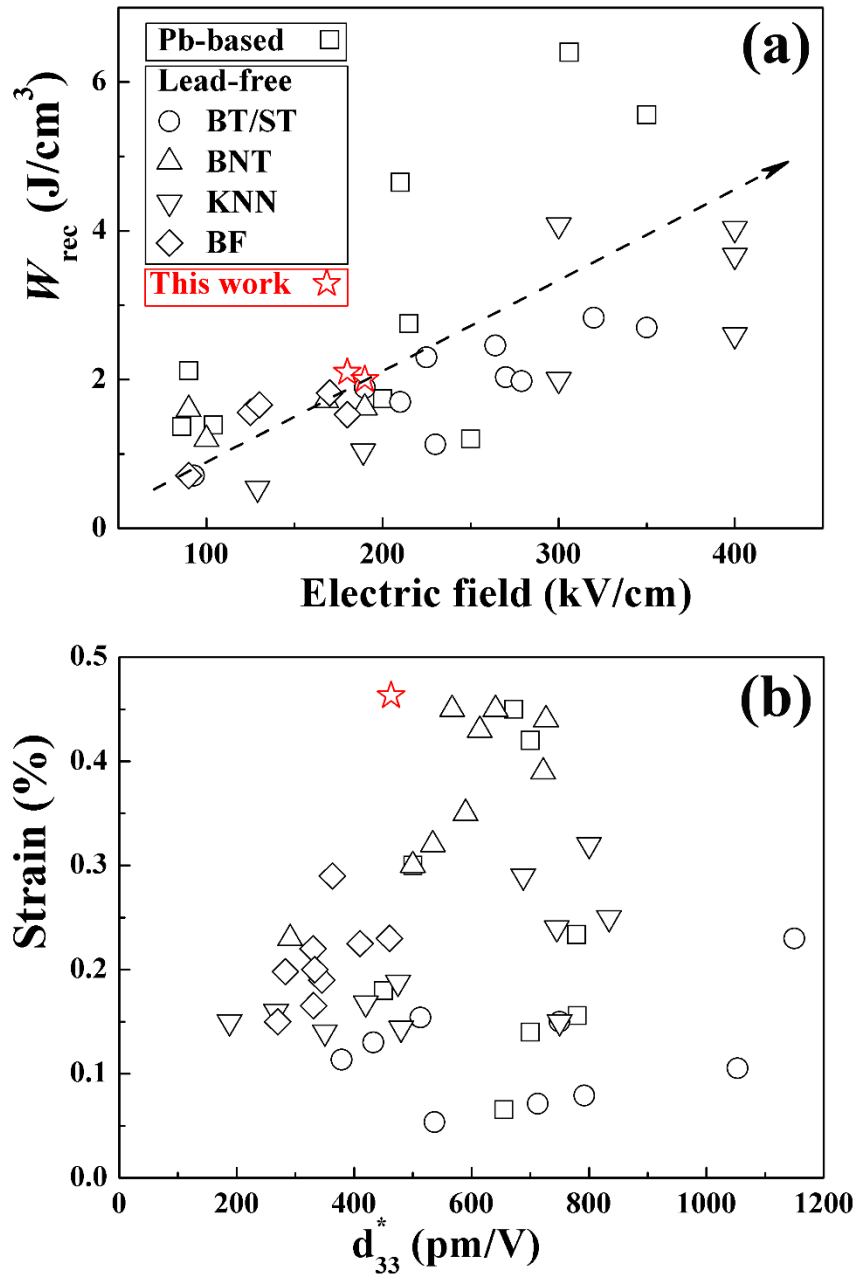


Fig. 8

Supporting Information

High Energy Storage Density and Large Strain in

Bi(Zn_{2/3}Nb_{1/3})O₃-Doped BiFeO₃-BaTiO₃ Ceramics

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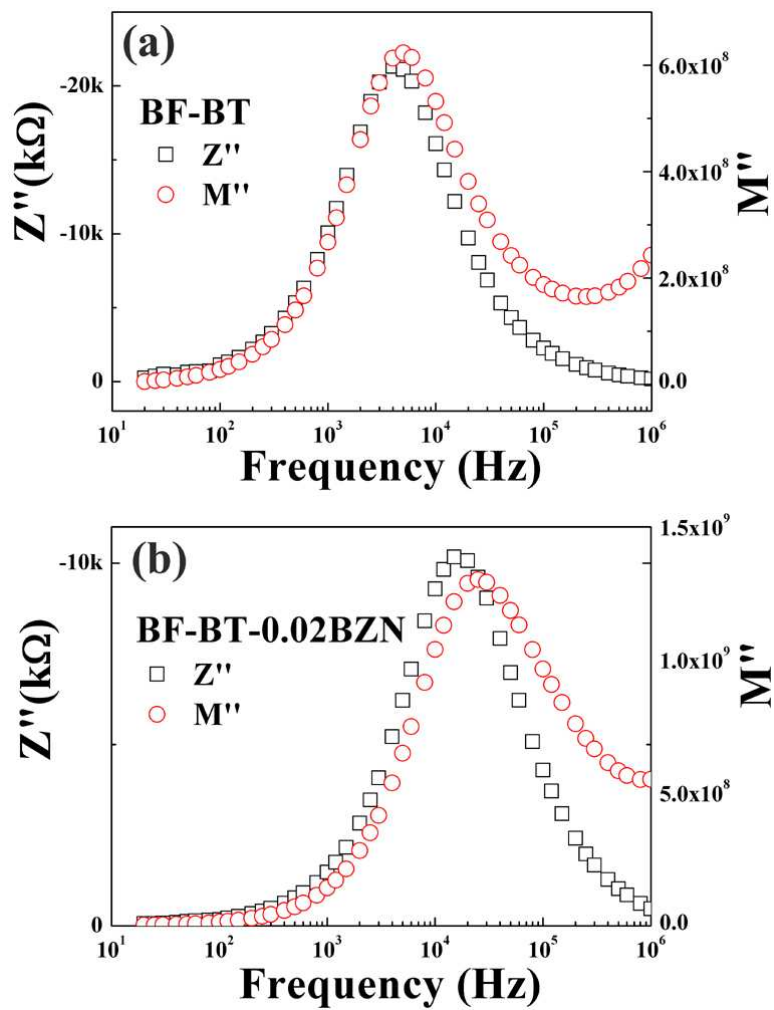


Figure S1. Spectroscopic plots of Z'' and M'' for (a) BF-BT and (b) BF-BT-0.02BZN.

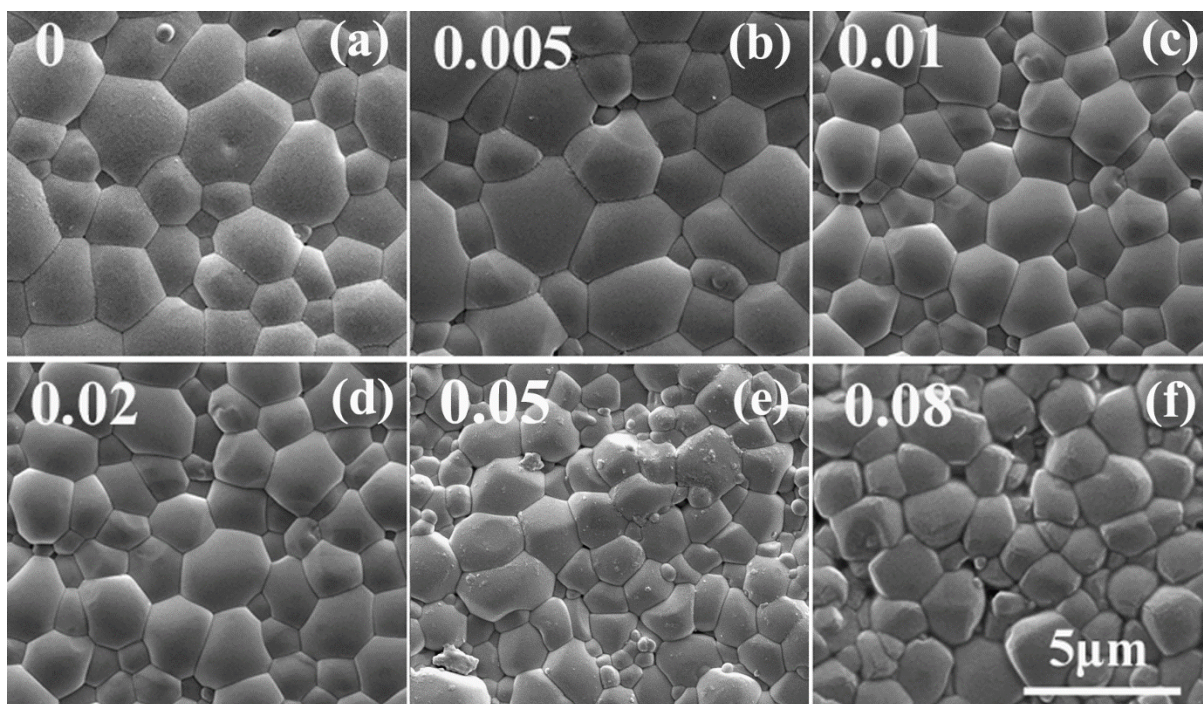


Figure S2. SEM images of BF-BT-xBZN (a) $x = 0$, (b) $x = 0.005$, (c) $x = 0.01$, (d) $x = 0.02$, (e) $x = 0.05$ and (f) $x = 0.08$.

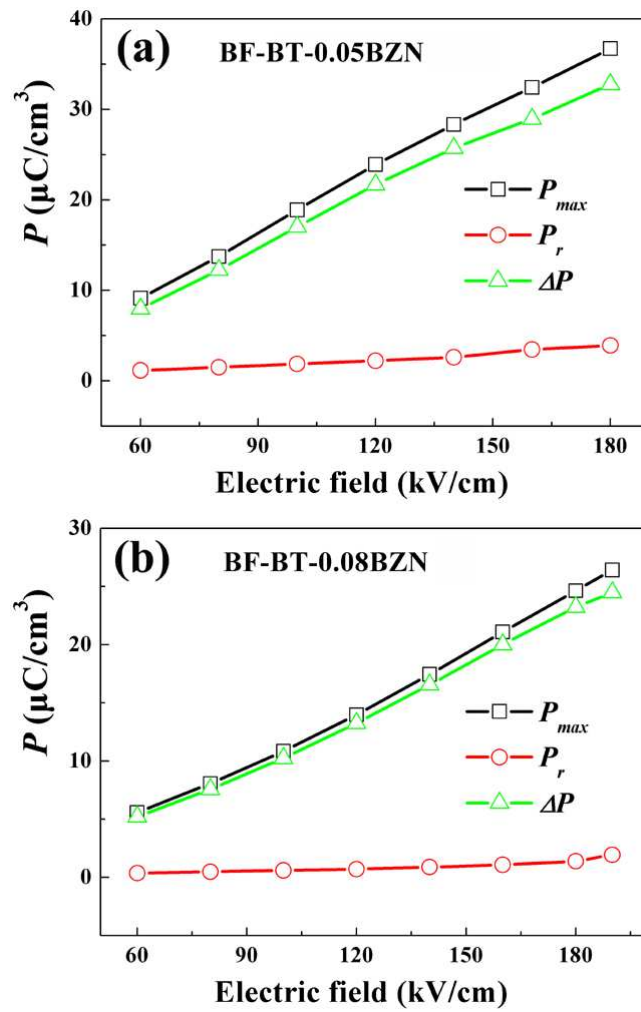


Figure S3. P_{max} , P_r and ΔP as a function of electrical field for (a) BF-BT-0.05BZN and (b) BF-BT-0.08BZN.

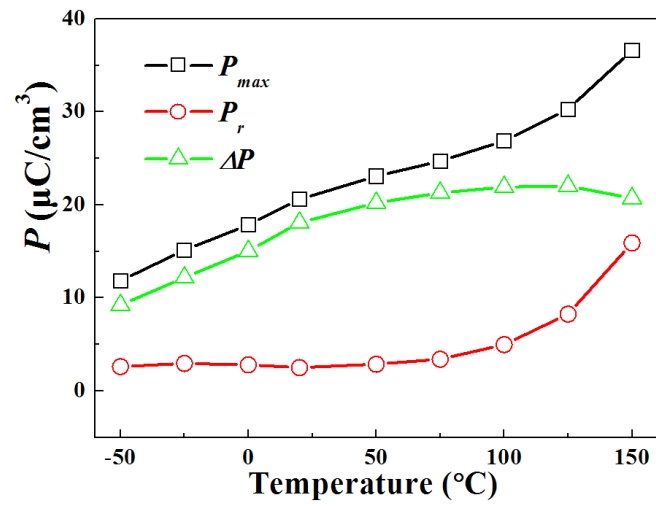


Figure S4. P_{max} , P_r and ΔP of BF-BT-0.05BZN as a function of temperature at 120 kV/cm.

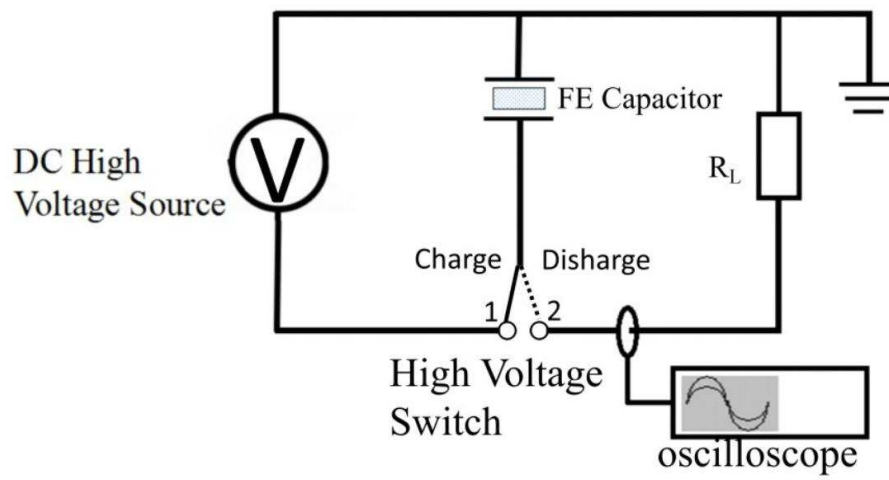
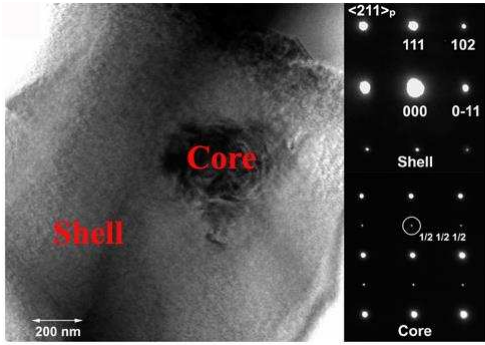
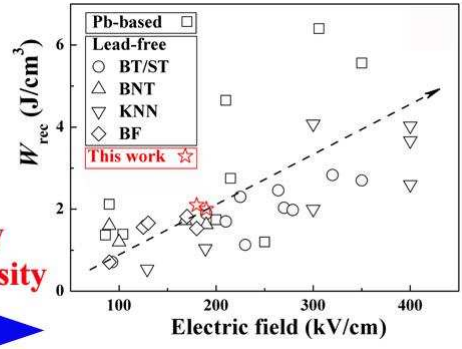


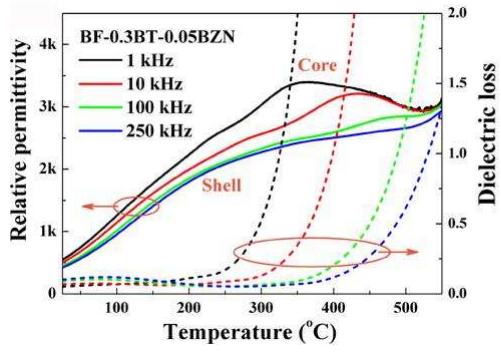
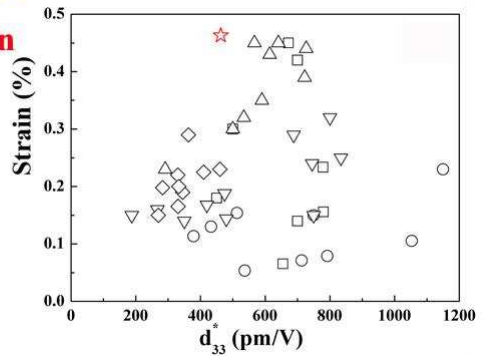
Figure S5. the schematic diagram of the discharge circuit.



High Energy Storage Density



Large Strain



TOC