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Programmable Medicine: Autonomous, Ingestible, Deployable Hydrogel Patch and Plug for Stomach Ulcer Therapy

Alexis du Plessis d'Argentré[1*], Samuel Perry[2*], Yoshitaka Iwata[3], Haruna Iwasaki[3], Eiji Iwase[3], Assunta Fabozzo[4], Iain Will[2], Daniela Rus[5], Dana D. Damian[6], and Shuhei Miyashita[2]

Abstract—Gastric ulcer is a chronic and complex (and often complete) erosion of the stomach wall that happens as a complication of a previous chronic, inflammatory process. It represents a catastrophic situation in which the patient is critical and its conditions need to be treated fast. This study presents a remotely navigatable and deployable ingestible patch and plug for gastric ulcer treatment. The patch/plug structure is made of agarose hydrogel that can change rigidity through hydration and dehydration. When dehydrated, it is rigid and can maintain a folded configuration so it can be ingested as a "pill". This can be guided to the targeted location by a magnetic field, and be deployed instantly by hydration, namely by supplying water from the mouth. Due to the deployable origami design, it exhibits an expansion of 10 times its initial surface area, making the device suitable for the use of dressing a surface as a patch, and filling a hole as a plug.

I. INTRODUCTION

Medical robotics has shown historic impact in healthcare, supporting surgeons to carry out surgeries in a minimally invasive way, as well as patients, e.g. by automatically regulating glucose levels in patients with diabetes [1]. The next frontier in the field is the realization of technologies that can carry out treatments non-invasively and without obstruction, minimizing the deleterious effects that a treatment or intervention can have on the human body. Programmable medicine is required for treating patients with chronic diseases as well as for shortening the time and complexity of medical and surgical interventions [2]–[4]. With its scale ranging from nanometer [5] to micrometer [6], and up to centimeter scale [7], it has found irreplaceable roles and provided new approaches to the field. Such medicine, however, often lacks programmability in comparison to traditional robotics because of the limited body space to carry electro-mechanical components, and because of the restricted number of usable materials in the human body. One of the current challenges is how to realize the intelligent materials from which programmable medicines are made, such that they can act autonomously in-vivo without human intervention.

Capsule endoscopy and some advanced models have been developed and used as efficient and non-invasive tools to

[1]Ecole Supérieure d'Electronique de l'Ouest, France. [2]Department of Electronic Engineering, University of York. Heslington, York, YO10 5DD, UK. `shuhei.miyashita@york.ac.uk` [3]Department of Applied Mechanics, Waseda University, Japan. [4]Hospital of Padua, Italy. [5]Computer Science and Artificial Intelligence Laboratory, MIT, USA. [6]Department of Automatic Control and System Engineering, Centre of Assistive Technology and Connected Healthcare, University of Sheffield, UK. *Alexis du Plessis d'Argentré and Samuel Perry contributed equally. Support for this work was provided by the Department of Electronic Engineering, University of York.
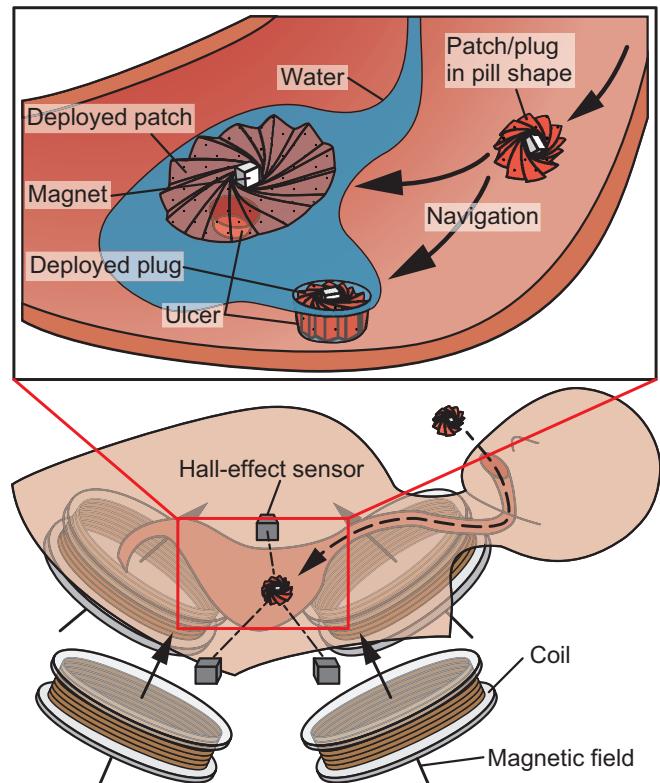
Fig. 1. The use scenario of programmable patch and plug. The patient, who has an ulcer in the stomach, ingests the origami structure folded into its pill form. After the pill reaches the stomach, it is remotely navigated to the location of ulcer by an external magnetic field. Once in place, the patient drinks water, which causes an instant deployment of the structure, reconfiguring it into a patch or plug. The structure is held in position by the magnetic field during and after deployment.

diagnose various gastrointestinal diseases [8]–[11]. Some models focus on the release of medicine [12], [13]. Some devices feature reconfigurability [14]–[16] and conduct various tasks such as becoming a stent [17], or feature functionality such as carrying out biopsies or releasing drugs [18]–[20].

For the replacement of surgical stitches and staples, various types of in-vivo patch/sealant for ulcer closure have been developed. Fibrin glue is one of the most common materials, although the adhesion it provides is relatively weak [21]. Recent developments have yielded bio-compatible sealants usable in both wet and dry conditions; chemical sealants such as glue-based adhesives [22], poly-based adhesives including hydrogels [23], [24], and mechanical sealants such as ulcer-dressing patches including a bio-inspired one [25], [26].

Most of the patches/sealants are currently used for surgical purposes and must therefore be both simple to use and reliable.

This study aims to develop a "programmable pill" that a patient with perforated gastric ulcers and general gastrointestinal lesions can simply swallow, especially in an emergency situation, which aids in the healing of the affected area (Fig. 1). This pill has an embedded magnet at the center, which allows it to be guided through the stomach towards the ulcer site using an external magnetic field. Once at the site, the structure deploys, patching or plugging the ulcer. In our previous work, we developed a bio-degradable origami device that can remove a foreign obstacle such as a button battery and also act as a patch and release a drug to treat an ulcer in the stomach [27]. This work further develops the device [28], [29], and describes a newly designed biodegradable, instantly water activated, highly deployable origami structure for ulcer treatment in the stomach. While there exist some approaches to patches that focus on chemically-activated bonding to the tissue [22]–[24], in this work the structure realizes a mechanical contact to the wounded site through either an expansion to fill and plug a wound, or a patch being held in place using a constant magnetic field. The structure can expand its surface area to 10 times its initial size by absorbing water, typically within a minute. The robot can be autonomously navigated to the wound site and can deploy as a patch or deploy as a plug to fill a hollow wound. The navigation was developed based on our previous work in [30], but with fewer sensors, in that three 3-axis hall-effect sensors detect the 3D position and orientation of a magnet using a localization method.

The contributions of this paper are:

1) Development of an autonomous, ingestible, deployable patch and plug for gastric ulcer treatment.
2) Method of realizing the quick and expanding agarose hydrogel sheet by hydration.
3) Geometric analysis of origami sheet deployment with a mathematical model.
4) Demonstration of 3D localization, automatic control, deployment, and patching and plugging in sequence.

In the following sections, we first explain the methods of origami structure design and fabrication (Sec II), followed by 3D localization method for navigation (Sec III), then we show experimental results (Sec IV), we discuss and conclude the study (Sec V).

II. METHODS

A. Deployable Origami Patch/Plug Design

The deployment of the origami structure relies on the shape memory properties of dried agarose hydrogel. When dried in a particular shape, an structure made of agarose can be deformed to any new shape, and will return to its original shape when placed in water. We take advantage of this property by drying our structure in the unfolded origami shape, then folding it up into its smaller form when dry. Fig. 2 shows the origami structure in both its folded and
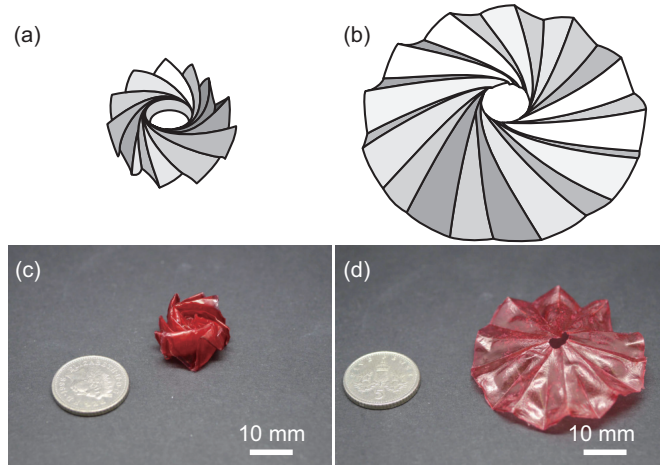

Fig. 2. The deployable origami structure. (a),(c) Folded "pill" state, (b),(d) deployed state.

deployed forms. For this study, the origami structures were made to be $5\,\mathrm{cm}$ in diameter when it fully deployed, but the design could easily be scaled to work with different sized structures depending on the task requirement.

Fig. 3 (a) and (b) show the folded and fully deployed forms of the origami structure from both the top and side view. We explain the design principle for optimizing the expansion rate and targeted thickness using the following variables and constant values:

- $n_c \geqq 6$ [-]: Number of folding creases; must be at least 6 to make a hole in the center of the origami structure
- $r_{out}(n_c)$ [mm]: Outer radius in the folded state
- $r_{in}(n_c)$ [mm]: Inner radius in the folded state
- R_{out} ($= 25\,\mathrm{mm}$): Outer radius in the deployed state
- R_{in} ($= 2.5\,\mathrm{mm}$): Inner radius in the deployed state; radius of a hole provided at center of origami structure
- $t(n_c)$ [mm]: Thickness of origami structure in the folded state
- T ($= 0.2\,\mathrm{mm}$): Thickness of origami structure in the deployed state (thickness of agarose patch)
- $s(n_c)$ [mm^2]: Area of the origami structure in the folded state
- S [mm]: Area of the origami structure in the deployed state
- $v(n_c)$ [mm^3]: Volume of the origami structure in the folded state
- i [-]: Number of overlapping sections of agarose
- k_i [mm]: Length of overlapping crease line
- K [mm]: Length of crease line in the deployed state

The thickness of the origami structure at the folded state can be geometrically defined from Fig. 3 (a) and (b) as:

$$t(n_c) \sim \sqrt{R_{out}^2 - R_{in}^2} \sin\left(\frac{2\pi}{n_c}\right). \tag{1}$$

We now model the area of the origami structure in its folded state. Fig. 3 (c) shows a schematic we can use to determine the number of overlapping sections of agarose i. The actual origami structure in its folded state has several overlapping
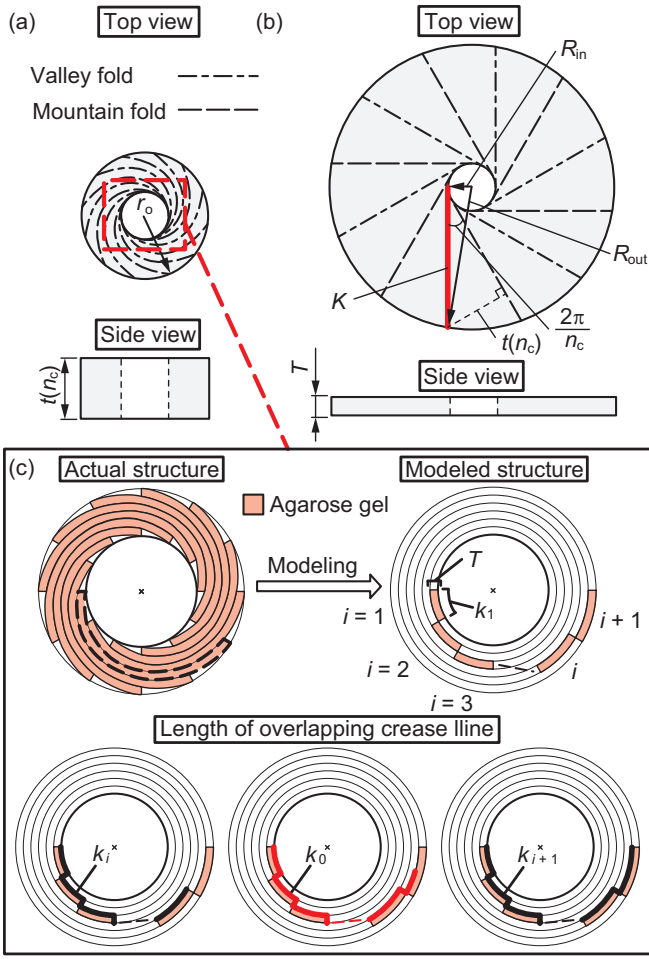
Fig. 3. Schematics of the origami structure. (a) Folded state. (b) Fully deployed state. (c) Schematics to determine the number of overlapping sections. Red line K is the length of crease line at deployed state. Black lines (k_i and k_{i+1}) are the assumed length to determine the number of overlapping sections i.

sections, like the left image of Fig.3 (c). To determine the number i, we modeled the overlapping sections as shown to the right image of Fig.3 (c). When the number of over lapping sections is $i = 1$, the length of each crease line is:

$$k_1 = \frac{2\pi R_{in}}{n_c}. \tag{2}$$

When the number of over lapping sections is $i = 2$, the radius is larger by the thickness of the agarose patch T. The length of each crease line is then:

$$k_2 = \frac{2\pi R_{in}}{n_c} + \frac{2\pi (R_{in} + T)}{n_c}. \tag{3}$$

If the number of overlapping sections is i, the length of each crease line is defined as:

$$k_i = \frac{2\pi}{n_c}\left[R_{in}i + T\frac{(i-1)i}{2}\right]. \tag{4}$$

The length of the crease lines at deployed state K must be between k_i and k_{i+1}:
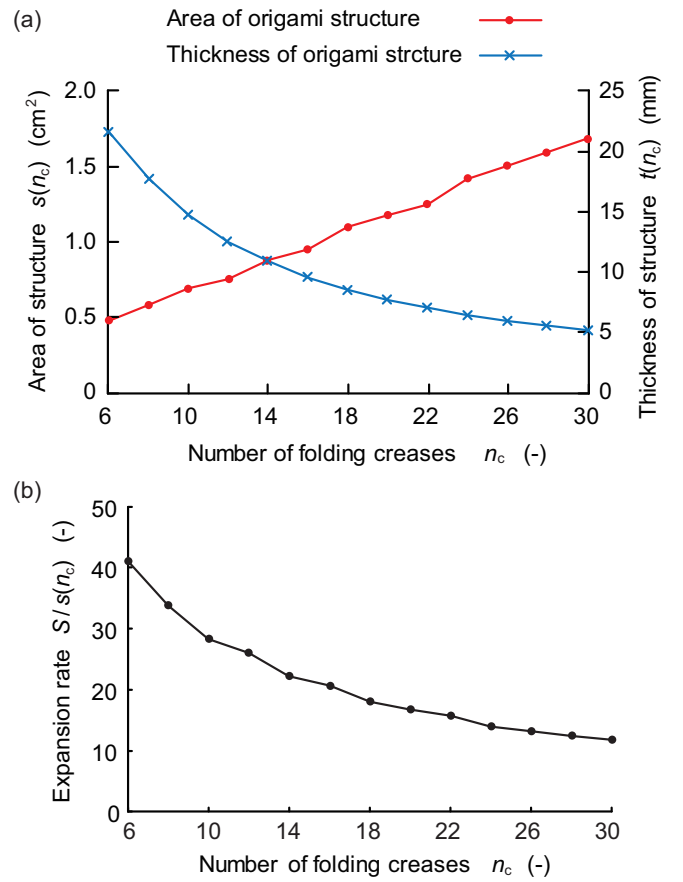
$$k_i \leqq K < k_{i+1}. \tag{5}$$

Fig. 4. Geometric analysis of the origami structure. (a) Area and thickness of the structure in its folded state over the number of creases. (b) Expansion rate of the surface over the number of creases.

When the previous eq. (5) is satisfied, the number of overlapping sections of agarose i is defined. eq. (5) is expressed using eq. (4) to:

$$\frac{2\pi}{n_c}\left[R_{in}i + T\frac{(i-1)i}{2}\right] \leqq \sqrt{R_{out}^2 - R_{in}^2}$$
$$< \frac{2\pi}{n_c}\left[R_{in}(i+1) + T\frac{i(i+1)}{2}\right]. \tag{6}$$

We can get the number of overlapping sections of agarose i by calculating eq. (6). The outer diameter of the patch in its folded state $r_{out}(n)$ is shown using i:

$$r_{out}(n_c) = R_{in} + Ti. \tag{7}$$

Thus, the area and volume of the folded structure are given by:

$$s(n_c) = \pi r_{out}^2, \tag{8}$$

$$v(n_c) = st. \tag{9}$$

Fig. 4 shows a geometric analysis of the origami design. As shown in Fig. 4 (a), the vertical axes represent the area of the origami structure $s(n_c)$ and thickness of the origami structure in its folded state $t(n_c)$. The horizontal axis represents the number of folding creases n_c. When

the number of folding creases is increased, the area of the origami structure increases linearly. Conversely, the thickness of the folded origami structure decreases to convergence as the number of creases is increased. Fig. 4 (b) shows the expansion rate of the origami structure (from its folded state to the deployed state). The expansion rate is calculated using:

$$\frac{S}{s(n_{\mathrm{c}})} = \frac{\pi R_{\mathrm{out}}^2}{\pi r_{\mathrm{out}}(n_{\mathrm{c}})^2} = \frac{R_{\mathrm{out}}}{r_{\mathrm{out}}(n_{\mathrm{c}})}. \qquad (10)$$

The vertical axis represents the expansion rate of the surface area, and the horizontal axis represents the number of folding creases. The expansion rate decreases gently as the number of folding creases is increased. Using these results, the desired folded state for an origami structure can be designed.

When the origami structure has fewer creases, it is easy to fold during fabrication, however these creases will be long and narrow, so a thicker structure with a smaller area is developed. The long and narrow structure may not stand stably. Considering these results and the fabrication process, we decided to use $n_{\mathrm{c}=20}$ as our number of folding creases to develop a stable and easily fabricated origami structure.

B. Fabrication

Fig. 5 shows the fabrication process of the origami structure. The structure is fabricated using Melford MB1200 Agarose powder and water mixed at a ratio of $1 : 100$ by mass. The solution is mixed in a beaker which is covered and placed in a larger beaker of water heated to $90°$C. Once the agarose powder has dissolved fully, the solution is poured into a container to cool and solidify Fig. 5 (a). For our
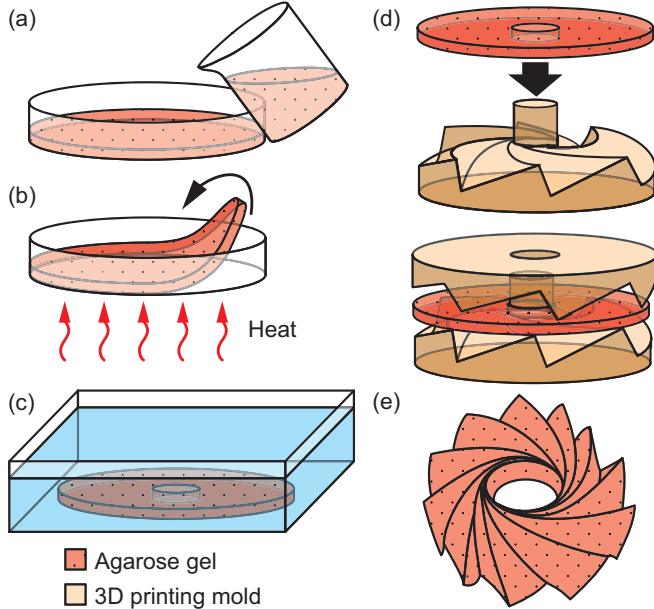

Fig. 5. Fabrication process of the origami structure. (a) Pour liquid agarose hydrogel into a petri dish. (b) Cure in the oven for approximately 5 hours at $45°$C until dry, then peel off. (c) Place the patch in water for 1 min to re-hydrate and soften. (d) Place the patch in the mold, with the lid on, and leave to dry. (e) Once dry, fold the structure. A magnet is attached at the centre of the structure before use.

experiments, red food colouring was added before pouring the solution out. The thickness of the gel here determines the thickness of the final dried agarose which makes up the origami structure. We found that a gel thickness of approximately $4\,$mm gives the best result for both strength and flexibility of the patch. The gel takes around $10\,$min to set. It is then placed in an oven to dry out (cure) at $45°$C, for around 5 hours Fig. 5 (b). Curing the agarose outside of the mold allows the gel to dehydrate evenly with no internal mechanical stress. This unstressed, relaxed, state is that of the deployed structure. Once cured, the agarose is cut to the diameter of the 3D printed origami mold, then it is placed in water for $1\,$min to partially re-hydrate Fig. 5 (c). The agarose gel will only reabsorb a relatively small amount of water compared to what was lost in the curing stage (Pre-curing agarose sections weigh around $14\,$g. Post curing agarose sections weigh around 0.2g. After re-hydration the agarose sections weigh around 0.8g). At this point, the softened gel is pressed into the mold and allowed to dry out once more Fig. 5 (d). This is done to form the creases along which the agarose is folded in order to package the structure for deployment. It also determines the shape that the structure will return to after deployment. The dried structure is then folded along the creases into the packaged, pleated shape. This induces locked-in strain in the folded areas Fig. 5 (e). When fully hydrated, during deployment, the structure will return to the molded shape. This is because internal strain relaxation occurs within the gel structure after re-hydration, during deployment. This strain induced 'shape memory' forms the basis of the structure deployment. The shape can be reprogrammed by wetting the structure and drying it again in the desired shape. The final step of the fabrication is adding the magnet. We use two cubic neodymium magnets oriented perpendicularly to the surface of the agarose to pinch the structure from either side, avoiding the need for an adhesive.

III. Localization and Navigation

A. Electromagnetic Coil Platform

We use the coil system to control a magnet embedded within the origami structure, autonomously guiding it to the target area before deployment. The control system consists of four pairs of coaxial electromagnetic coils, with each pair consisting of one larger and one smaller coil. These coils are set up below the operating stage at an angle of $\frac{\pi}{4}$ radians to the horizontal, ensuring the point of intersection of the magnetic fields is at the centre of the stage. The system uses the superposition of the magnetic fields from each of the four coil pairs to create a net magnetic field [28]. Since the amplitude and direction (positive or negative) of the field from each coil can be controlled, the net field can be oriented in any direction in 3D space. Altering this net magnetic field allows us to produce the necessary force and torque to manoeuvre a magnet on the operating stage. The actuation of the pill is done by applying a rotating magnetic field of approximately $1.4\,$mT which causes the magnet to rotate in the same way, as it magnetically aligns itself. The application of the rotational magnetic field is repeated until

(a)

(b)

Sensor 3

Sensor 1   L = 100 mm   Sensor 2

Caption
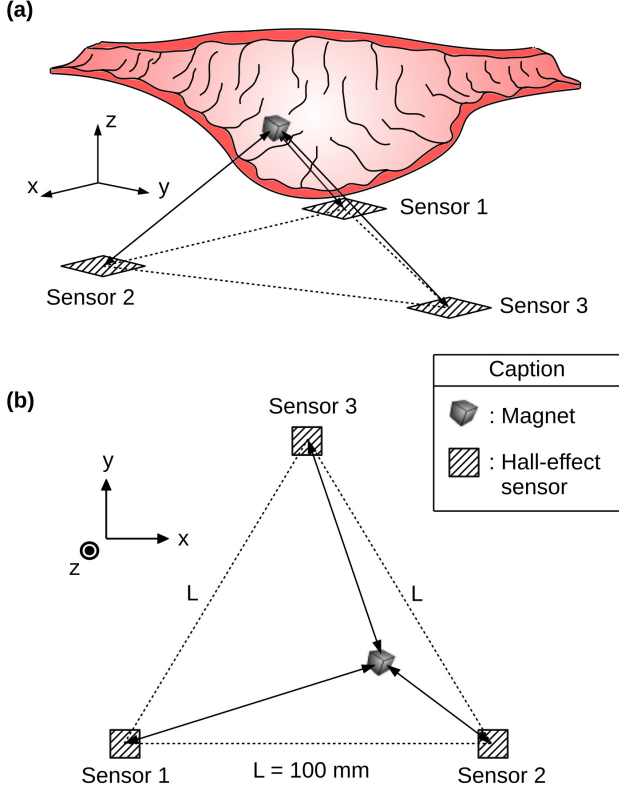
: Magnet

: Hall-effect sensor

Fig. 6. Schematics of 3D magnetic localization. (a) Angled view. (b) Top view.

the structure reaches the targeted location (see Sec III-B). Currents running in the coils are controlled using an Arduino DUE microcontroller, along with four motor-drivers (Syren 50, Dimension Engineering) which communicate via serial.

B. Localization and Navigation

For the navigation of the pill, we developed a magnetically achievable localization system that utilized only three hall-effect sensors. The hall-effect sensors (Freescale MAG3110, a small 3-axis PCB mounted magnetometer able to measure fields of $\pm1000\,\mu$T with a sensitivity of $0.10\,\mu$T) are placed at the vertices of a $100\,$mm edged equilateral triangle (Fig. 6). The position of the magnet is detected by trilateration with the readings from the sensors. The sensors are connected to the Arduino DUE, communicating via the I2C protocol. Since the sensors have the same fixed I2C address (0x0E) and the Arduino DUE has only one set of I2C pins (SDA and SCL), an I2C multiplexer is incorporated to allow multiple sensors to be used. The magnetic field density $\vec{B}(\vec{r})$ measured by a hall-effect sensor at location $\vec{r}$ with respect to the sensor location is:

$$\vec{B}(\vec{r}) = \frac{\mu_0}{4\pi}\left[\frac{3(\vec{m}\cdot\vec{r})\vec{r}}{\|\vec{r}\|^5} - \frac{\vec{m}}{\|\vec{r}\|^3}\right], \tag{11}$$

where $\vec{m}$ is the magnetic moment of the magnet and μ_0 is the permeability of free space.

Localization of the magnet is achieved by first taking a reading from one sensor. This value corresponds to the distance of the magnet from the sensor and can be used as the radius for a sphere, centred on the sensor, on which the magnet must lie. The measurement is repeated for the other two sensors, giving us three spheres which we can use to calculate the magnet position by trilateration. To do this we must find the intersection points (x, y, z) of the three spheres. Referring to Fig. 6, and assuming Sensor 1 is at the origin of the Cartesian space, we can derive the equations of the three spheres. We know that Sensor 1 is positioned at $(0,0,0)$, Sensor 2 at $(0,l,0)$, and Sensor 3 at $(\frac{l}{2}, \frac{\sqrt{3}l}{2}, 0)$, so we get:

$$\begin{cases} \textbf{Sphere1}: r_1^2 = x^2 + y^2 + z^2, \\ \textbf{Sphere2}: r_2^2 = (x-l)^2 + y^2 + z^2, \\ \textbf{Sphere3}: r_3^2 = \left(x-\frac{l}{2}\right)^2 + \left(y - \frac{\sqrt{3}l}{2}\right)^2 + z^2, \end{cases} \tag{12}$$

where r_n is the distance of the magnet from sensor n and thus the radius of sphere n. We use (11) - (13) to find the intersections of the three spheres, which are:

$$\begin{cases} r_1^2 = x^2 + y^2 + z^2 \\ r_2^2 = (x-l)^2 + y^2 + z^2 \\ r_3^2 = (x-\frac{l}{2})^2 + (y - \frac{\sqrt{3}l}{2})^2 + z^2 \end{cases} \tag{13}$$

Resolving to get the position (x, y, z) of the magnet:

$$\begin{cases} x = \frac{r_1^2 - r_2^2 + l^2}{2l}, \\ y = \frac{1}{\sqrt{3}l}(l^2 - xl - r_3^2 + r_1^2), \\ z = \pm\sqrt{r_1^2 - y^2 - x^2}. \end{cases} \tag{14}$$

This gives us 2 solutions: one where z is positive and one where z is negative. We use the positive solution since we ensure that the origami structure is always above the sensors.

To convert the values from the sensors to distances in millimeters, we took measurements at set distances from the magnet (every $5\,$mm between 0 and $150\,$mm). We approximated the equation for the distance from the sensor by adding a power-type trend line. This way, we can determine the distance d of the magnet from a sensor s as a function of the norm of the sensor values on each axis:

$$\text{norm}_s = \sqrt{x_s^2 + y_s^2 + z_s^2}. \tag{15}$$

The three sensors have similar equations, which can be averaged as:

$$d(\text{norm}_s) = 380 \cdot \text{norm}_s^{-0.385}. \tag{16}$$

Testing of the localization system using a magnet placed at various points on a $10\,$cm diameter circle centered on the midpoint of the three sensors determined that the average position error for the system is $3.6\,$mm.

C. Anchoring

To anchor the pill in place over the target, we apply a strong magnetic field which acts on the magnet. Since the magnetic moment of the pill is oriented towards the top of the pill, the applied magnetic field is oriented parallel to the pill to avoid moving it. The magnetic field gradient generated by the coils attracts the pill towards the surface, holding it in

place. The magnetic flux density applied is $5\,\mathrm{mT}$, which is strong enough to anchor the pill to the ulcer when water is poured over it. This anchoring field is automatically enabled once the pill reaches the ulcer.

IV. Experimental Results

A. Path Following

Fig. 7 shows the experimental results of the trajectories obtained with a cubic magnet with a rolling motion (shown in blue lines) and the targeted circular trajectories (shown in red, diameters are $8\,\mathrm{cm}$ and $10\,\mathrm{cm}$). The magnet was placed on a flat surface and was able to follow a circular path accurately enough for our purpose. The movement of the magnet was recorded using Tracker software to compare the actual trajectory of the magnet to the desired one.
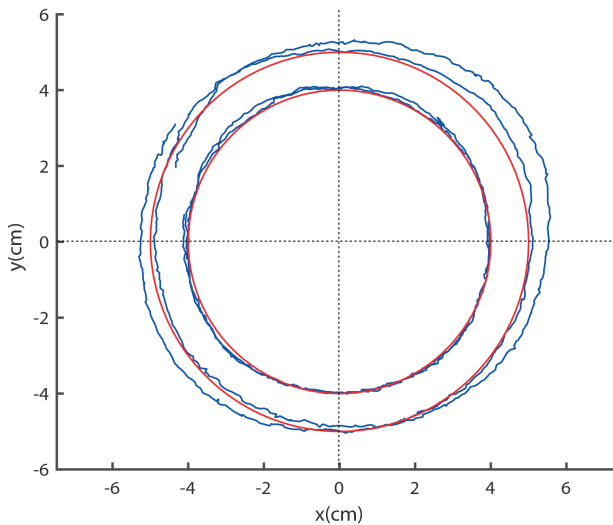

Fig. 7. Targeted paths (red) and experimentally measured magnet trajectories (blue; the magnet travelled along the circular path twice for each experiment). Path diameters are $8\,\mathrm{cm}$ and $10\,\mathrm{cm}$.

In order to autonomously guide the pill to an ulcer, we first need to know the position of both the pill and the ulcer. Our localization system gives us the position of the pill, and the ulcer can be located using ultrasound or a similar medical imaging technique. Once the positions are known, a path for the pill can be planned. In our experiment on a 2D surface, the path is set straight. The pill then rolls in the direction of the ulcer, stopping after each full rotation (by turning off the coils) for $2.5\,\mathrm{s}$ to obtain sensor readings for localization without any magnetic interference from the coils. Once located, the path of the pill is recalculated.

B. Patch Deployment

The deployment speeds of the origami structure were measured by pouring water at room temperature ($20^\circ\mathrm{C}$) and at body temperature ($37^\circ\mathrm{C}$) onto the pill. The results, plotted in Fig. 8, show that an increase in temperature has the effect of speeding up the deployment process of the structure. These plots were traced with a Matlab script which detects
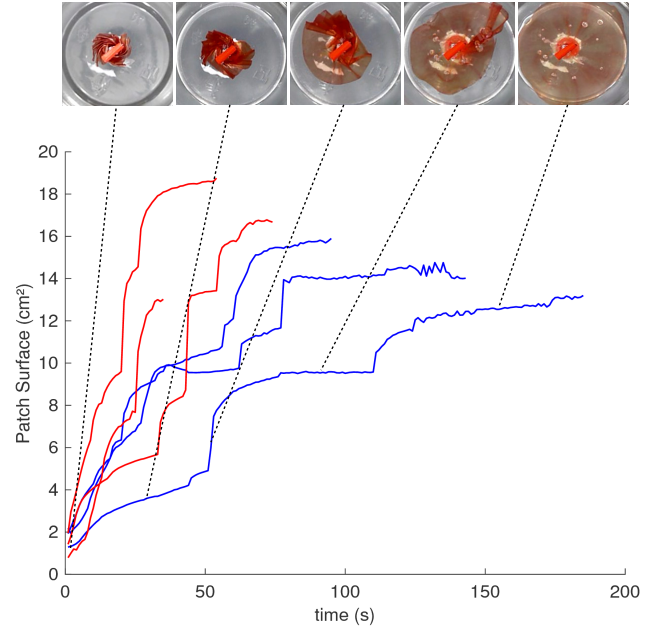

Fig. 8. Origami structure diameter against time during deployment. Temperature has a significant effect on the time taken for the structure to deploy. Red line is with $37^\circ\mathrm{C}$ water and blue line is with $20^\circ\mathrm{C}$ water.

the surface area of the patch. It should be noted that the initial and final surface areas stay similar for the two cases. For both, the area expanded to about 10 times its initial size.

C. Entire Demonstration

Fig. 9 (a)-(f) shows the entire experiment from ingestion to the ulcer being patched by the origami structure. Fig. 9 (g)-(l) shows the same process but with the origami structure acting as a plug to fill an ulcer. For the substrate, Ecoflex 00-50 was used to represent the stomach surface, with a small sticker marking the location of the ulcer to be patched, and a $1.7\,\mathrm{cm}$ diameter hole representing the ulcer to be plugged. The process started with the pill configuration (Fig. 9 (a)). The structure was autonomously navigated to the desired location by the system sensing the pill location magnetically, and producing a rotating magnetic field to provide the required locomotion (Fig. 9 (b),(c)). Once the targeted location was reached, the applied magnetic field was changed to a constant strong vertical magnetic field to fix the structure in place. Body temperature water ($37^\circ\mathrm{C}$) was then poured over to initiate deployment (Fig. 9 (d)). The structure deployed to a patch, covering the ulcer area (Fig. 9 (e),(f)). The task was completed in approximately 90 sec, in which 50 sec was spent for full deployment. Similarly, the structure could plug a hole (Fig. 9 (g)-(l)). The process completed in approximately 80 sec. The demonstrations display effective navigation and patching/plugging.

V. Conclusion

This study presents a novel programmable medicine that can be used as a patch or plug for treating gastric ulcers. The developed deployable structure can be ingested and
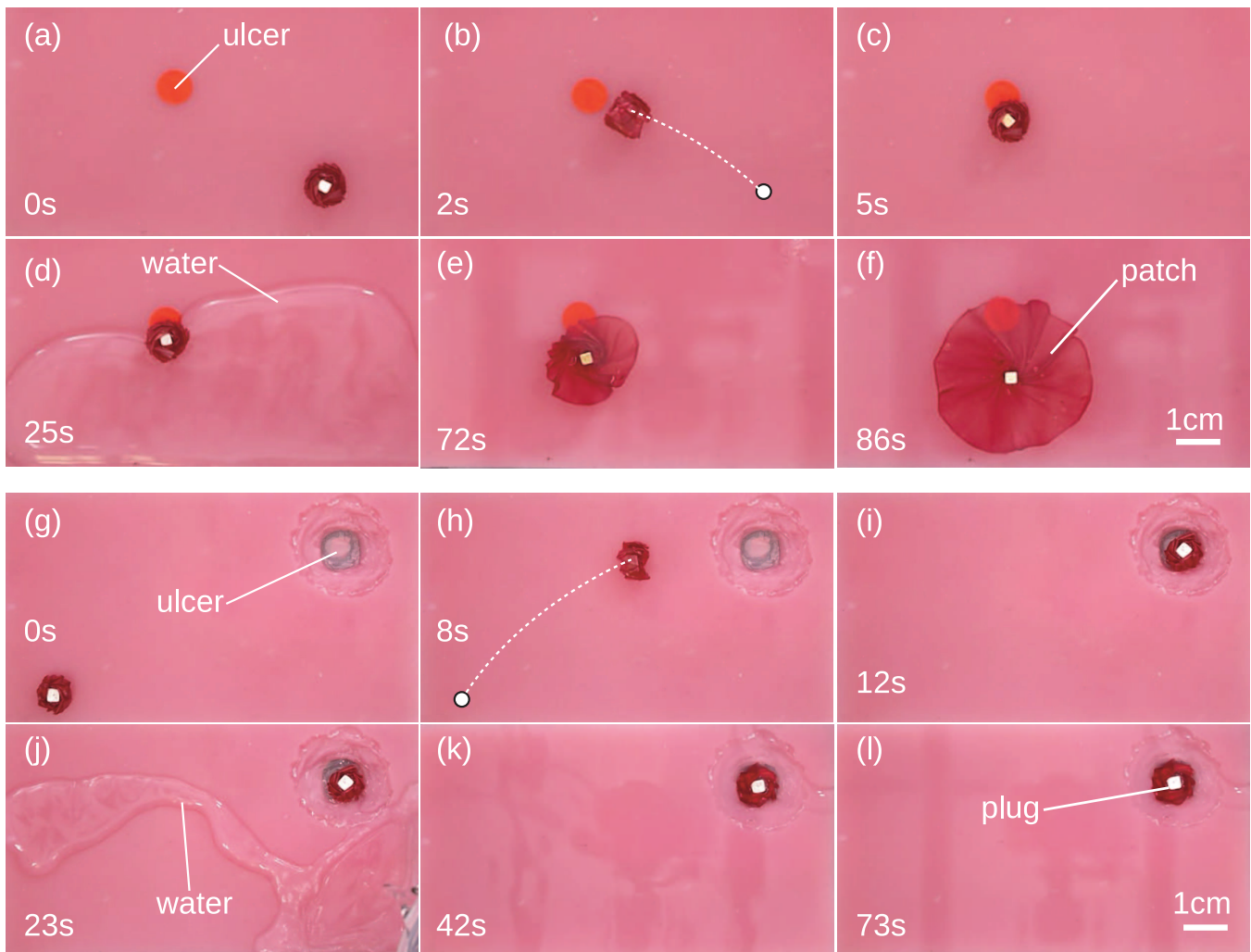
Fig. 9. Entire demonstration of the autonomous patch (a)-(f) and plug (g)-(l). (a),(g) The folded structure is placed on the surface (Ecoflex 00-50), and (b), (h) autonomously navigates to the desired location. (c),(i) Once the structure is in position, a magnetic field is applied to hold it in place. (d)-(e), (j)-(k) Warm water (37°C) is poured over to initiate the deployment of the structure, and (f),(l) within 50 sec the structure is fully deployed, plugging or patching the ulcer. We obtained a high success rate for autonomous navigation, and a reasonable rate of beyond 50% for the deployment of the structure, as in some cases the deployment causes the centre of the structure to move. This can be seen between (d) and (e), where the magnet at the centre moves positions.

autonomously navigated to the target location through a controllable magnetic field. By drinking and supplying water, the structure, which is made of agarose, swells and can be deployed while it is held in place by a constant magnetic field. Due to the origami-inspired design, the structure spreads to 10 times its original size in the horizontal direction, enabling the size of the structure in its pill form to be small. While the patch in this study is designed to be able to fit inside a size 000 pill (the largest available pill size for human consumption), to expand and cover an ulcer with an assumed size of 5 cm, the result in Fig. 3 implies the pill size 00 would be sufficient for a smaller patch of 3cm diameter. We also intend to combine mechanical and chemical bonding to the tissue, taking advantage of the currently available adhesives. Adhesive patches that adhere to the human skin and organs have been developed for surgical treatment, drug delivery and monitoring the human body.

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