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COMPARATIVE STUDY ON THERMAL MANAGEMENT SCHEMES WITH WASTE HEAT RECOVERY FROM ELECTRIC VEHICLE POWER TRAIN

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Jens Endrulat, Daimler, Germany



The
University
Of
Sheffield.

Outline

- **Research Motivation**
- **HVAC Architectures**
- **Electro-thermally Coupled Models for Machine and Inverter**
- **Powertrain Specification**
- **Simulation Model**
- **Simulation Results and Discussion**
- **Conclusion**

Research Motivation

Cold weather condition (e.g. $< 0^{\circ} \text{C}$)

Heating power + Compressor power + Powertrain loss



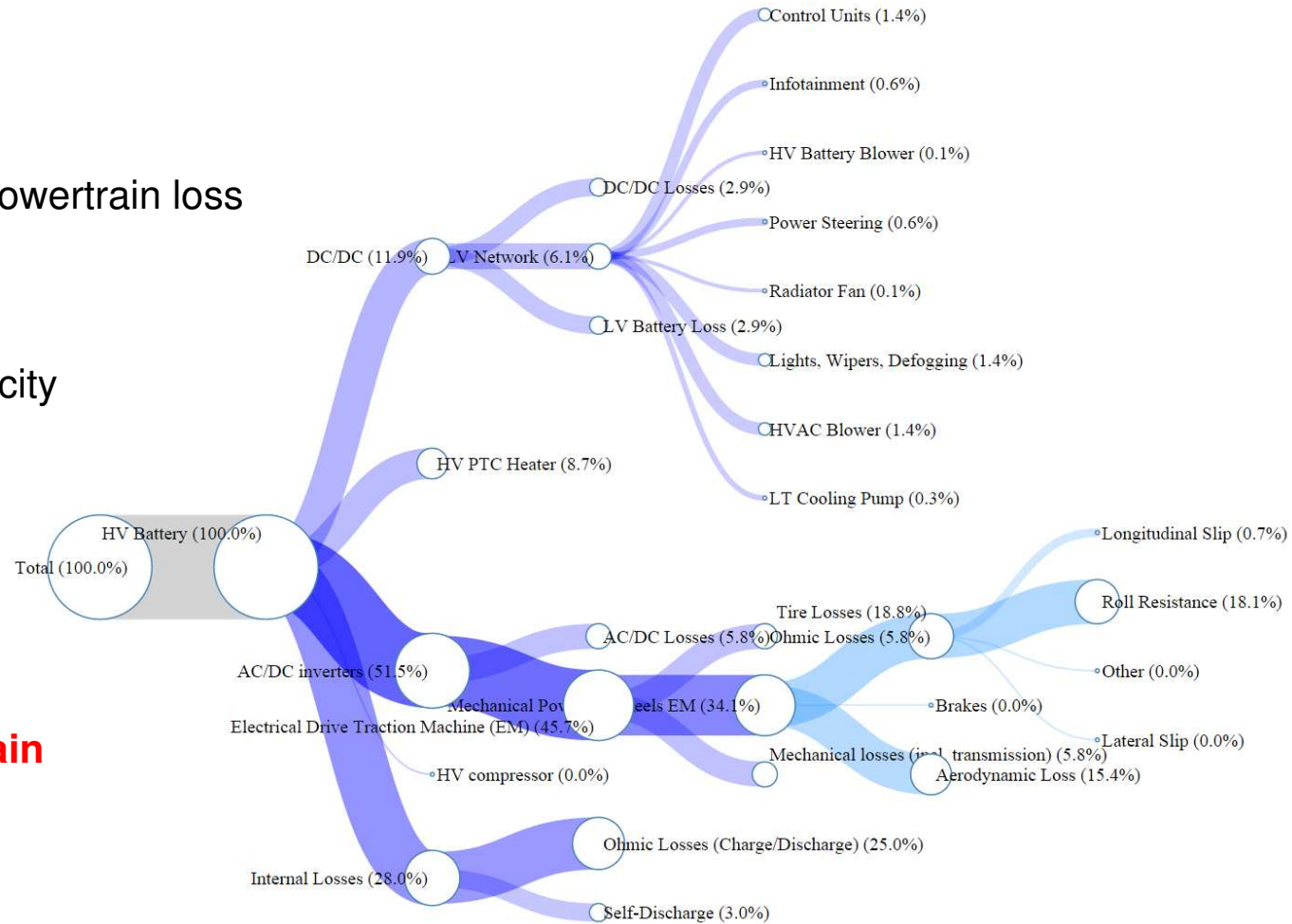
Consumes up to 50% of batteries' capacity



Mile range reduced by half



Recover waste heat in the powertrain



HVAC Architectures (Heating Mode)

➤ Conventional HVAC architecture

Evaporator, compressor, condenser, expansion valve

Evaporator absorbs ambient energy, and condenser heats up cabin

➤ Waste heat-only HVAC architecture

Chiller (working as evaporator), compressor, condenser, expansion valve

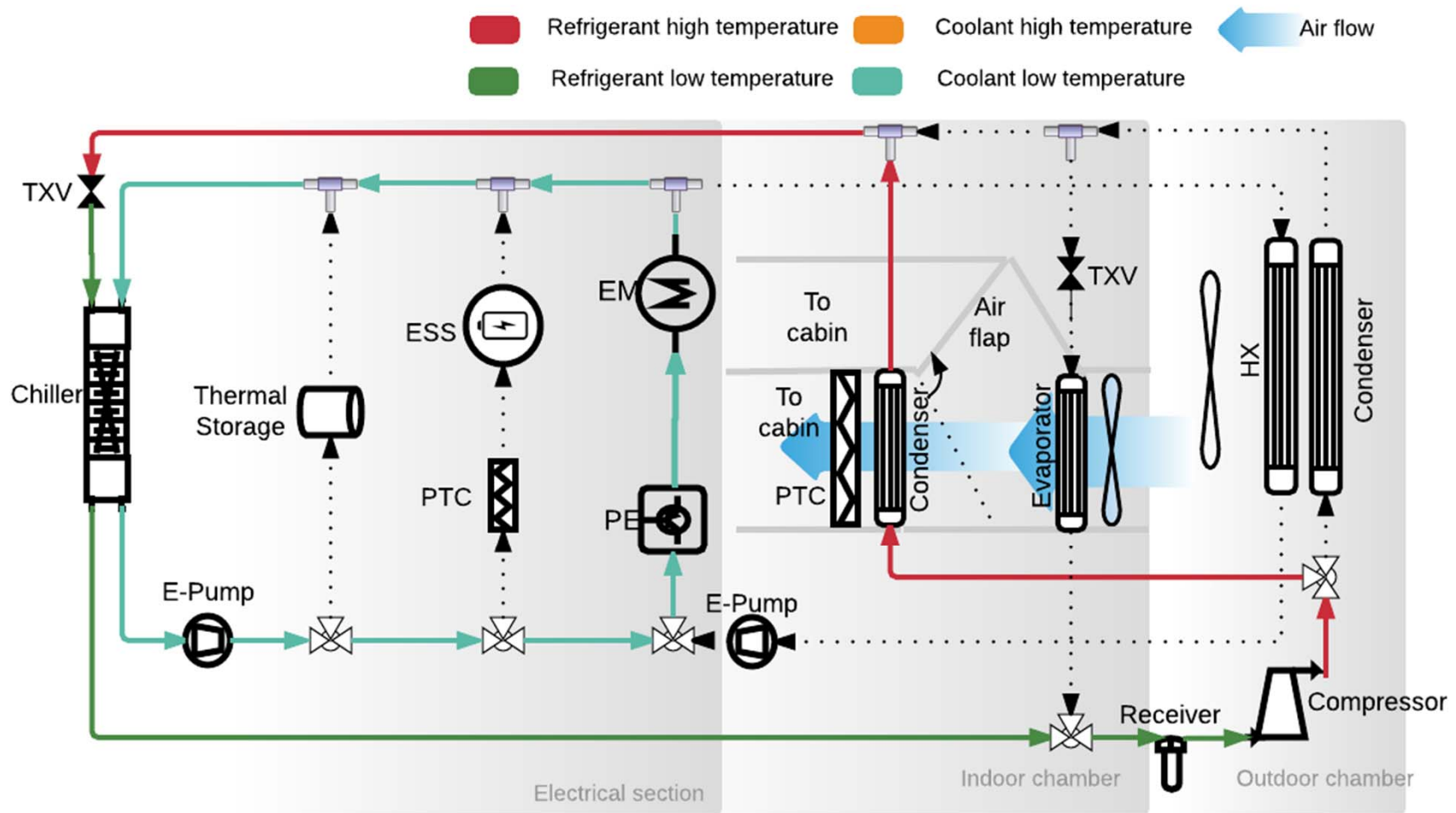
Chiller absorbs waste heat from powertrain, and condenser heats up cabin

➤ Dual heat source HVAC architecture

Chiller (working as evaporator), evaporator, compressor, condenser, expansion valve

Chiller absorbs waste heat from powertrain, Evaporator absorbs ambient energy, and condenser heats up cabin

Waste Heat Recovery -- Waste Heat Only

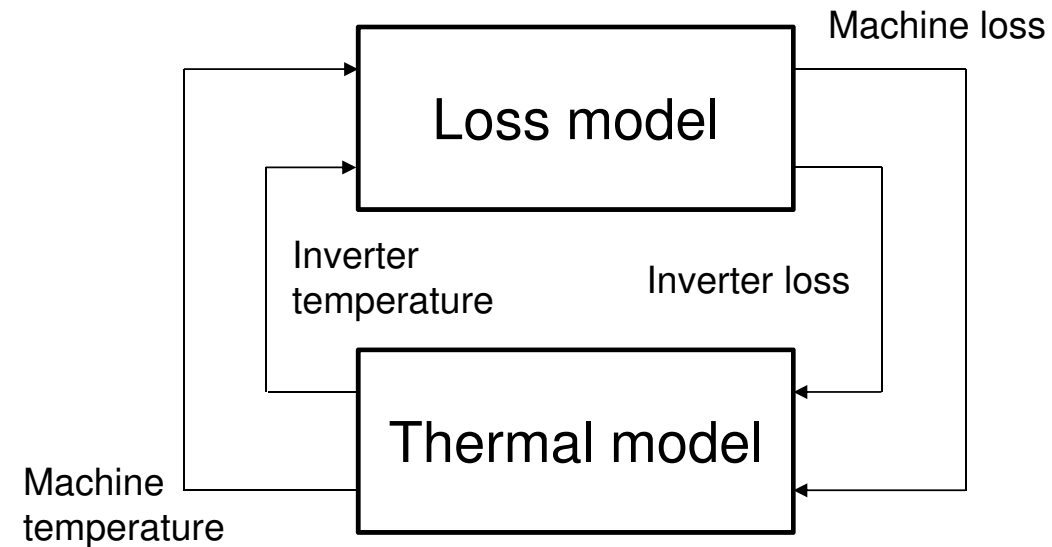


Electro-thermally Coupled Model for Powertrain system

Challenges:

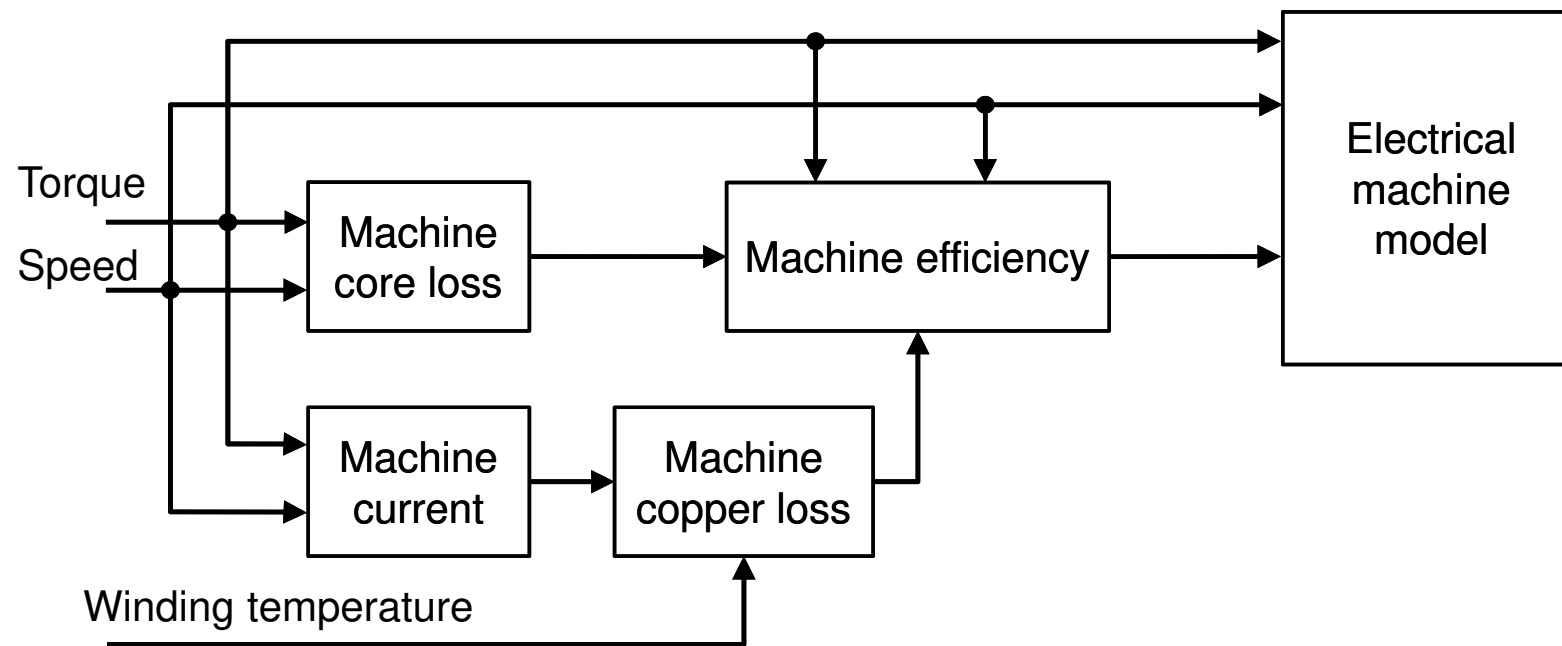
- **Electrical machine and inverter temperatures are subject to their losses.**
- **Machine and inverter losses are largely affected by their temperatures.**

- Machine copper loss increases by 39% for every 100°C temperature rise (assuming same current);
- Inverter loss increases by ~20% for every 100°C temperature rise.



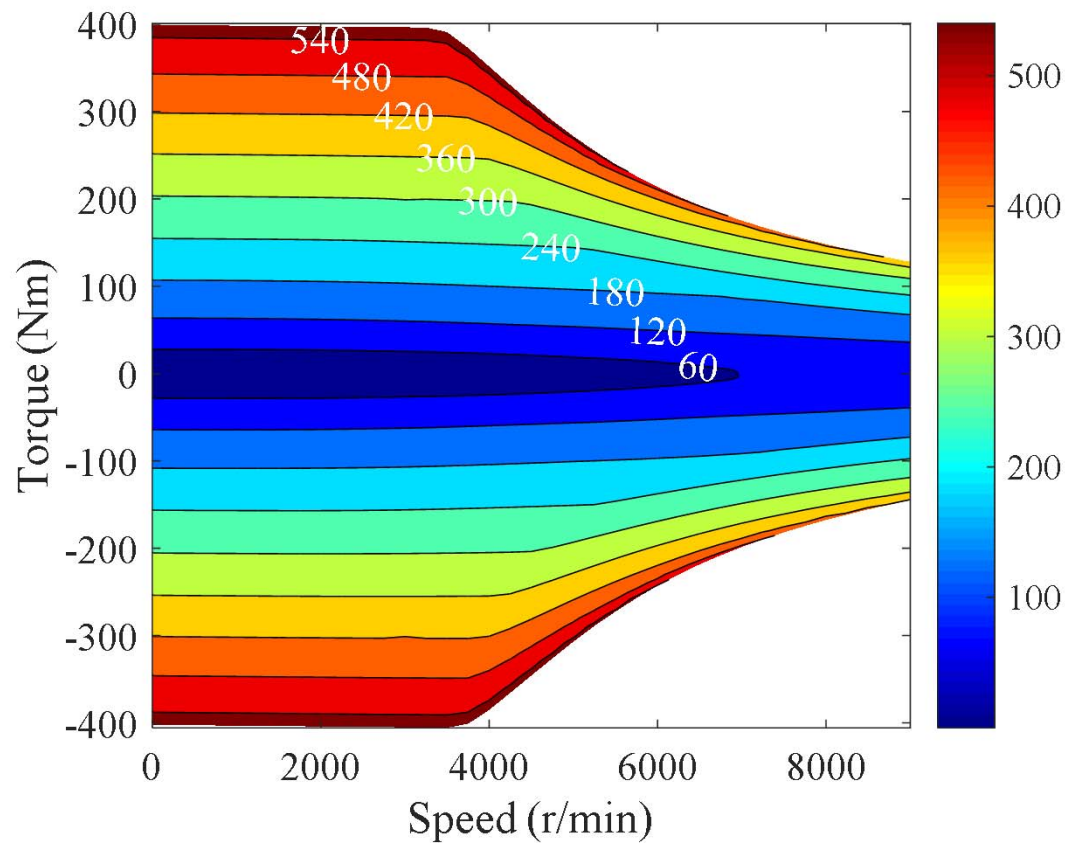
Electro-thermally Coupled Model for Electrical Machine

Schematic

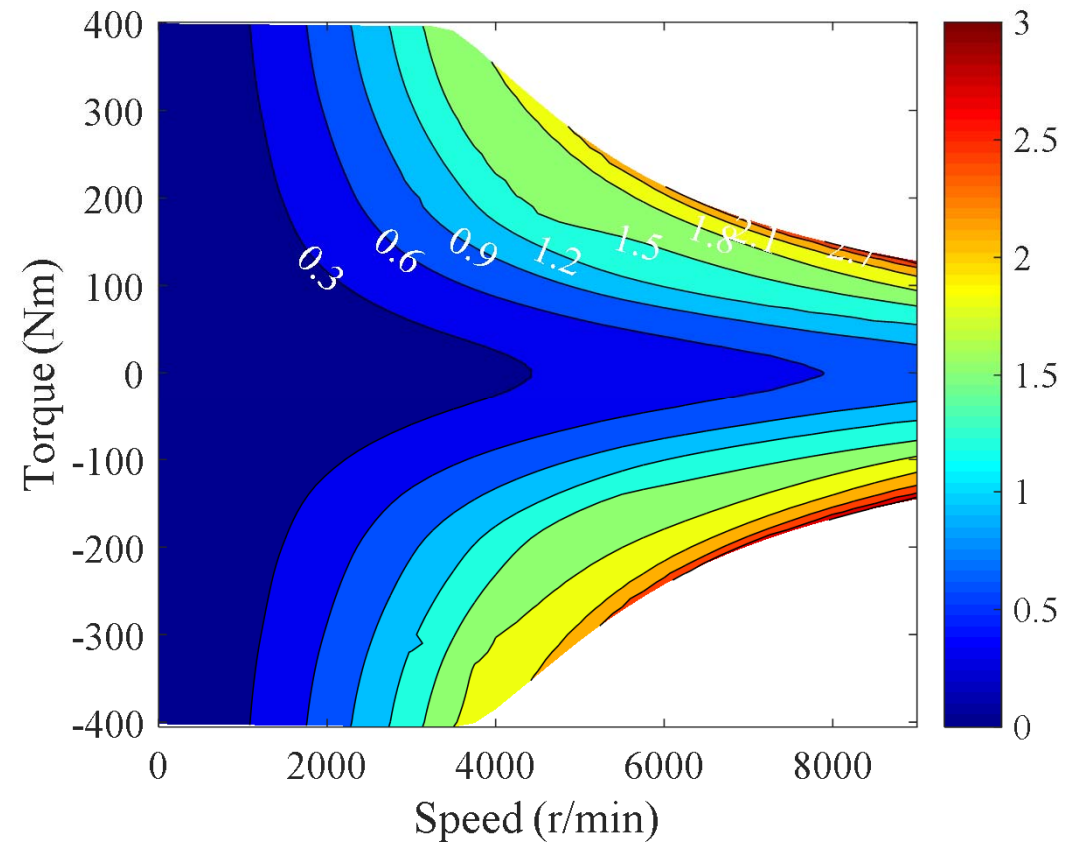


Electro-thermally Coupled Model for Electrical Machine

Machine phase current in A (RMS)

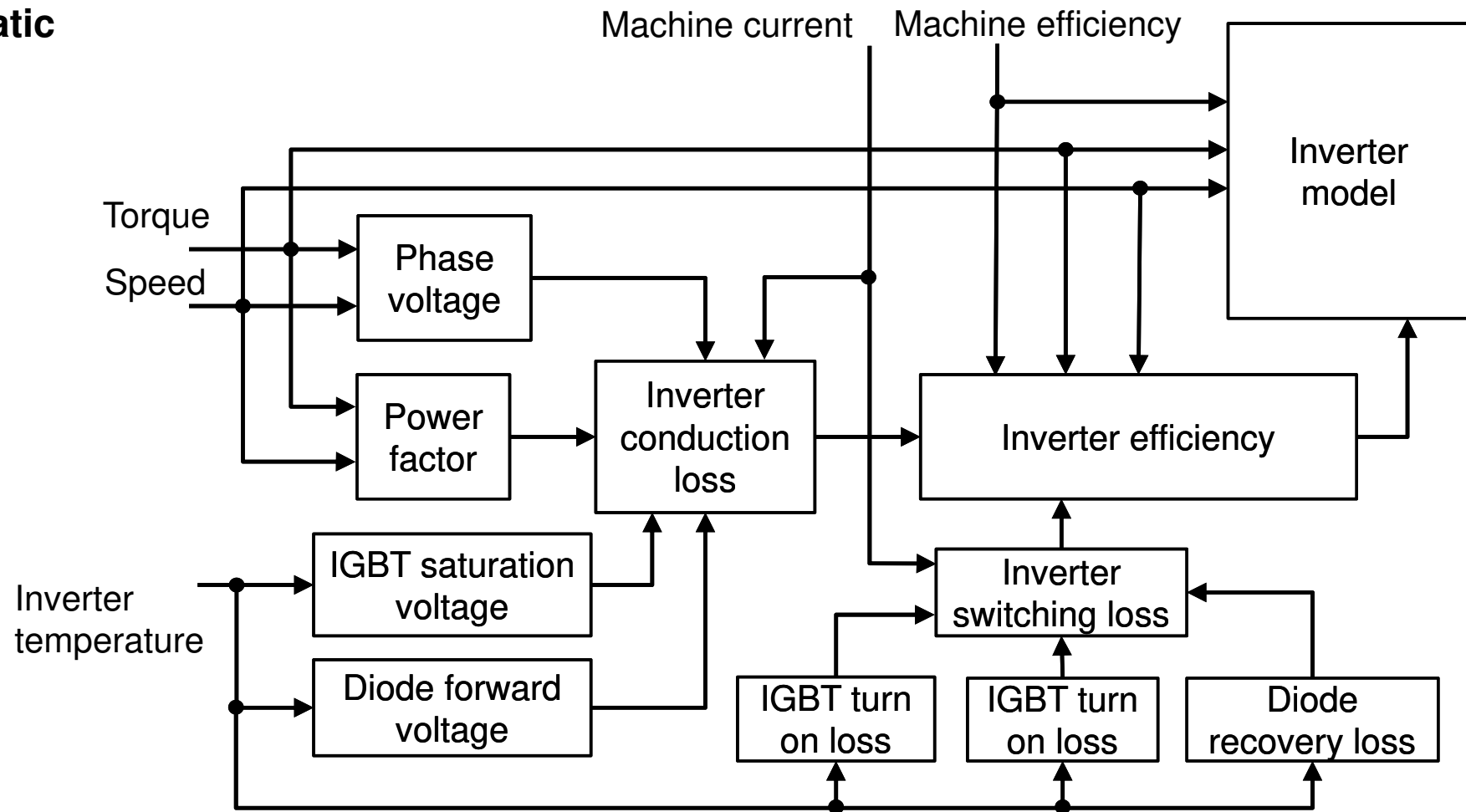


Machine core loss in kW



Electro-thermally Coupled Model for Inverter

Schematic



Powertrain Specification

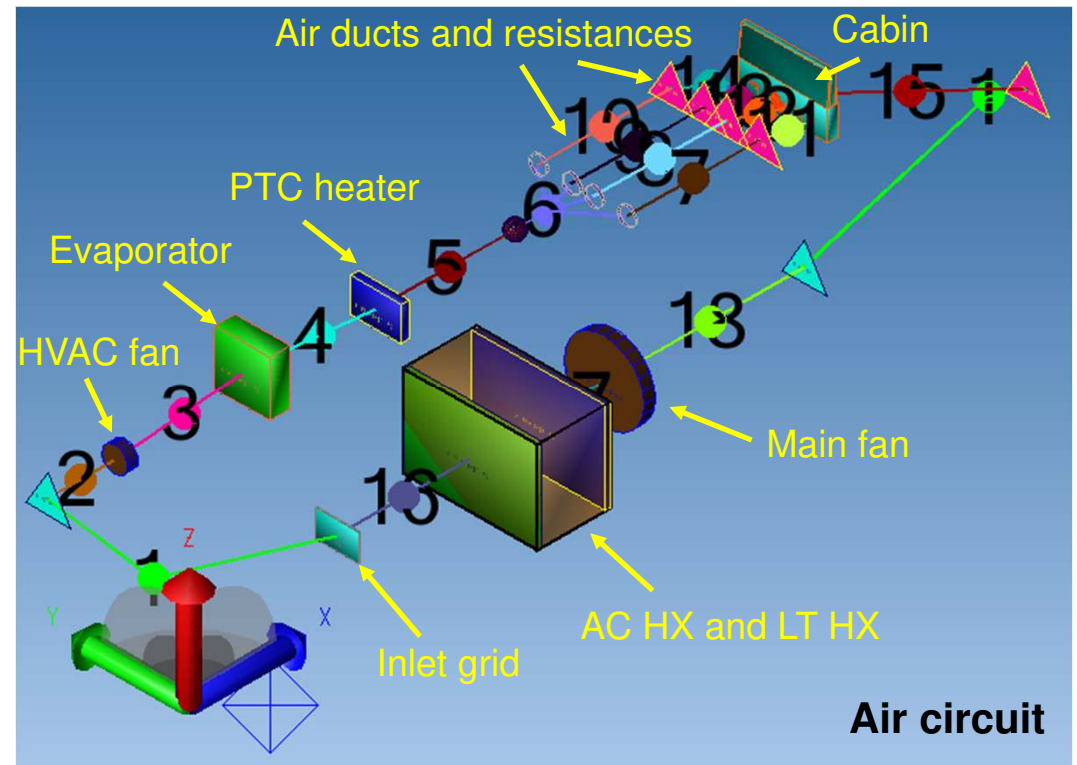
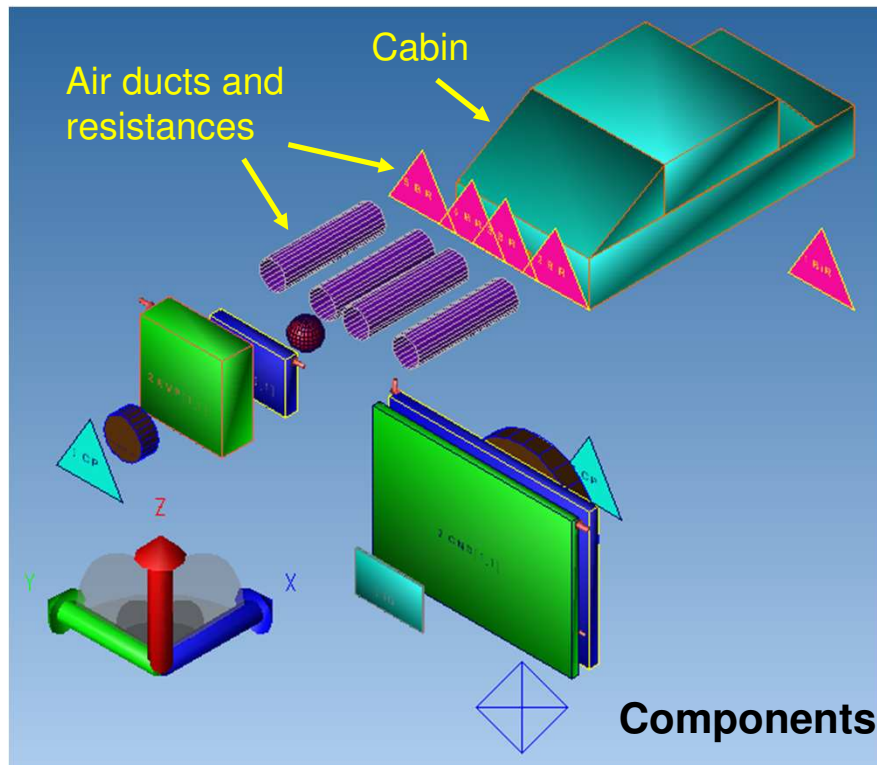


Item	Value
Kerb weight	1,708 kg
Gross weight	2,170 kg
Length	4,358 mm
Width	1,812 mm
Height	1,599 mm
Wheel base	2,699 mm
Wheel size	205/60 R16
Gear ratio	5.98 : 1
Axle ratio	1.12 : 1
Aerodynamic drag coefficient	0.28
Frontal area	2.55 m ²
Tyre dynamic radius	316.4 mm
Cabin volume	3.5 m ³
Window surface (for solar load)	1.4 m ²

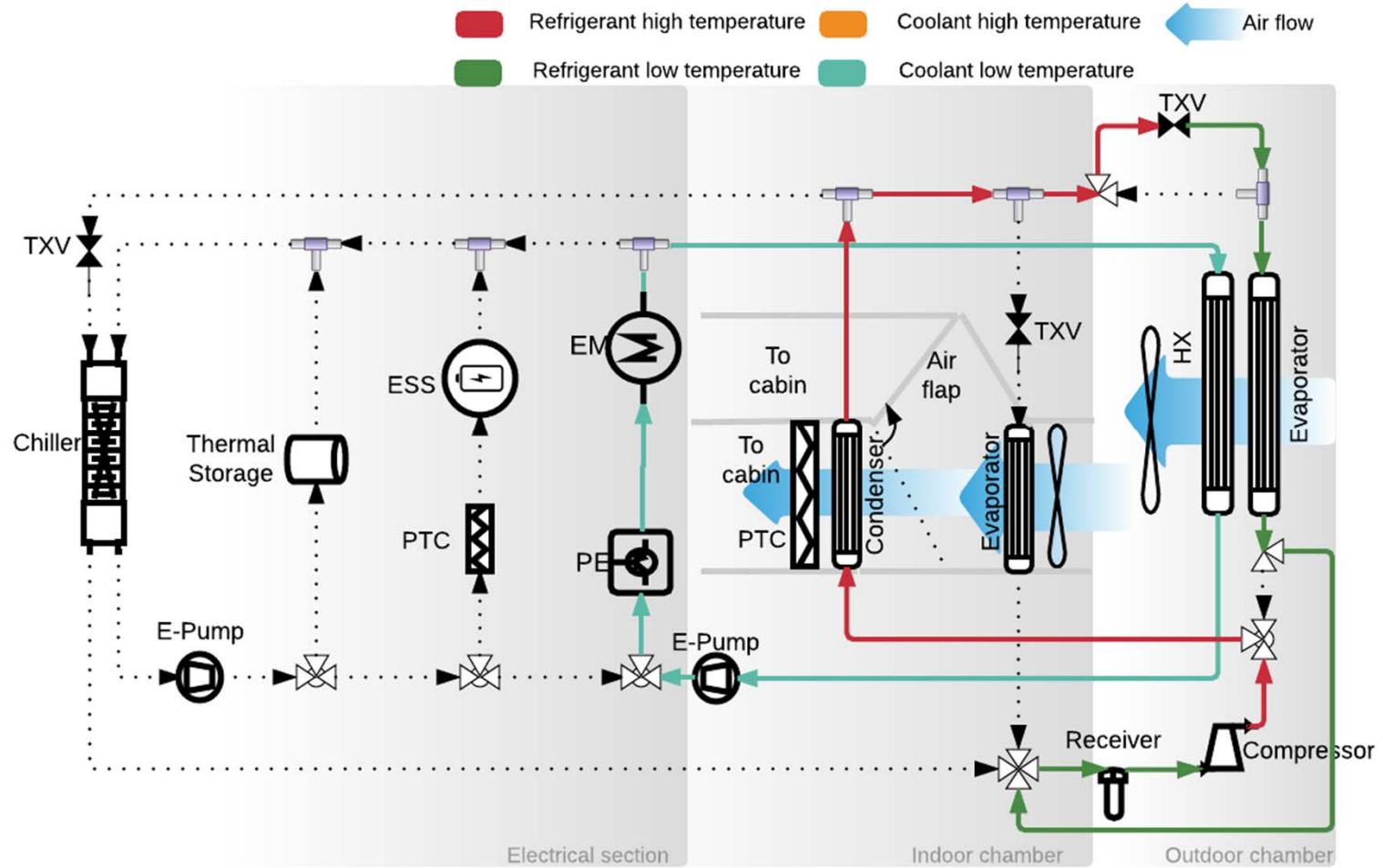
Simulation Model

KULI – 1D simulation software for vehicle energy management

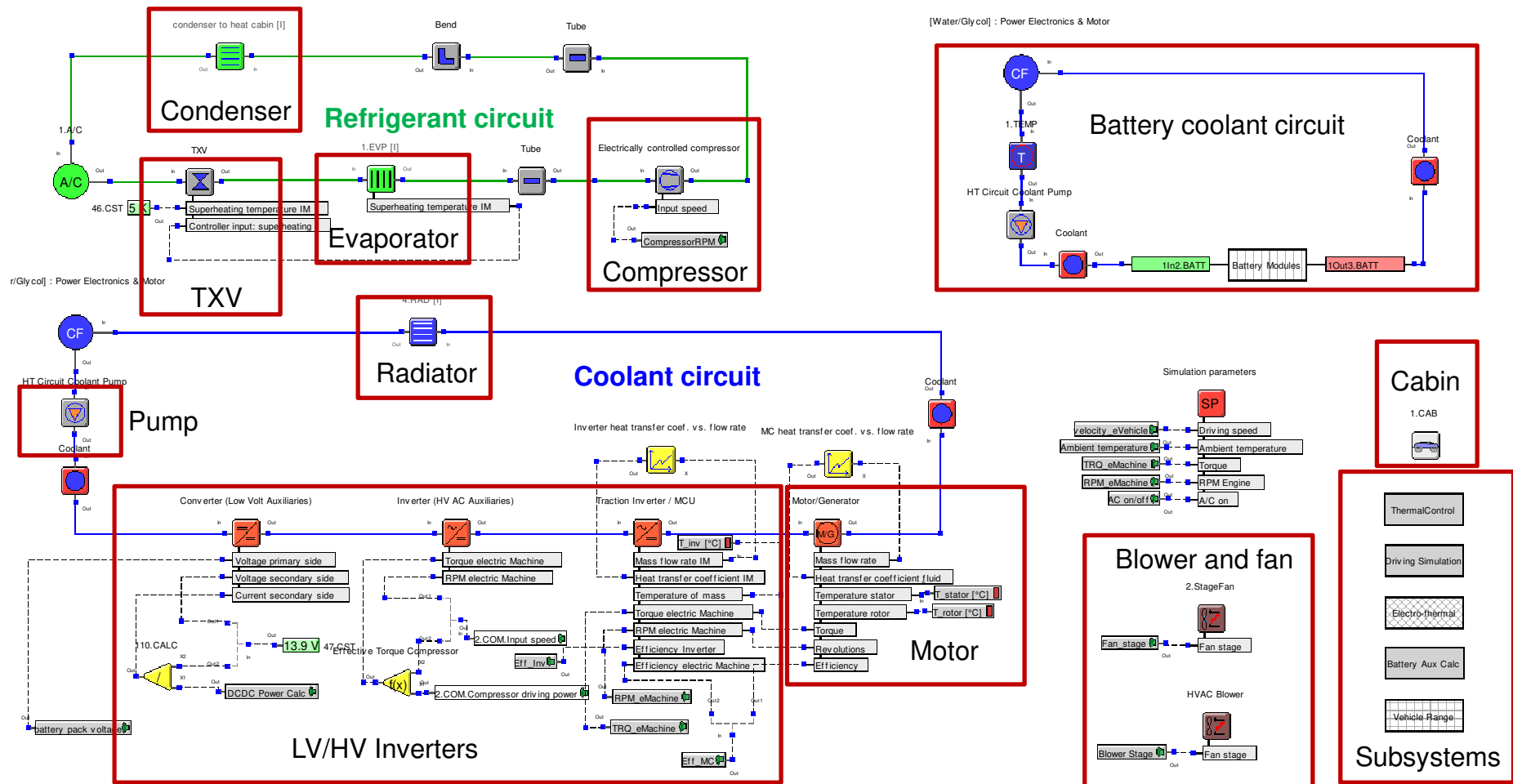
Components readily available: Cabin, compressor, heat exchanger, thermostatic expansion valve, blower, pump, electrical machine, inverter, battery, etc.



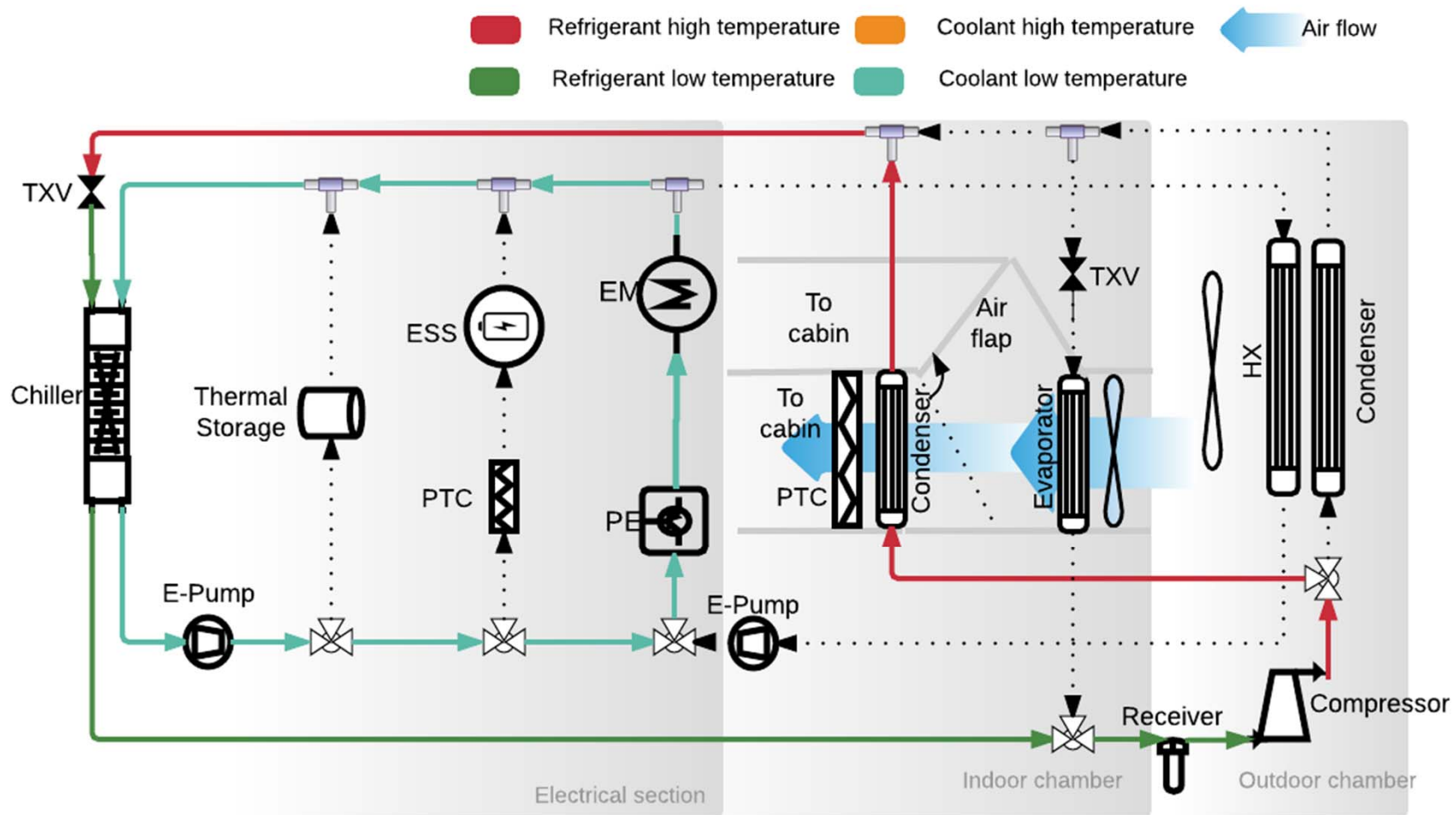
Conventional Powertrain and HVAC system



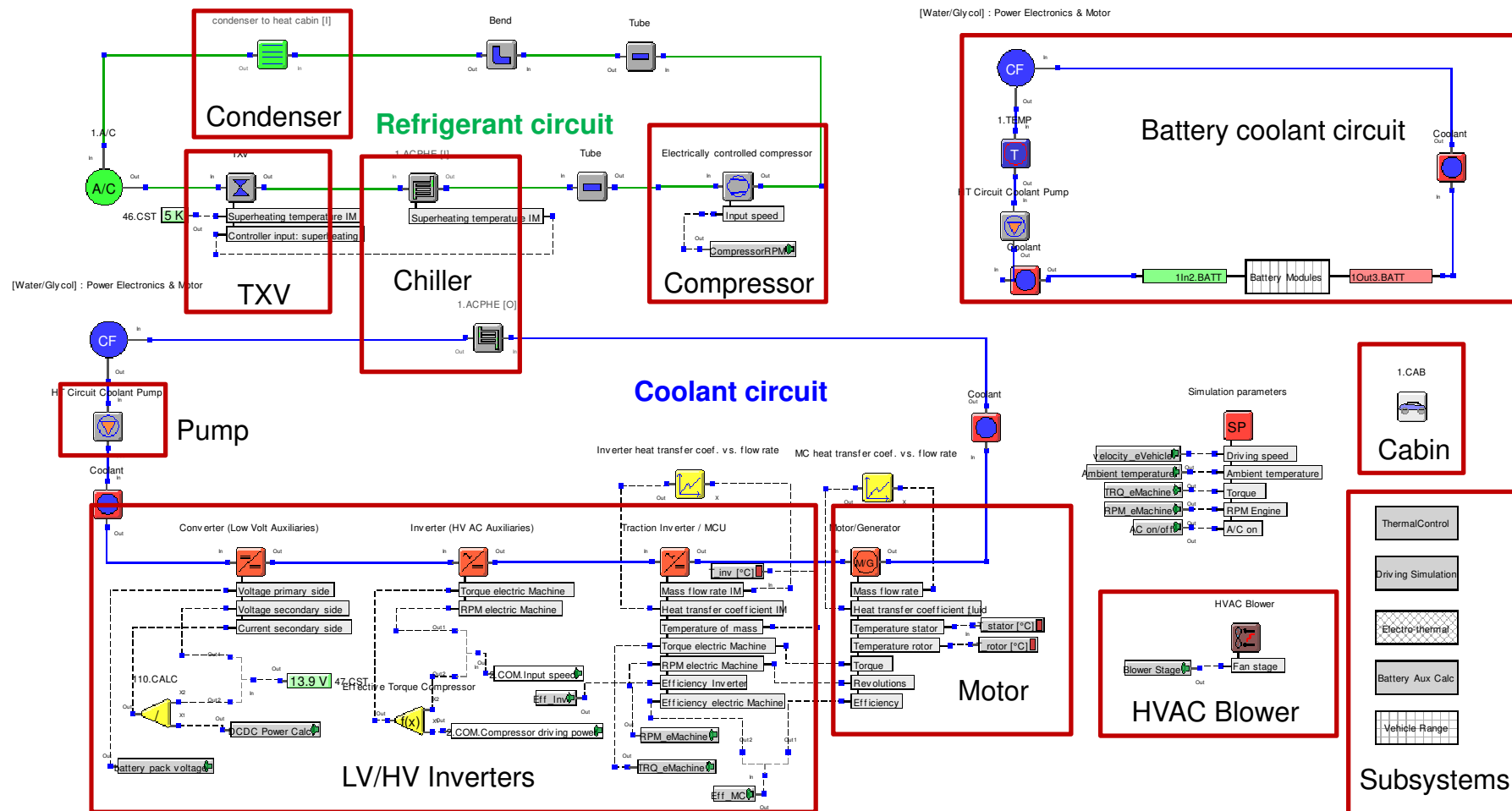
Simulation Model – Ambient Heat Only



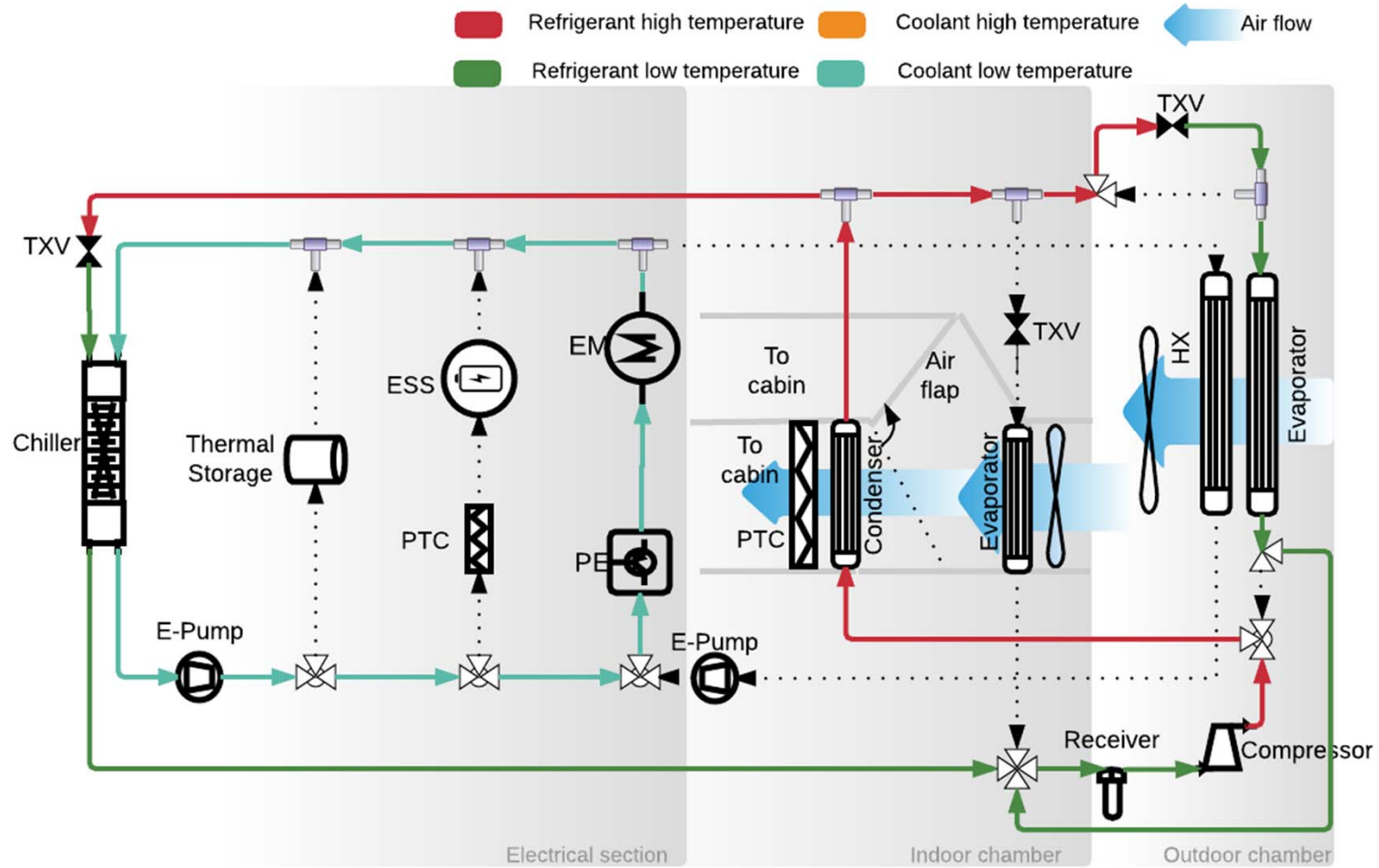
Waste Heat Recovery -- Waste Heat Only



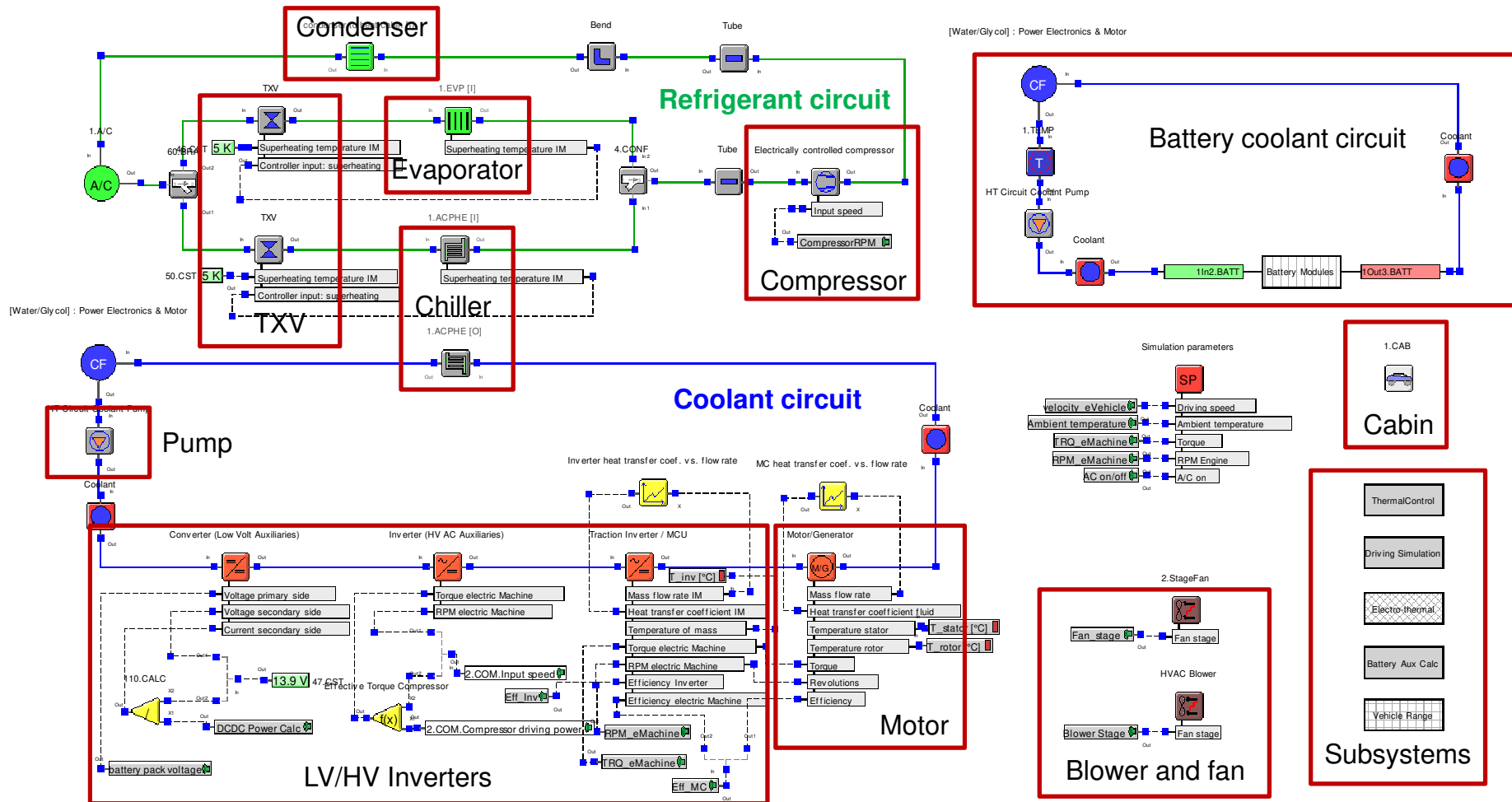
Simulation Model – Waste Heat Only



Waste Heat Recovery -- Dual Heat source

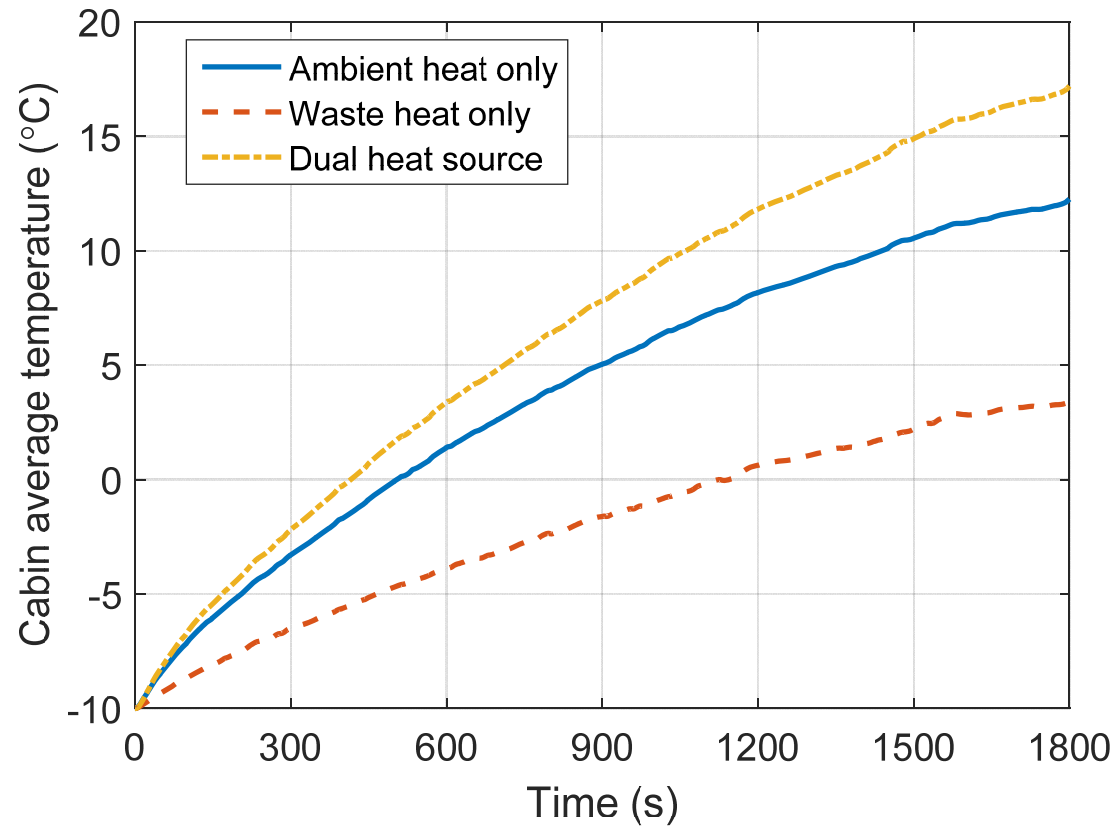


Simulation Model – Dual Heat Source

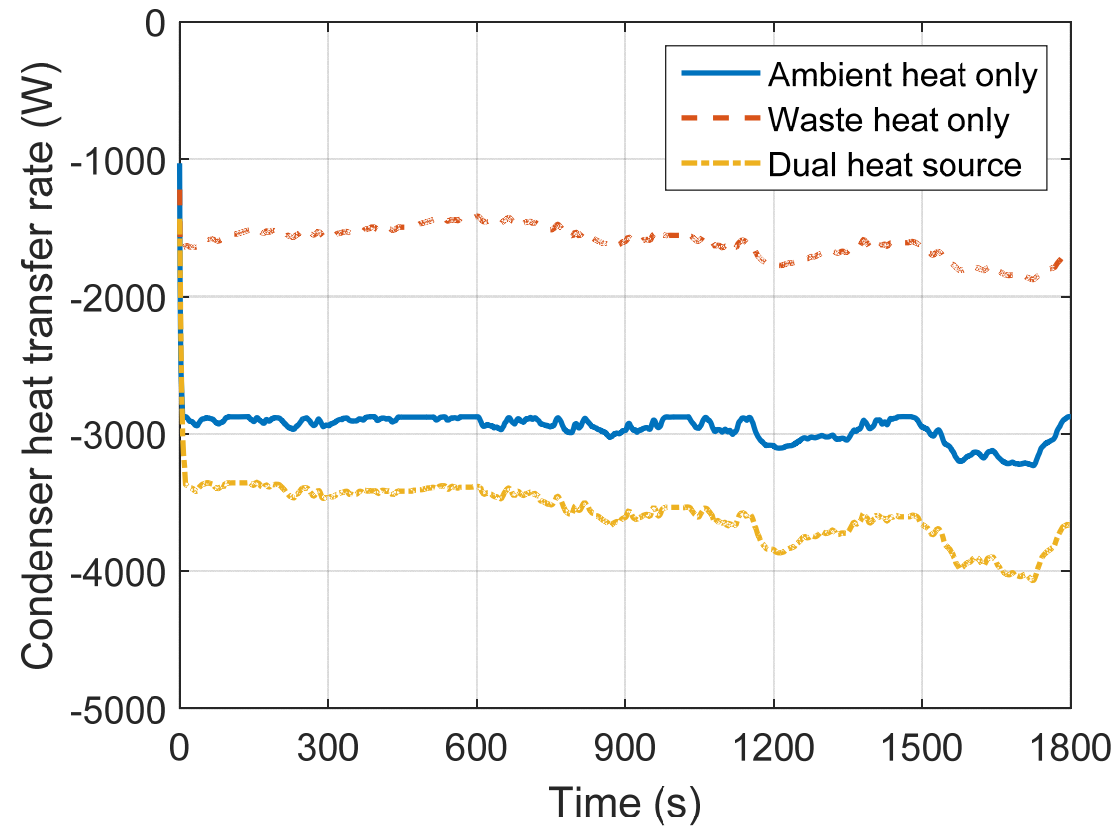


-10° C Ambient, 1 WLTC Driving Cycle

Cabin air average temperature

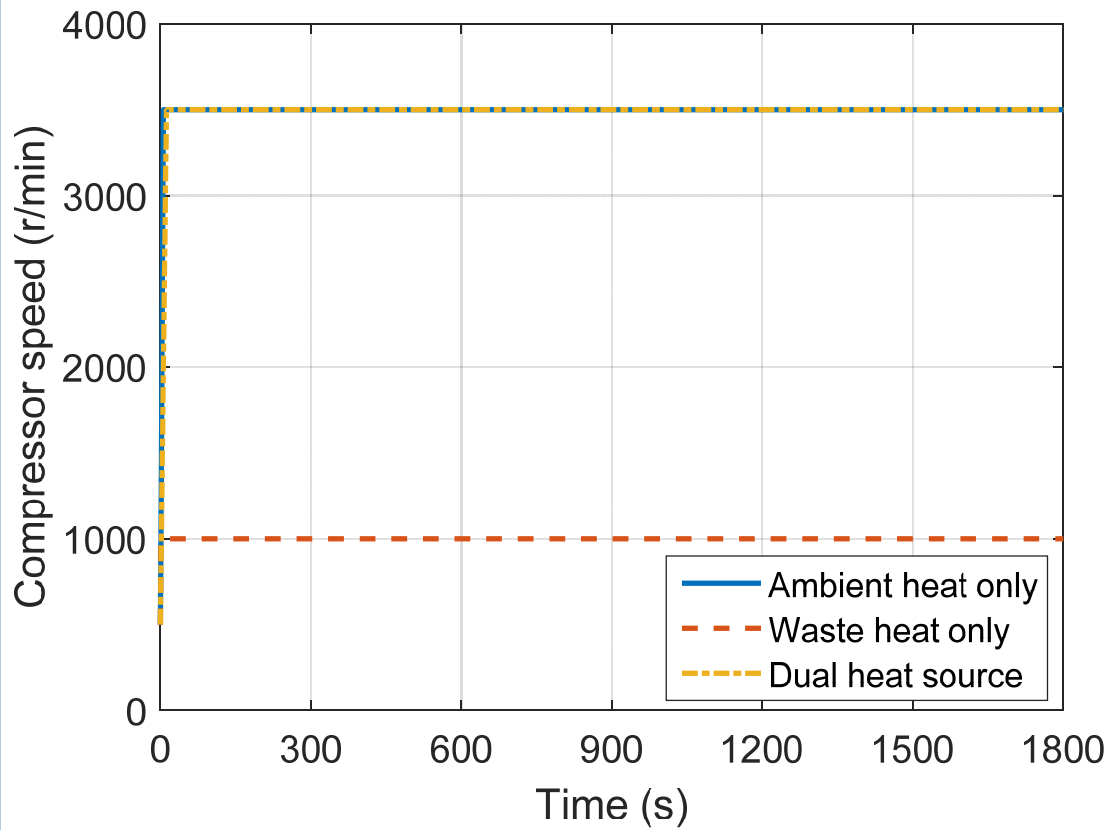


Condenser heat transfer rate

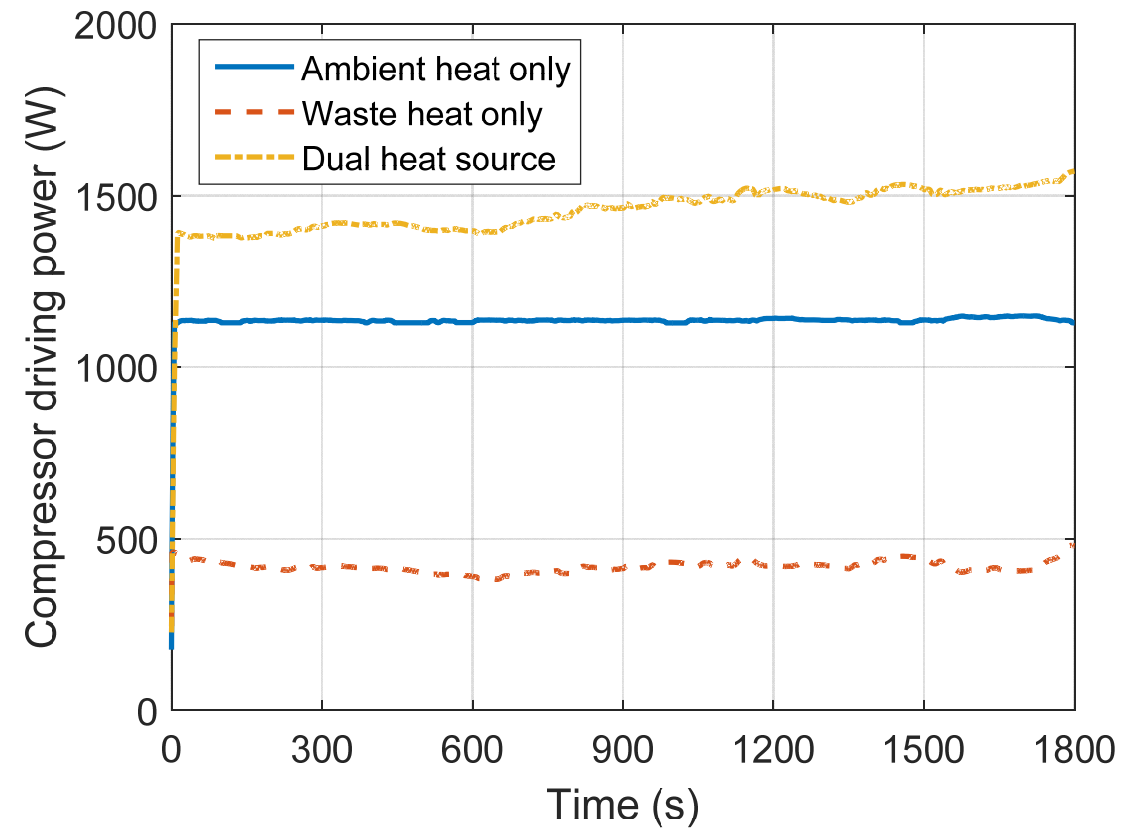


-10° C Ambient, 1 WLTC Driving Cycle

Compressor input speed

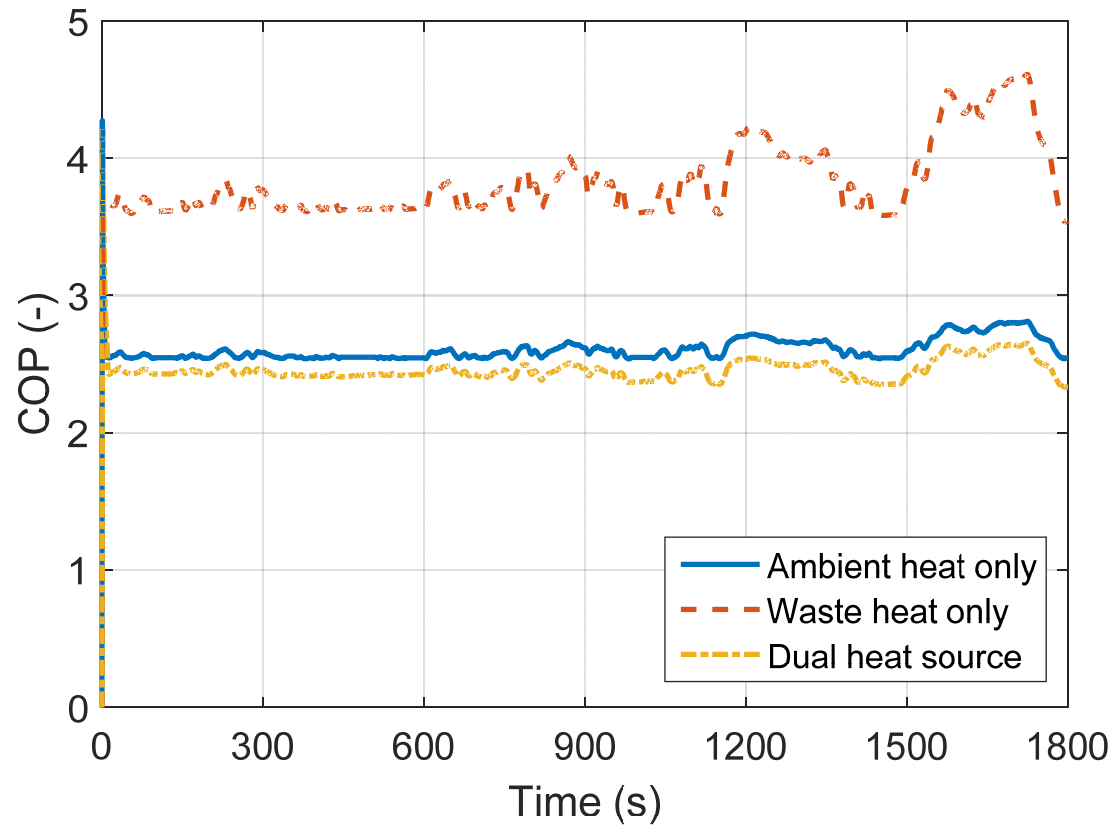


Compressor driving power



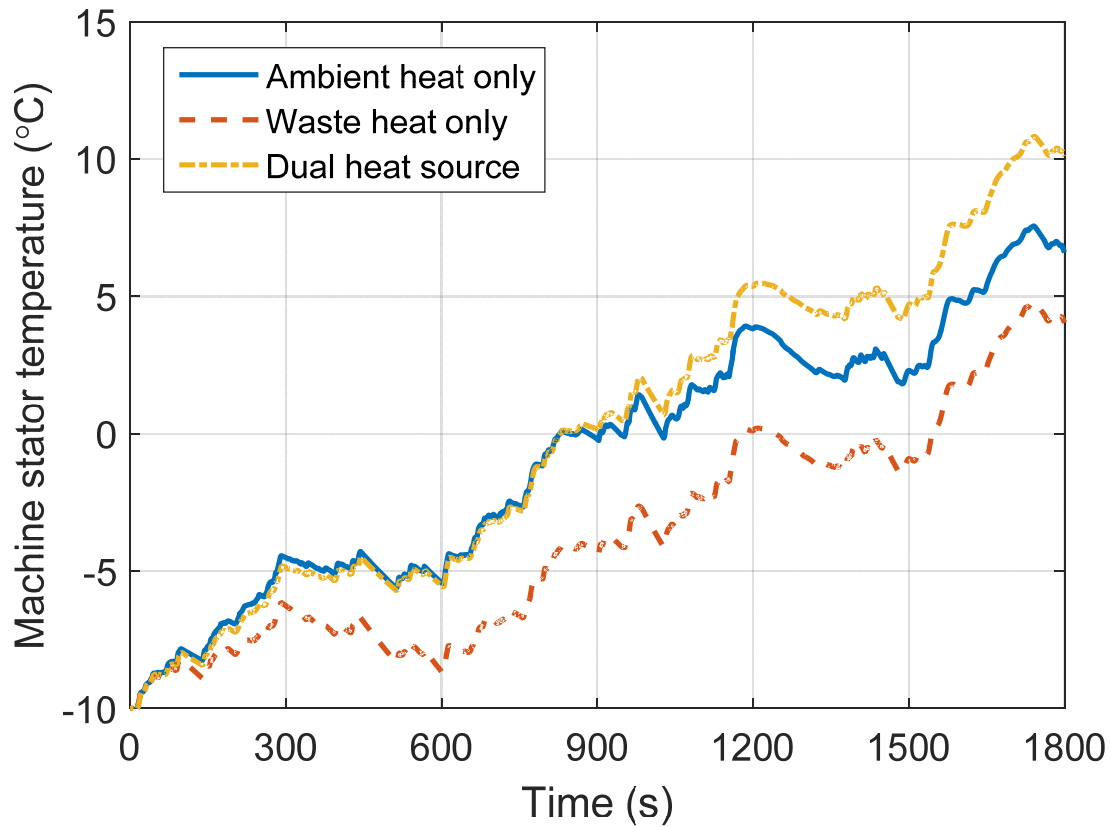
-10° C Ambient, 1 WLTC Driving Cycle

COP

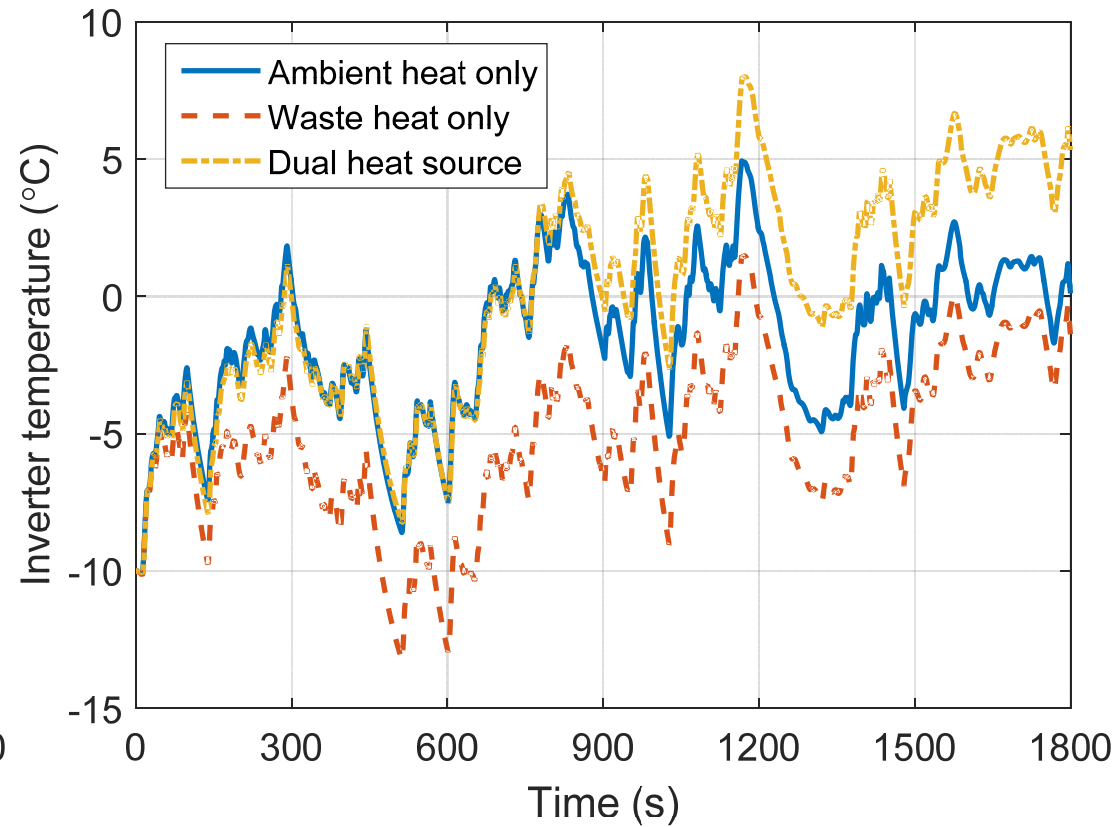


-10° C Ambient, 1 WLTC Driving Cycle

Machine stator temperature



Inverter temperature



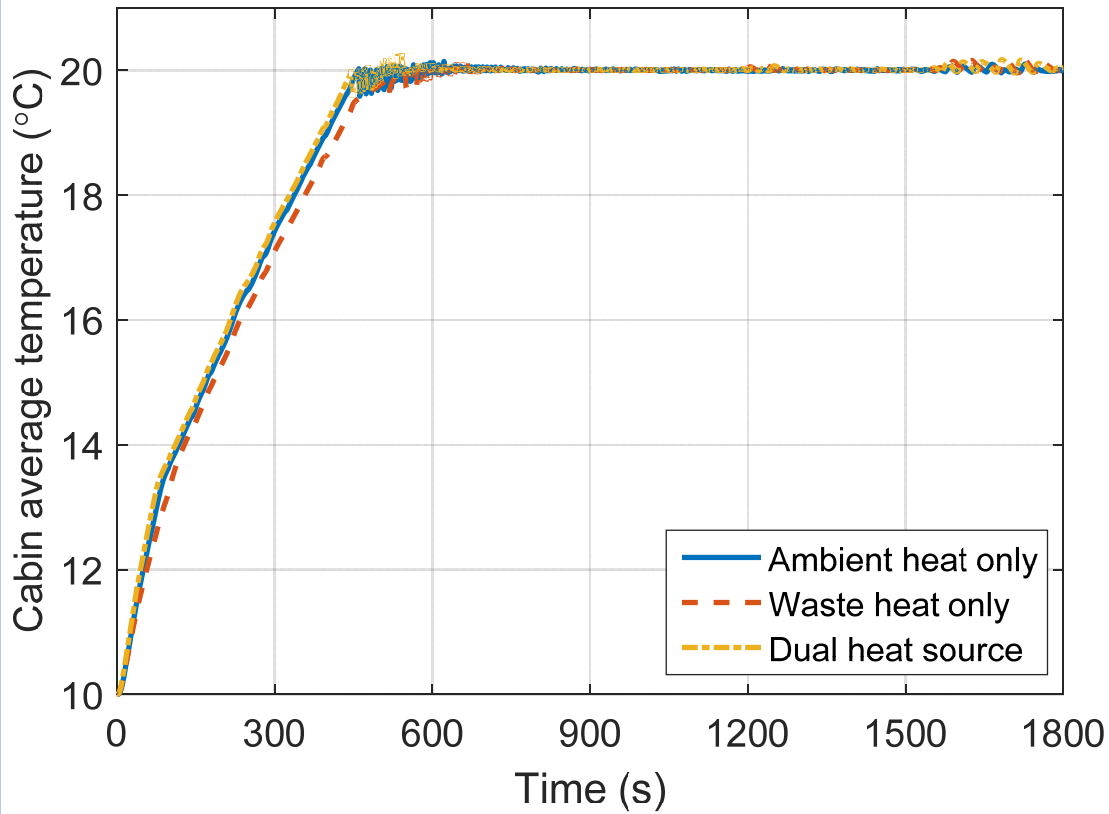
-10° C Ambient, 1 WLTC Driving Cycle

Net energy gain

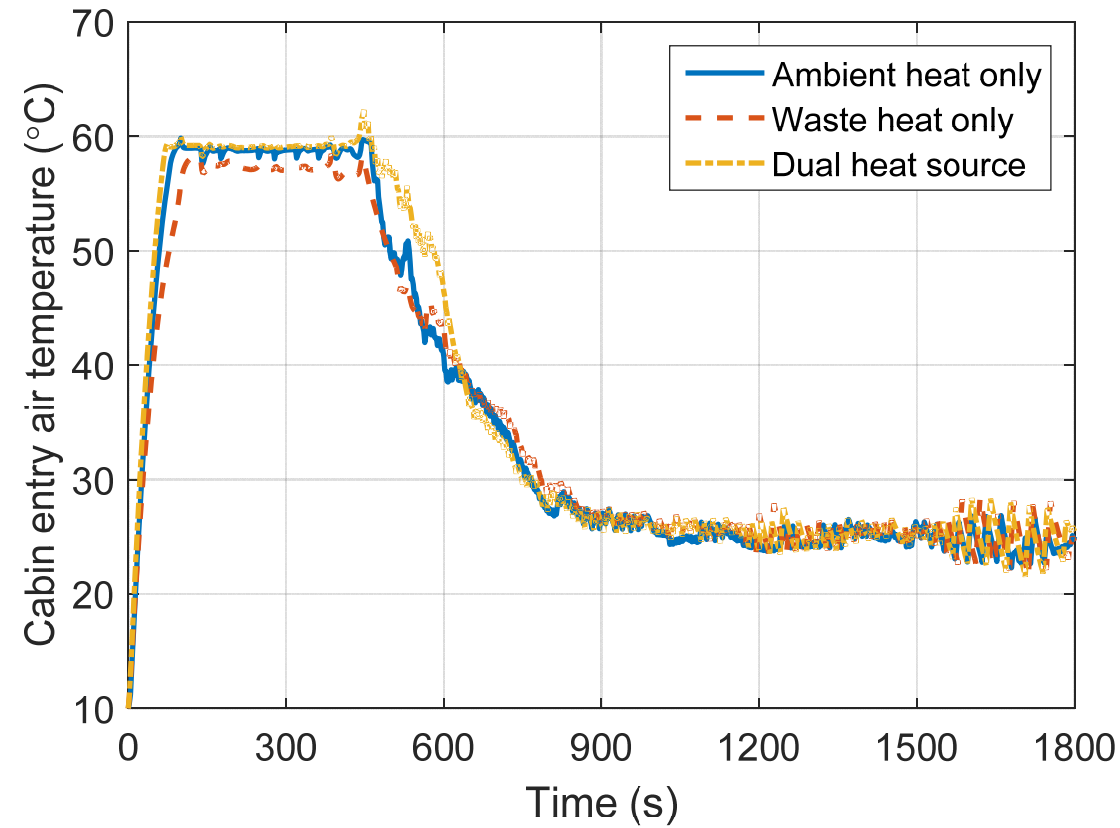
Quantity	Unit	Ambient heat only	Waste heat only	Dual heat source
Compressor driving energy W_{com} (including compressor loss)	MJ	2.04	0.75	2.63
Condenser energy W_{con} (heat up cabin)	MJ	5.33	2.88	6.46
Evaporator energy W_{eva} (waste energy recovery)	MJ	3.79	2.20	2.26 (Ambient heat) 2.25 (Waste heat)
Net energy gain W_{net} ($W_{net}=W_{con}-W_{com}$)	MJ	3.29	2.13	3.83
Total energy consumption W_{tot} (Consumed battery energy)	MJ	17.96	15.07	18.93
Net energy gain ratio R_{net} ($R_{net}=W_{net}/W_{tot} * 100\%$)	%	18.32%	14.13%	20.23%
Average COP	-	2.61	3.84	2.46

10° C Ambient, 1 WLTC Driving Cycle

Cabin air average temperature

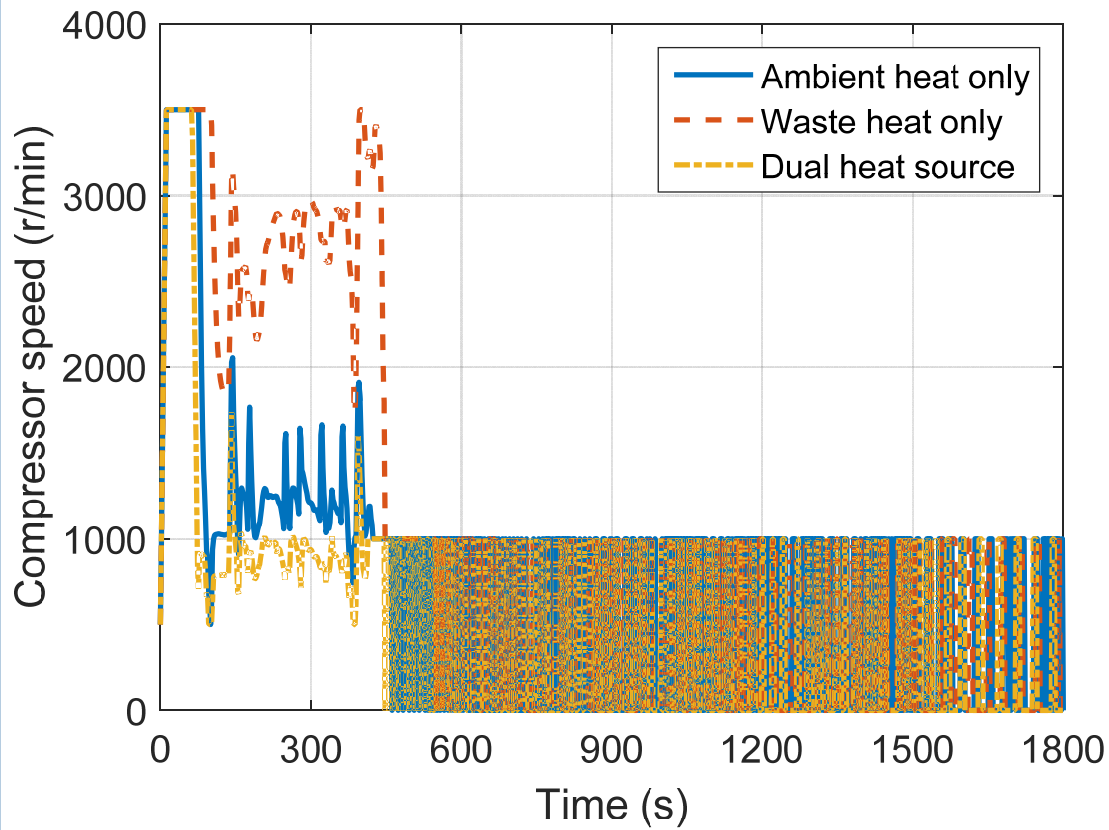


Cabin air entry temperature

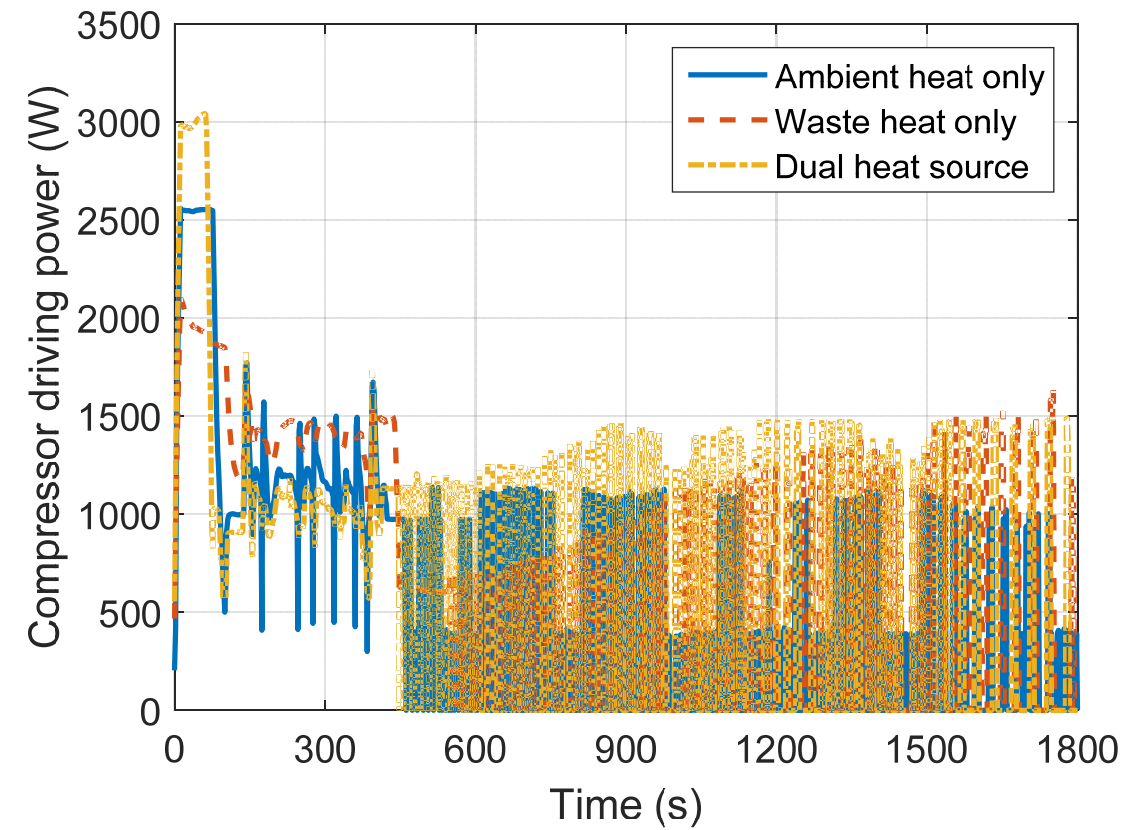


10° C Ambient, 1 WLTC Driving Cycle

Compressor input speed



Compressor driving power



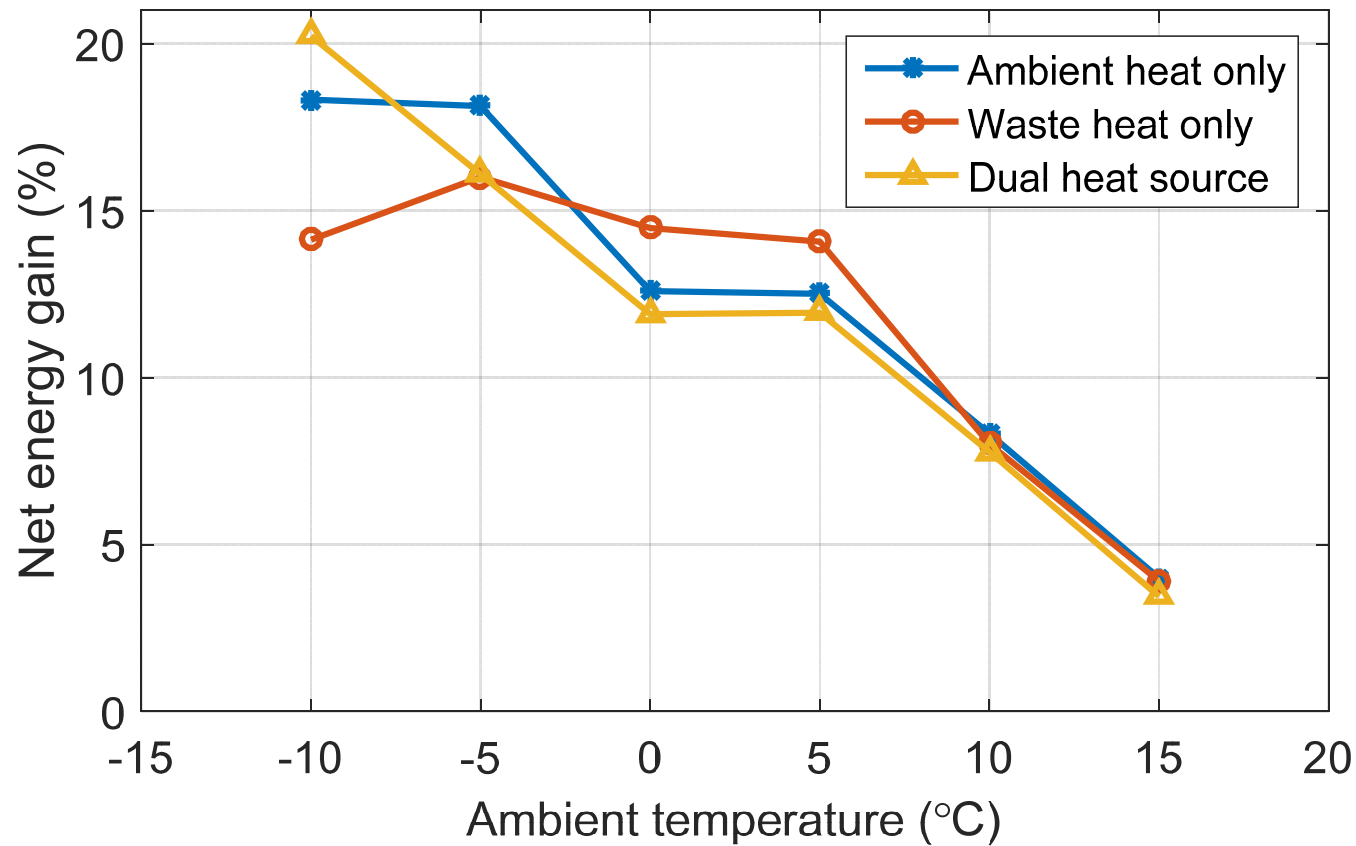
10° C Ambient, 1 WLTC Driving Cycle

Net energy gain

Quantity	Unit	Ambient heat only	Waste heat only	Dual heat source
Compressor driving energy W_{com} (including compressor loss)	MJ	1.01	1.11	1.04
Condenser energy W_{con} (heat up cabin)	MJ	2.41	2.38	2.36
Evaporator energy W_{eva} (waste energy recovery)	MJ	1.82	1.56	0.56 (Ambient heat) 1.10 (Waste heat)
Net energy gain W_{net} ($W_{net}=W_{con}-W_{com}$)	MJ	1.40	1.27	1.32
Total energy consumption W_{tot} (Consumed battery energy)	MJ	16.83	15.85	16.99
Net energy gain ratio R_{net} ($R_{net}=W_{net}/W_{tot} * 100\%$)	%	8.32%	8.01%	7.77%
Average COP	-	2.39	2.14	2.27

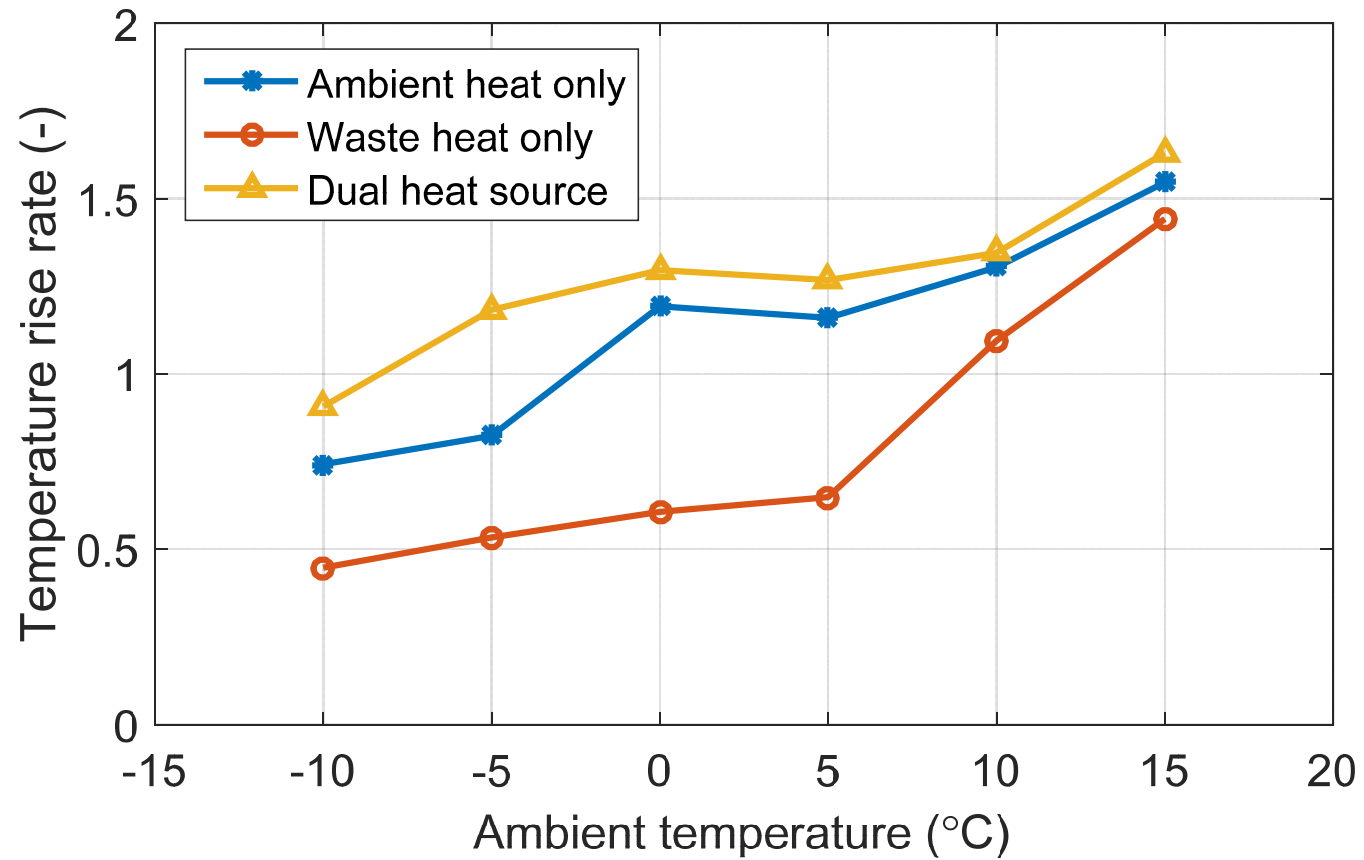
Influence of ambient temperature

Net energy gain vs. ambient temperature



Thermal Comfort Comparison

Mean temperature rise rate before reaching 20° C target temperature



Conclusions and Future work

- Compared to the ambient heat only scheme, the dual heat sources scheme can work at lower temperatures, exhibits higher heating power and thus takes less time to reach thermal comfort temperature, and also has higher net energy gain.
- Compared to the waste heat only scheme, the dual heat source scheme can satisfy the thermal comfort without introducing new key components, has much higher heating power, and also higher net energy gain.
- The main trend of the net energy gain is decreasing with the increase of ambient temperature since the required energy for thermal comfort is lower at higher ambient temperature.
- The main trend of the temperature rise rate is increasing with the increase of ambient temperature because more ambient heat is available at higher ambient temperature.
- Experimental test will be performed after setting up the test rig and demo car.

Thank you for your attention!