

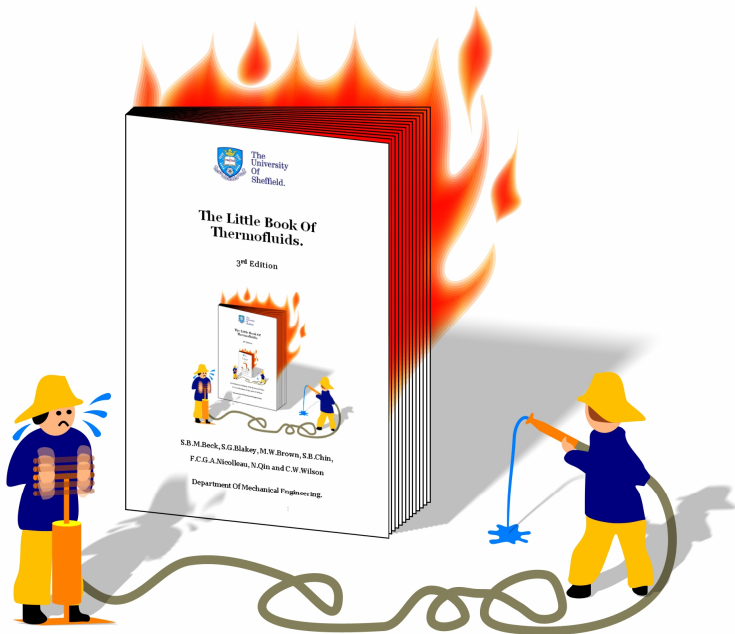


The
University
Of
Sheffield.

Department
Of
Mechanical
Engineering.

The Little Book Of Thermofluids.

3rd Edition



**S.B.M. Beck, S.G. Blakey, M.W. Brown, S.B. Chin, F.C.G.A. Nicolleau,
N. Qin, C.W. Wilson and R. Woolley**

Published¹

**Department of Mechanical Engineering, University of Sheffield ,
Sheffield, UK.²**

First edition: September 2004.

Second edition: October 2005.

Reprinted: March 2006.

Third edition: October 2006^{3,4}.

Reprinted: August 2010.

ISBN 1-89940- 01-2

It is with some reservation that I supply equations to this book. One of the most common failings for engineering students is that they solve problems through memory rather than by applying the correct methodology based upon a fundamental understanding. This type of training does not serve the students well when they move into industry. Thus, while I welcome you to use this book as a quick reference and a study aid, I expect you to be able to derive each of these equations from basic principles. Do not be content with a shallow understanding of this subject!

CWW

Tabulated data has been generated from fitted formulæ to certain accuracies. Where differences arise between other published steam tables, these are small. This book of tables should furnish sufficient accuracy for both student and general engineering use.

MWB

The authors wish to be forgiven for any errors and take no responsibility at all for any disasters caused through the use of this book.

SBMB

¹ Printed in The United Kingdom by The University Print Service
Bolsover Street, Sheffield, S3 7NA

² The University Of Sheffield, © 2004-6

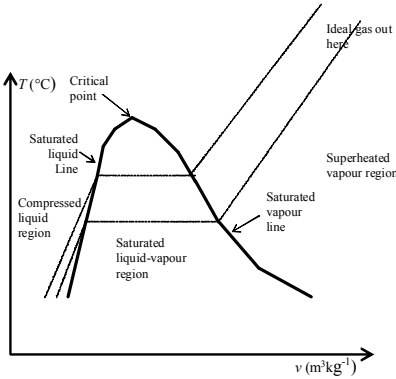
³ Changes in this edition were made in part by P. Mylon

⁴ Cover illustrations Simon Beck (AlphaBeck.co.uk)

Table of Contents

INTRODUCTION TO THERMODYNAMICS	2
Combustion Equations	4
Vapour mixtures	5
Formulæ related to combustion engines	7
Some Dimensionless Groups	8
Steam and Refrigerant Tables	10
Saturated steam: liquid and vapour: temperature based	10
Superheated steam - enthalpy and entropy up to 300°C	14
Supercritical steam	18
Low pressure (<100 kPa) superheated steam - enthalpy and entropy	19
Compressed liquid water	20
Psychrometric chart	22
R134a saturated refrigerant: liquid and vapour	24
R134a superheated refrigerant	26
P-h diagram for R134a	28
Combustion Information	29
CO - enthalpy, internal energy and entropy at atmospheric pressure	34
H ₂ O- enthalpy, internal energy and entropy at atmospheric pressure	36
N ₂ - enthalpy, internal energy and entropy at atmospheric pressure	38
O ₂ - enthalpy, internal energy and entropy at atmospheric pressure	40
CO ₂ - enthalpy, internal energy and entropy at atmospheric pressure	42
H ₂ - enthalpy, internal energy and entropy at atmospheric pressure	44
Specific heat of gases at constant pressure	46
Molar Gibbs function at atmospheric pressure	47
Heat Transfer	48
Convection heat transfer	49
Heat exchangers	51
Radiation	53
Correction factors for LMTD method	54
NTU-effectiveness	55
Thermodynamic Properties of Gases, Liquids and Solids	56
Thermodynamic properties of gaseous steam and R134a, and air	58
FLOW OF FLUIDS	60
Pressure loss coefficients	62
Moody diagram	63
Boundary layers	64
Equations of Motion	65
Turbulence	67
Aerodynamics and High-Speed Flow	68
Shock waves	69
Renewable Energy Data	76
GENERAL INFORMATION	81

INTRODUCTION TO THERMODYNAMICS



Quality v used as illustration

$$\frac{v_{total} - v_f}{v_g - v_f} = x$$

where x is the quality

$$v_{total} = v_f + x(v_g - v_f)$$

Ideal gas behaviour

$$\begin{matrix} \text{kPa} & \text{m}^3 & \text{kg} & \text{kJkg}^{-1}\text{K}^{-1} & \text{K} \\ \downarrow & \downarrow & \downarrow & \downarrow & \downarrow \end{matrix}$$

$$p \times V = m \times R \times T$$

$$\text{where } R = \frac{R_u}{M} \text{ and } \frac{p_1 V_1}{T_1} = \frac{p_2 V_2}{T_2}$$

where R_u is $8.314 \text{ kJ kmol}^{-1} \text{ K}^{-1}$.

Gas Phase Property Summary

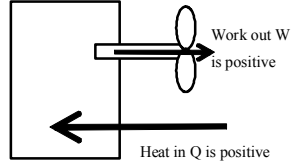
	Ideal Gas	Real Gas or Vapour	
Equation of State	$pv = RT$	Proprietary equation <u>or</u> chart for $z = \frac{pv}{RT}$	
Internal Energy	$u = h - RT$	$u = h - pv$	
	'Perfect' Gas	'Semi'-Perfect Gas	Real Gas or Vapour
Specific Heat Capacities	c_p, c_v, γ all constant $c_p = \frac{\gamma}{\gamma - 1} R$ where $\gamma = \frac{c_p}{c_v}$	$c_p = c_p(T)$ $c_v = c_p - R$ $\gamma = \gamma(T)$	$c_p = c_p(p, T)$ $c_v = c_v(p, T)$
Enthalpy	$h_2 - h_1 = c_p(T_2 - T_1)$	$h = h_0 + \int_{T_0}^T c_p dT = h^*$ (e.g. $h_0 = 0$ when $T_0 = 25^\circ\text{C}$ for table of \tilde{h})	$h = h(p, T)$ <u>or</u> chart for $\frac{h^* - h}{RT_c}$
Entropy	$s_2 - s_1 = c_p \ln \frac{T_2}{T_1} - R \ln \frac{p_2}{p_1}$ (but if $s_2 = s_1$ use $pv^\gamma = \text{constant}$)	$s = s^\ominus - R \ln \frac{p}{p^\ominus} = s^* \text{ and}$ $\tilde{s}_2 - \tilde{s}_1 = \tilde{s}_2^\ominus - \tilde{s}_1^\ominus - R_u \ln \frac{p_2}{p_1}$ where $\tilde{s}^\ominus = \int_0^T \tilde{c}_p \frac{dT}{T}$ s^\ominus	$s = s(p, T)$ <u>or</u> chart for $\frac{s^* - s}{R}$

Polytropic processes

Polytropic expansion:

$$pV^n = \text{constant} \quad \frac{T_2}{T_1} = \left(\frac{p_2}{p_1}\right)^{\frac{n-1}{n}} = \left(\frac{V_1}{V_2}\right)^{n-1}$$

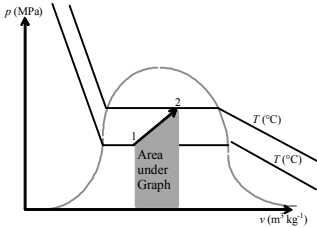
For an isentropic process, $n = \gamma$, where $\gamma = \frac{c_p}{c_v}$.



The first law of thermodynamics

The first law of thermodynamics for a closed system is:

$$Q - W = \Delta U \text{ or } Q - W = m\Delta u$$



For a reversible process, $W_{rev} = \int p dV$

For any process the value of the integral $\int_1^2 p dV$ is the area under the p - V graph.

For an ideal gas polytropic process ($n \neq 1$):

$$W = \int_1^2 p dV = \frac{p_1 V_1 - p_2 V_2}{n - 1} \text{ and } Q = W \times \left(\frac{\gamma - n}{\gamma - 1}\right)$$

For an isothermal process ($n = 1$):

$$\int_1^2 p dV = p_1 V_1 \ln\left(\frac{V_2}{V_1}\right)$$

The steady flow energy equation for a single stream is:

$$\dot{Q} - \dot{W} = \frac{1}{2} \dot{m}(C_2^2 - C_1^2) + \dot{m}g(z_2 - z_1) + \dot{m}(h_2 - h_1)$$

(Be careful to use consistent units)

For an ideal gas, a solid and most liquids:

$$\Delta h = c_p \Delta T \text{ and } \Delta u = c_v \Delta T$$

Entropy and the Second Law

In general, $dS = \left(\frac{dQ}{T}\right)_{rev}$. For ideal gases:

$$s_2 - s_1 = c_v \ln \frac{T_2}{T_1} + R \ln \frac{v_2}{v_1} = c_p \ln \frac{T_2}{T_1} - R \ln \frac{p_2}{p_1}$$

Isentropic efficiency of an expansion:

Isentropic efficiency of a compression:

$$\eta_E = \frac{h_1 - h_{2a}}{h_1 - h_{2s}}$$

$$\eta_C = \frac{h_{2s} - h_1}{h_{2a} - h_1}$$

Gibbs free energy:

$$\tilde{g} = \tilde{h} - T\tilde{s}$$

Maximum efficiencies of cycles

Reversible heat engine:

Reversible refrigerator:

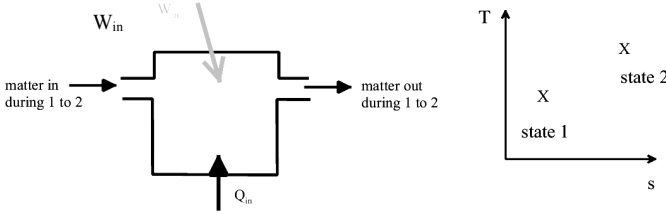
Reversible heat pump:

$$\eta_{Th} = \frac{T_{high} - T_{low}}{T_{high}}$$

$$COP_R = \frac{T_{low}}{T_{high} - T_{low}}$$

$$COP_{HP} = COP_R + 1 = \frac{T_{high}}{T_{high} - T_{low}}$$

Global energy conservation or Unsteady Flow Energy Equation (UFEE)



$$m_2 u_2 - m_1 u_1 = \sum m_i h_i - \sum m_e h_e + W + Q$$

Exergy

Specific exergy (function):

$$\beta = h - T_0 s$$

Thermal exergy:

$$\varepsilon^q = q \left(1 - \frac{T_0}{T} \right)$$

Rational efficiency:

$$\Psi = \frac{\sum \Delta \dot{\varepsilon}_{output}}{\sum \Delta \dot{\varepsilon}_{input}} = 1 - \frac{I}{\sum \Delta \dot{\varepsilon}_{input}} = \frac{W_{net}}{W_{max}}$$

or when applicable:

$$\Psi = \frac{W_{net}}{-\Delta G_0} \quad i = T_0 \pi = T_0 \left(s_{out} - s_{in} - \sum \frac{q}{T} \right)$$

Combustion Equations

Combustion calculations are based on the conservation of mass principle which states that the mass of each element is conserved during a chemical reaction. The ratio of mass of air to mass of fuel is called the Air Fuel Ratio.

$$AFR = \frac{m_{air}}{m_{fuel}}$$

The heating value of a fuel is defined as the amount of heat released when a fuel is burned completely in a steady process and the reactants are returned to the initial state. The higher heating value represents the value when water in the products is in the liquid form.

$$HHV = LHV + (m_{H_2O} h_{fg})_{H_2O}$$

Taking heat transfer to the system and work done by the system to be positive.

Conservation of energy for a chemical reacting steady flow system per unit mole of fuel is given by:

$$Q_{net} - W_{net} = \sum_{Products} N_e [\bar{h}_f^\circ + (\bar{h}_T - \bar{h}^\circ)]_e - \sum_{Reactants} N_i [\bar{h}_f^\circ + (\bar{h}_T - \bar{h}^\circ)]_i$$

For a closed system this becomes:

$$Q_{net} - W_{net} = \sum_{Products} N_e [\bar{h}_f^\circ + (\bar{h}_T - \bar{h}^\circ) - P\bar{v}]_e - \sum_{Reactants} N_i [\bar{h}_f^\circ + (\bar{h}_T - \bar{h}^\circ) - P\bar{v}]_i$$

Vapour mixtures

For temperatures in the range about -10 to about 50°C the enthalpy of the dry air is given by:

$$\Delta h_a = [1.005(kJ/kg^{-1})]\Delta T, \text{ with } T \text{ in } ^\circ\text{C}, \text{ and } \Delta h_a \text{ in } kJ/kg^{-1}$$

Water / air mixtures can be treated as an ideal gas, whose pressure is the sum of that of dry air and water vapour:

$$P = P_a + P_v$$

The saturated vapour value of the enthalpy is a function of temperature and can be expressed as:

$$h_v = h_g(T)2501.5 + 1.82T(kJ/kg^{-1}) \text{ with } T \text{ in } ^\circ\text{C}, \text{ and } \Delta h_v \text{ in } kJ/kg^{-1}$$

The absolute and relative humidity are defined by:

$$\omega = \frac{m_v}{m_a} = \frac{P_v V / (R_v T)}{P_a V / (R_a T)} = \frac{P_v / (R_v)}{P_a / (R_a)} = 0.622 \frac{P_v}{P_a} \quad \phi = \frac{m_v}{m_g} = \frac{P_v}{P_g}$$

The absolute and relative humidity are related by:

$$\phi = \frac{\omega P}{(0.622 + \omega)P_g} \text{ and } \omega = \frac{0.622\phi P_g}{P - \phi P_g}$$

Mixture Formulæ

The composition of a gas mixture is described by specifying either the *mass fraction* mf_i or the *mole fraction* y_i of each component i :

$$mf_i = \frac{m_i}{m_m} \text{ and } y_i = \frac{N_i}{N_m}$$

The total mass of the mixture m_m and the total moles of mixture N_m are defined as:

$$N_m = \sum_{i=1}^k N_i \text{ and } m_m = \sum_{i=1}^k m_i$$

The average molar mass and gas constant are given as:

$$M_m = \frac{m_m}{N_m} = \frac{\sum m_i}{N_m} = \frac{\sum N_i M_i}{N_m} = \sum_{i=1}^k y_i M_i \text{ and } R_m = \frac{R_u}{M_m}$$

To change between a mole fraction analysis and a mass fraction analysis use:

$$mf_i = \frac{y_i M_i}{\sum_{i=1}^k y_i M_i} \text{ and } y_i = \frac{mf_i / M_i}{\sum_{i=1}^k mf_i / M_i}$$

Amagat's law of additive volumes states that the volume of a gas mixture is equal to the sum of the volumes each gas would occupy if it existed alone at the mixture temperature and pressure.

Amagat's law:
$$V_m = \sum_{i=1}^k V_i(T_m, P_m)$$

The partial pressure of component i is defined as the product of the mole fraction and the mixture pressure according to Dalton's law. For the component i :

$$P_i = y_i P_m$$

Dalton's law:
$$P_m = \sum_{i=1}^k P_i(T_m, V_m)$$

The extensive properties of a gas mixture

The *extensive properties* of a gas mixture, in general, can be determined by summing the contributions of each component of the mixture. The evaluation of *intensive properties* of a gas mixture, however, involves averaging in terms of mass or mole fractions:

$$\begin{aligned}
 U_m &= \sum_{i=1}^k U_i = \sum_{i=1}^k m_i u_i = \sum_{i=1}^k N_i \bar{u}_i \quad (\mathbf{kJ}) \\
 H_m &= \sum_{i=1}^k H_i = \sum_{i=1}^k m_i h_i = \sum_{i=1}^k N_i \bar{h}_i \quad (\mathbf{kJ}) \\
 S_m &= \sum_{i=1}^k S_i = \sum_{i=1}^k m_i s_i = \sum_{i=1}^k N_i \bar{s}_i \quad (\mathbf{kJK}^{-1})
 \end{aligned}$$

and

$$\begin{aligned}
 u_m &= \sum_{i=1}^k m f_i u_i \quad \text{and} \quad \bar{u}_m = \sum_{i=1}^k y_i \bar{u}_i \quad (\mathbf{kJ kg}^{-1} \text{ or } \mathbf{kJ kmol}^{-1}) \\
 h_m &= \sum_{i=1}^k m f_i h_i \quad \text{and} \quad \bar{h}_m = \sum_{i=1}^k y_i \bar{h}_i \quad (\mathbf{kJ kg}^{-1} \text{ or } \mathbf{kJ kmol}^{-1}) \\
 s_m &= \sum_{i=1}^k m f_i s_i \quad \text{and} \quad \bar{s}_m = \sum_{i=1}^k y_i \bar{s}_i \quad (\mathbf{kJ kg}^{-1} \mathbf{K}^{-1} \text{ or } \mathbf{kJ kmol}^{-1} \mathbf{K}^{-1})
 \end{aligned}$$

Specific heat capacities of mixtures

$$\begin{aligned}
 C_{v,m} &= \sum_{i=1}^k m f_i C_{v,i} \quad \text{and} \quad \bar{C}_{v,m} = \sum_{i=1}^k y_i \bar{C}_{v,i} \\
 C_{p,m} &= \sum_{i=1}^k m f_i C_{p,i} \quad \text{and} \quad \bar{C}_{p,m} = \sum_{i=1}^k y_i \bar{C}_{p,i}
 \end{aligned}$$

The entropy change of a mixture

The entropy change of the mixture per mass of mixture is:

$$\Delta S_m = \frac{\Delta S_m}{m_m} = \sum_{i=1}^k m f_i \Delta s_i = \sum_{i=1}^k m f_i \left(C_{p,i} \ln \left(\frac{T_2}{T_1} \right) - R_i \ln \left(\frac{P_{i,2}}{P_{i,1}} \right) \right)$$

The entropy change of the mixture per mole of mixture is:

$$\Delta \bar{s}_m = \frac{\Delta S_m}{N_m} = \sum_{i=1}^k y_i \Delta \bar{s}_i = \sum_{i=1}^k y_i \left(\bar{C}_{p,i} \ln \left(\frac{T_2}{T_1} \right) - R_i \ln \left(\frac{P_{i,2}}{P_{i,1}} \right) \right)$$

In these last two equations, remember:

$$P_{i,1} = y_{i,1} P_{m,1} \quad \text{and} \quad P_{i,2} = y_{i,2} P_{m,2}$$

Formulæ related to combustion engines

Scavenge ratio or delivery ratio, λ :

$$\lambda = \frac{m_s}{m_i}$$

Scavenge efficiency, η_{sc} :

$$\eta_{sc} = \frac{m_a}{m_a + m_g}$$

Charging efficiency, η_{ch} :

$$\eta_{ch} = \frac{m_a}{m_i}$$

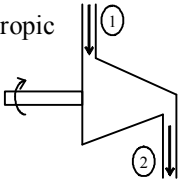
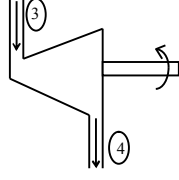
Trapping efficiency, η_{tr} :

$$\eta_{tr} = \frac{m_a}{m_s} = \frac{\eta_{ch}}{\lambda}$$

- V_t : cylinder trapping volume
- m_i : ideal trapped air mass = $\rho_s V_t$
- m_a : actual air mass in the cylinder

Where we use the following definition

- m_g : mass of residual gas in the cylinder
- m_s : mass of air supplied to the cylinder
- Perfect displacement : $\eta_{ch} = \lambda$
- Perfect mixing : $d\eta_{ch} = d\lambda(1 - \eta_{ch})$
- Short circuit : $d\eta_{ch} = 0$

Compressor efficiency	polytropic		Turbine efficiency	polytropic	

$$\frac{T_{02}}{T_{01}} = \left(\frac{p_{02}}{p_{01}}\right)^{\frac{\gamma-1}{\gamma\eta_{sc}}}$$

$$\frac{T_{04}}{T_{03}} = \left(\frac{p_{04}}{p_{03}}\right)^{\frac{\gamma-1}{\gamma}\eta_{\delta t}}$$

Choked

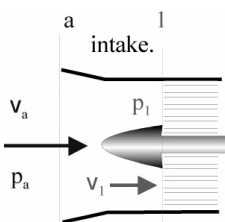
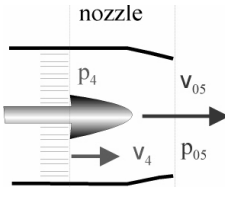
$$T_5 = \frac{2}{\gamma + 1} T_{04}, \quad V_5 = \sqrt{\gamma R T_5}$$

nozzle:

T_5 static temperature of the jet, T_{04} total temperature after the turbine.

Propulsive thrust:

$$\eta_p = \frac{\text{thrust power}}{\text{total power}}$$

	<p>Intake nozzle efficiency</p> $\eta_i = \frac{T_{01'} - T_a}{T_{01} - T_a}$		<p>Propelling nozzle efficiency</p> $\eta_j = \frac{T_{04} - T_5}{T_{04} - T_{5'}}$
---	--	---	--

Some Dimensionless Groups

Biot Number	$Bi = \frac{h_t \Delta x}{k}$	$\frac{\text{Thermal internal resistance}}{\text{Surface film resistance}}$ $\Delta x = \text{mid-plane distance}$
Cauchy Number	$Ca = \frac{\rho u^2}{E_v}$	$\frac{\text{Inertia force}}{\text{Compressibility force}}$
Froude Number	$Fr = \frac{u}{\sqrt{gL}} \left(\text{or } \frac{u^2}{gL} \right)$	$\frac{\text{Inertia force}}{\text{Gravity force}}$
Grashof Number (free convection)	$Gr = \frac{\beta g L^3 \theta}{\nu^2}$	$\frac{\text{Buoyancy force}}{\text{Viscous force}}$
Knudsen Number	$Kn = \frac{\lambda}{L}$	$\frac{\text{Length of mean free path}}{\text{Characteristic dimension}}$ or number of particles across dimension
Mach. Number	$M = \frac{u}{a}$	$\frac{\text{Inertia force}}{\text{Compressibility force}}$
Nusselt Number	$Nu_L = \frac{h_c L}{k}$	$\frac{\text{Convective heat transfer}}{\text{Conductive heat transfer}}$
Peclet Number	$Pe_L = \frac{c_p \rho u L}{k} = Re_L \cdot Pr$	$\frac{\text{Bulk heat transfer}}{\text{Conductive heat transfer}}$
Prandtl Number	$Pr = \frac{c_p \mu}{k}$	$\frac{\text{Thickness of thermal boundary layer}}{\text{Thickness of fluid boundary layer}}$
Reynolds Number	$Re_L = \frac{\rho u L}{\mu} = \frac{u L}{\nu}$	$\frac{\text{Inertia force}}{\text{Viscous force}}$
Stanton Number	$St = \frac{h_c}{\rho u c_p} = \frac{Nu_L}{Pe_L}$	$\frac{\text{Heat transferred}}{\text{Thermal capacity of fluid}}$
Stokes Number	$\frac{nL^2}{\nu} = \frac{nL^2 \rho}{\mu} = Re_L \cdot Sr$	$\frac{\text{Local inertial force}}{\text{Viscous force}}$
Strouhal Number	$Sr = \frac{nL}{u}$	$\frac{\text{Local inertial force}}{\text{Inertial force}}$
Weber Number	$We_L = \frac{\rho u^2 L}{\sigma}$	$\frac{\text{Inertia force}}{\text{Surface tension force}}$
Force Coefficient	$\frac{F}{\frac{1}{2} \rho u^2 L^2}$	$\frac{\text{Force}}{\text{Inertial force}}$
Pressure Loss Coefficient <i>Euler number</i>	$\frac{\Delta p}{\frac{1}{2} \rho u^2}$	$\frac{\text{Pressure loss}}{\text{Dynamic pressure}}$
Friction Coefficient	$(f \text{ or } c_f) = \frac{\tau_0}{\frac{1}{2} \rho \bar{u}^2}$	(Where τ_0 is fluid shear stress at a wall)

This page is intentionally left blank

Steam and Refrigerant Tables

Saturated steam: liquid and vapour: temperature based

T °C	P(sat) kPa	$v_f \times 10^3$ $m^3 kg^{-1}$	v_g $m^3 kg^{-1}$	u_f $kJ kg^{-1}$	u_g $kJ kg^{-1}$	h_f $kJ kg^{-1}$	h_g $kJ kg^{-1}$	s_f $kJ kg^{-1}K^{-1}$	s_g $kJ kg^{-1}K^{-1}$
0.01	0.6117	1.000	206	0.0	2375	0	2501	0.0	9.156
5	0.8725	1.000	147.0	21.0	2382	21.0	2510	0.07625	9.025
10	1.228	1.000	106.3	42.0	2389	42.0	2519	0.1511	8.900
15	1.706	1.000	77.89	63.0	2396	63.0	2528	0.2245	8.780
20	2.339	1.001	57.76	83.9	2402	83.9	2537	0.2965	8.666
25	3.17	1.003	43.34	105	2409	105	2547	0.3672	8.557
30	4.247	1.004	32.88	126	2416	126	2556	0.4368	8.452
35	5.629	1.006	25.20	147	2423	147	2565	0.5051	8.352
40	7.385	1.007	19.51	168	2429	168	2574	0.5724	8.256
45	9.595	1.009	15.25	188	2436	188	2582	0.6386	8.163
50	12.35	1.012	12.03	209	2443	209	2591	0.7038	8.075
55	15.76	1.014	9.564	230	2449	230	2600	0.768	7.990
60	19.95	1.017	7.667	251	2456	251	2609	0.8313	7.908
65	25.04	1.019	6.193	272	2462	272	2618	0.8937	7.830
70	31.2	1.022	5.040	293	2469	293	2626	0.9551	7.754
75	38.6	1.025	4.129	314	2475	314	2635	1.016	7.681
80	47.42	1.029	3.405	335	2482	335	2643	1.076	7.611
85	57.87	1.032	2.826	356	2488	356	2651	1.135	7.543
90	70.18	1.036	2.359	377	2494	377	2660	1.193	7.478
95	84.61	1.039	1.981	398	2500	398	2668	1.25	7.415
100	101.4	1.043	1.672	419	2506	419	2676	1.307	7.354
110	143.4	1.051	1.209	461	2518	461	2691	1.419	7.238
120	198.7	1.060	0.8913	504	2529	504	2706	1.528	7.129
130	270.3	1.069	0.6681	546	2540	546	2720	1.635	7.027
140	361.5	1.079	0.5085	589	2550	589	2733	1.739	6.929
150	476.2	1.090	0.3925	632	2559	632	2746	1.842	6.837
160	618.2	1.102	0.3068	675	2568	676	2757	1.943	6.749
170	792.2	1.114	0.2426	718	2576	719	2768	2.042	6.665
180	1003	1.127	0.1938	762	2583	763	2777	2.139	6.584
190	1255	1.141	0.1564	806	2589	807	2785	2.235	6.506
200	1555	1.156	0.1272	851	2594	852	2792	2.331	6.430
220	2320	1.190	0.08609	941	2601	944	2801	2.518	6.284
240	3347	1.229	0.05971	1033	2603	1037	2803	2.702	6.142
260	4692	1.275	0.04218	1129	2599	1135	2797	2.885	6.002
280	6417	1.332	0.03015	1228	2586	1237	2780	3.068	5.858
300	8588	1.403	0.02166	1333	2564	1345	2750	3.255	5.706
320	11280	1.498	0.01547	1445	2526	1462	2701	3.449	5.537
340	14600	1.638	0.01078	1571	2465	1595	2622	3.66	5.336
360	18670	1.895	0.00695	1726	2352	1762	2482	3.916	5.054
374.14	22050	2.864	0.00339	1978	2058	2041	2133	4.341	4.482

Saturated steam: liquid and vapour: up to 1 bar

P kPa	T(sat) °C	$v_f \times 10^3$ $m^3 kg^{-1}$	v_g $m^3 kg^{-1}$	u_f $kJ kg^{-1}$	u_g $kJ kg^{-1}$	h_f $kJ kg^{-1}$	h_g $kJ kg^{-1}$	s_f $kJ kg^{-1} K^{-1}$	s_g $kJ kg^{-1} K^{-1}$
0.6113	0.0	1.000	206.1	0	2375	0	2501	0.000	9.156
1.0	7.0	1.000	129.2	29.30	2384	29.30	2514	0.106	8.975
2.0	17.5	1.001	66.99	54.69	2399	73.43	2533	0.261	8.723
2.5	21.1	1.002	54.24	88.42	2404	88.42	2539	0.312	8.642
3.0	24.1	1.003	45.65	101.0	2408	101.0	2545	0.354	8.576
3.5	26.7	1.003	39.47	111.8	2411	111.8	2550	0.391	8.521
4.0	29.0	1.004	34.79	121.4	2415	121.4	2554	0.422	8.473
4.5	31.0	1.004	31.13	130.0	2417	130.0	2557	0.451	8.431
5.0	32.9	1.005	28.19	137.7	2420	137.8	2561	0.476	8.394
5.5	34.58	1.005	25.76	144.9	2422	144.9	2564	0.499	8.360
6.0	36.2	1.006	23.73	151.5	2424	151.5	2567	0.521	8.329
7.0	39.0	1.008	20.52	163.3	2428	163.4	2572	0.559	8.274
8.0	41.5	1.008	18.10	173.8	2431	173.8	2576	0.593	8.227
9.0	43.7	1.009	16.20	183.2	2434	183.3	2580	0.622	8.186
10	45.8	1.010	14.67	191.8	2437	191.8	2584	0.649	8.149
11	47.7	1.011	13.41	199.6	2440	199.7	2587	0.674	8.115
12	49.4	1.012	12.36	206.9	2442	206.9	2590	0.696	8.085
13	51.0	1.013	11.46	213.7	2444	213.7	2593	0.717	8.057
14	52.5	1.013	10.69	220.0	2446	220.0	2596	0.737	8.031
15	54.0	1.014	10.02	225.9	2448	225.9	2598	0.755	8.007
16	55.3	1.015	9.431	231.5	2450	231.6	2601	0.772	7.985
17	56.6	1.015	8.909	236.9	2451	236.9	2603	0.788	7.964
18	57.8	1.016	8.443	241.9	2453	242.0	2605	0.804	7.944
20	60.1	1.017	7.648	251.4	2456	251.4	2609	0.832	7.907
25	65.0	1.020	6.203	271.9	2462	272.0	2617	0.893	7.830
30	69.1	1.022	5.229	289.2	2468	289.3	2625	0.944	7.768
35	72.7	1.024	4.525	304.3	2472	304.3	2631	0.988	7.715
40	75.9	1.026	3.993	317.6	2476	317.6	2636	1.026	7.669
45	78.7	1.028	3.576	329.6	2480	329.6	2641	1.060	7.629
50	81.3	1.030	3.240	340.5	2483	340.5	2645	1.091	7.593
55	83.7	1.032	2.964	350.5	2486	350.6	2649	1.119	7.561
60	85.9	1.033	2.732	359.8	2489	359.9	2653	1.145	7.531
65	88.0	1.035	2.535	368.5	2492	368.6	2656	1.170	7.504
70	89.9	1.036	2.365	376.7	2494	376.8	2659	1.192	7.479
75	91.8	1.037	2.217	384.4	2496	384.4	2662	1.213	7.456
80	93.5	1.039	2.087	391.6	2498	391.7	2665	1.233	7.434
85	95.1	1.040	1.972	398.5	2500	398.6	2668	1.252	7.414
90	96.7	1.041	1.870	405.1	2502	405.2	2670	1.270	7.394
95	98.2	1.042	1.777	411.4	2504	411.5	2673	1.287	7.376
100	99.6	1.043	1.694	417.4	2506	417.5	2675	1.303	7.359

Note: The actual values of v_f are 10^3 times smaller than the figures given. For example, the specific volume of saturated liquid water at 20kPa is $0.001017 m^3 kg^{-1}$.

Saturated steam: liquid and vapour: 1 to 15 bar

P kPa	T(sat) °C	$v_f \times 10^3$ $m^3 kg^{-1}$	v_g $m^3 kg^{-1}$	u_f $kJ kg^{-1}$	u_g $kJ kg^{-1}$	h_f $kJ kg^{-1}$	h_g $kJ kg^{-1}$	s_f $kJ kg^{-1} K^{-1}$	s_g $kJ kg^{-1} K^{-1}$
100	99.6	1.043	1.694	417.4	2506	417.5	2675	1.303	7.359
110	102.3	1.045	1.550	428.7	2509	428.8	2679	1.333	7.327
120	104.8	1.047	1.429	439.2	2512	439.4	2683	1.361	7.298
130	107.1	1.049	1.325	449.1	2514	449.2	2687	1.387	7.271
140	109.3	1.051	1.237	458.3	2517	458.4	2690	1.411	7.246
150	111.4	1.053	1.159	467.0	2519	467.1	2693	1.434	7.223
175	116.0	1.057	1.004	486.8	2525	487.0	2700	1.485	7.172
200	120.2	1.061	0.886	504.5	2529	504.7	2706	1.530	7.127
225	124.0	1.064	0.793	520.5	2533	520.7	2712	1.571	7.088
250	127.4	1.067	0.719	535.1	2537	535.3	2717	1.607	7.053
275	130.6	1.070	0.657	548.6	2540	548.9	2721	1.641	7.021
300	133.5	1.073	0.606	561.1	2543	561.4	2725	1.672	6.992
325	136.3	1.076	0.562	572.8	2546	573.2	2729	1.700	6.965
350	138.9	1.079	0.524	583.9	2549	584.3	2732	1.727	6.940
375	141.3	1.081	0.491	594.3	2551	594.7	2735	1.753	6.917
400	143.6	1.084	0.462	604.2	2553	604.7	2738	1.776	6.896
425	145.8	1.086	0.437	613.7	2555	614.1	2741	1.799	6.875
450	147.9	1.088	0.414	622.7	2557	623.1	2743	1.820	6.856
475	149.9	1.090	0.393	631.3	2559	631.8	2746	1.841	6.838
500	151.8	1.093	0.375	639.5	2561	640.1	2748	1.860	6.821
550	155.5	1.097	0.343	655.2	2564	655.8	2752	1.897	6.789
600	158.8	1.101	0.316	669.7	2567	670.4	2756	1.931	6.759
650	162.0	1.104	0.293	683.4	2569	684.1	2760	1.962	6.732
700	165.0	1.108	0.273	696.2	2572	697.0	2763	1.992	6.707
750	167.8	1.111	0.256	708.4	2574	709.2	2766	2.019	6.684
800	170.4	1.115	0.240	720.0	2576	720.9	2768	2.046	6.662
850	173.0	1.118	0.227	731.0	2578	732.0	2771	2.070	6.641
900	175.4	1.121	0.215	741.6	2580	742.6	2773	2.094	6.621
950	177.7	1.124	0.204	751.7	2581	752.7	2775	2.117	6.603
1000	179.9	1.127	0.194	761.4	2583	762.5	2777	2.138	6.585
1050	182.0	1.130	0.186	770.7	2584	771.9	2779	2.159	6.568
1100	184.1	1.133	0.177	779.8	2585	781.0	2781	2.178	6.552
1150	186.1	1.136	0.170	788.5	2587	789.8	2782	2.198	6.537
1200	188.0	1.138	0.163	797.0	2588	798.3	2784	2.216	6.522
1250	189.8	1.141	0.157	805.2	2589	806.6	2785	2.234	6.507
1300	191.6	1.144	0.151	813.1	2590	814.6	2786	2.251	6.494
1350	193.4	1.146	0.146	820.8	2591	822.4	2788	2.267	6.480
1400	195.1	1.149	0.141	828.4	2592	830.0	2789	2.284	6.467
1450	196.7	1.151	0.136	835.7	2593	837.3	2790	2.299	6.455
1500	198.3	1.154	0.132	842.8	2593	844.5	2791	2.314	6.443

Saturated steam: liquid and vapour: 15 bar to critical

P(sat) kPa	T(sat) °C	$v_f \times 10^3$ $m^3 kg^{-1}$	v_g $m^3 kg^{-1}$	u_f $kJ kg^{-1}$	u_g $kJ kg^{-1}$	h_f $kJ kg^{-1}$	h_g $kJ kg^{-1}$	s_f $kJ kg^{-1} K^{-1}$	s_g $kJ kg^{-1} K^{-1}$
1500	198.3	1.154	0.132	842.8	2593	844.5	2791	2.314	6.443
1600	201.4	1.159	0.124	856.6	2595	858.4	2793	2.343	6.420
1700	204.3	1.163	0.117	869.7	2596	871.7	2794	2.371	6.398
1800	207.1	1.168	0.110	882.4	2597	884.5	2796	2.397	6.377
1900	209.8	1.172	0.105	894.5	2598	896.7	2797	2.423	6.358
2000	212.4	1.177	0.100	906.1	2599	908.5	2798	2.447	6.339
2200	217.3	1.185	0.091	928.2	2601	930.8	2800	2.492	6.304
2400	221.8	1.193	0.083	949.0	2602	951.8	2801	2.534	6.271
2600	226.1	1.201	0.077	968.5	2602	971.6	2802	2.574	6.241
2800	230.1	1.209	0.071	987.0	2603	990.4	2803	2.611	6.212
3000	233.9	1.217	0.067	1004.6	2603	1008.3	2803	2.645	6.186
3500	242.6	1.235	0.057	1045.4	2603	1049.7	2803	2.725	6.124
4000	250.4	1.252	0.050	1082.4	2602	1087.4	2801	2.797	6.070
4500	257.5	1.269	0.044	1116.4	2600	1122.1	2798	2.861	6.020
5000	264.0	1.286	0.039	1148.1	2597	1154.5	2794	2.921	5.974
5500	270.0	1.303	0.036	1177.8	2594	1184.9	2790	2.976	5.931
6000	275.6	1.319	0.032	1205.8	2590	1213.8	2785	3.027	5.890
6500	280.9	1.335	0.030	1232.5	2586	1241.2	2779	3.076	5.852
7000	285.9	1.352	0.027	1258.0	2581	1267.5	2773	3.122	5.815
7500	290.6	1.368	0.025	1282.5	2576	1292.7	2766	3.166	5.779
8000	295.0	1.384	0.024	1306.0	2570	1317.1	2759	3.208	5.745
8500	299.3	1.401	0.022	1328.8	2565	1340.7	2751	3.248	5.712
9000	303.4	1.418	0.020	1350.9	2559	1363.7	2743	3.287	5.679
9500	307.3	1.435	0.019	1372.4	2552	1386.0	2734	3.324	5.647
10000	311.0	1.452	0.018	1393.3	2545	1407.8	2725	3.36	5.616
10500	314.6	1.470	0.017	1413.8	2538	1429.2	2716	3.396	5.585
11000	318.1	1.488	0.016	1433.9	2530	1450.2	2706	3.43	5.554
11500	321.5	1.507	0.015	1453.6	2523	1470.9	2696	3.464	5.524
12000	324.7	1.526	0.014	1473.0	2514	1491.3	2685	3.496	5.494
12500	327.9	1.546	0.013	1492.1	2506	1511.4	2674	3.529	5.464
13000	330.9	1.566	0.0128	1511.0	2497	1531.4	2663	3.561	5.434
14000	336.7	1.610	0.0115	1548.4	2477	1571.0	2638	3.623	5.373
15000	342.2	1.657	0.0103	1585.5	2456	1610.3	2611	3.685	5.311
16000	347.4	1.710	0.0093	1622.6	2432	1649.9	2581	3.746	5.247
17000	352.3	1.770	0.0084	1660.2	2405	1690.3	2548	3.808	5.179
18000	357.0	1.840	0.0075	1699.1	2375	1732.2	2510	3.872	5.106
19000	361.5	1.926	0.0067	1740.3	2339	1776.8	2466	3.94	5.026
20000	365.8	2.038	0.0058	1785.8	2295	1826.6	2412	4.015	4.931
21000	369.9	2.207	0.0050	1841.6	2233	1888.0	2338	4.107	4.808
22060	374.0	2.938	0.003	1990.1	2044	2054.9	2117	4.362	4.457

Superheated steam - enthalpy and entropy up to 300°C

		Saturation		100°C		150°C		200°C		250°C		300°C	
P kPa	T(sat) °C	h_g kJkg ⁻¹	s_g kJkg ⁻¹ K ⁻¹	h kJkg ⁻¹	s kJkg ⁻¹ K ⁻¹	h kJkg ⁻¹	s kJkg ⁻¹ K ⁻¹	h kJkg ⁻¹	s kJkg ⁻¹ K ⁻¹	h kJkg ⁻¹	s kJkg ⁻¹ K ⁻¹	h kJkg ⁻¹	s kJkg ⁻¹ K ⁻¹
20	60.06	2609	7.907	2686	8.126	2782	8.368	2879	8.584	2977	8.781	3077	8.963
40	75.86	2636	7.669	2684	7.801	2781	8.046	2878	8.263	2976	8.46	3076	8.642
60	85.93	2653	7.531	2681	7.608	2780	7.856	2877	8.074	2976	8.272	3076	8.454
80	93.49	2665	7.434	2678	7.470	2778	7.720	2876	7.940	2975	8.139	3075	8.321
100	99.61	2675	7.359	2676	7.361	2777	7.615	2875	7.836	2975	8.035	3075	8.217
120	104.8	2683	7.298			2775	7.528	2875	7.750	2974	7.950	3074	8.132
140	109.3	2690	7.246			2774	7.454	2874	7.677	2973	7.877	3074	8.061
160	113.3	2696	7.201			2772	7.39	2873	7.614	2973	7.815	3073	7.998
180	116.9	2701	7.162			2771	7.332	2872	7.558	2972	7.760	3073	7.943
200	120.2	2706	7.127			2769	7.281	2871	7.508	2971	7.710	3072	7.894
250	127.4	2717	7.053			2765	7.171	2868	7.401	2970	7.605	3071	7.789
300	133.5	2725	6.992			2761	7.079	2866	7.313	2968	7.518	3070	7.704
350	138.9	2732	6.940			2757	7.000	2863	7.238	2966	7.444	3068	7.631
400	143.6	2738	6.896			2753	6.931	2861	7.172	2964	7.38	3067	7.568
500	151.8	2748	6.821					2856	7.061	2961	7.272	3065	7.461
600	158.8	2756	6.759					2851	6.968	2958	7.183	3062	7.374
700	164.9	2763	6.707					2845	6.888	2954	7.107	3059	7.299
800	170.4	2768	6.662					2840	6.818	2950	7.04	3057	7.234
900	175.4	2773	6.621					2834	6.754	2947	6.981	3054	7.177
1000	179.9	2777	6.585					2828	6.696	2943	6.927	3052	7.125
1500	198.3	2791	6.443					2796	6.454	2924	6.711	3038	6.920
2000	212.4	2798	6.339							2903	6.547	3024	6.768
2500	223.9	2802	6.256							2881	6.411	3010	6.646
3000	233.9	2803	6.186							2857	6.289	2994	6.541
3500	242.6	2803	6.124							2830	6.176	2978	6.448
4000	250.4	2801	6.070									2962	6.364
4500	257.4	2798	6.020									2944	6.285
5000	263.9	2794	5.974									2926	6.211
5500	270.0	2790	5.931									2906	6.140
6000	275.6	2785	5.890									2886	6.070
6500	280.9	2779	5.852									2864	6.002
7000	285.8	2773	5.815									2840	5.934
7500	290.5	2766	5.779									2814	5.865
8000	295.0	2759	5.745									2786	5.794
9000	303.3	2743	5.679										
10000	311	2725	5.616										
11000	318.1	2706	5.554										
12000	324.7	2685	5.494										
13000	330.9	2663	5.434										
14000	336.7	2638	5.373										
15000	342.2	2611	5.311										
16000	347.4	2581	5.247										
17000	352.3	2548	5.179										
18000	357.0	2510	5.106										
20000	365.7	2412	4.931										

Superheated steam – enthalpy and entropy 350°C to 700°C

350°C		400°C		450°C		500°C		600°C		700°C		P kPa
h kJkg ⁻¹	s kJkg ⁻¹ K ⁻¹	h kJkg ⁻¹	s kJkg ⁻¹ K ⁻¹	h kJkg ⁻¹	s kJkg ⁻¹ K ⁻¹	h kJkg ⁻¹	s kJkg ⁻¹ K ⁻¹	h kJkg ⁻¹	s kJkg ⁻¹ K ⁻¹	h kJkg ⁻¹	s kJkg ⁻¹ K ⁻¹	
3177	9.131	3280	9.289	3384	9.438	3490	9.58	3706	9.843	3930	10.09	20
3177	8.811	3279	8.969	3384	9.118	3489	9.26	3706	9.523	3930	9.766	40
3177	8.623	3279	8.782	3383	8.931	3489	9.072	3706	9.336	3930	9.578	60
3176	8.49	3279	8.649	3383	8.798	3489	8.939	3706	9.203	3930	9.446	80
3176	8.387	3279	8.545	3383	8.695	3489	8.836	3706	9.100	3929	9.342	100
3175	8.302	3278	8.461	3383	8.610	3489	8.752	3705	9.016	3929	9.258	120
3175	8.23	3278	8.389	3382	8.539	3488	8.68	3705	8.944	3929	9.187	140
3175	8.168	3278	8.327	3382	8.477	3488	8.619	3705	8.883	3929	9.125	160
3174	8.114	3277	8.273	3382	8.422	3488	8.564	3705	8.828	3929	9.071	180
3174	8.064	3277	8.224	3382	8.373	3488	8.515	3705	8.779	3929	9.022	200
3173	7.96	3276	8.12	3381	8.270	3487	8.412	3704	8.676	3929	8.919	250
3172	7.875	3275	8.035	3380	8.185	3487	8.327	3704	8.591	3928	8.834	300
3171	7.803	3275	7.963	3380	8.113	3486	8.255	3704	8.520	3928	8.763	350
3170	7.74	3274	7.9	3379	8.051	3486	8.193	3703	8.458	3928	8.701	400
3168	7.635	3272	7.796	3378	7.947	3484	8.089	3702	8.354	3927	8.598	500
3166	7.548	3271	7.71	3376	7.861	3483	8.004	3702	8.270	3926	8.513	600
3164	7.475	3269	7.637	3375	7.789	3482	7.932	3701	8.198	3926	8.442	700
3162	7.411	3268	7.573	3374	7.726	3481	7.869	3700	8.135	3925	8.379	800
3160	7.354	3266	7.517	3373	7.670	3480	7.814	3699	8.080	3925	8.325	900
3158	7.303	3264	7.467	3371	7.620	3479	7.764	3699	8.031	3924	8.276	1000
3148	7.104	3256	7.271	3365	7.426	3474	7.572	3695	7.841	3921	8.086	1500
3138	6.958	3248	7.129	3358	7.287	3468	7.434	3691	7.704	3918	7.951	2000
3127	6.842	3240	7.017	3352	7.177	3463	7.325	3687	7.598	3915	7.846	2500
3116	6.745	3232	6.923	3345	7.086	3457	7.236	3683	7.510	3912	7.759	3000
3105	6.66	3223	6.843	3338	7.007	3452	7.159	3679	7.436	3909	7.685	3500
3093	6.584	3214	6.771	3331	6.939	3446	7.092	3675	7.371	3906	7.621	4000
3081	6.515	3206	6.707	3324	6.877	3440	7.032	3671	7.313	3903	7.565	4500
3069	6.452	3197	6.648	3317	6.821	3435	6.978	3667	7.261	3900	7.514	5000
3057	6.392	3188	6.594	3310	6.770	3429	6.928	3663	7.213	3897	7.467	5500
3044	6.336	3178	6.543	3303	6.722	3423	6.883	3659	7.169	3894	7.425	6000
3031	6.282	3169	6.495	3296	6.677	3417	6.840	3655	7.129	3891	7.385	6500
3017	6.23	3159	6.45	3288	6.635	3411	6.800	3651	7.091	3888	7.349	7000
3003	6.181	3149	6.407	3281	6.596	3405	6.762	3647	7.056	3885	7.314	7500
2988	6.132	3139	6.366	3273	6.558	3400	6.727	3642	7.022	3882	7.282	8000
2957	6.038	3119	6.288	3258	6.487	3387	6.66	3634	6.960	3876	7.223	9000
2924	5.946	3097	6.214	3242	6.422	3375	6.599	3626	6.905	3870	7.169	10000
2888	5.854	3075	6.144	3226	6.361	3363	6.543	3617	6.853	3864	7.12	11000
2848	5.761	3052	6.076	3210	6.303	3350	6.490	3609	6.805	3858	7.075	12000
2804	5.664	3028	6.011	3193	6.248	3337	6.441	3600	6.761	3852	7.033	13000
2753	5.56	3002	5.946	3176	6.195	3324	6.393	3592	6.719	3845	6.994	14000
2693	5.444	2976	5.882	3158	6.143	3311	6.348	3583	6.680	3839	6.957	15000
2617	5.305	2948	5.818	3140	6.094	3297	6.305	3574	6.642	3833	6.922	16000
		2918	5.754	3121	6.045	3284	6.263	3566	6.606	3827	6.889	17000
		2886	5.688	3102	5.998	3270	6.222	3557	6.572	3820	6.858	18000
		2817	5.553	3062	5.904	3241	6.145	3539	6.508	3808	6.799	20000

Superheated steam – internal energy and specific volume up to 300°C

P kPa	T(sat) °C	Saturation		100°C		150°C		200°C		250°C		300°C	
		u _g kJkg ⁻¹	v _g m ³ kg ⁻¹	u	v	u	v	u	v	u	v	u	v
0.6117	36.6	2425	23.26	2516	28.07	2588	31.84	2661	35.61	2736	39.38	2812	43.15
20	60.1	2456	7.648	2515	8.586	2587	9.749	2661	10.91	2736	12.06	2812	13.22
40	75.9	2476	3.993	2513	4.280	2586	4.866	2660	5.448	2735	6.028	2812	6.607
60	85.9	2489	2.732	2510	2.845	2585	3.239	2660	3.628	2735	4.016	2811	4.402
80	93.5	2498	2.087	2508	2.127	2584	2.425	2659	2.718	2734	3.01	2811	3.300
100	99.6	2506	1.694	2506	1.696	2583	1.937	2658	2.172	2734	2.406	2811	2.639
120	104.8	2512	1.429			2582	1.611	2658	1.808	2733	2.004	2810	2.198
140	109.3	2517	1.237			2581	1.379	2657	1.548	2733	1.716	2810	1.883
160	113.3	2521	1.091			2579	1.204	2656	1.353	2732	1.501	2810	1.647
180	116.9	2525	0.9776			2578	1.068	2655	1.202	2732	1.333	2809	1.463
200	120.2	2529	0.8858			2577	0.9599	2655	1.0800	2731	1.199	2809	1.316
250	127.4	2537	0.7187			2574	0.7644	2653	0.8621	2730	0.9574	2808	1.052
300	133.5	2543	0.6058			2571	0.6340	2651	0.7164	2729	0.7964	2807	0.8753
350	138.9	2549	0.5242			2568	0.5408	2649	0.6124	2728	0.6815	2806	0.7494
400	143.6	2553	0.4624			2564	0.4709	2647	0.5343	2726	0.5952	2805	0.6549
500	151.8	2561	0.3748					2643	0.425	2724	0.4744	2803	0.5226
600	158.8	2567	0.3156					2639	0.3521	2721	0.3939	2801	0.4344
700	164.9	2572	0.2728					2635	0.3000	2719	0.3364	2799	0.3714
800	170.4	2576	0.2403					2631	0.2609	2716	0.2932	2798	0.3242
900	175.4	2580	0.2149					2627	0.2304	2713	0.2596	2796	0.2874
1000	179.9	2583	0.1944					2622	0.206	2710	0.2327	2794	0.2580
1500	198.3	2593	0.1317							2696	0.1520	2784	0.1697
2000	212.4	2599	0.0996							2680	0.1115	2773	0.1255
2500	223.9	2602	0.0800							2663	0.0870	2762	0.09894
3000	233.9	2603	0.0667							2645	0.0706	2751	0.08118
3500	242.6	2603	0.0571							2624	0.0587	2739	0.06845
4000	250.4	2602	0.0498									2726	0.05887
4500	257.4	2600	0.0441									2713	0.05138
5000	263.9	2597	0.0395									2699	0.04535
5500	270.0	2594	0.0356									2684	0.04037
6000	275.6	2590	0.0325									2668	0.03619
6500	280.9	2586	0.0297									2652	0.03261
7000	285.8	2581	0.0274									2633	0.02949
7500	290.5	2576	0.0253									2614	0.02674
8000	295.0	2570	0.0235									2592	0.02428
9000	303.3	2559	0.0205										
10000	311.0	2545	0.0180										
11000	318.1	2530	0.0160										
12000	324.7	2514	0.0143										
13000	330.9	2497	0.0128										
14000	336.7	2477	0.0115										
15000	342.2	2456	0.0103										
16000	347.4	2432	0.0093										
17000	352.3	2405	0.0084										
18000	357.0	2375	0.0075										
20000	365.7	2295	0.0059										

Superheated steam – internal energy and specific volume 350°C to 700°C

350°C		400°C		450°C		500°C		600°C		700°C		P kPa
u kJkg ⁻¹	v m ³ kg ⁻¹	u kJkg ⁻¹	v m ³ kg ⁻¹	u kJkg ⁻¹	v m ³ kg ⁻¹	u kJkg ⁻¹	v m ³ kg ⁻¹	u kJkg ⁻¹	v m ³ kg ⁻¹	u kJkg ⁻¹	v m ³ kg ⁻¹	
2890	46.91	2969	50.68	3050	54.71	3133	58.49	3303	66.06	3481	73.63	0.611
2890	14.37	2969	15.53	3050	16.68	3133	17.84	3303	20.15	3481	22.46	20
2890	7.185	2969	7.763	3050	8.340	3133	8.918	3303	10.07	3481	11.23	40
2889	4.788	2969	5.174	3050	5.559	3133	5.944	3303	6.714	3481	7.484	60
2889	3.590	2969	3.879	3050	4.169	3132	4.458	3303	5.035	3480	5.613	80
2889	2.871	2968	3.103	3049	3.334	3132	3.566	3303	4.028	3480	4.490	100
2888	2.392	2968	2.585	3049	2.778	3132	2.971	3303	3.356	3480	3.741	120
2888	2.049	2968	2.215	3049	2.381	3132	2.546	3303	2.877	3480	3.207	140
2888	1.792	2968	1.938	3049	2.083	3132	2.227	3302	2.517	3480	2.806	160
2888	1.593	2967	1.722	3049	1.851	3132	1.908	3302	2.237	3480	2.494	180
2887	1.433	2967	1.549	3048	1.665	3131	1.781	3302	2.013	3480	2.244	200
2887	1.145	2967	1.239	3048	1.332	3131	1.4250	3302	1.610	3480	1.795	250
2886	0.9536	2966	1.032	3048	1.109	3131	1.187	3302	1.341	3479	1.496	300
2885	0.8167	2965	0.8836	3047	0.9503	3130	1.017	3301	1.149	3479	1.282	350
2884	0.7140	2965	0.7726	3047	0.8311	3130	0.8894	3301	1.006	3479	1.122	400
2883	0.5702	2964	0.6173	3046	0.6642	3129	0.7109	3300	0.8041	3479	0.8970	500
2882	0.4743	2963	0.5137	3045	0.5503	3128	0.5920	3300	0.6698	3478	0.7472	600
2880	0.4058	2961	0.4398	3044	0.4735	3127	0.5070	3299	0.5738	3478	0.6403	700
2879	0.3544	2960	0.3843	3043	0.4139	3127	0.4433	3299	0.5019	3477	0.5601	800
2877	0.3145	2959	0.3411	3042	0.3675	3126	0.3938	3298	0.4459	3477	0.4977	900
2876	0.2825	2958	0.3066	3041	0.3304	3125	0.3541	3297	0.4011	3476	0.4478	1000
2868	0.1866	2952	0.2030	3036	0.2192	3121	0.2352	3295	0.2668	3474	0.2981	1500
2860	0.1386	2946	0.1512	3031	0.1635	3117	0.1757	3292	0.1996	3472	0.2233	2000
2853	0.1098	2940	0.1201	3026	0.1302	3113	0.1400	3289	0.1593	3469	0.1783	2500
2844	0.09056	2934	0.09938	3021	0.1079	3109	0.1162	3286	0.1324	3467	0.1484	3000
2836	0.07680	2927	0.08456	3016	0.09198	3104	0.09919	3282	0.1133	3465	0.1270	3500
2827	0.06647	2921	0.07343	3011	0.08004	3100	0.08644	3279	0.09886	3462	0.1110	4000
2819	0.05842	2914	0.06477	3006	0.07076	3096	0.07652	3276	0.08766	3460	0.0985	4500
2809	0.05197	2907	0.05784	3001	0.06332	3092	0.06858	3273	0.0787	3458	0.08852	5000
2800	0.04668	2901	0.05216	2995	0.05724	3087	0.06209	3270	0.07137	3455	0.08035	5500
2790	0.04225	2894	0.04742	2990	0.05217	3083	0.05667	3267	0.06527	3453	0.07355	6000
2780	0.03849	2887	0.04340	2984	0.04787	3079	0.05209	3264	0.06010	3451	0.06779	6500
2770	0.03526	2879	0.03996	2979	0.04419	3074	0.04816	3261	0.05567	3448	0.06285	7000
2759	0.03245	2872	0.03697	2973	0.04099	3070	0.04475	3258	0.05182	3446	0.05857	7500
2748	0.02997	2865	0.03434	2968	0.03819	3065	0.04177	3255	0.04846	3444	0.05483	8000
2725	0.02582	2849	0.02996	2956	0.03352	3056	0.03679	3248	0.04286	3439	0.04859	9000
2700	0.02244	2833	0.02644	2945	0.02978	3047	0.03281	3242	0.03838	3434	0.04360	10000
2672	0.01963	2816	0.02354	2932	0.02671	3038	0.02955	3236	0.03471	3429	0.03951	11000
2641	0.01722	2799	0.02111	2920	0.02415	3028	0.02683	3229	0.03165	3424	0.03611	12000
2607	0.01512	2780	0.01903	2907	0.02197	3018	0.02452	3223	0.02906	3420	0.03323	13000
2568	0.01323	2761	0.01724	2894	0.02010	3008	0.02254	3216	0.02684	3415	0.03076	14000
2521	0.01148	2741	0.01567	2881	0.01848	2998	0.02083	3209	0.02492	3410	0.02862	15000
2461	0.009766	2719	0.01428	2867	0.01705	2988	0.01932	3203	0.02324	3405	0.02675	16000
		2696	0.01304	2853	0.01578	2978	0.01799	3196	0.02175	3400	0.02510	17000
		2672	0.01192	2838	0.01465	2967	0.01681	3189	0.02043	3395	0.02363	18000
		2618	0.00995	2807	0.01272	2945	0.01479	3175	0.01818	3385	0.02113	20000

Supercritical steam

Supercritical steam - enthalpy and entropy

T (°C)	400°C		600°C		800°C		1000°C		2000°C	
P (MPa)	h kJ kg ⁻¹	s kJkg ⁻¹ K ⁻¹	h kJkg ⁻¹	s kJkg ⁻¹ K ⁻¹	h kJkg ⁻¹	s kJkg ⁻¹ K ⁻¹	h kJkg ⁻¹	s kJkg ⁻¹ K ⁻¹	h kJkg ⁻¹	s kJkg ⁻¹ K ⁻¹
22	2736	5.405	3521	6.447	4058	7.002	4579	7.447	7372	9.056
24	2637	5.237	3503	6.391	4049	6.955	4573	7.403	7371	9.016
26	2510	5.030	3484	6.337	4039	6.911	4567	7.362	7371	8.978
28	2335	4.756	3466	6.286	4030	6.869	4562	7.324	7371	8.943
30	2153	4.476	3447	6.237	4020	6.830	4556	7.288	7370	8.911
35	1989	4.214	3399	6.123	3996	6.741	4542	7.207	7369	8.838
40	1931	4.115	3350	6.017	3973	6.661	4527	7.135	7368	8.775
45	1898	4.051	3301	5.918	3949	6.589	4513	7.071	7367	8.719
50	1874	4.003	3253	5.825	3926	6.523	4499	7.013	7366	8.669
55	1857	3.964	3204	5.736	3903	6.461	4486	6.960	7365	8.624
60	1843	3.932	3157	5.653	3880	6.403	4472	6.910	7364	8.582
70	1823	3.878	3067	5.500	3836	6.298	4446	6.820	7363	8.508
80	1809	3.834	2988	5.367	3793	6.204	4421	6.741	7361	8.444
90	1799	3.797	2921	5.254	3753	6.118	4396	6.669	7360	8.387
100	1791	3.764	2865	5.158	3715	6.041	4373	6.604	7359	8.335
150	1777	3.640	2707	4.848	3566	5.737	4275	6.344	7357	8.136
200	1782	3.552	2645	4.673	3477	5.532	4205	6.156	7359	7.992

Supercritical steam - internal energy and specific volume

T (°C)	400°C		600°C		800°C		1000°C		2000°C	
P (MPa)	u kJkg ⁻¹	v m ³ kg ⁻¹	u kJkg ⁻¹	v m ³ kg ⁻¹	u kJkg ⁻¹	v m ³ kg ⁻¹	u kJkg ⁻¹	v m ³ kg ⁻¹	u kJkg ⁻¹	v m ³ kg ⁻¹
22	2554	0.008256	3161	0.01635	3582	0.02162	3999	0.026350	5108	0.03744
24	2476	0.006732	3147	0.01481	3575	0.01975	3994	0.024130	5106	0.03434
26	2373	0.005285	3133	0.01352	3567	0.01816	3989	0.022250	5103	0.03172
28	2227	0.003854	3118	0.01241	3559	0.01680	3984	0.020640	5101	0.02947
30	2069	0.002798	3103	0.01144	3551	0.01563	3979	0.019240	5099	0.02752
35	1915	0.002105	3066	0.009523	3532	0.01328	3966	0.016450	5092	0.02363
40	1855	0.001911	3027	0.008089	3512	0.01152	3953	0.014360	5086	0.02071
45	1817	0.001803	2987	0.006983	3492	0.01016	3940	0.012740	5080	0.01844
50	1788	0.001731	2947	0.006108	3472	0.009072	3927	0.011440	5074	0.01663
55	1765	0.001676	2907	0.005405	3452	0.008188	3915	0.010380	5068	0.01514
60	1745	0.001633	2867	0.004833	3433	0.007456	3902	0.009504	5062	0.01391
70	1713	0.001566	2789	0.003975	3394	0.006317	3877	0.008129	5050	0.01197
80	1688	0.001516	2717	0.003384	3355	0.005477	3852	0.007105	5038	0.01052
90	1666	0.001476	2653	0.002969	3318	0.004836	3828	0.006316	5027	0.00939
100	1647	0.001443	2598	0.002672	3282	0.004336	3804	0.005690	5015	0.00849
150	1577	0.001331	2412	0.001969	3125	0.002942	3694	0.003869	4961	0.00582
200	1530	0.001262	2306	0.001697	3008	0.002343	3602	0.003017	4911	0.00450

Low pressure (<100 kPa) superheated steam - enthalpy and entropy

T (°C)	Saturation		50°C		100°C		200°C		400°C	
P (kPa)	h_g kJ kg ⁻¹	s_g kJkg ⁻¹ K ⁻¹	h kJkg ⁻¹	s kJkg ⁻¹ K ⁻¹	h kJkg ⁻¹	s kJkg ⁻¹ K ⁻¹	h kJkg ⁻¹	s kJkg ⁻¹ K ⁻¹	h kJkg ⁻¹	s kJkg ⁻¹ K ⁻¹
0.61	2504	9.156	2594	9.408	2689	9.679	2880	10.13	3280	10.84
1	2514	8.975	2594	9.243	2689	9.514	2880	9.968	3280	10.67
2	2533	8.723	2594	8.922	2688	9.194	2880	9.648	3280	10.35
4	2554	8.473	2594	8.601	2688	8.873	2880	9.328	3280	10.03
6	2567	8.329	2593	8.413	2688	8.686	2880	9.141	3280	9.845
8	2576	8.227	2593	8.279	2688	8.552	2880	9.008	3280	9.712
10	2584	8.149	2592	8.174	2687	8.449	2880	8.905	3280	9.609
12	2590	8.085	2591	8.088	2687	8.364	2880	8.821	3280	9.525
15	2598	8.007			2687	8.260	2879	8.717	3280	9.422
20	2609	7.907			2686	8.126	2879	8.584	3280	9.289
30	2625	7.768			2685	7.937	2879	8.396	3280	9.102
40	2636	7.669			2684	7.801	2878	8.263	3279	8.969
50	2645	7.593			2682	7.695	2878	8.159	3279	8.866
60	2653	7.531			2681	7.608	2877	8.074	3279	8.782
70	2659	7.479			2680	7.534	2877	8.002	3279	8.710
80	2665	7.434			2678	7.470	2876	7.940	3279	8.649
90	2670	7.394			2677	7.413	2876	7.885	3279	8.594
100	2675	7.359			2676	7.361	2875	7.836	3279	8.545

Low pressure (<100 kPa) superheated steam – int. energy and specific volume

T (°C)	Saturation		50°C		100°C		200°C		400°C	
P (kPa)	u_g kJkg ⁻¹	v_g m ³ kg ⁻¹	u kJkg ⁻¹	v m ³ kg ⁻¹	u kJkg ⁻¹	v m ³ kg ⁻¹	u kJkg ⁻¹	v m ³ kg ⁻¹	u kJkg ⁻¹	v m ³ kg ⁻¹
0.61	2378	206.1	2445	213	2516	24.06	2662	311.9	2969	509.3
1	2384	129.2	2445	149.1	2516	172.2	2662	218.4	2969	310.7
2	2399	66.99	2445	74.52	2516	86.08	2662	109.2	2969	155.3
4	2415	34.79	2445	37.24	2516	43.03	2662	54.58	2969	77.66
6	2424	23.73	2444	24.81	2516	28.68	2661	36.38	2969	51.77
8	2431	18.10	2444	18.60	2516	21.50	2661	27.28	2969	38.83
10	2437	14.67	2443	14.87	2516	17.20	2661	21.83	2969	31.06
12	2442	12.36	2443	12.38	2515	14.33	2661	18.19	2969	25.89
15	2448	10.02			2515	11.46	2661	14.55	2969	20.71
20	2456	7.648			2515	8.586	2661	10.91	2969	15.53
30	2468	5.229			2514	5.715	2661	7.268	2969	10.35
40	2476	3.993			2513	4.280	2660	5.448	2969	7.763
50	2483	3.240			2511	3.419	2660	4.356	2969	6.209
60	2489	2.732			2510	2.845	2660	3.628	2969	5.174
70	2494	2.365			2509	2.434	2659	3.108	2969	4.434
80	2498	2.087			2508	2.127	2659	2.718	2969	3.879
90	2502	1.870			2507	1.887	2659	2.415	2968	3.448
100	2506	1.694			2506	1.696	2658	2.172	2968	3.103

Compressed liquid water

This table is provided for completeness.

Generally speaking, the enthalpy and internal energy of a compressed liquid are almost equal to a saturated liquid at the same temperature.

The exception to this is that the enthalpy change after a compression in the compressed liquid region can be defined as:

$$\Delta h = v(p_2 - p_1)/\eta_{isen}$$

Compressed liquid water - enthalpy and entropy

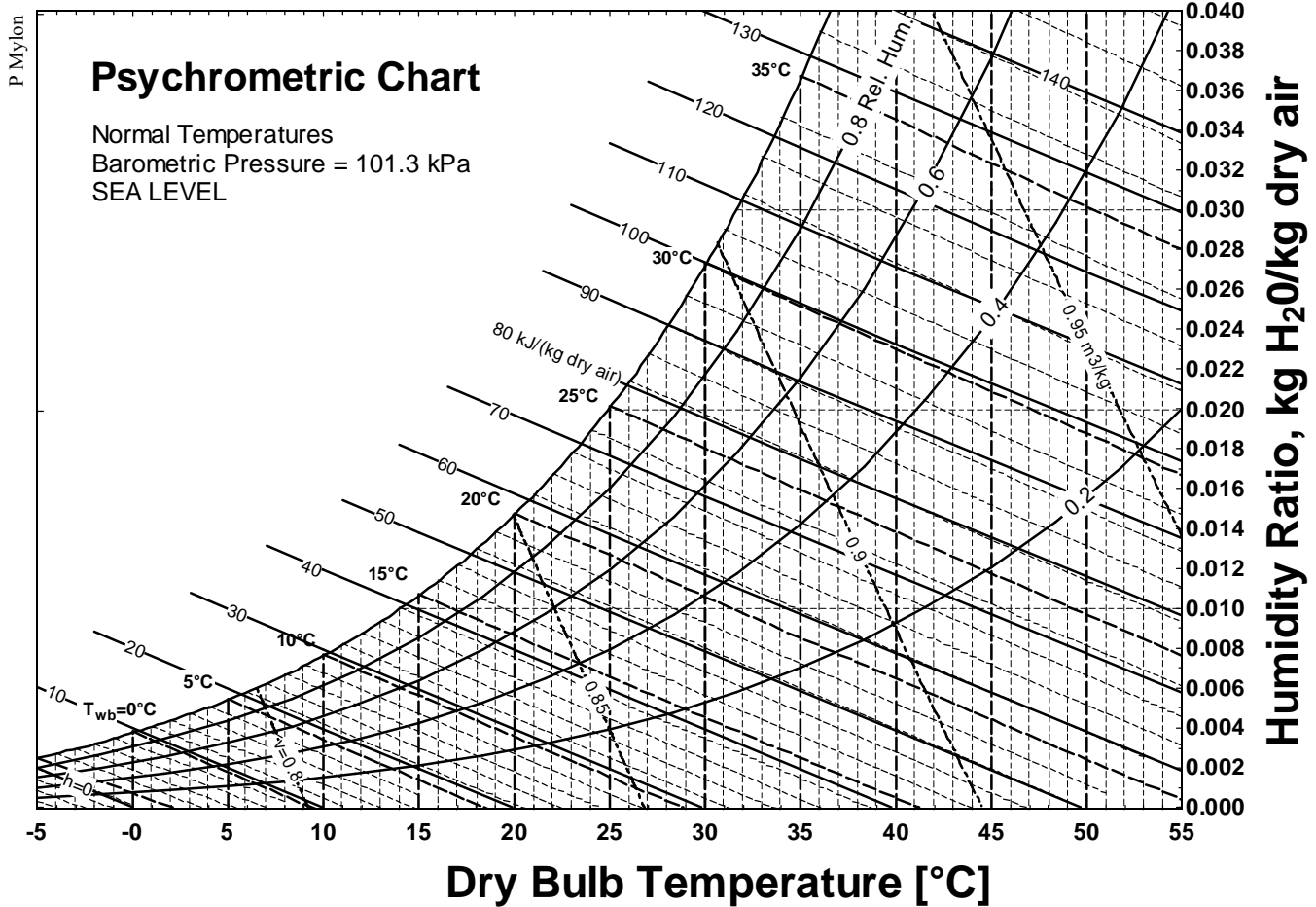
T (°C)	25		100		200		300		350	
	P _{sat} (MPa) 0.00317		P _{sat} (MPa) 0.101325		P _{sat} (MPa) 1.554		P _{sat} (MPa) 8.588		P _{sat} (MPa) 16.54	
	h _f kJ kg ⁻¹	s _f kJ kg ⁻¹ K ⁻¹	h _f kJ kg ⁻¹	s _f kJ kg ⁻¹ K ⁻¹	h _f kJ kg ⁻¹	s _f kJ kg ⁻¹ K ⁻¹	h _f kJ kg ⁻¹	s _f kJ kg ⁻¹ K ⁻¹	h _f kJ kg ⁻¹	s _f kJ kg ⁻¹ K ⁻¹
	104.8	0.367	419.1	1.307	852.3	2.330	1345	3.255	1672	3.781
P (MPa)	h	s	h	s	h	s	h	s	h	s
	kJ kg ⁻¹	kJ kg ⁻¹ K ⁻¹	kJ kg ⁻¹	kJ kg ⁻¹ K ⁻¹	kJ kg ⁻¹	kJ kg ⁻¹ K ⁻¹	kJ kg ⁻¹	kJ kg ⁻¹ K ⁻¹	kJ kg ⁻¹	kJ kg ⁻¹ K ⁻¹
1	105.7	0.367	419.7	1.306						
10	114.0	0.364	426.5	1.299	855.9	2.318	1343	3.249		
20	123.1	0.362	434.0	1.292	860.4	2.303	1334	3.209	1647	3.731
30	132.2	0.359	441.6	1.284	865.2	2.289	1329	3.176	1610	3.645
40	141.2	0.356	449.2	1.277	870.2	2.276	1325	3.147	1590	3.588
50	150.2	0.353	456.8	1.270	875.4	2.263	1324	3.121	1576	3.542
60	159.1	0.349	464.4	1.263	880.7	2.251	1323	3.097	1566	3.501
70	167.9	0.346	472.1	1.256	886.2	2.239	1323	3.074	1558	3.465
80	176.7	0.342	479.7	1.249	891.8	2.227	1324	3.053	1553	3.434
90	185.3	0.338	487.4	1.243	897.6	2.216	1326	3.034	1550	3.407
100	193.9	0.334	495.1	1.236	903.5	2.205	1329	3.017	1551	3.385

Compressed liquid water - internal energy and specific volume*

T (°C)	25		100		200		300		350	
	P _{sat} (MPa) 0.00317		P _{sat} (MPa) 0.101325		P _{sat} (MPa) 1.554		P _{sat} (MPa) 8.588		P _{sat} (MPa) 16.54	
	u _f kJ kg ⁻¹	v _f ×10 ³ m ³ kg ⁻¹	u _f kJ kg ⁻¹	v _f ×10 ³ m ³ kg ⁻¹	u _f kJ kg ⁻¹	v _f ×10 ³ m ³ kg ⁻¹	u _f kJ kg ⁻¹	v _f ×10 ³ m ³ kg ⁻¹	u _f kJ kg ⁻¹	v _f ×10 ³ m ³ kg ⁻¹
	104.8	1.003	419.0	1.044	850.5	1.157	1333	1.404	1643	1.739
P (MPa)	u	v×10 ³	u	v×10 ³	u	v×10 ³	u	v×10 ³	u	v×10 ³
	kJ kg ⁻¹	m ³ kg ⁻¹	kJ kg ⁻¹	m ³ kg ⁻¹	kJ kg ⁻¹	m ³ kg ⁻¹	kJ kg ⁻¹	m ³ kg ⁻¹	kJ kg ⁻¹	m ³ kg ⁻¹
1	104.7	1.002	418.7	1.043						
10	104.0	0.998	416.1	1.038	844.4	1.148	1329	1.399		
20	103.3	0.994	413.4	1.034	837.7	1.139	1307	1.361	1614	1.667
30	102.5	0.990	410.8	1.029	831.3	1.130	1289	1.332	1563	1.553
40	101.8	0.986	408.2	1.025	825.3	1.122	1273	1.307	1530	1.490
50	101.1	0.982	405.8	1.020	819.7	1.115	1259	1.287	1504	1.443
60	100.4	0.978	403.5	1.016	814.3	1.108	1247	1.269	1481	1.404
70	99.7	0.975	401.3	1.012	809.2	1.101	1235	1.253	1461	1.372
80	99.0	0.971	399.1	1.008	804.3	1.094	1225	1.239	1444	1.347
90	98.2	0.967	397.1	1.004	799.7	1.088	1215	1.226	1430	1.328
100	97.5	0.963	395.1	1.000	795.3	1.082	1207	1.215	1419	1.314

*Note: The actual values of v_f and v are 10³ times smaller than the figures given. For example, the specific volume of compressed liquid water at 100°C and 40 MPa is 0.001025 m³ kg⁻¹.

This page is intentionally left blank



How to use the psychrometric chart

Find the wet bulb temperature on the top, left-hand (curved) edge of the chart which is the saturation line. Travel down the dotted line of constant wet bulb temperature (at around 30° to the horizontal) until it intersects the vertical line coming up from the dry bulb temperature (which is found on the horizontal axis). The point at which the two lines meet fully describes the conditions. The humidity ratio (or specific humidity) can be read off the vertical axis. The specific enthalpy of the air/vapour mixture per kg of dry air can be found by travelling up the solid lines approximately parallel to the wet bulb lines, while the specific volume of the mixture can be found by interpolating between the lines at approximately 70° to the horizontal.

Thermodynamic properties of dry and saturated air

T_{db} (°C)	h_{dry} kJkg^{-1}	h_{sat} kJkg^{-1}	V_{dry} kgm^{-3}	V_{sat} kgm^{-3}
-5	-5.03	1.16	0.76	0.76
0	0.00	9.48	0.77	0.78
5	5.03	18.65	0.79	0.80
10	10.06	29.37	0.80	0.81
15	15.10	42.13	0.82	0.83
20	20.13	57.58	0.83	0.85
25	25.16	76.52	0.84	0.87
30	30.20	100.01	0.86	0.90
35	35.23	129.43	0.87	0.92

R134a saturated refrigerant: liquid and vapour

Pressure table

P kPa	T(sat) °C	v_f $m^3 kg^{-1}$	v_g $m^3 kg^{-1}$	h_f $kJ kg^{-1}$	h_g $kJ kg^{-1}$	s_f $kJ kg^{-1} K^{-1}$	s_g $kJ kg^{-1} K^{-1}$
60	-36.95	0.000710	0.3112	3.841	227.8	0.01634	0.9644
80	-31.13	0.000719	0.2375	11.21	231.5	0.04711	0.9571
100	-26.37	0.000726	0.1925	17.28	234.4	0.07188	0.9518
120	-22.32	0.000732	0.1621	22.49	237.0	0.09275	0.9478
140	-18.77	0.000738	0.1401	27.08	239.2	0.1109	0.9446
160	-15.60	0.000744	0.1235	31.21	241.1	0.1269	0.9419
180	-12.73	0.000749	0.1104	34.97	242.9	0.1414	0.9397
200	-10.09	0.000753	0.09987	38.43	244.5	0.1546	0.9377
240	-5.384	0.000762	0.08390	44.66	247.3	0.1779	0.9346
280	-1.247	0.000770	0.07235	50.18	249.7	0.1983	0.9321
320	2.457	0.000777	0.06360	55.16	251.9	0.2164	0.9301
360	5.821	0.000784	0.05674	59.72	253.8	0.2327	0.9284
400	8.910	0.000791	0.05120	63.94	255.6	0.2476	0.9269
500	15.71	0.000806	0.04112	73.33	259.3	0.2802	0.9240
600	21.55	0.000820	0.03430	81.51	262.4	0.3080	0.9218
700	26.69	0.000833	0.02936	88.82	265.0	0.3323	0.9199
800	31.31	0.000846	0.02562	95.47	267.3	0.3540	0.9183
900	35.51	0.000858	0.02268	101.6	269.3	0.3738	0.9169
1000	39.37	0.000870	0.02031	107.3	271.0	0.3919	0.9156
1200	46.29	0.000893	0.01672	117.8	273.9	0.4244	0.9130
1400	52.40	0.000917	0.01411	127.2	276.1	0.4532	0.9105
1600	57.88	0.000940	0.01212	135.9	277.9	0.4791	0.9078
1800	62.87	0.000964	0.01056	144.1	279.2	0.5029	0.9050
2000	67.45	0.000989	0.009288	151.8	280.1	0.5251	0.9018
2500	77.54	0.001057	0.006936	169.6	280.8	0.5753	0.8923
3000	86.16	0.001141	0.005275	186.5	279.1	0.6212	0.8789

R134a saturated refrigerant: temperature table

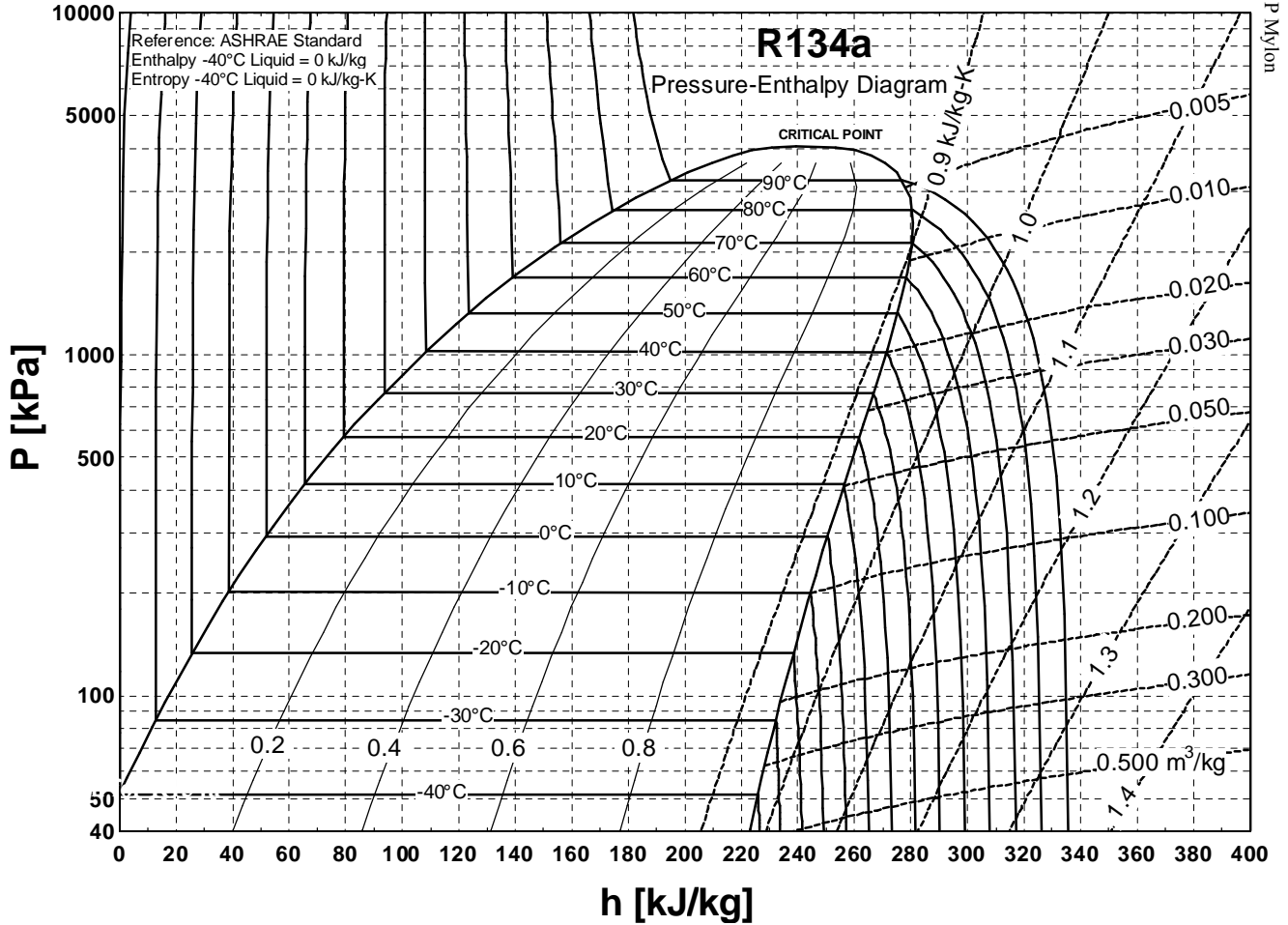
T °C	P(sat) kPa	v_f $m^3 kg^{-1}$	v_g $m^3 kg^{-1}$	h_f $kJ kg^{-1}$	h_g $kJ kg^{-1}$	s_f $kJ kg^{-1}K^{-1}$	s_g $kJ kg^{-1}K^{-1}$
-40	51.25	0.000705	0.3608	0	225.9	0	0.9687
-36	62.95	0.000711	0.2975	5.037	228.4	0.02138	0.9631
-32	76.71	0.000717	0.2471	10.10	230.9	0.04253	0.9581
-28	92.76	0.000723	0.2067	15.20	233.4	0.06344	0.9536
-26	101.7	0.000727	0.1895	17.76	234.7	0.07382	0.9514
-24	111.4	0.000730	0.1739	20.33	235.9	0.08414	0.9494
-22	121.7	0.000733	0.1600	22.91	237.2	0.09441	0.9475
-20	132.8	0.000736	0.1473	25.49	238.4	0.1046	0.9456
-18	144.7	0.000740	0.1358	28.09	239.6	0.1148	0.9439
-16	157.4	0.000743	0.1254	30.69	240.9	0.1249	0.9422
-12	185.4	0.000750	0.1074	35.92	243.3	0.1450	0.9391
-8	217.1	0.000757	0.09235	41.19	245.7	0.1650	0.9363
-4	252.9	0.000765	0.07980	46.50	248.1	0.1848	0.9337
0	293.0	0.000772	0.06925	51.86	250.5	0.2044	0.9314
4	337.9	0.000780	0.06034	57.25	252.8	0.2239	0.9293
8	387.9	0.000789	0.05276	62.69	255.0	0.2432	0.9273
12	443.3	0.000798	0.04603	68.18	257.3	0.2625	0.9255
16	504.6	0.000807	0.04075	73.73	259.5	0.2816	0.9239
20	572.1	0.000816	0.03597	79.32	261.6	0.3006	0.9223
24	646.2	0.000826	0.03183	84.98	263.7	0.3196	0.9209
26	685.8	0.000831	0.02998	87.83	264.7	0.3290	0.9202
28	727.3	0.000837	0.02824	90.69	265.7	0.3385	0.9195
30	770.6	0.000842	0.02662	93.58	266.7	0.3479	0.9188
32	815.9	0.000848	0.02511	96.48	267.6	0.3573	0.9181
34	863.1	0.000854	0.02369	99.40	268.6	0.3667	0.9174
36	912.4	0.000860	0.02236	102.3	269.5	0.3761	0.9167
38	963.7	0.000866	0.02112	105.3	270.4	0.3855	0.9161
40	1017	0.000872	0.01995	108.3	271.3	0.3949	0.9154
42	1073	0.000879	0.01885	111.3	272.1	0.4042	0.9146
44	1131	0.000885	0.01782	114.3	273.0	0.4136	0.9139
48	1254	0.000900	0.01594	120.4	274.5	0.4324	0.9124
52	1386	0.000915	0.01426	126.6	276.0	0.4513	0.9107
56	1529	0.000932	0.01277	132.9	277.3	0.4702	0.9088
60	1683	0.000950	0.01143	139.4	278.5	0.4892	0.9067
70	2118	0.001004	0.008642	156.1	280.5	0.5376	0.8998
80	2635	0.001077	0.006436	174.2	280.6	0.5880	0.8891
90	3247	0.001193	0.004599	194.8	277.1	0.6434	0.8701
100	3975	0.001527	0.002630	224.8	258.4	0.7222	0.8122

R134a superheated refrigerant – 60 to 400 kPa

T °C	P=60 kPa, Tsat=-36.94°C			P=100 kPa, Tsat=-26.37°C			P=140 kPa, Tsat=-18.77°C		
	v m ³ kg ⁻¹	h kJ kg ⁻¹	s kJ kg ⁻¹ K ⁻¹	v m ³ kg ⁻¹	h kJ kg ⁻¹	s kJ kg ⁻¹ K ⁻¹	v m ³ kg ⁻¹	h kJ kg ⁻¹	s kJ kg ⁻¹ K ⁻¹
-20	0.3361	240.8	1.0170	0.1984	239.5	0.9721			
-10	0.3505	248.6	1.0480	0.2074	247.5	1.0030	0.1461	246.4	0.9724
0	0.3648	256.5	1.0770	0.2163	255.6	1.0330	0.1526	254.6	1.0030
10	0.3789	264.7	1.1070	0.2251	263.8	1.0630	0.1591	262.9	1.0330
20	0.3930	272.9	1.1350	0.2337	272.2	1.0920	0.1654	271.4	1.0620
30	0.4070	281.4	1.1640	0.2423	280.7	1.1200	0.1717	280.0	1.0910
40	0.4210	290.0	1.1920	0.2509	289.3	1.1480	0.1779	288.7	1.1200
50	0.4349	298.7	1.2190	0.2594	298.2	1.1760	0.1841	297.6	1.1470
60	0.4488	307.7	1.2460	0.2678	307.1	1.2040	0.1903	306.6	1.1750
70	0.4627	316.8	1.2730	0.2763	316.3	1.2310	0.1964	315.8	1.2020
80	0.4765	326.0	1.3000	0.2847	325.5	1.2570	0.2024	325.1	1.2290
90	0.4903	335.4	1.3260	0.2930	335.0	1.2840	0.2085	334.6	1.2550
100	0.5041	345.0	1.3520	0.3014	344.6	1.3100	0.2145	344.2	1.2810
110	0.5179	354.7	1.3780	0.3097	354.4	1.3350	0.2205	354.0	1.3070
120	0.5316	364.6	1.4030	0.3180	364.3	1.3610	0.2265	363.9	1.3330
	P=180 kPa, Tsat=-12.73°C			P=200 kPa, Tsat=-10.0°C			P=240 kPa, Tsat=-5.38°C		
-10	0.1119	245.2	0.9484	0.0999	244.5	0.9380			
0	0.1172	253.6	0.9798	0.1048	253.1	0.9698	0.0862	252.0	0.9519
10	0.1224	262.0	1.0100	0.1096	261.6	1.0000	0.0903	260.6	0.9831
20	0.1275	270.6	1.0400	0.1142	270.2	1.0300	0.0942	269.4	1.0130
30	0.1325	279.3	1.0690	0.1187	278.9	1.0600	0.0981	278.2	1.0430
40	0.1374	288.0	1.0980	0.1232	287.7	1.0880	0.1019	287.1	1.0720
50	0.1423	297.0	1.1260	0.1277	296.7	1.1160	0.1057	296.1	1.1000
60	0.1471	306.0	1.1530	0.1321	305.8	1.1440	0.1094	305.2	1.1280
70	0.1520	315.3	1.1800	0.1364	315.0	1.1710	0.1131	314.5	1.1550
80	0.1567	324.6	1.2070	0.1407	324.4	1.1980	0.1168	323.9	1.1830
90	0.1615	334.1	1.2340	0.1450	333.9	1.2250	0.1204	333.5	1.2090
100	0.1662	343.8	1.2600	0.1493	343.6	1.2510	0.1240	343.2	1.2360
110	0.1709	353.6	1.2860	0.1536	353.4	1.2770	0.1276	353.1	1.2620
120	0.1756	363.6	1.3120	0.1578	363.4	1.3030	0.1311	363.1	1.2870
130	0.1803	373.7	1.3370	0.1621	373.5	1.3280	0.1347	373.2	1.3130
	P=280 kPa, Tsat=-1.25°C			P=320 kPa, Tsat=2.46°C			P=400 kPa, Tsat=8.91°C		
0	0.0728	250.8	0.9362						
10	0.0765	259.7	0.9680	0.0661	258.7	0.9544	0.0515	256.6	0.9305
20	0.0800	268.5	0.9987	0.0693	267.7	0.9856	0.0542	265.9	0.9628
30	0.0834	277.4	1.0280	0.0723	276.6	1.0160	0.0568	275.1	0.9937
40	0.0867	286.4	1.0580	0.0753	285.7	1.0450	0.0593	284.3	1.0240
50	0.0900	295.5	1.0860	0.0782	294.8	1.0740	0.0617	293.6	1.0530
60	0.0932	304.7	1.1140	0.0811	304.1	1.1020	0.0641	303.0	1.0810
70	0.0964	314.0	1.1420	0.0840	313.5	1.1300	0.0664	312.4	1.1090
80	0.0996	323.5	1.1690	0.0868	323.0	1.1570	0.0688	322.0	1.1370
90	0.1028	333.1	1.1960	0.0895	332.6	1.1840	0.0710	331.7	1.1640
100	0.1059	342.8	1.2220	0.0923	342.4	1.2110	0.0733	341.6	1.1910
110	0.1090	352.7	1.2480	0.0950	352.3	1.2370	0.0755	351.5	1.2170
120	0.1121	362.7	1.2740	0.0978	362.3	1.2630	0.0777	361.6	1.2430
130	0.1151	372.9	1.3000	0.1005	372.5	1.2880	0.0799	371.9	1.2690

R134a superheated refrigerant – 500 to 2000 kPa

T °C	P=500 kPa, Tsat=15.71°C			P=600 kPa, Tsat=21.55°C			P=700 kPa, Tsat=26.69°C		
	v m ³ kg ⁻¹	h kJ kg ⁻¹	s kJ kg ⁻¹ K ⁻¹	v m ³ kg ⁻¹	h kJ kg ⁻¹	s kJ kg ⁻¹ K ⁻¹	v m ³ kg ⁻¹	h kJ kg ⁻¹	s kJ kg ⁻¹ K ⁻¹
20	0.0421	263.5	0.9383						
30	0.0443	273.0	0.9703	0.0360	270.8	0.9499	0.0300	268.5	0.9313
40	0.0465	282.5	1.0010	0.0379	280.6	0.9816	0.0317	278.6	0.9641
50	0.0485	292.0	1.0310	0.0397	290.3	1.0120	0.0333	288.5	0.9954
60	0.0505	301.5	1.0600	0.0414	300.0	1.0420	0.0349	298.4	1.0260
70	0.0524	311.1	1.0880	0.0431	309.7	1.0710	0.0364	308.3	1.0550
80	0.0543	320.8	1.1160	0.0447	319.6	1.0990	0.0378	318.3	1.0830
90	0.0562	330.6	1.1440	0.0463	329.5	1.1260	0.0393	328.3	1.1110
100	0.0581	340.5	1.1710	0.0479	339.5	1.1540	0.0406	338.4	1.1390
110	0.0599	350.6	1.1970	0.0495	349.6	1.1800	0.0420	348.6	1.1660
120	0.0617	360.7	1.2230	0.0510	359.8	1.2070	0.0434	358.9	1.1920
130	0.0635	371.0	1.2490	0.0525	370.2	1.2330	0.0447	369.3	1.2190
140	0.0653	381.5	1.2750	0.0540	380.7	1.2580	0.0460	379.9	1.2440
150	0.0670	392.0	1.3000	0.0555	391.3	1.2840	0.0473	390.5	1.2700
160	0.0688	402.7	1.3250	0.0570	402.0	1.3090	0.0486	401.3	1.2950
	P=800 kPa, Tsat=31.31°C			P=1000 kPa, Tsat=39.37°C			P=1200 kPa, Tsat=46.29°C		
40	0.0270	276.4	0.9480	0.0204	271.7	0.9179			
50	0.0286	286.7	0.9802	0.0218	282.7	0.9525	0.0172	278.3	0.9267
60	0.0300	296.8	1.0110	0.0231	293.4	0.9850	0.0184	289.6	0.9614
70	0.0313	306.9	1.0410	0.0243	303.9	1.0160	0.0195	300.6	0.9938
80	0.0327	317.0	1.0700	0.0254	314.3	1.0460	0.0205	311.4	1.0250
90	0.0339	327.1	1.0980	0.0265	324.6	1.0750	0.0215	322.1	1.0550
100	0.0352	337.3	1.1260	0.0276	335.1	1.1030	0.0224	332.7	1.0840
110	0.0364	347.6	1.1530	0.0286	345.5	1.1310	0.0234	343.4	1.1120
120	0.0376	358.0	1.1800	0.0296	356.1	1.1580	0.0242	354.1	1.1390
130	0.0388	368.5	1.2060	0.0306	366.7	1.1850	0.0251	364.9	1.1660
140	0.0400	379.0	1.2320	0.0316	377.4	1.2110	0.0259	375.7	1.1930
150	0.0411	389.8	1.2580	0.0325	388.2	1.2370	0.0268	386.7	1.2190
160	0.0423	400.6	1.2830	0.0335	399.2	1.2620	0.0276	397.7	1.2450
170	0.0434	411.6	1.3080	0.0344	410.2	1.2880	0.0284	408.8	1.2700
180	0.0446	422.6	1.3330	0.0353	421.4	1.3120	0.0292	420.1	1.2950
	P=1400 kPa, Tsat=52.4°C			P=1600 kPa, Tsat=57.88°C			P=2000 kPa, Tsat=67.45°C		
60	0.0150	285.5	0.9389	0.0124	280.7	0.9163			
70	0.0161	297.1	0.9733	0.0134	293.2	0.9535	0.0096	283.9	0.9130
80	0.0170	308.3	1.0060	0.0144	305.1	0.9875	0.0105	297.6	0.9524
90	0.0179	319.4	1.0360	0.0152	316.5	1.0190	0.0114	310.2	0.9876
100	0.0188	330.3	1.0660	0.0160	327.8	1.0500	0.0121	322.3	1.0200
110	0.0196	341.2	1.0950	0.0168	338.9	1.0790	0.0128	334.1	1.0520
120	0.0204	352.1	1.1230	0.0175	350.0	1.1080	0.0134	345.7	1.0810
130	0.0212	363.0	1.1500	0.0182	361.1	1.1360	0.0141	357.2	1.1100
140	0.0219	374.0	1.1770	0.0189	372.3	1.1630	0.0146	368.6	1.1380
150	0.0226	385.1	1.2040	0.0196	383.4	1.1900	0.0152	380.1	1.1660
160	0.0234	396.2	1.2300	0.0202	394.7	1.2160	0.0158	391.6	1.1930
170	0.0241	407.4	1.2550	0.0208	406.0	1.2420	0.0163	403.1	1.2190
180	0.0248	418.8	1.2810	0.0215	417.4	1.2680	0.0168	414.7	1.2450



Combustion Information

Enthalpy of formation

Substance	Formula	M	kJ kmol ⁻¹
Air		28.97	0
Oxygen	O ₂	32	0
Hydrogen	H ₂	2	0
Nitrogen	N ₂	28	0
Carbon dioxide	CO ₂	44	-393,520
Carbon monoxide	CO	28	-110,530
Water (vapour)	H ₂ O(vap)	18	-241,820
Water (liquid)	H ₂ O(liq)	18	-285,830
Methane	CH ₄	16	-74,850
Acetylene	C ₂ H ₂	26	+226,730
Ethane	C ₂ H ₆	30	-84,680
Propane	C ₃ H ₈	44	-103,850
Butane	C ₄ H ₁₀	58	-126,150
Octane (vapour)	C ₈ H ₁₈	114	-208,450
Dodecane	C ₁₂ H ₂₆	170	-291,010

Reactions

All species are vapour unless stated otherwise. The convention here is such that it is the heat **received** by the system. Enthalpy variation per mol of fuel (first species on the LHS). $\Delta\tilde{h}^\ominus$ in J mol⁻¹ at standard condition T=25°C.

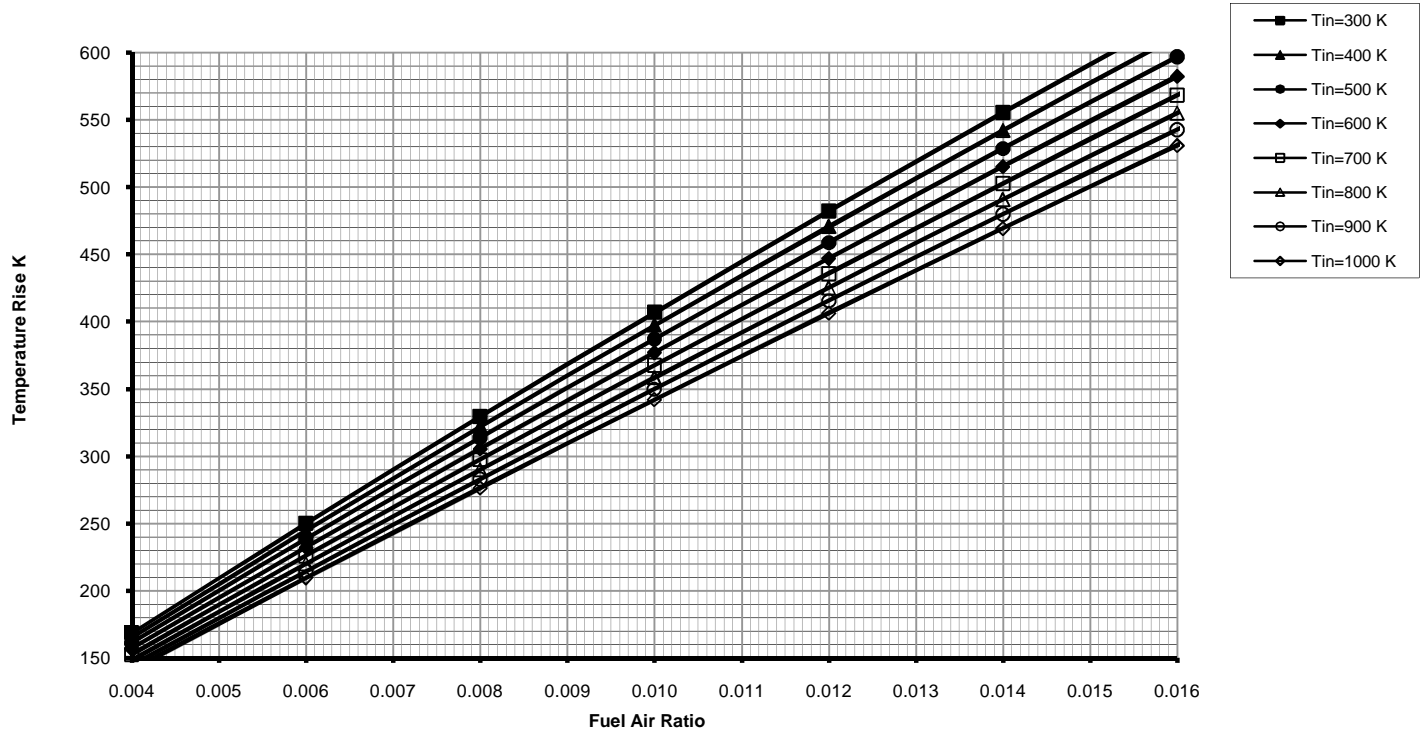
$C_{solid} + O_2 \rightarrow CO_2$	-393 520	$C_8H_{18} + \frac{25}{2}O_2 \rightarrow 8CO_2 + 9H_2O$	-5 116 180
$CO + \frac{1}{2}O_2 \rightarrow CO_2$	-282 990	$CO_2 + H_2 \rightarrow CO + H_2O$	41 169
$H_2 + \frac{1}{2}O_2 \rightarrow H_2O$	-241 830	$\frac{1}{2}H_2 + OH \rightarrow H_2O$	-281 540
$CH_4 + 2O_2 \rightarrow CO_2 + 2H_2O$	-802 310	$\frac{1}{2}N_2 + \frac{1}{2}O_2 \rightarrow NO$	90 290
$C_2H_4 + 3O_2 \rightarrow 2CO_2 + 2H_2O$	-1 323 170	$H_2O(liquid) \rightarrow H_2O$	43 990
$C_2H_6 + \frac{7}{2}O_2 \rightarrow 2CO_2 + 3H_2O$	-1 427 860	$C_6H_6(liquid) \rightarrow C_6H_6$	33 800
$C_6H_6 + \frac{15}{2}O_2 \rightarrow 6CO_2 + 3H_2O$	-3 169 540	$C_8H_{18}(liquid) \rightarrow C_8H_{18}$	41 500

Energy values of various fuels by mass

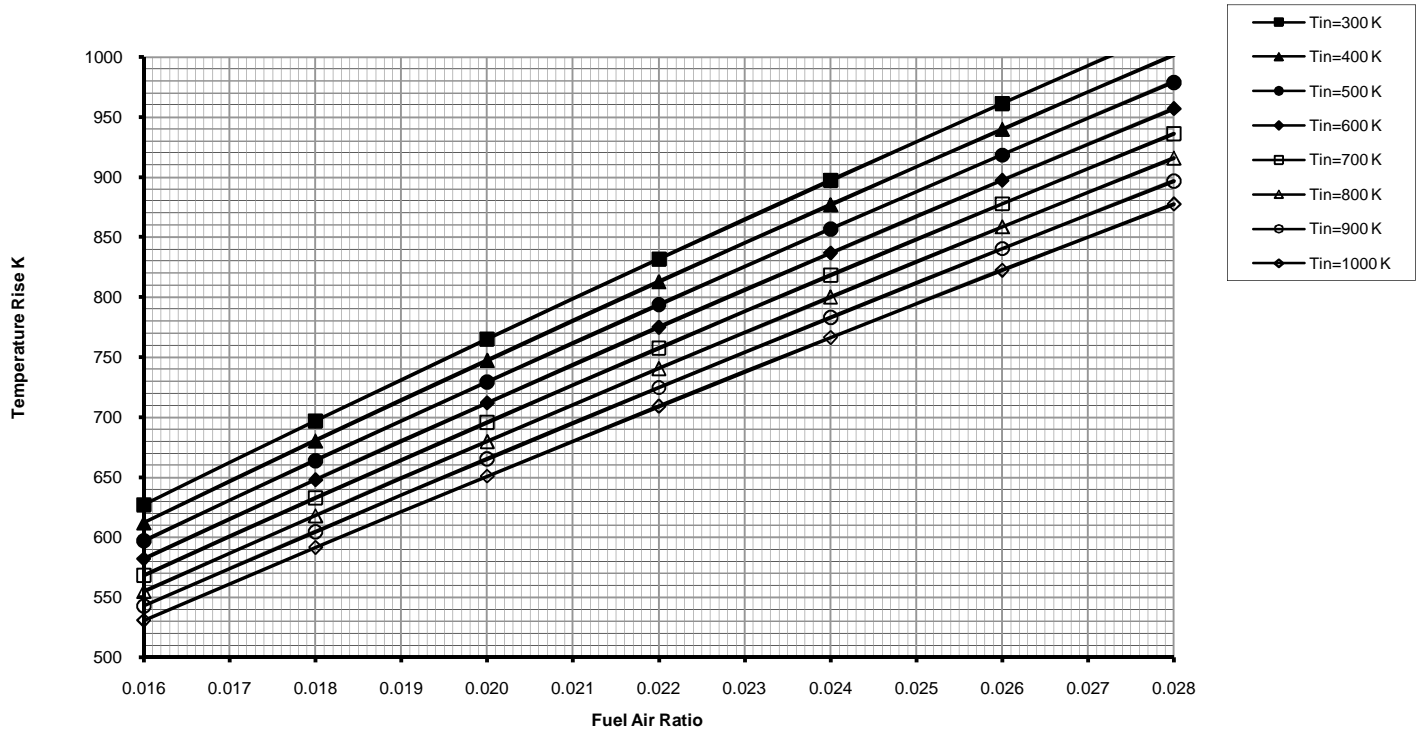
Liquid Fuels	LCV (MJ kg ⁻¹)	ρ (kgm ⁻³) at 15°C	Notes
Petrol (or gasoline)	43.7	737	80 octane
Fuel oil, light	43.4	921	3.5% S (w/w)
Diesel oil	43.3	836	Medium grade (No. 7)
Fuel oil, medium	42.9	939	4.0% S (w/w)
Fuel oil, heavy	42.5	952	3.5% S (w/w)
Kerosine (or kerosene)	42.4	817	
	LCV (MJ kg ⁻¹)	ρ (kgm ⁻³) at b.p.	Boiling Point (K)
Liq. Hydrogen (LH ₂)	116	71	21
Liquid Methane	49	424	111
Liquid Propane	46	585	231
Gaseous Fuels	LCV (MJ kg ⁻¹)	LCV (MJ m ⁻³) at 15°C and 1bar, gas phase	
Hydrogen gas	119.7	10.1	
Methane (CH ₄)	50.0	34.0	
Acetylene (C ₂ H ₂)	48.3	53.1	
Propane gas (C ₃ H ₈)	46.4	86.5	
Butane (C ₄ H ₁₀)	45.8	112.5	
Iso-octane (C ₈ H ₁₈)	44.7	215.7	
Ethanol	26.8	52.2	
Solid Fuels	LCV (MJ kg ⁻¹)	Notes	
Rubber	37.7		
Coal	26.4		
Straw	18.0		
Wood pellets [†]	17.0	8% moisture (w/w)	
Paper	16.6		
Logwood (soft) [†]	14.4	20% moisture (w/w)	
Logwood (hard) [†]	13.0	25% moisture (w/w)	
Wood chips (soft) [†]	12.3	30% moisture (w/w)	
Wood chips (hard) [†]	10.9	35% moisture (w/w)	
Municipal waste	10.7	Edmonton (1968)	

[†]LCV refers to fresh wood, as opposed to GCV for dry mass only

Kerosene temperature rise



Kerosene temperature rise



Equilibrium constants

T (K)	$\ln K^\ominus$							
	$\frac{(p_{\text{H}_2\text{O}})(p^\ominus)^{\frac{1}{2}}}{(p_{\text{H}_2})(p_{\text{O}_2})^{\frac{1}{2}}}$	$\frac{(p_{\text{CO}_2})(p^\ominus)^{\frac{1}{2}}}{(p_{\text{CO}})(p_{\text{O}_2})^{\frac{1}{2}}}$	$\frac{(p_{\text{H}_2\text{O}})(p_{\text{CO}})}{(p_{\text{H}_2})(p_{\text{CO}_2})}$	$\frac{(p_{\text{H}_2\text{O}})(p^\ominus)^{\frac{1}{2}}}{(p_{\text{OH}})(p_{\text{H}_2})^{\frac{1}{2}}}$	$\frac{(p_{\text{NO}})}{(p_{\text{N}_2})^{\frac{1}{2}}(p_{\text{O}_2})^{\frac{1}{2}}}$	$\frac{(p_{\text{H}_2})(p^\ominus)}{(p_{\text{H}})^2}$	$\frac{(p_{\text{O}_2})(p^\ominus)}{(p_{\text{O}})^2}$	$\frac{(p_{\text{N}_2})(p^\ominus)^{\frac{1}{2}}}{(p_{\text{N}})^2}$
298.15	92.207	103.762	-11.554	106.329	-34.933	164.005	186.961	367.479
300	91.604	103.057	-11.453	105.626	-34.707	162.922	185.723	365.126
400	67.321	74.669	-7.348	77.360	-25.655	119.164	135.710	270.329
600	42.897	46.245	-3.348	48.956	-16.602	75.226	85.519	175.356
800	30.593	32.036	-1.444	34.670	-12.072	53.135	60.319	127.753
1000	23.162	23.528	-0.366	26.063	-9.353	39.808	45.145	99.128
1200	18.182	17.871	0.311	20.307	-7.541	30.878	35.005	80.012
1400	14.608	13.841	0.767	16.181	-6.245	24.468	27.742	66.329
1600	11.921	10.829	1.091	13.086	-5.273	19.637	22.285	56.055
1800	9.825	8.497	1.329	10.673	-4.518	15.865	18.030	48.051
2000	8.145	6.634	1.510	8.741	-3.912	12.840	14.622	41.645
2200	6.768	5.119	1.649	7.161	-3.417	10.358	11.827	36.391
2400	5.619	3.859	1.759	5.844	-3.005	8.281	9.497	32.011
2600	4.647	2.800	1.847	4.730	-2.657	6.517	7.521	28.304
2800	3.811	1.893	1.918	3.774	-2.360	5.002	5.826	25.117
3000	3.086	1.110	1.976	2.945	-2.102	3.689	4.357	22.358
3500	1.641	-0.436	2.077	1.299	-1.592	1.063	1.431	16.849
4000	0.541	-1.600	2.141	0.051	-1.207	-0.934	-0.796	12.660
4500	-0.313	-2.491	2.177	-0.914	-0.914	-2.482	-2.514	9.414
5000	-0.997	-3.198	2.201	-1.683	-0.682	-3.725	-3.895	6.807
5500	-1.561	-3.771	2.210	-2.314	-0.493	-4.743	-5.024	4.666
6000	-2.033	-4.246	2.213	-2.839	-0.338	-5.590	-5.963	2.865

Where $p^\ominus = 1 \text{ bar} = 10^5 \text{ Pa}$

CO - enthalpy, internal energy and entropy at atmospheric pressure

T	h	u	s	T	h	u	s
K	kJ kmol ⁻¹	kJ kmol ⁻¹	kJ kmol ⁻¹ K ⁻¹	K	kJ kmol ⁻¹	kJ kmol ⁻¹	kJ kmol ⁻¹ K ⁻¹
0	0	0	0	600	17614	12625	218.1
220	6355	4526	188.5	610	17920	12848	218.6
230	6657	4745	189.8	620	18227	13072	219.1
240	6957	4961	191.1	630	18535	13296	219.6
250	7255	5176	192.3	640	18843	13522	220.1
260	7550	5389	193.4	650	19152	13748	220.6
270	7845	5600	194.6	660	19462	13974	221.1
280	8138	5810	195.6	670	19772	14202	221.5
290	8431	6020	196.7	680	20084	14430	222.0
298.15	8669	6190	197.5	690	20396	14659	222.4
300	8723	6229	197.6	700	20708	14888	222.9
310	9014	6437	198.6	710	21022	15119	223.3
320	9306	6645	199.5	720	21336	15349	223.8
330	9597	6853	200.4	730	21651	15581	224.2
340	9887	7061	201.3	740	21966	15813	224.6
350	10178	7268	202.1	750	22282	16046	225.1
360	10470	7476	202.9	760	22599	16280	225.5
370	10761	7685	203.7	770	22916	16514	225.9
380	11053	7893	204.5	780	23234	16749	226.3
390	11345	8102	205.3	790	23553	16985	226.7
400	11637	8311	206.0	800	23872	17221	227.1
410	11930	8521	206.7	810	24192	17458	227.5
420	12223	8731	207.5	820	24513	17695	227.9
430	12517	8942	208.1	830	24834	17933	228.3
440	12811	9153	208.8	840	25156	18172	228.7
450	13106	9365	209.5	850	25479	18412	229.1
460	13402	9577	210.1	860	25802	18651	229.4
470	13698	9791	210.8	870	26126	18892	229.8
480	13995	10004	211.4	880	26450	19133	230.2
490	14293	10219	212.0	890	26775	19375	230.6
500	14591	10434	212.6	900	27100	19617	230.9
510	14890	10650	213.2	910	27426	19860	231.3
520	15190	10866	213.8	920	27753	20104	231.6
530	15490	11084	214.4	930	28080	20348	232.0
540	15792	11302	214.9	940	28408	20592	232.3
550	16093	11520	215.5	950	28736	20838	232.7
560	16396	11740	216.0	960	29065	21083	233.0
570	16699	11960	216.6	970	29395	21330	233.4
580	17003	12181	217.1	980	29725	21576	233.7
590	17308	12403	217.6	990	30055	21824	234.0

CO - enthalpy, internal energy and entropy at atmospheric pressure

T K	h kJ kmol ⁻¹	u kJ kmol ⁻¹	s kJ kmol ⁻¹ K ⁻¹	T K	h kJ kmol ⁻¹	u kJ kmol ⁻¹	s kJ kmol ⁻¹ K ⁻¹
1000	30386	22072	234.4	1800	58154	43188	254.7
1020	31050	22569	235.0	1820	58872	43740	255.1
1040	31717	23069	235.7	1840	59591	44293	255.5
1060	32383	23569	236.3	1860	60311	44847	255.9
1080	33052	24073	236.9	1880	61033	45402	256.1
1100	33724	24578	237.6	1900	61754	45956	256.3
1120	34397	25085	238.2	1920	62476	46512	256.6
1140	35072	25594	238.8	1940	63199	47069	257.0
1160	35749	26104	239.4	1960	63923	47627	257.4
1180	36428	26617	239.9	1980	64647	48185	257.8
1200	37108	27131	240.5	2000	65373	48744	258.1
1220	37790	27647	241.1	2050	67189	50144	258.5
1240	38474	28164	241.6	2100	69009	51548	259.4
1260	39159	28683	242.2	2150	70832	52956	260.3
1280	39846	29203	242.7	2200	72660	54368	261.1
1300	40534	29726	243.2	2250	74491	55783	262.0
1320	41224	30249	243.8	2300	76325	57202	262.8
1340	41915	30774	244.3	2350	78162	58623	263.6
1360	42608	31301	244.8	2400	80002	60047	264.4
1380	43302	31828	245.3	2450	81844	61474	265.2
1400	43998	32358	245.8	2500	83689	62903	265.9
1420	44695	32888	246.3	2550	85536	64335	266.7
1440	45393	33420	246.8	2600	87386	65768	267.4
1460	46092	33953	247.3	2650	89237	67204	268.1
1480	46793	34488	247.8	2700	91091	68642	268.8
1500	47495	35023	248.2	2750	92946	70081	269.5
1520	48198	35560	248.7	2800	94802	71522	270.2
1540	48902	36098	249.1	2850	96660	72964	270.9
1560	49608	36637	249.6	2900	98520	74408	271.5
1580	50314	37178	250.1	2950	100380	75853	272.2
1600	51022	37719	250.5	3000	102242	77299	272.8
1620	51731	38261	250.9	3050	104105	78746	273.4
1640	52441	38805	251.4	3100	105969	80194	274.1
1660	53151	39349	251.8	3150	107833	81643	274.7
1680	53863	39895	252.2	3200	109698	83093	275.3
1700	54576	40442	252.7	3250	106497	79476	275.8
1720	55290	40989	253.1				
1740	56005	41537	253.5				
1760	56720	42087	253.9				
1780	57437	42637	254.3				

For low pressures, h and u are virtually independent of pressure. If s_a is given at atmospheric pressure, then:

$$s = s_a - R_0 \ln \left(\frac{P}{P_a} \right)$$

H₂O- enthalpy, internal energy and entropy at atmospheric pressure

T	h	u	s	T	h	u	s
K	kJ kmol ⁻¹	kJ kmol ⁻¹	kJ kmol ⁻¹ K ⁻¹	K	kJ kmol ⁻¹	kJ kmol ⁻¹	kJ kmol ⁻¹ K ⁻¹
0	0	0	0	600	20391	15402	212.8
220	7259	5430	178.3	610	20755	15683	213.4
230	7600	5687	179.9	620	21119	15964	214.0
240	7939	5944	181.3	630	21486	16247	214.6
250	8278	6200	182.7	640	21853	16532	215.2
260	8616	6455	184.0	650	22221	16817	215.8
270	8954	6709	185.3	660	22591	17104	216.3
280	9292	6964	186.5	670	22962	17392	216.9
290	9629	7218	187.7	680	23335	17681	217.4
298.15	9904	7425	188.6	690	23708	17971	218.0
300	9966	7472	188.8	700	24083	18263	218.5
310	10304	7726	190.0	710	24459	18556	219.1
320	10641	7981	191.0	720	24837	18850	219.6
330	10979	8235	192.1	730	25216	19146	220.1
340	11317	8490	193.1	740	25596	19443	220.6
350	11656	8746	194.1	750	25977	19741	221.1
360	11995	9001	195.0	760	26360	20041	221.6
370	12334	9258	195.9	770	26743	20341	222.1
380	12674	9515	196.8	780	27129	20643	222.6
390	13015	9772	197.7	790	27515	20947	223.1
400	13357	10031	198.6	800	27903	21251	223.6
410	13699	10290	199.4	810	28292	21557	224.1
420	14042	10550	200.3	820	28682	21864	224.6
430	14386	10811	201.1	830	29074	22173	225.1
440	14731	11073	201.9	840	29467	22482	225.5
450	15077	11335	202.6	850	29861	22793	226.0
460	15423	11599	203.4	860	30256	23106	226.5
470	15771	11863	204.2	870	30653	23419	226.9
480	16120	12129	204.9	880	31051	23734	227.4
490	16470	12396	205.6	890	31450	24050	227.8
500	16820	12663	206.3	900	31850	24367	228.3
510	17172	12932	207.0	910	32252	24686	228.7
520	17525	13202	207.7	920	32655	25006	229.1
530	17879	13473	208.4	930	33060	25327	229.6
540	18235	13745	209.0	940	33465	25649	230.0
550	18591	14018	209.7	950	33872	25973	230.4
560	18949	14293	210.3	960	34280	26298	230.9
570	19308	14568	211.0	970	34689	26624	231.3
580	19667	14845	211.6	980	35100	26951	231.7
590	20029	15123	212.2	990	35511	27280	232.1

H₂O - enthalpy, internal energy and entropy at atmospheric pressure

T	h	u	s	T	h	u	s
K	kJ kmol ⁻¹	kJ kmol ⁻¹	kJ kmol ⁻¹ K ⁻¹	K	kJ kmol ⁻¹	kJ kmol ⁻¹	kJ kmol ⁻¹ K ⁻¹
1000	35924	27610	232.6	1800	72498	57532	259.2
1020	36754	28273	233.4	1820	73490	58358	259.7
1040	37588	28941	234.2	1840	74485	59186	260.3
1060	38428	29614	235	1860	75483	60018	260.8
1080	39272	30292	235.8	1880	76484	60853	261.4
1100	40121	30975	236.6	1900	77488	61691	261.9
1120	40974	31662	237.3	1920	78495	62531	262.4
1140	41832	32354	238.1	1940	79505	63375	262.9
1160	42695	33050	238.8	1960	80518	64222	263.5
1180	43563	33752	239.6	1980	81534	65071	264.0
1200	44435	34457	240.3	2000	82553	65924	264.5
1220	45311	35168	241.0	2050	85111	68067	265.8
1240	46192	35882	241.7	2100	87687	70227	267.0
1260	47078	36602	242.5	2150	90280	72404	268.2
1280	47968	37325	243.2	2200	92887	74596	269.4
1300	48862	38053	243.8	2250	95511	76803	270.6
1320	49760	38785	244.5	2300	98148	79025	271.7
1340	50663	39522	245.2	2350	100800	81261	272.9
1360	51570	40262	245.9	2400	103465	83510	274.0
1380	52481	41007	246.6	2450	106143	85772	275.1
1400	53396	41756	247.2	2500	108833	88047	276.2
1420	54315	42509	247.9	2550	111535	90333	277.3
1440	55239	43266	248.5	2600	114248	92631	278.3
1460	56166	44027	249.1	2650	116972	94939	279.4
1480	57097	44792	249.8	2700	119707	97258	280.4
1500	58032	45561	250.4	2750	122451	99586	281.4
1520	58972	46334	251.0	2800	125204	101924	282.4
1540	59914	47110	251.6	2850	127966	104270	283.4
1560	60861	47890	252.3	2900	130737	106625	284.3
1580	61811	48675	252.9	2950	133515	108987	285.3
1600	62765	49462	253.5	3000	136300	111357	286.2
1620	63723	50254	254.1	3050	139093	113734	287.1
1640	64684	51049	254.6	3100	141892	116117	288.0
1660	65649	51847	255.2	3150	144697	118506	288.9
1680	66617	52649	255.8	3200	147507	120901	289.8
1700	67589	53455	256.4	3250	106497	79476	205.8
1720	68564	54263	257.0				
1740	69543	55076	257.5				
1760	70525	55891	258.1				
1780	71510	56710	258.6				

N₂ - enthalpy, internal energy and entropy at atmospheric pressure

T	h	u	s	T	h	u	s
K	kJ kmol ⁻¹	kJ kmol ⁻¹	kJ kmol ⁻¹ K ⁻¹	K	kJ kmol ⁻¹	kJ kmol ⁻¹	kJ kmol ⁻¹ K ⁻¹
0	0	0	0	600	17558	12570	212.0
220	6446	4617	182.8	610	17860	12788	212.5
230	6716	4803	184.0	620	18163	13008	213.0
240	6993	4997	185.2	630	18466	13228	213.5
250	7276	5197	186.3	640	18771	13449	213.9
260	7562	5400	187.4	650	19075	13671	214.4
270	7850	5605	188.5	660	19381	13893	214.9
280	8140	5812	189.6	670	19687	14116	215.3
290	8431	6020	190.6	680	19994	14340	215.8
298.15	8669	6190	191.4	690	20302	14565	216.2
300	8723	6229	191.6	700	20610	14790	216.7
310	9015	6437	192.6	710	20919	15016	217.1
320	9307	6646	193.5	720	21229	15243	217.6
330	9599	6855	194.4	730	21539	15470	218.0
340	9891	7064	195.3	740	21851	15698	218.4
350	10183	7272	196.1	750	22162	15927	218.8
360	10474	7481	196.9	760	22475	16156	219.2
370	10766	7690	197.7	770	22788	16386	219.6
380	11058	7898	198.5	780	23102	16617	220.1
390	11349	8107	199.3	790	23417	16848	220.5
400	11641	8315	200.0	800	23732	17080	220.8
410	11933	8524	200.7	810	24048	17313	221.2
420	12225	8733	201.4	820	24364	17546	221.6
430	12518	8942	202.1	830	24682	17781	222.0
440	12810	9152	202.8	840	24999	18015	222.4
450	13103	9362	203.4	850	25318	18251	222.8
460	13396	9572	204.1	860	25637	18487	223.1
470	13690	9782	204.7	870	25957	18723	223.5
480	13984	9993	205.3	880	26277	18960	223.9
490	14279	10205	205.9	890	26598	19198	224.2
500	14574	10417	206.5	900	26920	19437	224.6
510	14870	10629	207.1	910	27242	19676	225.0
520	15166	10842	207.7	920	27564	19915	225.3
530	15463	11056	208.3	930	27888	20155	225.7
540	15760	11270	208.8	940	28212	20396	226.0
550	16058	11485	209.4	950	28536	20637	226.3
560	16357	11701	209.9	960	28861	20879	226.7
570	16656	11917	210.4	970	29187	21122	227.0
580	16956	12134	211.0	980	29513	21365	227.4
590	17257	12351	211.5	990	29840	21608	227.7

N₂ - enthalpy, internal energy and entropy at atmospheric pressure

T	h	u	s	T	h	u	s
K	kJ kmol ⁻¹	kJ kmol ⁻¹	kJ kmol ⁻¹ K ⁻¹	K	kJ kmol ⁻¹	kJ kmol ⁻¹	kJ kmol ⁻¹ K ⁻¹
1000	30167	21852	228.0	1800	57640	42674	248.1
1020	30823	22342	228.7	1820	58351	43219	248.5
1040	31481	22834	229.3	1840	59063	43764	248.9
1060	32141	23328	229.9	1860	59776	44311	249.3
1080	32803	23824	230.6	1880	60488	44857	249.7
1100	33468	24322	231.2	1900	61202	45405	250.1
1120	34134	24821	231.8	1920	61917	45953	250.4
1140	34801	25323	232.4	1940	62633	46503	250.8
1160	35471	25826	232.9	1960	63349	47053	251.2
1180	36142	26331	233.5	1980	64066	47603	251.5
1200	36816	26838	234.1	2000	64784	48155	251.9
1220	37490	27347	234.6	2050	66581	49537	252.8
1240	38167	27857	235.2	2100	68383	50923	253.6
1260	38845	28369	235.7	2150	70189	52313	254.5
1280	39525	28882	236.3	2200	71998	53707	255.3
1300	40206	29397	236.8	2250	73812	55104	256.1
1320	40888	29913	237.3	2300	75628	56505	256.9
1340	41572	30431	237.8	2350	77449	57910	257.7
1360	42258	30950	238.3	2400	79272	59318	258.5
1380	42945	31471	238.8	2450	81099	60729	259.2
1400	43633	31993	239.3	2500	82928	62142	260.0
1420	44322	32516	239.8	2550	84761	63559	260.7
1440	45013	33041	240.3	2600	86596	64979	261.4
1460	45705	33566	240.8	2650	88434	66401	262.1
1480	46399	34093	241.3	2700	90275	67826	262.8
1500	47093	34622	241.7	2750	92118	69253	263.5
1520	47789	35151	242.2	2800	93963	70683	264.2
1540	48486	35682	242.6	2850	95810	72115	264.8
1560	49184	36214	243.1	2900	97660	73549	265.5
1580	49883	36746	243.5	2950	99512	74985	266.1
1600	50583	37280	244.0	3000	101366	76423	266.7
1620	51285	37815	244.4	3050	103222	77864	267.3
1640	51987	38351	244.8	3100	105080	79306	267.9
1660	52690	38888	245.3	3150	106940	80750	268.5
1680	53395	39426	245.7	3200	108802	82196	269.1
1700	54100	39965	246.1				
1720	54806	40505	246.5				
1740	55513	41046	246.9				
1760	56221	41588	247.3				
1780	56930	42131	247.7				

O₂ - enthalpy, internal energy and entropy at atmospheric pressure

T	h	u	s	T	h	u	s
K	kJ kmol ⁻¹	kJ kmol ⁻¹	kJ kmol ⁻¹ K ⁻¹	K	kJ kmol ⁻¹	kJ kmol ⁻¹	kJ kmol ⁻¹ K ⁻¹
0	0	0	0	600	17933	12945	226.3
220	6323	4494	195.8	610	18255	13183	226.8
230	6637	4724	197.2	620	18578	13423	227.3
240	6945	4950	198.5	630	18902	13664	227.8
250	7249	5171	199.7	640	19227	13905	228.4
260	7550	5388	200.9	650	19552	14148	228.9
270	7849	5604	202.0	660	19879	14391	229.4
280	8146	5818	203.1	670	20206	14635	229.8
290	8441	6030	204.1	680	20534	14880	230.3
298.15	8682	6203	205.0	690	20863	15126	230.8
300	8737	6242	205.1	700	21192	15372	231.3
310	9031	6454	206.1	710	21523	15619	231.8
320	9326	6665	207.0	720	21854	15867	232.2
330	9621	6877	207.9	730	22185	16116	232.7
340	9917	7090	208.8	740	22518	16365	233.1
350	10213	7302	209.7	750	22851	16615	233.6
360	10509	7516	210.5	760	23185	16866	234.0
370	10807	7730	211.3	770	23520	17118	234.5
380	11105	7945	212.1	780	23855	17370	234.9
390	11404	8162	212.9	790	24191	17623	235.3
400	11704	8379	213.7	800	24528	17876	235.7
410	12006	8597	214.4	810	24865	18130	236.2
420	12308	8816	215.1	820	25203	18385	236.6
430	12612	9036	215.9	830	25542	18641	237.0
440	12916	9258	216.6	840	25881	18897	237.4
450	13222	9480	217.2	850	26220	19153	237.8
460	13528	9704	217.9	860	26561	19410	238.2
470	13836	9928	218.6	870	26902	19668	238.6
480	14145	10154	219.2	880	27243	19926	239.0
490	14455	10381	219.9	890	27585	20185	239.4
500	14766	10609	220.5	900	27928	20445	239.7
510	15078	10838	221.1	910	28271	20705	240.1
520	15391	11068	221.7	920	28615	20965	240.5
530	15706	11299	222.3	930	28959	21226	240.9
540	16021	11531	222.9	940	29303	21488	241.2
550	16337	11764	223.5	950	29649	21750	241.6
560	16654	11998	224.1	960	29994	22013	242.0
570	16973	12233	224.6	970	30341	22276	242.3
580	17292	12470	225.2	980	30687	22539	242.7
590	17612	12707	225.7	990	31035	22803	243.0

O₂ - enthalpy, internal energy and entropy at atmospheric pressure

T	h	u	s	T	h	u	s
K	kJ kmol ⁻¹	kJ kmol ⁻¹	kJ kmol ⁻¹ K ⁻¹	K	kJ kmol ⁻¹	kJ kmol ⁻¹	kJ kmol ⁻¹ K ⁻¹
1000	31382	23068	243.4	1800	60356	45390	264.6
1020	32079	23598	244.1	1820	61103	45971	265.0
1040	32777	24130	244.8	1840	61852	46554	265.4
1060	33478	24664	245.4	1860	62602	47138	265.8
1080	34180	25200	246.1	1880	63352	47721	266.2
1100	34884	25738	246.7	1900	64104	48306	266.6
1120	35589	26277	247.4	1920	64856	48892	267.0
1140	36296	26818	248.0	1940	65609	49479	267.4
1160	37004	27360	248.6	1960	66364	50067	267.8
1180	37715	27904	249.2	1980	67119	50656	268.2
1200	38426	28449	249.8	2000	67875	51246	268.6
1220	39139	28996	250.4	2050	69769	52724	269.5
1240	39854	29544	251.0	2100	71669	54208	270.4
1260	40570	30094	251.5	2150	73574	55698	271.3
1280	41287	30645	252.1	2200	75484	57193	272.2
1300	42006	31197	252.7	2250	77400	58693	273.0
1320	42726	31751	253.2	2300	79321	60198	273.9
1340	43447	32306	253.8	2350	81248	61709	274.7
1360	44169	32862	254.3	2400	83180	63225	275.5
1380	44893	33419	254.8	2450	85117	64747	276.3
1400	45618	33978	255.3	2500	87059	66273	277.1
1420	46345	34538	255.9	2550	89006	67805	277.9
1440	47072	35099	256.4	2600	90959	69341	278.6
1460	47801	35662	256.9	2650	92916	70883	279.4
1480	48531	36225	257.4	2700	94879	72430	280.1
1500	49262	36790	257.9	2750	96847	73982	280.8
1520	49994	37356	258.3	2800	98820	75539	281.6
1540	50727	37923	258.8	2850	100798	77102	282.3
1560	51462	38491	259.3	2900	102780	78669	282.9
1580	52197	39060	259.8	2950	104768	80241	283.6
1600	52934	39630	260.2	3000	106762	81818	284.3
1620	53671	40202	260.7	3050	108760	83401	285.0
1640	54410	40774	261.1	3100	110763	84988	285.6
1660	55149	41348	261.6	3150	112771	86581	286.3
1680	55890	41922	262.0	3200	114784	88178	286.9
1700	56632	42498	262.5				
1720	57375	43074	262.9				
1740	58119	43651	263.3				
1760	58863	44230	263.8				
1780	59609	44809	264.2				

CO₂ - enthalpy, internal energy and entropy at atmospheric pressure

T	h	u	s	T	h	u	s
K	kJ kmol ⁻¹	kJ kmol ⁻¹	kJ kmol ⁻¹ K ⁻¹	K	kJ kmol ⁻¹	kJ kmol ⁻¹	kJ kmol ⁻¹ K ⁻¹
0	0	0	0	600	22261	17273	243.1
220	6637	4808	203.0	610	22735	17664	243.8
230	6967	5055	204.5	620	23212	18057	244.6
240	7302	5307	205.9	630	23691	18453	245.4
250	7644	5565	207.3	640	24172	18851	246.1
260	7991	5829	208.7	650	24655	19251	246.9
270	8343	6099	210.0	660	25141	19653	247.6
280	8701	6373	211.3	670	25629	20058	248.4
290	9064	6653	212.6	680	26118	20465	249.1
298.15	9364	6885	213.6	690	26610	20873	249.8
300	9432	6938	213.8	700	27104	21284	250.5
310	9805	7228	215.1	710	27600	21697	251.2
320	10183	7522	216.3	720	28098	22112	251.9
330	10565	7821	217.4	730	28598	22529	252.6
340	10952	8125	218.6	740	29100	22947	253.3
350	11343	8433	219.7	750	29604	23368	254.0
360	11738	8745	220.8	760	30109	23790	254.6
370	12137	9061	221.9	770	30616	24214	255.3
380	12541	9381	223.0	780	31125	24640	256.0
390	12948	9705	224.1	790	31636	25068	256.6
400	13359	10033	225.1	800	32149	25497	257.3
410	13774	10365	226.1	810	32663	25928	257.9
420	14192	10700	227.1	820	33179	26361	258.5
430	14614	11039	228.1	830	33696	26795	259.2
440	15040	11381	229.1	840	34215	27231	259.8
450	15469	11727	230.1	850	34736	27669	260.4
460	15901	12076	231.0	860	35258	28108	261.0
470	16336	12428	232.0	870	35782	28548	261.6
480	16775	12784	232.9	880	36307	28990	262.2
490	17216	13142	233.8	890	36834	29434	262.8
500	17661	13504	234.7	900	37362	29879	263.4
510	18109	13868	235.6	910	37891	30325	264.0
520	18559	14236	236.4	920	38422	30773	264.6
530	19013	14606	237.3	930	38954	31222	265.1
540	19469	14979	238.2	940	39488	31672	265.7
550	19928	15355	239.0	950	40023	32124	266.3
560	20389	15733	239.8	960	40559	32577	266.8
570	20853	16114	240.7	970	41097	33032	267.4
580	21320	16498	241.5	980	41636	33488	267.9
590	21790	16884	242.3	990	42176	33944	268.5

CO₂ - enthalpy, internal energy and entropy at atmospheric pressure

T	h	u	s	T	h	u	s
K	kJ kmol ⁻¹	kJ kmol ⁻¹	kJ kmol ⁻¹ K ⁻¹	K	kJ kmol ⁻¹	kJ kmol ⁻¹	kJ kmol ⁻¹ K ⁻¹
1000	42717	34403	269.0	1800	88735	73770	302.7
1020	43803	35323	270.1	1820	89931	74799	303.4
1040	44894	36247	271.2	1840	91129	75830	304.0
1060	45990	37176	272.2	1860	92329	76864	304.7
1080	47089	38110	273.2	1880	93528	77897	305.3
1100	48193	39048	274.3	1900	94730	78932	305.9
1120	49302	39990	275.3	1920	95932	79969	306.6
1140	50414	40935	276.2	1940	97136	81006	307.2
1160	51530	41885	277.2	1960	98342	82045	307.8
1180	52650	42839	278.2	1980	99548	83086	308.4
1200	53773	43796	279.1	2000	100756	84127	309.0
1220	54900	44757	280.0	2050	103779	86735	310.5
1240	56031	45721	281.0	2100	106809	89349	312.0
1260	57165	46688	281.9	2150	109846	91970	313.4
1280	58302	47659	282.8	2200	112888	94596	314.8
1300	59442	48633	283.6	2250	115935	97228	316.2
1320	60585	49610	284.5	2300	118988	99864	317.5
1340	61731	50590	285.4	2350	122045	102506	318.8
1360	62880	51572	286.2	2400	125107	105152	320.1
1380	64032	52558	287.1	2450	128173	107803	321.4
1400	65186	53546	287.9	2500	131243	110457	322.6
1420	66343	54537	288.7	2550	134318	113116	323.8
1440	67503	55530	289.5	2600	137396	115779	325.0
1460	68665	56526	290.3	2650	140478	118445	326.2
1480	69829	57524	291.1	2700	143563	121115	327.4
1500	70996	58525	291.9	2750	146652	123788	328.5
1520	72165	59527	292.7	2800	149745	126465	329.6
1540	73336	60532	293.5	2850	152841	129145	330.7
1560	74510	61539	294.2	2900	155940	131829	331.8
1580	75685	62548	295.0	2950	159043	134515	332.8
1600	76863	63560	295.7	3000	162149	137206	333.9
1620	78042	64573	296.4	3050	165258	139900	334.9
1640	79223	65588	297.2	3100	168371	142597	335.9
1660	80406	66604	297.9	3150	171487	145297	336.9
1680	81591	67623	298.6	3200	174607	148001	337.9
1700	82778	68643	299.3				
1720	83966	69665	300.0				
1740	85156	70689	300.7				
1760	86348	71714	301.3				
1780	87541	72741	302.0				

H₂ - enthalpy, internal energy and entropy at atmospheric pressure

T	h	u	s	T	h	u	s
K	kJ kmol ⁻¹	kJ kmol ⁻¹	kJ kmol ⁻¹ K ⁻¹	K	kJ kmol ⁻¹	kJ kmol ⁻¹	kJ kmol ⁻¹ K ⁻¹
0	0	0	0	600	17265	12276	151.0
220	6329	4500	122.3	610	17557	12485	151.5
230	6585	4673	123.4	620	17850	12695	151.9
240	6849	4853	124.6	630	18142	12904	152.4
250	7118	5040	125.7	640	18435	13113	152.9
260	7393	5231	126.7	650	18727	13323	153.3
270	7671	5426	127.8	660	19020	13532	153.8
280	7952	5624	128.8	670	19313	13742	154.2
290	8235	5824	129.8	680	19606	13952	154.6
298.15	8468	5989	130.6	690	19899	14163	155.1
300	8521	6027	130.8	700	20193	14373	155.5
310	8808	6231	131.7	710	20487	14584	155.9
320	9097	6436	132.6	720	20781	14794	156.3
330	9386	6642	133.5	730	21075	15005	156.7
340	9676	6849	134.4	740	21369	15217	157.1
350	9967	7057	135.2	750	21664	15428	157.5
360	10258	7265	136.1	760	21959	15640	157.9
370	10550	7473	136.9	770	22254	15852	158.3
380	10842	7682	137.6	780	22550	16064	158.7
390	11134	7891	138.4	790	22845	16277	159.0
400	11426	8100	139.1	800	23141	16490	159.4
410	11718	8309	139.9	810	23438	16703	159.8
420	12010	8518	140.6	820	23734	16917	160.2
430	12302	8727	141.2	830	24031	17130	160.5
440	12594	8936	141.9	840	24329	17344	160.9
450	12886	9145	142.6	850	24626	17559	161.2
460	13178	9354	143.2	860	24924	17774	161.6
470	13470	9563	143.8	870	25222	17989	161.9
480	13762	9771	144.5	880	25521	18204	162.3
490	14054	9980	145.1	890	25820	18420	162.6
500	14346	10189	145.6	900	26119	18636	162.9
510	14638	10398	146.2	910	26418	18852	163.3
520	14930	10606	146.8	920	26718	19069	163.6
530	15222	10815	147.3	930	27019	19286	163.9
540	15514	11024	147.9	940	27319	19504	164.2
550	15805	11232	148.4	950	27620	19722	164.5
560	16097	11441	149.0	960	27922	19940	164.9
570	16389	11650	149.5	970	28223	20158	165.2
580	16681	11859	150.0	980	28526	20377	165.5
590	16973	12068	150.5	990	28828	20597	165.8

H₂ - enthalpy, internal energy and entropy at atmospheric pressure

T	h	u	s	T	h	u	s
K	kJ kmol ⁻¹	kJ kmol ⁻¹	kJ kmol ⁻¹ K ⁻¹	K	kJ kmol ⁻¹	kJ kmol ⁻¹	kJ kmol ⁻¹ K ⁻¹
1000	29131	20817	166.1	1800	54657	39691	184.8
1020	29738	21257	166.7	1820	55327	40195	185.1
1040	30346	21699	167.3	1840	55999	40700	185.5
1060	30956	22143	167.9	1860	56673	41208	185.9
1080	31568	22588	168.4	1880	57346	41715	186.2
1100	32181	23035	169	1900	58022	42225	186.6
1120	32796	23484	169.6	1920	58699	42736	186.9
1140	33412	23934	170.1	1940	59378	43248	187.3
1160	34030	24386	170.6	1960	60058	43762	187.6
1180	34650	24839	171.2	1980	60740	44277	188.0
1200	35271	25294	171.7	2000	61423	44794	188.3
1220	35894	25751	172.2	2050	63136	46091	189.2
1240	36519	26209	172.7	2100	64858	47397	190.0
1260	37145	26669	173.2	2150	66588	48712	190.8
1280	37773	27130	173.7	2200	68326	50034	191.6
1300	38402	27593	174.2	2250	70072	51365	192.4
1320	39033	28058	174.7	2300	71827	52704	193.2
1340	39666	28525	175.2	2350	73589	54050	193.9
1360	40300	28993	175.6	2400	75358	55404	194.7
1380	40936	29462	176.1	2450	77135	56765	195.4
1400	41574	29934	176.6	2500	78920	58134	196.1
1420	42213	30407	177	2550	80712	59510	196.8
1440	42854	30881	177.5	2600	82511	60893	197.5
1460	43496	31357	177.9	2650	84317	62284	198.2
1480	44140	31835	178.3	2700	86130	63681	198.9
1500	44786	32314	178.8	2750	87949	65085	199.6
1520	45433	32795	179.2	2800	89776	66496	200.2
1540	46082	33278	179.6	2850	91609	67913	200.9
1560	46732	33762	180.0	2900	93448	69337	201.5
1580	47384	34248	180.5	2950	95294	70767	202.1
1600	48038	34735	180.9	3000	97146	72203	202.8
1620	48693	35224	181.3	3050	99005	73646	203.4
1640	49349	35714	181.7	3100	100869	75094	204.0
1660	50008	36206	182.1	3150	102739	76549	204.6
1680	50667	36699	182.5	3200	104615	78009	205.2
1700	51328	37194	182.9				
1720	51991	37690	183.2				
1740	52655	38188	183.6				
1760	53321	38688	184.0				
1780	53988	39189	184.4				

Specific heat of gases at constant pressure

T (K)	c_p (kJkg ⁻¹ K ⁻¹)						
	CH ₄	CO ₂	CO	H ₂	H ₂ O	N ₂	O ₂
220	2.251	0.742	1.084	12.500	1.894	0.946	0.991
230	2.230	0.756	1.074	12.900	1.888	0.978	0.972
240	2.216	0.769	1.066	13.230	1.883	1.001	0.956
250	2.210	0.782	1.059	13.490	1.879	1.016	0.945
260	2.210	0.795	1.054	13.700	1.876	1.026	0.936
270	2.215	0.807	1.049	13.870	1.874	1.033	0.930
280	2.224	0.819	1.046	14.010	1.873	1.038	0.926
290	2.237	0.831	1.043	14.120	1.872	1.040	0.923
298	2.250	0.840	1.042	14.190	1.872	1.041	0.922
300	2.253	0.842	1.041	14.210	1.872	1.042	0.922
320	2.295	0.863	1.039	14.330	1.874	1.042	0.921
340	2.345	0.884	1.039	14.410	1.878	1.042	0.924
360	2.402	0.903	1.040	14.460	1.883	1.041	0.928
380	2.464	0.921	1.042	14.480	1.890	1.041	0.934
400	2.531	0.938	1.045	14.490	1.898	1.042	0.940
420	2.600	0.955	1.048	14.490	1.907	1.043	0.947
440	2.671	0.971	1.052	14.490	1.917	1.045	0.953
460	2.743	0.986	1.057	14.490	1.927	1.048	0.960
480	2.816	1.000	1.061	14.480	1.939	1.051	0.967
500	2.890	1.014	1.066	14.480	1.950	1.054	0.974
550	3.074	1.046	1.079	14.480	1.982	1.065	0.990
600	3.255	1.075	1.092	14.490	2.015	1.077	1.005
650	3.431	1.101	1.105	14.520	2.049	1.089	1.019
700	3.601	1.125	1.118	14.570	2.085	1.102	1.031
750	3.763	1.146	1.130	14.620	2.120	1.114	1.043
800	3.918	1.166	1.141	14.690	2.156	1.126	1.053
900	4.207	1.202	1.163	14.850	2.226	1.149	1.071
1000	4.466	1.231	1.183	15.030	2.296	1.169	1.087
1100	4.698	1.257	1.200	15.230	2.362	1.187	1.101
1200	4.905	1.278	1.216	15.430	2.426	1.203	1.113
1300	5.089	1.297	1.230	15.630	2.488	1.217	1.124
1400	5.252	1.313	1.243	15.830	2.546	1.230	1.134
1500	5.396	1.327	1.254	16.030	2.601	1.241	1.143
1600	5.521	1.339	1.264	16.230	2.653	1.251	1.152
1700	5.631	1.349	1.273	16.420	2.702	1.260	1.160

Molar Gibbs function at atmospheric pressure

T (K)	\tilde{g}^g (kJkmol ⁻¹)								
	CH ₄	C ₂ H ₄	CO	CO ₂	H ₂	H ₂ O	N ₂	NO	O ₂
220	-31354	-38311	-35122	-38047	-20597	-31995	-33786	-37519	-36762
250	-36686	-44611	-40837	-44206	-24319	-37415	-39326	-43623	-42698
298.15	-45507	-55023	-50228	-54346	-30495	-46363	-48427	-53646	-52449
300	-45852	-55430	-50594	-54742	-30737	-46712	-48782	-54036	-52828
400	-65063	-78139	-70805	-76713	-44260	-66115	-68390	-75581	-73795
500	-85297	-102174	-91757	-99722	-58519	-86382	-88736	-97882	-95522
600	-106460	-127455	-113309	-123627	-73366	-107355	-109678	-120799	-117876
700	-128494	-153911	-135373	-148321	-88703	-128937	-131124	-144240	-140767
800	-151355	-181476	-157885	-173724	-104461	-151056	-153013	-168142	-164131
900	-175001	-210088	-180798	-199769	-120589	-173661	-175296	-192454	-187917
1000	-199398	-239690	-204074	-226403	-137051	-196713	-197938	-217137	-212084

Heat Transfer

Fourier's Law

$$\dot{Q} = -kA \frac{\partial T}{\partial x}$$

Newton's Law of Cooling

$$\dot{Q}_{Conv} = hA_s(T_s - T_\infty)$$

Radiation heat transfer

$$\dot{Q}_{Emit} = \varepsilon \sigma A_s T_s^4$$

1-D heat conduction equation

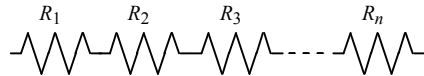
$$\frac{1}{r^n} \frac{\partial}{\partial r} \left(r^n k \frac{\partial T}{\partial r} \right) + \dot{g} = \rho C \frac{\partial T}{\partial t},$$

where $n = 0$ for a flat wall, $n = 1$ cylinder and $n = 2$ sphere

Thermal resistance

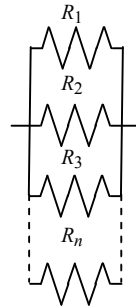
Resistors in series:

$$R_{total} = R_1 + R_2 + R_3 + \dots + R_n$$



Resistors in parallel:

$$\frac{1}{R_{total}} = \frac{1}{R_1} + \frac{1}{R_2} + \frac{1}{R_3} + \dots + \frac{1}{R_n}$$



Resistance for 1D heat flow through a plate:

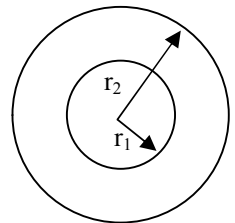
$$R_{total} = \frac{1}{Ah_1} + \frac{L_1}{Ak} + \frac{1}{Ah_2}$$

Resistance for 1D heat flow through a cylinder:

$$R_{total} = \frac{1}{(2\pi r_1 L)h_1} + \frac{\ln(r_2/r_1)}{2\pi Lk} + \frac{1}{(2\pi r_2 L)h_2}$$

Resistance for 1D heat flow through a sphere:

$$R_{total} = \frac{1}{(4\pi r_1^2)h_1} + \frac{r_2 - r_1}{4\pi r_1 r_2 k} + \frac{1}{(4\pi r_2^2)h_2}$$



Heat flow in multilayered cylinders and spheres:

$$\dot{Q} = \frac{T_i - T_j}{R_{total,i-j}} \quad \text{between any two interfaces } i \text{ and } j$$

Radiative heat transfer coefficient:

$$h_{Rad} = \varepsilon \sigma (T_s^2 + T_{Surr}^2)(T_s + T_{Surr})$$

Finned surfaces

$$m^2 = \frac{hp}{kA_c}$$

Temperature profile (insulated tip):

$$\frac{T(x) - T_\infty}{T_b - T_\infty} = e^{-mx}$$

Fin heat transfer:

$$\dot{Q}_{long\ fin} = \sqrt{hpkA_c}(T_b - T_\infty)$$

$$\dot{Q}_{insulated\ tip} = \sqrt{hpkA_c}(T_b - T_\infty) \tanh mL$$

Fin efficiency:

$$\eta_{long\ fin} = \frac{\dot{Q}_{fin}}{\dot{Q}_{fin,max}} = \frac{1}{mL}$$

$$\eta_{insulated\ tip} = \frac{\tanh mL}{mL}$$

Fin effectiveness:

$$\varepsilon_{long\ fin} = \frac{\dot{Q}_{fin}}{\dot{Q}_{no\ fin}} = \sqrt{\frac{kp}{hA_c}}$$

Convection heat transfer

Flow over a flat plate	Range of Re	Nusselt number
Laminar	$0 - 5 \times 10^5$	$Nu = 0.664Re_L^{0.5}Pr^{1/3}$
Turbulent	$5 \times 10^5 - 10^7$	$Nu = 0.037Re_L^{0.8}Pr^{1/3}$
Combined	$5 \times 10^5 \leq Re \leq 10^7$	$Nu = (0.037Re_L^{0.8} - 871)Pr^{1/3}$

Flow across a cylinder

Fluid	Range of Re	Nusselt Number
Gas or liquid	0.4 - 4	$Nu = 0.989Re^{0.330}Pr^{1/3}$
	4 - 40	$Nu = 0.911Re^{0.385}Pr^{1/3}$
	40 - 4000	$Nu = 0.683Re^{0.466}Pr^{1/3}$
	4000 - 40,000	$Nu = 0.193Re^{0.618}Pr^{1/3}$
	40,000 - 400,000	$Nu = 0.027Re^{0.805}Pr^{1/3}$

Flow across banks of tubes

<p>In Line</p>	$V_{max} = \frac{S_T}{S_T - D} V$	
<p>Staggered</p>	$V_{max} = \frac{S_T}{2(S_D - D)} V$ $S_D = \sqrt{S_L^2 + \left(\frac{S_T}{2}\right)^2}$	

Arrangement	Range of Re_D	Correlation
In Line	0 – 100	$Nu_D = 0.9 Re_D^{0.4} Pr^{0.36} (Pr/Pr_s)^{0.25}$
	100 – 1000	$Nu_D = 0.52 Re_D^{0.5} Pr^{0.36} (Pr/Pr_s)^{0.25}$
	1000 – 2×10^5	$Nu_D = 0.27 Re_D^{0.63} Pr^{0.36} (Pr/Pr_s)^{0.25}$
	2×10^5 – 2×10^6	$Nu_D = 0.033 Re_D^{0.8} Pr^{0.36} (Pr/Pr_s)^{0.25}$
Staggered	0 – 500	$Nu_D = 1.04 Re_D^{0.4} Pr^{0.36} (Pr/Pr_s)^{0.25}$
	500 – 1000	$Nu_D = 0.71 Re_D^{0.5} Pr^{0.36} (Pr/Pr_s)^{0.25}$
	1000 – 2×10^5	$Nu_D = 0.35 (S_T/S_L)^{0.2} Re_D^{0.5} Pr^{0.36} (Pr/Pr_s)^{0.25}$
	2×10^5 – 2×10^6	$Nu_D = 0.031 (S_T/S_L)^{0.2} Re_D^{0.8} Pr^{0.36} (Pr/Pr_s)^{0.25}$

Correction factor for less than 16 banks:

N_L	1	2	3	4	5	7	10	13
In Line	0.7	0.8	0.86	0.9	0.93	0.96	0.98	0.99
Staggered	0.64	0.76	0.84	0.89	0.93	0.96	0.98	0.99

Flow in tubes (Internal forced convection)

Constant surface heat flux:

$$\frac{dT_s}{dx} = \frac{dT_m}{dx} = \frac{\dot{q}_s p}{\dot{m}c_p} = \text{const.}$$

Constant surface temperature:

$$\ln \frac{T_s - T_e}{T_s - T_i} = - \frac{hA_s}{\dot{m}c_p} \text{ where } A_s = pL$$

Laminar (Re < 2300)

Constant surface heat flux:

$$Nu = \frac{hD}{k} = 4.36$$

Constant surface temperature:

$$Nu = \frac{hD}{k} = 3.66$$

Turbulent (Re > 10,000)

Dittus–Boelter equation:

$$Nu = 0.023Re^{0.8}Pr^n$$

where $n = 0.4$ for heating the fluid, $n = 0.3$ for cooling the fluid.

Heat exchangers

Heat transfer in a well insulated heat exchanger is given by the heat transfer from the hot or to the cold fluids:

$$\dot{Q} = C_c(T_{c,out} - T_{c,in}) = C_h(T_{h,in} - T_{h,out}) \text{ where } C = \dot{m}c_p$$

It can also be determined using:

$$\dot{Q} = UA\Delta T_{lm} \text{ where } \Delta T_{lm} = \frac{\Delta T_1 - \Delta T_2}{\ln(\Delta T_1/\Delta T_2)}$$

Counter-flow:

$$\Delta T_1 = T_{h,in} - T_{c,out}; \Delta T_2 = T_{h,out} - T_{c,in}$$

Parallel-flow:

$$\Delta T_1 = T_{h,in} - T_{c,in}; \Delta T_2 = T_{h,out} - T_{c,out}$$

Heat exchanger effectiveness

Heat exchanger effectiveness:

$$\varepsilon = \frac{\dot{Q}}{Q_{max}}$$

Double pipe parallel flow

$$\varepsilon = \frac{1 - e^{-NTU(1+c)}}{1 + c}$$

Double pipe counter flow

$$\varepsilon = \frac{1 - e^{-NTU(1-c)}}{1 - ce^{-NTU(1-c)}}$$
$$NTU = \frac{UA_s}{C_{min}} = \frac{UA_s}{(\dot{m}c_p)_{min}} \quad \text{and} \quad c = \frac{C_{min}}{C_{max}}$$

Radiation

Stefan-Boltzmann law:

$$E_b(T) = \sigma T^4 \text{ W/m}^2$$

View factor relationships

Reciprocity:

$$A_i F_{ij} = A_j F_{ji}$$

Summation:

$$\sum_{j=1}^N F_{ij} = 1$$

Superposition:

$$F_{1 \rightarrow (2,3)} = F_{1 \rightarrow 2} + F_{1 \rightarrow 3}$$

Symmetry: if the surfaces j and k are symmetric about surface i then:

$$F_{i \rightarrow j} = F_{i \rightarrow k}$$

Net radiation heat transfer from 1 surface:

$$\dot{Q}_i = \frac{E_{bi} - J_i}{R_i}, \text{ where } R_i = \frac{1 - \varepsilon_i}{A_i \varepsilon_i}$$

Direct Method:

$$\dot{Q}_i = A_i \sum_{j=1}^N F_{ij} (J_i - J_j)$$

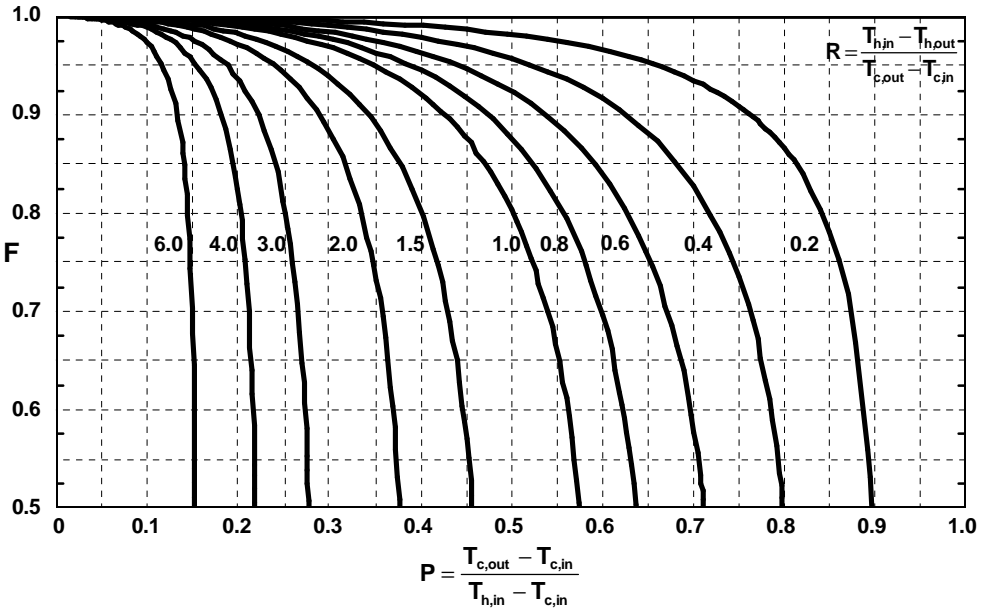
$$\sigma T_i^4 = J_i + \frac{1 - \varepsilon_i}{\varepsilon_i} \sum_{j=1}^N F_{ij} (J_i - J_j)$$

Network Method – radiation between two surfaces:

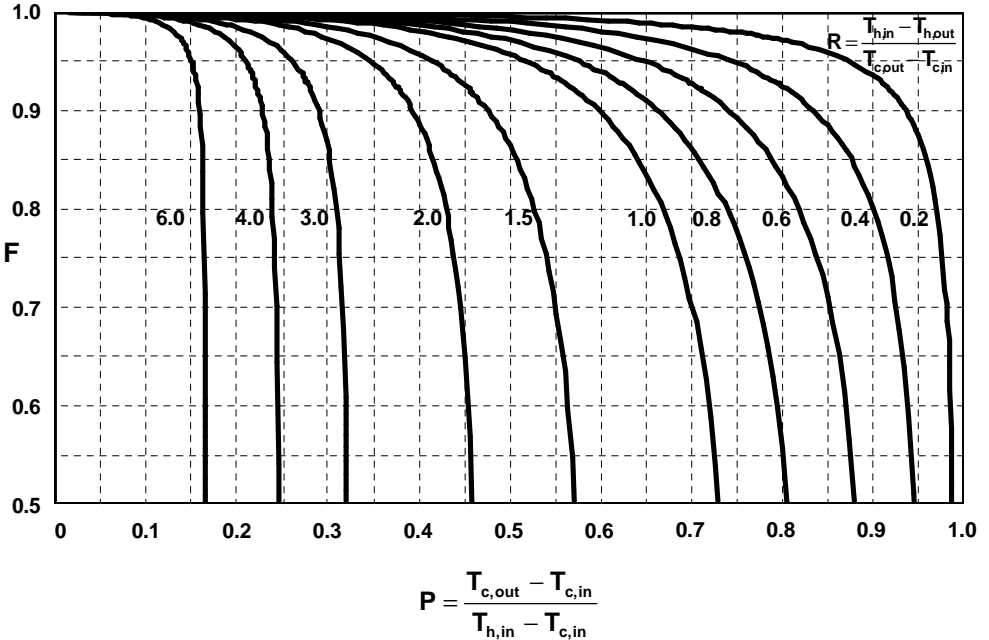
$$\dot{Q}_{12} = \frac{E_{b1} - E_{b2}}{R_1 + R_{12} + R_2} = \frac{\sigma(T_1^4 - T_2^4)}{\frac{1 - \varepsilon_1}{A_1 \varepsilon_1} + \frac{1}{A_1 F_{12}} + \frac{1 - \varepsilon_2}{A_2 \varepsilon_2}}$$

Correction factors for LMTD method

Shell-and-tube heat exchanger with *one* shell pass and $2n$ tube passes ($n=1,2,3,..$)

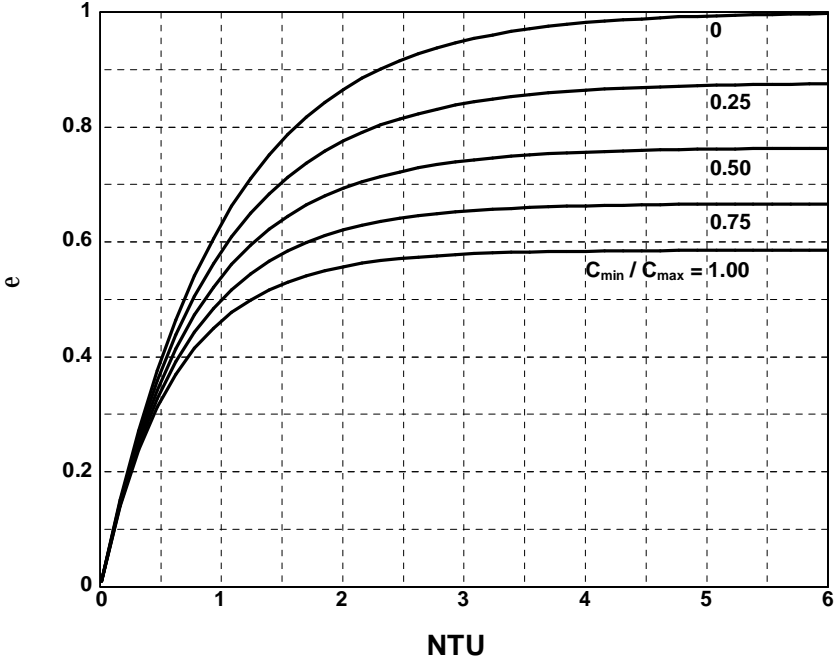


Shell-and-tube heat exchanger with *two* shell passes and $4n$ tube passes ($n=1,2,3,..$)

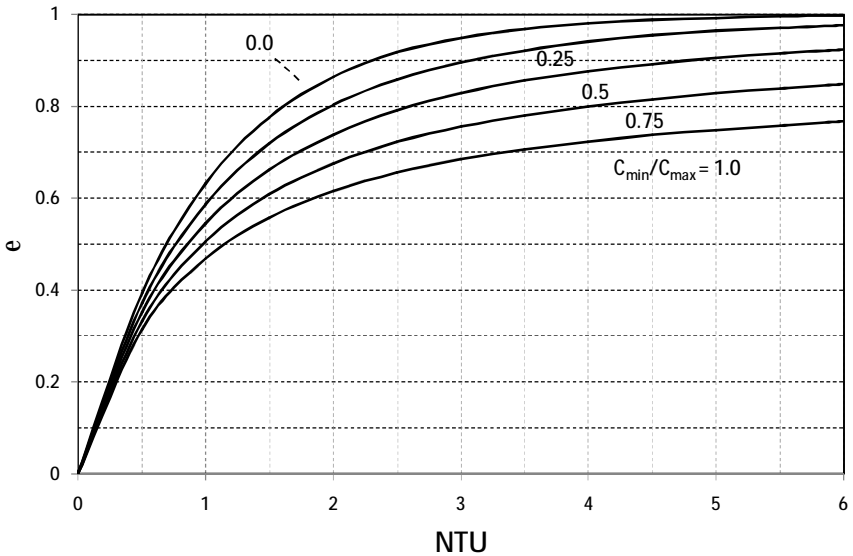


NTU-effectiveness

Shell-and-tube heat exchanger with *one* shell pass and $2n$ tube passes ($n=1,2,3,..$)



Cross-flow heat exchanger with both fluids unmixed



Thermodynamic Properties of Gases, Liquids and Solids

Properties of various gases (100 kPa and 300K)

	Molar Mass kg kmol ⁻¹	C _v kJkg ⁻¹ K ⁻¹	C _p kJkg ⁻¹ K ⁻¹	γ	k Wm ⁻¹ K ⁻¹	μ × 10 ⁵ kgm ⁻¹ s ⁻¹	P _c MPa	T _c K
Air	28.97	0.7197	1.007	1.399	0.02565	1.857	3.786	132.5
Ammonia	17.03	1.661	2.180	1.313	0.02486	1.031	11.30	405.4
Argon	39.95	0.3124	0.5215	1.669	0.01787	2.285	4.863	150.7
Carbon Dioxide	44.01	0.6593	0.8525	1.293	0.01677	1.502	7.377	304.1
Helium	4.003	3.116	5.193	1.667	0.1572	2.027	0.2275	5.195
Hydrogen	2.016	10.19	14.31	1.405	0.1779	0.9093	1.315	33.19
Methane	16.04	1.713	2.236	1.305	0.03438	1.125	4.599	190.6
Isobutane	58.12	1.701	1.541	1.104	0.01712	0.7561	36.40	407.8
Nitrogen	28.01	0.7441	1.042	1.401	0.02588	1.823	3.398	126.2
Oxygen	32.00	0.6581	0.9193	1.397	0.02669	2.099	5.043	154.6
Propane	44.10	1.698	1.496	1.135	0.01852	0.8295	42.47	369.8
Steam	18.02	-	-	-	0.01867	0.9815	22.06	647.1

Note: the actual values of μ are 10⁵ times smaller than the figures given e.g. μ_{air} = 0.00001857 kgm⁻¹s⁻¹.

Transport properties of various liquids

Name	Temp (°C)	Density kg m ⁻³	C _v kJkg ⁻¹ K ⁻¹	k Wm ⁻¹ K ⁻¹	μ kgm ⁻¹ s ⁻¹
Water	10	1000	4.182	0.5672	0.001312
Glycerine	10	1270	2.319	0.2846	4.293
Engine Oil-SAE60	10	893.7	1.839	0.1443	1.819
Engine Oil-SAE60	100	840	2.22	0.1367	0.01718
Mercury	10	13571	0.14	8.313	0.001627
Sodium	400	846.5	1.293	70.18	0.0002637
Ethanol	25	783	0.977	-	0.001144
R134a (1MPa)	0	1298	0.8787	0.09522	0.0002686
n-butane (2MPa)	10	592.7	1.669	0.1123	0.0001886

Thermodynamic properties of various metals at 300K (unless stated)

Name	ρ kg m ⁻³	C _v kJkg ⁻¹ K ⁻¹	k Wm ⁻¹ K ⁻¹	ε (polished) Wm ⁻² K ⁻⁴	ε (oxidised) W m ⁻² K ⁻⁴
Aluminium	2702	0.903	237	0.07	0.82 (anodised)
Carbon steel	7854	0.434	60.5	0.066	0.90
Copper	8933	0.385	401	0.03	0.50 (600K)
Gold	19300	0.129	317	0.07	0.025
Iron and steel	7870	0.447	80.2	0.3	0.61 (rusted)
Lead	11340	0.129	35.3	0.28 (grey)	0.63
Magnesium	1740	1.024	156	0.55	0.20
Stainless steel	8053	0.4815	15.2	0.17	0.33 (800K)
Titanium	4500	0.522	21.9	0.12	0.49 (800K)

Thermodynamic properties of various solids at 300K

Name	ρ kg m ⁻³	C_v kJkg ⁻¹ K ⁻¹	k Wm ⁻¹ K ⁻¹	ϵ W m ⁻² K ⁻⁴
Al-silica blanket	64	0.903	0.003	0.40
Brick-common	1920	0.4593	0.72	0.95
Cement mortar	1860	0.78	0.72	0.90
Concrete and stone mix	2100	0.88	1.38	0.90
Glass fibre duct liner	32	0.835	0.038	-
Glass-soda lime	2500	0.75	1.4	0.90
Gypsum plaster	1440	0.85	0.48	0.91
Hardwoods (oak, maple)	720	1.255	0.16	0.82
Ice (<273K)	920	2.168	1.678	0.96
Particle board-high density	1000	1.3	0.17	-
Polyethylene	960	2.1	0.33	-
Polystyrene moulded beads	16	1.21	0.04	-
PVC (poly vinyl chloride)	1700	1.1	0.09	-
Rock-granite	2630	0.775	2.79	0.88
Rock-limestone	2320	0.81	2.15	0.95
Rockwool Loosely packed	64	-	0.067	-
Rubber-vulcanized soft	1100	2.01	0.13	-
Silicon Carbide	3150	0.68	490	0.87
Softwoods (fir, pine)	510	1.38	0.12	0.92
Soil	2050	1.84	0.52	0.95
Urethane (two part, rigid)	70	1.04	0.026	-
Vermiculite flakes	120	0.065	900	-

Emissivities of various surfaces at 300K

Name	ϵ W m ⁻² K ⁻⁴
Aluminium paint	0.50
Asphalt	0.88
Enamel (white)	0.90
Paint (black)	0.98
Paint (white)	0.90
Paper (white)	0.95
Snow (<273K)	0.86
Zinc (galvanised surface)	0.23

Thermodynamic properties of gaseous steam and R134a, and air

Gaseous steam at low pressure

Gaseous R134a at low pressure

T (°C)	C_p kJkg ⁻¹ K ⁻¹	k Wm ⁻¹ K ⁻¹	$\mu \times 10^5$ kgm ⁻¹ s ⁻¹	Pr	T (°C)	C_p kJkg ⁻¹ K ⁻¹	k Wm ⁻¹ K ⁻¹	$\mu \times 10^5$ kgm ⁻¹ s ⁻¹	Pr
0	1.858	0.01707	0.9216	1.003	-40	0.6703	0.008113	0.9335	0.771
20	1.866	0.01823	0.9727	0.995	-30	0.7006	0.009131	0.9727	0.746
40	1.874	0.01960	1.031	0.986	-20	0.7324	0.01009	1.012	0.735
60	1.882	0.02119	1.093	0.971	-10	0.7654	0.011000	1.051	0.731
80	1.891	0.02301	1.159	0.953	0	0.7995	0.01188	1.089	0.733
100	1.900	0.02508	1.227	0.930	10	0.8349	0.01273	1.128	0.740
150	1.924	0.02886	1.418	0.945	20	0.8712	0.01354	1.166	0.750
200	1.950	0.03328	1.618	0.948	30	0.9089	0.01432	1.205	0.765
250	1.977	0.03817	1.822	0.944	40	0.9478	0.01507	1.243	0.782
300	2.005	0.04342	2.029	0.937	50	0.9879	0.01579	1.281	0.801
350	2.035	0.04897	2.237	0.929	60	1.0287	0.01647	1.319	0.824
400	2.065	0.05476	2.445	0.922	70	1.0719	0.01712	1.357	0.850
450	2.097	0.06077	2.652	0.915	80	1.1159	0.01774	1.395	0.877
500	2.129	0.06698	2.857	0.908	90	1.1611	0.01832	1.433	0.908
600	2.196	0.07990	3.262	0.896					
700	2.264	0.09338	3.655	0.886					
800	2.331	0.10730	4.038	0.877					

Note: the actual values of μ are 10^5 times smaller than the figures given. For example, the viscosity of gaseous R134a at 0°C is 0.00001089 kgm⁻¹s⁻¹.

Air tables (100 kPa, but usable for most pressures)

T (K)	C_p kJkg ⁻¹ K ⁻¹	C_v kJkg ⁻¹ K ⁻¹	γ	k Wm ⁻¹ K ⁻¹	$\mu \times 10^5$ kgm ⁻¹ s ⁻¹	Pr
150	0.9432	0.6562	1.437	0.01393	1.045	0.7076
200	0.9882	0.7012	1.409	0.01797	1.346	0.7406
250	1.005	0.7176	1.400	0.02187	1.614	0.7414
260	1.006	0.7185	1.399	0.02264	1.664	0.7394
280	1.006	0.7194	1.399	0.02415	1.763	0.7345
300	1.007	0.7197	1.399	0.02565	1.857	0.7290
320	1.007	0.7199	1.399	0.02712	1.949	0.7236
340	1.007	0.7203	1.398	0.02858	2.038	0.7185
350	1.008	0.7207	1.398	0.02930	2.082	0.7161
400	1.012	0.7246	1.396	0.03283	2.292	0.7062
450	1.019	0.7316	1.392	0.03625	2.489	0.6996
500	1.028	0.7409	1.387	0.03955	2.676	0.6956
600	1.051	0.7636	1.376	0.04582	3.024	0.6935
700	1.075	0.7880	1.364	0.05168	3.344	0.6956
800	1.099	0.8117	1.354	0.05716	3.641	0.6999
1000	1.140	0.8532	1.336	0.06706	4.180	0.7108
1200	1.173	0.8863	1.324	0.07576	4.662	0.7220
1400	1.199	0.9122	1.315	0.08347	5.098	0.7325
1600	1.220	0.9326	1.308	0.09042	5.497	0.7415
1800	1.236	0.9489	1.302	0.09682	5.865	0.7486
2000	1.249	0.9621	1.298	0.1029	6.204	0.7531
2500	1.274	0.9866	1.291	0.1182	6.953	0.7491
3000	1.291	1.004	1.286	0.1364	7.582	0.7177

International standard atmosphere

z m	P kPa	T K	ρ kg m ⁻³
-2500	135.21	304.4	1.5473
-2000	127.78	301.2	1.4782
-1500	120.70	297.9	1.4114
-1000	113.93	294.7	1.3470
-500	107.48	291.4	1.2849
0	101.33	288.2	1.2250
500	95.46	284.9	1.1673
1000	89.88	281.7	1.1117
1500	84.56	278.4	1.0582
2000	79.50	275.2	1.0066
2500	74.69	271.9	0.9570
3000	70.12	268.7	0.9093
3500	65.78	265.4	0.8634
4000	61.66	262.2	0.8194
4500	57.75	258.9	0.7770
5000	54.05	255.7	0.7365
5500	50.54	252.4	0.6975
6000	47.22	249.2	0.6602
6500	44.08	245.9	0.6243
7000	41.11	242.7	0.5901
7500	38.30	239.5	0.5573
8000	35.65	236.2	0.5258
8500	33.15	233.0	0.4958
9000	30.80	229.7	0.4671
9500	28.58	226.5	0.4397
10000	26.50	223.3	0.4136

z m	P kPa	T K	ρ kg m ⁻³
10500	24.54	220.0	0.3886
11000	22.70	216.8	0.3648
11500	20.98	216.7	0.3375
12000	19.40	216.7	0.3119
12500	17.93	216.7	0.2884
13000	16.58	216.7	0.2666
13500	15.33	216.7	0.2465
14000	14.17	216.7	0.2279
14500	13.10	216.7	0.2107
15000	12.11	216.7	0.1948
15500	11.20	216.7	0.1801
16000	10.35	216.7	0.1665
16500	9.57	216.7	0.1539
17000	8.85	216.7	0.1423
17500	8.18	216.7	0.1316
18000	7.57	216.7	0.1216
18500	7.00	216.7	0.1125
19000	6.47	216.7	0.1040
19500	5.98	216.7	0.0962
20000	5.53	216.7	0.0889
22000	4.05	218.6	0.0645
24000	2.97	220.6	0.0469
26000	2.19	222.5	0.0343
28000	1.62	224.5	0.0251
30000	1.20	226.5	0.0184
32000	0.89	228.5	0.0136

Temperature lapse rates are based on the US standard atmosphere 1976.

FLOW OF FLUIDS

Nomenclature

b	wingspan	m
c	speed of sound	ms^{-1}
C	velocity	ms^{-1}
C_f	skin friction coefficient	-
D	diameter	m
D	drag force (p. 62)	N
f	force, body force	N
g	gravity	ms^{-2}
l	reference length (usually mean chord)	m
L	lift force	N
L_e	flow development length	m
P	pressure	Nm^{-2}
q	dynamic pressure	Nm^{-2}
\dot{Q}	heat transfer rate (heat in)	W
Q	volume flow rate	m^3s^{-1}
r	radial distance	m
R	radius	m
R	gas constant	$\text{kJkg}^{-1}\text{k}^{-1}$
Re	Reynolds number	-
S	reference area (usually wing area)	m^2
u, v, w	velocity components in the x, y, z directions, respectively	ms^{-1}
U_∞	free stream velocity	ms^{-1}
V	1D velocity	ms^{-1}
\dot{W}	power (work out)	W
x	axial distance	m
z	elevation from a datum	m
δ^*	displacement thickness	m
γ	ratio of specific heats	-
Λ	aspect ratio	-
μ	dynamic viscosity	Pas
θ	momentum thickness	m
ρ	density	m^3kg^{-1}
τ	shear stress	Nm^{-2}
ν	kinematic viscosity	Nms^{-1}
w	conditions at the wall	
∞	free stream conditions	

Bernoulli's equation:

$$P + \frac{1}{2}\rho C^2 + \rho gz = \text{constant}$$

Bernoulli's equation with losses:

$$\frac{1}{2}\rho(C_2^2 - C_1^2) + \rho g(z_2 - z_1) + P_2 - P_1 + P_{loss} = 0$$

Steady flow energy equation:

$$\frac{1}{2}\rho(C_2^2 - C_1^2) + \rho g(z_2 - z_1) + P_{loss} = \frac{\dot{Q} - \dot{W}}{Q} = \frac{\dot{Q} - \dot{W}}{C_1 A_1}$$

Newton's law of viscosity:

$$\tau = \mu \frac{du}{dy}$$

Laminar flow

For a horizontal tube (Poiseuille Flow):

$$u = -\frac{dP}{dx} \frac{1}{4\mu} (R^2 - r^2)$$

$$Q = -\frac{dP}{dx} \frac{\pi R^4}{8\mu} = \frac{\pi R^4 \Delta P}{8\mu l} = \frac{\pi d^4 \Delta P}{128\mu l}$$

For flow between parallel plates:

$$Q = -\frac{dP}{dx} \frac{bc^3}{12\mu} = \frac{bc^3 \Delta P}{12\mu l}$$

Mean hydraulic diameter:

$$\frac{4 \times \text{Area}}{\text{Perimeter}}$$

Force momentum equation (FME) about axis x :

$$\sum F_x = \sum (\dot{m}C)_{out} - \sum (\dot{m}C)_{in}$$

Torque momentum equation (TME)

General:

$$\sum T_A = \left(\sum \dot{O}_{out} - \sum \dot{O}_{in} \right)_A$$

where $\dot{O} = \dot{m}rC$ (for a liquid $\dot{O} = \rho ArC^2$)

1D:

$$\sum T_A = \dot{m}(r_{out}C_{out} - r_{in}C_{in})$$

Speed of sound (in a perfect gas):

$$a = \sqrt{\gamma RT}$$

Pressure loss coefficients

Pressure loss coefficient in circular pipes:

$$\Delta P = \frac{1}{2} \rho C^2 \frac{4fl}{d}$$

f is taken from the Moody Diagram (page 63) or:

Laminar flow

$$f = \frac{16}{Re}$$

Colebrook-White (implicit)

$$\frac{1}{\sqrt{f}} = \log_{10} \left(\frac{\epsilon}{3.7d} + \frac{1.255}{Re \times \sqrt{f}} \right)$$

Swami and Jaine (explicit)

$$\sqrt{f} = \frac{0.25}{\log_{10} \left(\frac{\epsilon}{3.7d} + \frac{5.745}{Re^{0.9}} \right)}$$

Pressure losses in expansions and contractions: k = loss coefficient:

Sudden expansion

$$\Delta P = k \times \frac{1}{2} \rho C_1^2$$

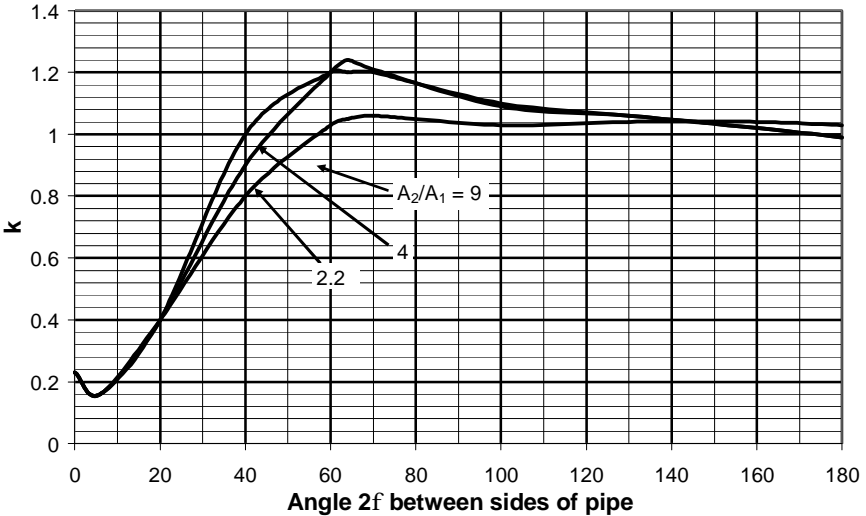
Sudden contraction

$$\Delta P = k \times \frac{1}{2} \rho C_2^2$$

where $k = \left(1 - \frac{A_1}{A_2}\right)^2$

d_2/d_1	0	0.2	0.4	0.6	0.8	1.0
k	0.50	0.45	0.38	0.28	0.14	0

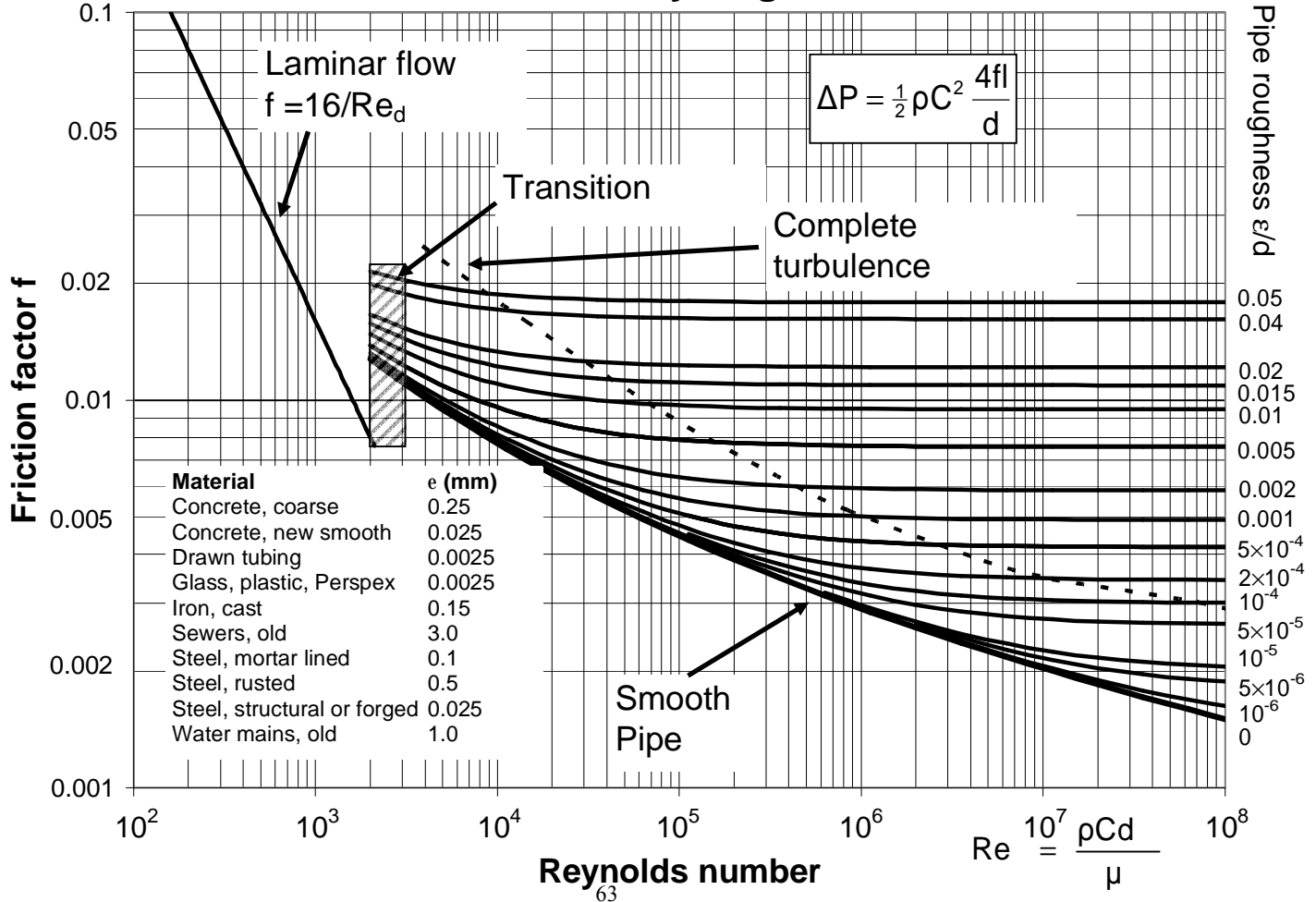
Pressure loss coefficient of conical diffuser



Loss coefficients for pipe fittings (smooth pipe). Tees assume equal flows.

90° Elbow (Sharp)	1.0	90° Elbow (Gradual)	0.2
45° Elbow (Sharp)	0.3	45° Elbow (Gradual)	0.1
90° Combining Tee (line flow)	0.5	90° Combining Tee (branch flow)	0.5
45° Combining Tee (line flow)	0.15	45° Combining Tee (branch flow)	0.15
90° Dividing Tee (line flow)	0.0	90° Dividing Tee (branch flow)	0.85
45° Dividing Tee (line flow)	0.0	45° Dividing Tee (branch flow)	0.45

Moody diagram



Boundary layers

Boundary layer on a flat-plate with zero pressure gradient

Boundary conditions $y = 0 : u = v = 0$ $y = \infty : u = U_\infty$

Blasius solution

$\eta = y \sqrt{\frac{U_\infty}{\nu x}}$	f	$f' = \frac{u}{U_\infty}$	f''	$\eta = y \sqrt{\frac{U_\infty}{\nu x}}$	f	$f' = \frac{u}{U_\infty}$	f''
0	0	0	0.33206	4.6	2.88826	0.98269	0.02948
0.2	0.00664	0.06641	0.33199	4.8	3.08534	0.98779	0.02187
0.4	0.02656	0.13277	0.33147	5.0	3.28329	0.99155	0.01591
0.6	0.05974	0.19894	0.33008	5.2	3.48189	0.99425	0.01134
0.8	0.10611	0.26471	0.32739	5.4	3.68094	0.99616	0.00793
1.0	0.16557	0.32979	0.32301	5.6	3.88031	0.99748	0.00543
1.2	0.23795	0.39378	0.31659	5.8	4.07990	0.99838	0.00365
1.4	0.32298	0.45627	0.30787	6.0	4.27964	0.99898	0.00240
1.6	0.42032	0.51676	0.29667	6.2	4.47946	0.99937	0.00155
1.8	0.52952	0.57477	0.28293	6.4	4.67938	0.99961	0.00098
2.0	0.65003	0.62977	0.26675	6.6	4.87931	0.99977	0.00061
2.2	0.78120	0.68132	0.24835	6.8	5.07928	0.99987	0.00037
2.4	0.92230	0.72899	0.22809	7.0	5.27926	0.99992	0.00022
2.6	1.07252	0.77246	0.20646	7.2	5.47925	0.99996	0.00013
2.8	1.23099	0.81152	0.18401	7.4	5.67924	0.99998	0.00007
3.0	1.39682	0.84605	0.16136	7.6	5.87924	0.99999	0.00004
3.2	1.56911	0.87609	0.13913	7.8	6.07923	1.00000	0.00002
3.4	1.74696	0.90177	0.11788	8.0	6.27923	1.00000	0.00001
3.6	1.92954	0.92333	0.09809	8.2	6.47923	1.00000	0.00001
3.8	2.11605	0.94112	0.08013	8.4	6.67923	1.00000	0.00000
4.0	2.30576	0.95552	0.06424	8.6	6.87923	1.00000	0.00000
4.2	2.49806	0.96696	0.05052	8.8	7.07923	1.00000	0.00000
4.4	2.69238	0.97587	0.03897				

Displacement: thickness: $\delta^* = 1.7208 \sqrt{\frac{\nu x}{U_\infty}}$

Momentum: thickness: $\theta = 0.664 \sqrt{\frac{\nu x}{U_\infty}}$

Skin friction coefficient: $C_f = \frac{\tau_w}{\frac{1}{2}\rho U_\infty^2} = \frac{0.664}{\sqrt{Re_x}} = 2 \frac{d\theta}{dx}$

Flow development length

Laminar flow: $L_e/D = 0.06 Re_D$

Turbulent flow: $L_e/D = 4.4 (Re_D)^{1/6}$

Equations of Motion in Cartesian Coordinates

Local energy conservation equation:

$$\frac{\partial(\rho u)}{\partial t} + \text{div}(p u \cdot \vec{v}) = -\text{div}(p \cdot \vec{v}) + \rho(\vec{g} \cdot \vec{v}) + \text{div}(\bar{\tau} \cdot \vec{v}) - \text{div}(\vec{q}) + \dot{q}_{\text{prod}}$$

Continuity equation:

$$\frac{\partial \rho}{\partial t} + \left[\frac{\partial(\rho u)}{\partial x} + \frac{\partial(\rho v)}{\partial y} + \frac{\partial(\rho w)}{\partial z} \right] = 0$$

Navier Stokes equations

x-direction : velocity component u

$$\begin{aligned} & \frac{\partial \rho u}{\partial t} + \frac{\partial(\rho u)u}{\partial x} + \frac{\partial(\rho v)u}{\partial y} + \frac{\partial(\rho w)u}{\partial z} = \\ & \frac{\partial}{\partial x} \left[\mu \left(2 \frac{\partial u}{\partial x} - \frac{2}{3} (\nabla \cdot \vec{v}) \right) \right] + \frac{\partial}{\partial y} \left[\mu \left(\frac{\partial v}{\partial x} + \frac{\partial u}{\partial y} \right) \right] + \frac{\partial}{\partial z} \left[\mu \left(\frac{\partial w}{\partial x} + \frac{\partial u}{\partial z} \right) \right] - \frac{\partial P}{\partial x} + \rho f_x \end{aligned}$$

y-direction : velocity component v

$$\begin{aligned} & \frac{\partial \rho v}{\partial t} + \frac{\partial(\rho u)v}{\partial x} + \frac{\partial(\rho v)v}{\partial y} + \frac{\partial(\rho w)v}{\partial z} = \\ & \frac{\partial}{\partial x} \left[\mu \left(\frac{\partial v}{\partial x} + \frac{\partial u}{\partial y} \right) \right] + \frac{\partial}{\partial y} \left[\mu \left(2 \frac{\partial v}{\partial y} - \frac{2}{3} (\nabla \cdot \vec{v}) \right) \right] + \frac{\partial}{\partial z} \left[\mu \left(\frac{\partial w}{\partial y} + \frac{\partial v}{\partial z} \right) \right] - \frac{\partial P}{\partial y} + \rho f_y \end{aligned}$$

z-direction : velocity component w

$$\begin{aligned} & \frac{\partial \rho w}{\partial t} + \frac{\partial(\rho u)w}{\partial x} + \frac{\partial(\rho v)w}{\partial y} + \frac{\partial(\rho w)w}{\partial z} = \\ & \frac{\partial}{\partial x} \left[\mu \left(\frac{\partial w}{\partial x} + \frac{\partial u}{\partial z} \right) \right] + \frac{\partial}{\partial y} \left[\mu \left(\frac{\partial w}{\partial y} + \frac{\partial v}{\partial z} \right) \right] + \frac{\partial}{\partial z} \left[\mu \left(2 \frac{\partial w}{\partial z} - \frac{2}{3} (\nabla \cdot \vec{v}) \right) \right] - \frac{\partial P}{\partial z} + \rho f_z \end{aligned}$$

Divergence of a vector in Cartesian coordinates:

$$\text{div} \vec{A} = \frac{\partial A_x}{\partial x} + \frac{\partial A_y}{\partial y} + \frac{\partial A_z}{\partial z}$$

Equations of Motion in Cylindrical Coordinates

Continuity equation:

$$\frac{\partial \rho}{\partial t} + \frac{1}{r} \frac{\partial \rho v_r}{\partial r} + \frac{1}{r} \frac{\partial \rho v_\theta}{\partial \theta} + \frac{\partial \rho v_z}{\partial z} = 0$$

Navier Stokes equation

r-direction : velocity component, v_r

$$\frac{\partial v_r}{\partial t} + v_r \frac{\partial v_r}{\partial r} + \frac{v_\theta}{r} \frac{\partial v_r}{\partial \theta} + v_z \frac{\partial v_r}{\partial z} - \frac{v_\theta^2}{r} =$$

$$\frac{1}{3} v \frac{\partial}{\partial r} (\nabla \cdot \vec{V}) + v \left[\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial v_r}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2 v_r}{\partial \theta^2} + \frac{\partial^2 v_r}{\partial z^2} - \frac{v_r}{r^2} - \frac{2}{r^2} \frac{\partial v_\theta}{\partial \theta} \right] - \frac{1}{\rho} \frac{\partial P}{\partial r} + \rho f_r$$

θ -direction : velocity component, v_θ

$$\frac{\partial v_\theta}{\partial t} + v_r \frac{\partial v_\theta}{\partial r} + \frac{v_\theta}{r} \frac{\partial v_\theta}{\partial \theta} + v_z \frac{\partial v_\theta}{\partial z} + \frac{v_r v_\theta}{r} =$$

$$\frac{1}{3} v \frac{\partial}{\partial \theta} (\nabla \cdot \vec{V}) + v \left[\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial v_\theta}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2 v_\theta}{\partial \theta^2} + \frac{\partial^2 v_\theta}{\partial z^2} - \frac{v_\theta}{r^2} + \frac{2}{r^2} \frac{\partial v_r}{\partial \theta} \right] - \frac{1}{\rho} \frac{\partial P}{\partial \theta} + \rho f_\theta$$

z-direction : velocity component, v_z

$$\frac{\partial v_z}{\partial t} + v_r \frac{\partial v_z}{\partial r} + \frac{v_\theta}{r} \frac{\partial v_z}{\partial \theta} + v_z \frac{\partial v_z}{\partial z} =$$

$$\frac{1}{3} v \frac{\partial}{\partial z} (\nabla \cdot \vec{V}) + v \left[\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial v_z}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2 v_z}{\partial \theta^2} + \frac{\partial^2 v_z}{\partial z^2} \right] - \frac{1}{\rho} \frac{\partial P}{\partial z} + \rho f_z$$

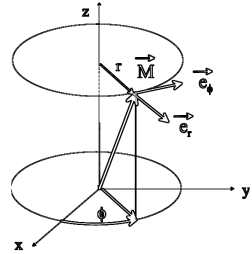
Divergence of a vector in cylindrical coordinates.

In cylindrical (polar) coordinates a vector, \vec{A} , is known by its components (A_r, A_ϕ, A_z) such that:

$$\vec{A} = A_r \vec{e}_r + A_\phi \vec{e}_\phi + A_z \vec{e}_z$$

In this system of coordinates but the divergence of a vector is:

$$\text{div} \vec{A} = \frac{1}{r} \frac{\partial}{\partial r} (r A_r) + \frac{1}{r} \frac{\partial}{\partial \phi} (A_\phi) + \frac{\partial}{\partial z} (A_z)$$



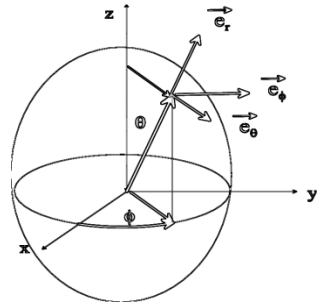
Divergence of a vector in spherical coordinates

In spherical coordinates a vector, \vec{A} , is known by its components (A_r, A_θ, A_ϕ) such that:

$$\vec{A} = A_r \vec{e}_r + A_\theta \vec{e}_\theta + A_\phi \vec{e}_\phi$$

And:

$$\text{div} \vec{A} = \frac{1}{r^2} \frac{\partial}{\partial r} (r^2 A_r) + \frac{1}{r \sin \theta} \frac{\partial}{\partial \theta} (\sin \theta A_\theta) + \frac{1}{r \sin \theta} \frac{\partial}{\partial \phi} (\sin \theta A_\phi)$$



Turbulence

Integral length scale (m):

$$L = \frac{3\pi}{4} \frac{\int E(k) k^{-1} dk}{\int E(k) dk}$$

The rms velocity u' associated to the energy spectrum $E(k)$ is defined as:

$$u'^2 = \frac{2}{3} \int E(k) dk$$

Kolmogorov length scale (m):

$$\eta \approx \varepsilon^{-\frac{1}{4}} \nu^{\frac{3}{4}}$$

Kolmogorov velocity (ms^{-1}):

$$v_k \approx \varepsilon^{\frac{1}{4}} \nu^{\frac{1}{4}}$$

Turbulence dissipation (m^2s^{-3}):

$$\varepsilon \approx \frac{u'^3}{L}$$

Reynolds number:

$$Re_L = \frac{u'L}{\nu} = \left(\frac{L}{\eta}\right)^{\frac{4}{3}}$$

where

$E(\mathbf{k})$	=	energy spectrum (m^3s^{-2})
u'	=	rms value of the turbulence velocity fluctuation (ms^{-1})
v_k	=	Kolmogorov velocity (ms^{-1})
ν	=	kinematic viscosity (m^2s^{-1})

so that:

$$Re_\eta = \frac{\eta v_k}{\nu} = 1$$

Aerodynamics and High-Speed Flow

Also see ‘Some Dimensionless Groups’ (page 8).

3D coefficients for wings

Pressure coefficient:

$$C_p = \frac{p - p_\infty}{q_\infty}$$

Skin friction coefficient:

$$C_f = \frac{\tau}{q_\infty}$$

Lift coefficient:

$$C_L = \frac{L}{q_\infty S}$$

Drag coefficient:

$$C_D = \frac{D}{q_\infty S}$$

Moment coefficient:

$$C_M = \frac{M}{q_\infty S l}$$

Induced drag coefficient:

$$C_{Di} = \frac{C_L^2}{\pi \Lambda}$$

$$\text{where } q = \frac{1}{2} \rho V^2 \text{ and } \Lambda = \frac{b^2}{S}$$

Velocity potential

Velocity potential function:

$$\mathbf{V} = \nabla \phi$$

Laplace equation for velocity potential:

$$\nabla^2 \phi = \frac{\partial^2 \phi}{\partial x^2} + \frac{\partial^2 \phi}{\partial y^2} + \frac{\partial^2 \phi}{\partial z^2} = 0$$

Shock waves

Dynamic relations for gas

$$e = c_v T$$

$$h = c_p T$$

$$c_p - c_v = R$$

$$\gamma = \frac{c_p}{c_v}$$

Isentropic flow properties

$$\begin{aligned} \gamma &= 1.400 \\ (\gamma - 1)/2 &= 0.200 \\ (\gamma + 1)/2(\gamma - 1) &= 3 \end{aligned}$$

$$\frac{A}{A^*} = \frac{1}{M} \left[\frac{1 + \frac{\gamma - 1}{2} M^2}{1 + \frac{\gamma - 1}{2}} \right]^{\frac{\gamma + 1}{2(\gamma - 1)}}$$

$$\frac{\rho_o}{\rho} = \left[1 + \frac{\gamma - 1}{2} M^2 \right]^{\frac{1}{\gamma - 1}}$$

$$\frac{T_o}{T} = 1 + \frac{\gamma - 1}{2} M^2$$

$$\frac{P_o}{P} = \left[1 + \frac{\gamma - 1}{2} M^2 \right]^{\frac{\gamma}{\gamma - 1}}$$

Normal shock properties

$$\begin{aligned} \gamma &= 1.400 \\ (\gamma - 1)/2 &= 0.200 \\ 2/(\gamma - 1) &= 5.000 \\ 2\gamma/(\gamma - 1) &= 7.000 \\ \gamma/(\gamma - 1) &= 3.5 \end{aligned}$$

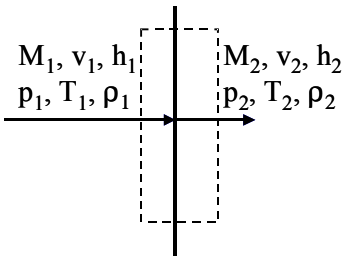
$$\frac{P_2}{P_1} = \frac{1 + \gamma M_1^2}{1 + \gamma M_2^2}$$

$$\frac{\rho_2}{\rho_1} = \frac{M_1}{M_2} \left[\frac{1 + \frac{\gamma - 1}{2} M_2^2}{1 + \frac{\gamma - 1}{2} M_1^2} \right]^{0.5}$$

$$\frac{T_2}{T_1} = \frac{1 + \frac{\gamma - 1}{2} M_1^2}{1 + \frac{\gamma - 1}{2} M_2^2}$$

$$\frac{P_{o2}}{P_{o1}} = \frac{P_2}{P_1} \left[\frac{1 + \frac{\gamma - 1}{2} M_2^2}{1 + \frac{\gamma - 1}{2} M_1^2} \right]^{\frac{\gamma}{\gamma - 1}}$$

$$\frac{P_{o2}}{P_{o1}} = \frac{P_{o2}}{P_{o1}} \frac{P_{o1}}{P_1}$$



Normal shock

Isentropic flow properties for $\gamma = 1.4$

M	A/A*	P ₀ /P	T ₀ /T	ρ_0/ρ	M	A/A*	P ₀ /P	T ₀ /T	ρ_0/ρ	M	A/A*	P ₀ /P	T ₀ /T	ρ_0/ρ
0.02	28.942	1.000	1.000	1.000	0.62	1.166	1.296	1.077	1.203	1.22	1.037	2.489	1.298	1.918
0.04	14.481	1.001	1.000	1.001	0.64	1.145	1.317	1.082	1.218	1.24	1.043	2.556	1.308	1.955
0.06	9.666	1.003	1.001	1.002	0.66	1.127	1.340	1.087	1.232	1.26	1.050	2.625	1.318	1.992
0.08	7.262	1.004	1.001	1.003	0.68	1.110	1.363	1.092	1.247	1.28	1.058	2.697	1.328	2.031
0.10	5.822	1.007	1.002	1.005	0.70	1.094	1.387	1.098	1.263	1.30	1.066	2.771	1.338	2.071
0.12	4.864	1.010	1.003	1.007	0.72	1.081	1.412	1.104	1.280	1.32	1.075	2.847	1.348	2.112
0.14	4.182	1.014	1.004	1.010	0.74	1.068	1.439	1.110	1.297	1.34	1.084	2.927	1.359	2.153
0.16	3.673	1.018	1.005	1.013	0.76	1.057	1.466	1.116	1.314	1.36	1.094	3.009	1.370	2.197
0.18	3.278	1.023	1.006	1.016	0.78	1.047	1.495	1.122	1.333	1.38	1.104	3.094	1.381	2.241
0.20	2.964	1.028	1.008	1.020	0.80	1.038	1.524	1.128	1.351	1.40	1.115	3.182	1.392	2.286
0.22	2.708	1.034	1.010	1.024	0.82	1.030	1.555	1.134	1.371	1.42	1.126	3.273	1.403	2.333
0.24	2.496	1.041	1.012	1.029	0.84	1.024	1.587	1.141	1.391	1.44	1.138	3.368	1.415	2.381
0.26	2.317	1.048	1.014	1.034	0.86	1.018	1.621	1.148	1.412	1.46	1.150	3.465	1.426	2.430
0.28	2.166	1.056	1.016	1.040	0.88	1.013	1.655	1.155	1.433	1.48	1.163	3.566	1.438	2.480
0.30	2.035	1.064	1.018	1.046	0.90	1.009	1.691	1.162	1.456	1.50	1.176	3.671	1.450	2.532
0.32	1.922	1.074	1.020	1.052	0.92	1.006	1.729	1.169	1.478	1.52	1.190	3.779	1.462	2.585
0.34	1.823	1.083	1.023	1.059	0.94	1.003	1.767	1.177	1.502	1.54	1.204	3.891	1.474	2.639
0.36	1.736	1.094	1.026	1.066	0.96	1.001	1.808	1.184	1.526	1.56	1.219	4.007	1.487	2.695
0.38	1.659	1.105	1.029	1.074	0.98	1.000	1.850	1.192	1.552	1.58	1.234	4.127	1.499	2.752
0.40	1.590	1.117	1.032	1.082	1.00	1.000	1.893	1.200	1.577	1.60	1.250	4.250	1.512	2.811
0.42	1.529	1.129	1.035	1.091	1.02	1.000	1.938	1.208	1.604	1.62	1.267	4.378	1.525	2.871
0.44	1.474	1.142	1.039	1.100	1.04	1.001	1.985	1.216	1.632	1.64	1.284	4.511	1.538	2.933
0.46	1.425	1.156	1.042	1.109	1.06	1.003	2.033	1.225	1.660	1.66	1.301	4.648	1.551	2.996
0.48	1.380	1.171	1.046	1.119	1.08	1.005	2.083	1.233	1.689	1.68	1.319	4.790	1.564	3.061
0.50	1.340	1.186	1.050	1.130	1.10	1.008	2.135	1.242	1.719	1.70	1.338	4.936	1.578	3.128
0.52	1.303	1.202	1.054	1.141	1.12	1.011	2.189	1.251	1.750	1.72	1.357	5.087	1.592	3.196
0.54	1.270	1.219	1.058	1.152	1.14	1.015	2.245	1.260	1.782	1.74	1.376	5.244	1.606	3.266
0.56	1.240	1.237	1.063	1.164	1.16	1.020	2.303	1.269	1.814	1.76	1.397	5.406	1.620	3.338
0.58	1.213	1.256	1.067	1.177	1.18	1.025	2.363	1.278	1.848	1.78	1.418	5.573	1.634	3.411
0.60	1.188	1.276	1.072	1.190	1.20	1.030	2.425	1.288	1.883	1.80	1.439	5.746	1.648	3.487

Isentropic flow properties for $g = 1.4$

M	A/A*	P ₀ /P	T ₀ /T	ρ ₀ /ρ	M	A/A*	P ₀ /P	T ₀ /T	ρ ₀ /ρ	M	A/A*	P ₀ /P	T ₀ /T	ρ ₀ /ρ
1.82	1.461	5.924	1.662	3.564	2.42	2.448	15.08	2.171	6.947	3.05	4.441	39.59	2.861	13.84
1.84	1.484	6.109	1.677	3.643	2.44	2.494	15.56	2.191	7.103	3.10	4.657	42.65	2.922	14.59
1.86	1.507	6.300	1.692	3.723	2.46	2.540	16.05	2.210	7.263	3.15	4.884	45.93	2.985	15.39
1.88	1.531	6.497	1.707	3.806	2.48	2.588	16.56	2.230	7.427	3.20	5.121	49.44	3.048	16.22
1.90	1.555	6.701	1.722	3.891	2.50	2.637	17.09	2.250	7.594	3.25	5.369	53.20	3.113	17.09
1.92	1.580	6.911	1.737	3.978	2.52	2.686	17.63	2.270	7.764	3.30	5.629	57.22	3.178	18.00
1.94	1.606	7.128	1.753	4.067	2.54	2.737	18.18	2.290	7.939	3.35	5.900	61.52	3.245	18.96
1.96	1.633	7.353	1.768	4.158	2.56	2.789	18.75	2.311	8.116	3.40	6.184	66.12	3.312	19.96
1.98	1.660	7.585	1.784	4.251	2.58	2.842	19.35	2.331	8.298	3.45	6.480	71.03	3.381	21.01
2.00	1.688	7.824	1.800	4.347	2.60	2.896	19.95	2.352	8.484	3.50	6.790	76.27	3.450	22.11
2.02	1.716	8.072	1.816	4.445	2.62	2.951	20.58	2.373	8.673	3.60	7.450	87.84	3.592	24.45
2.04	1.745	8.327	1.832	4.545	2.64	3.007	21.23	2.394	8.867	3.70	8.169	101.0	3.738	27.01
2.06	1.775	8.591	1.849	4.647	2.66	3.065	21.89	2.415	9.065	3.80	8.951	115.9	3.888	29.81
2.08	1.806	8.863	1.865	4.752	2.68	3.123	22.58	2.436	9.266	3.90	9.799	132.8	4.042	32.85
2.10	1.837	9.145	1.882	4.859	2.70	3.183	23.28	2.458	9.472	4.00	10.72	151.8	4.200	36.15
2.12	1.869	9.435	1.899	4.969	2.72	3.244	24.01	2.480	9.683	4.10	11.71	173.3	4.362	39.74
2.14	1.902	9.735	1.916	5.081	2.74	3.306	24.76	2.502	9.897	4.20	12.79	197.5	4.528	43.63
2.16	1.935	10.04	1.933	5.196	2.76	3.370	25.53	2.524	10.12	4.30	13.95	224.7	4.698	47.84
2.18	1.970	10.36	1.950	5.313	2.78	3.434	26.32	2.546	10.34	4.40	15.21	255.3	4.872	52.39
2.20	2.005	10.69	1.968	5.433	2.80	3.500	27.14	2.568	10.57	4.50	16.56	289.4	5.050	57.31
2.22	2.041	11.03	1.986	5.556	2.82	3.567	27.98	2.590	10.80	4.75	20.41	393.3	5.513	71.35
2.24	2.078	11.38	2.004	5.682	2.84	3.636	28.84	2.613	11.04	5.00	25.00	529.1	6.000	88.18
2.26	2.115	11.75	2.022	5.810	2.86	3.706	29.73	2.636	11.28	5.25	30.45	704.9	6.513	108.2
2.28	2.154	12.12	2.040	5.942	2.88	3.777	30.65	2.659	11.53	5.50	36.87	930.4	7.050	132.0
2.30	2.193	12.50	2.058	6.076	2.90	3.850	31.59	2.682	11.78	5.75	44.40	1217	7.613	159.9
2.32	2.233	12.90	2.076	6.213	2.92	3.924	32.56	2.705	12.04	6.00	53.18	1579	8.200	192.5
2.34	2.274	13.31	2.095	6.354	2.94	3.999	33.56	2.729	12.30	6.25	63.37	2032	8.813	230.5
2.36	2.316	13.73	2.114	6.497	2.96	4.076	34.59	2.752	12.57	6.50	75.13	2594	9.450	274.5
2.38	2.359	14.17	2.133	6.644	2.98	4.155	35.65	2.776	12.84	6.75	88.66	3289	10.11	325.2
2.40	2.403	14.62	2.152	6.794	3.00	4.235	36.73	2.800	13.12	7.00	104.1	4140	10.80	383.3

Normal shock properties

M_1	P_2/P_1	ρ_2/ρ_1	T_2/T_1	P_{o2}/P_{o1}	P_{o2}/P_1	M_2	M_1	P_2/P_1	ρ_2/ρ_1	T_2/T_1	P_{o2}/P_{o1}	P_{o2}/P_1	M_2
1.00	1.000	1.000	1.000	1.000	1.893	1.000	1.60	2.820	2.032	1.388	0.895	3.805	0.668
1.02	1.047	1.033	1.013	1.000	1.938	0.981	1.62	2.895	2.065	1.402	0.888	3.887	0.663
1.04	1.095	1.067	1.026	1.000	1.984	0.962	1.64	2.971	2.099	1.416	0.880	3.969	0.657
1.06	1.144	1.101	1.039	1.000	2.032	0.944	1.66	3.048	2.132	1.430	0.872	4.053	0.651
1.08	1.194	1.135	1.052	0.999	2.082	0.928	1.68	3.126	2.165	1.444	0.864	4.138	0.646
1.10	1.245	1.169	1.065	0.999	2.133	0.912	1.70	3.205	2.198	1.458	0.856	4.224	0.641
1.12	1.297	1.203	1.078	0.998	2.185	0.897	1.72	3.285	2.230	1.473	0.847	4.311	0.635
1.14	1.350	1.238	1.090	0.997	2.239	0.882	1.74	3.366	2.263	1.487	0.839	4.399	0.631
1.16	1.403	1.272	1.103	0.996	2.294	0.868	1.76	3.447	2.295	1.502	0.830	4.488	0.626
1.18	1.458	1.307	1.115	0.995	2.350	0.855	1.78	3.530	2.327	1.517	0.822	4.578	0.621
1.20	1.513	1.342	1.128	0.993	2.408	0.842	1.80	3.613	2.359	1.532	0.813	4.670	0.617
1.22	1.570	1.376	1.141	0.991	2.466	0.830	1.82	3.698	2.391	1.547	0.804	4.762	0.612
1.24	1.627	1.411	1.153	0.988	2.526	0.818	1.84	3.783	2.422	1.562	0.795	4.855	0.608
1.26	1.686	1.446	1.166	0.986	2.588	0.807	1.86	3.870	2.454	1.577	0.786	4.950	0.604
1.28	1.745	1.481	1.178	0.983	2.650	0.796	1.88	3.957	2.485	1.592	0.777	5.045	0.600
1.30	1.805	1.516	1.191	0.979	2.714	0.786	1.90	4.045	2.516	1.608	0.767	5.142	0.596
1.32	1.866	1.551	1.204	0.976	2.778	0.776	1.92	4.134	2.546	1.624	0.758	5.239	0.592
1.34	1.928	1.585	1.216	0.972	2.844	0.766	1.94	4.224	2.577	1.639	0.749	5.338	0.588
1.36	1.991	1.620	1.229	0.968	2.912	0.757	1.96	4.315	2.607	1.655	0.740	5.438	0.584
1.38	2.055	1.655	1.242	0.963	2.980	0.748	1.98	4.407	2.637	1.671	0.730	5.539	0.581
1.40	2.120	1.690	1.255	0.958	3.049	0.740	2.00	4.500	2.667	1.688	0.721	5.640	0.577
1.42	2.186	1.724	1.268	0.953	3.120	0.731	2.05	4.736	2.740	1.729	0.698	5.900	0.569
1.44	2.253	1.759	1.281	0.948	3.191	0.723	2.10	4.978	2.812	1.770	0.674	6.165	0.561
1.46	2.320	1.793	1.294	0.942	3.264	0.716	2.15	5.226	2.882	1.813	0.651	6.438	0.554
1.48	2.389	1.828	1.307	0.936	3.338	0.708	2.20	5.480	2.951	1.857	0.628	6.716	0.547
1.50	2.458	1.862	1.320	0.930	3.413	0.701	2.25	5.740	3.019	1.901	0.606	7.002	0.541
1.52	2.529	1.896	1.334	0.923	3.489	0.694	2.30	6.005	3.085	1.947	0.583	7.294	0.534
1.54	2.600	1.930	1.347	0.917	3.567	0.687	2.35	6.276	3.149	1.993	0.561	7.592	0.529
1.56	2.673	1.964	1.361	0.910	3.645	0.681	2.40	6.553	3.212	2.040	0.540	7.897	0.523
1.58	2.746	1.998	1.374	0.903	3.724	0.675	2.45	6.836	3.273	2.088	0.519	8.208	0.518

Normal shock properties

M_1	P_2/P_1	ρ_2/ρ_1	T_2/T_1	P_{o2}/P_{o1}	P_{o2}/P_1	M_2	M_1	P_2/P_1	ρ_2/ρ_1	T_2/T_1	P_{o2}/P_{o1}	P_{o2}/P_1	M_2
2.50	7.125	3.333	2.138	0.499	8.526	0.513	4.00	18.50	4.571	4.047	0.139	21.07	0.435
2.55	7.420	3.392	2.187	0.479	8.850	0.508	4.10	19.45	4.624	4.205	0.128	22.11	0.432
2.60	7.720	3.449	2.238	0.460	9.181	0.504	4.20	20.41	4.675	4.367	0.117	23.18	0.430
2.65	8.026	3.505	2.290	0.442	9.519	0.500	4.30	21.41	4.723	4.532	0.108	24.27	0.428
2.70	8.338	3.559	2.343	0.424	9.862	0.496	4.40	22.42	4.768	4.702	0.099	25.39	0.426
2.75	8.656	3.612	2.397	0.406	10.21	0.492	4.50	23.46	4.812	4.875	0.092	26.54	0.424
2.80	8.980	3.664	2.451	0.389	10.57	0.488	4.60	24.52	4.853	5.052	0.085	27.71	0.422
2.85	9.310	3.714	2.507	0.373	10.93	0.485	4.70	25.61	4.893	5.233	0.078	28.91	0.420
2.90	9.645	3.763	2.563	0.358	11.30	0.481	4.80	26.71	4.930	5.418	0.072	30.13	0.418
2.95	9.986	3.811	2.621	0.343	11.68	0.478	4.90	27.85	4.966	5.607	0.067	31.38	0.417
3.00	10.33	3.857	2.679	0.328	12.06	0.475	5.00	29.00	5.000	5.800	0.062	32.65	0.415
3.05	10.69	3.902	2.738	0.315	12.45	0.472	5.10	30.18	5.033	5.997	0.057	33.95	0.414
3.10	11.05	3.947	2.799	0.301	12.85	0.470	5.20	31.38	5.064	6.197	0.053	35.28	0.413
3.15	11.41	3.990	2.860	0.288	13.25	0.467	5.30	32.61	5.093	6.401	0.049	36.63	0.411
3.20	11.78	4.031	2.922	0.276	13.66	0.464	5.40	33.85	5.122	6.610	0.046	38.01	0.410
3.25	12.16	4.072	2.985	0.265	14.07	0.462	5.50	35.13	5.149	6.822	0.042	39.41	0.409
3.30	12.54	4.112	3.049	0.253	14.49	0.460	5.60	36.42	5.175	7.038	0.039	40.84	0.408
3.35	12.93	4.151	3.114	0.243	14.92	0.457	5.70	37.74	5.200	7.258	0.037	42.30	0.407
3.40	13.32	4.188	3.180	0.232	15.35	0.455	5.80	39.08	5.224	7.481	0.034	43.78	0.406
3.45	13.72	4.225	3.247	0.222	15.79	0.453	5.90	40.45	5.246	7.709	0.032	45.28	0.405
3.50	14.13	4.261	3.315	0.213	16.24	0.451	6.00	41.83	5.268	7.941	0.030	46.82	0.404
3.55	14.54	4.296	3.384	0.204	16.70	0.449	6.10	43.25	5.289	8.176	0.028	48.37	0.403
3.60	14.95	4.330	3.454	0.195	17.16	0.447	6.20	44.68	5.309	8.415	0.026	49.96	0.403
3.65	15.38	4.363	3.525	0.187	17.62	0.446	6.30	46.14	5.329	8.658	0.024	51.57	0.402
3.70	15.81	4.395	3.596	0.179	18.10	0.444	6.40	47.62	5.347	8.905	0.023	53.20	0.401
3.75	16.24	4.426	3.669	0.172	18.57	0.442	6.50	49.13	5.365	9.156	0.021	54.86	0.400
3.80	16.68	4.457	3.743	0.164	19.06	0.441	6.60	50.65	5.382	9.411	0.020	56.55	0.400
3.85	17.13	4.487	3.817	0.158	19.55	0.439	6.70	52.21	5.399	9.670	0.019	58.26	0.399
3.90	17.58	4.516	3.893	0.151	20.05	0.438	6.80	53.78	5.415	9.933	0.017	60.00	0.398
3.95	18.04	4.544	3.969	0.145	20.56	0.436	6.90	55.38	5.430	10.20	0.016	61.76	0.398
							7.00	57.00	5.444	10.47	0.015	63.55	0.397

Oblique shocks

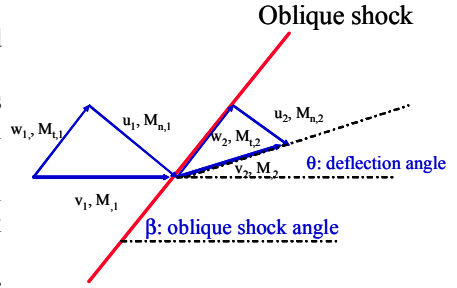
Flow can be decomposed into normal and tangential components.

The tangential velocity component is constant across a oblique shock (tangential momentum equation), $w_1=w_2$.

The three equations for the normal component are the same as the normal shock case.

The normal shock relations are therefore applicable to the normal component of the velocity.

Normal shock is a special case for $\beta=\pi/2$.



$$\sin b = \frac{u_1}{v_1}$$

$$\sin(b - q) = \frac{u_2}{v_2}$$

Oblique shock relations

Flow downstream of a oblique shock is defined by M_1 and β .

Mach number downstream of shock can be either supersonic(mostly) or subsonic

You can use the normal shock table for M_{n1} .

$$w_2 = w_1$$

$$M_{n1} = M_1 \sin \beta$$

$$\frac{\rho_2}{\rho_1} = \frac{(\gamma + 1) M_{n1}^2}{2 + (\gamma - 1) M_{n1}^2}$$

$$\frac{T_2}{T_1} = \frac{h_2}{h_1} = \frac{p_2 \rho_1}{p_1 \rho_2} = \left[1 + \frac{2\gamma}{\gamma + 1} (M_{n1}^2 - 1) \right] \frac{2 + (\gamma - 1) M_{n1}^2}{(\gamma + 1) M_{n1}^2}$$

$$M_{n2}^2 = \frac{1 + [(\gamma - 1)/2] M_{n1}^2}{\gamma M_{n1}^2 - (\gamma - 1)/2}$$

$$M_2 = \frac{M_{n2}}{\sin(\beta - \theta)}$$

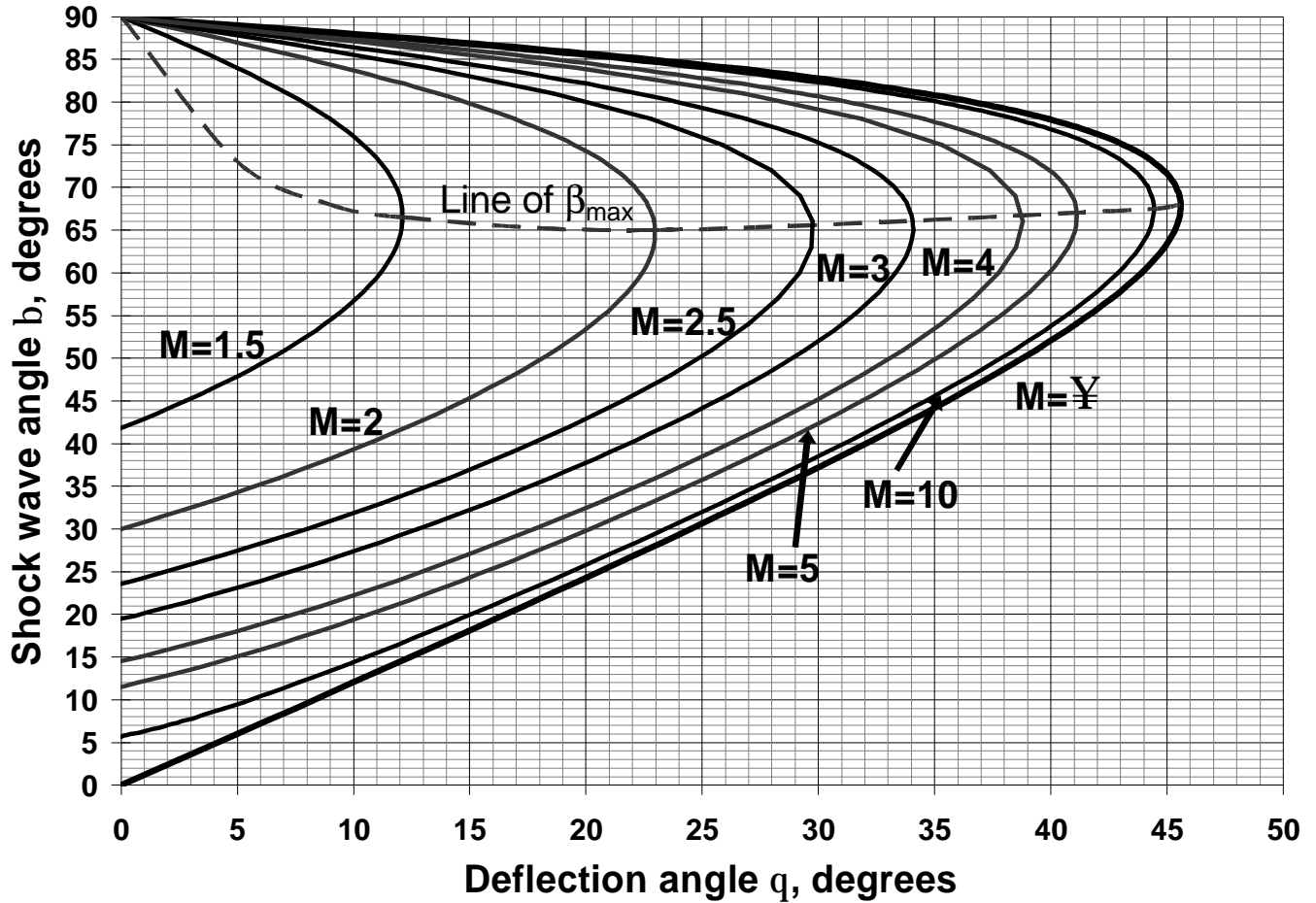
Angle of oblique shock for q-b-M chart

There is a maximum deflection for a given Mach number. There is no straight oblique shock solution for larger dynamic pressures, because the shock wave has become detached.

$$\tan \theta = 2 \cot \beta \left[\frac{M_1^2 \sin^2 \beta - 1}{M_1^2 (\gamma + \cos 2\beta) + 2} \right]$$

For a given dynamic pressure, there is both a weak and a strong shock solution. The weaker one is naturally favoured as this flow is generally supersonic.

When the dynamic pressure is zero, there is either a normal shock or a Mach wave.



Renewable Energy Data

Flat plate collector efficiency

$$\eta = \frac{GAF'(\tau\alpha) - AU'\Delta t}{AG}$$
$$\Delta t = \frac{(t_{cout} + t_{cin})}{2} - (t_o - 3)$$

Heat rise across plate:

$$\Delta T = \frac{\dot{Q}}{\dot{m}C_v}$$

Assume environmental temperature = $t_o - 3$

Hydroelectricity

$$v = \sqrt{2gH} = \sqrt{2gh\eta_h}, \text{ and } Q = v \times A$$

Ideal energy flow rate:

$$\text{Power} = Q \times h \times g \times r \quad (\text{W})$$

With energy losses and the 'effective' head.

Power	=	$(\rho \times g \times h \times \eta_h) \times (A \times v) \times \eta_f$	(W)
h	=	head	(m)
η_f	=	turbine efficiency	
η_h	=	efficiency	
v	=	fluid velocity	(m s^{-1})
A	=	cross sectional area	(m^2)
Q	=	volume flow rate	($\text{m}^3 \text{s}^{-1}$)

Tidal power

Available Energy:

$$\frac{\rho AR^2 g}{2}$$

Ground source heat pumps

kW Work (electricity) required per kW heat:

$$\frac{1}{COP_R + 1}$$

Calculations for vertical coils:

$$Length (m) = \frac{Heat\ Evaporator\ Capacity\ (W)}{Specific\ Heat\ Extraction\ Rate\ (W/m)}$$

Typical values of SHER range between 40-70 W/m

Or from ASHRAE's GSHP Engineering Manual:

$$Length (m) = \frac{0.05506 \times Annual\ energy\ rejected\ to\ the\ ground\ (MJ)}{Deep\ ground\ temp.\ (^{\circ}C) - Maximum\ entering\ liquid\ temp.\ (^{\circ}C)}$$

Calculations for horizontal coils:

$$Area (m^2) = \frac{Evaporator\ capacity\ (W)}{Average\ solar\ energy\ (W/m^2)}$$

Wind power

Weibull Distribution (H = hours/year during which V is exceeded):

$$H = 8760 \exp \left[- \left(\frac{V}{C} \right)^k \right]$$

Total energy in wind per m² per year:

$$E = 0.043V_{50}^3 (GJm^{-2}yr^{-1})$$

Power coefficient:

$$C_P = \frac{P}{\bar{E}} = \frac{P}{\frac{1}{2}\rho AV^3}$$

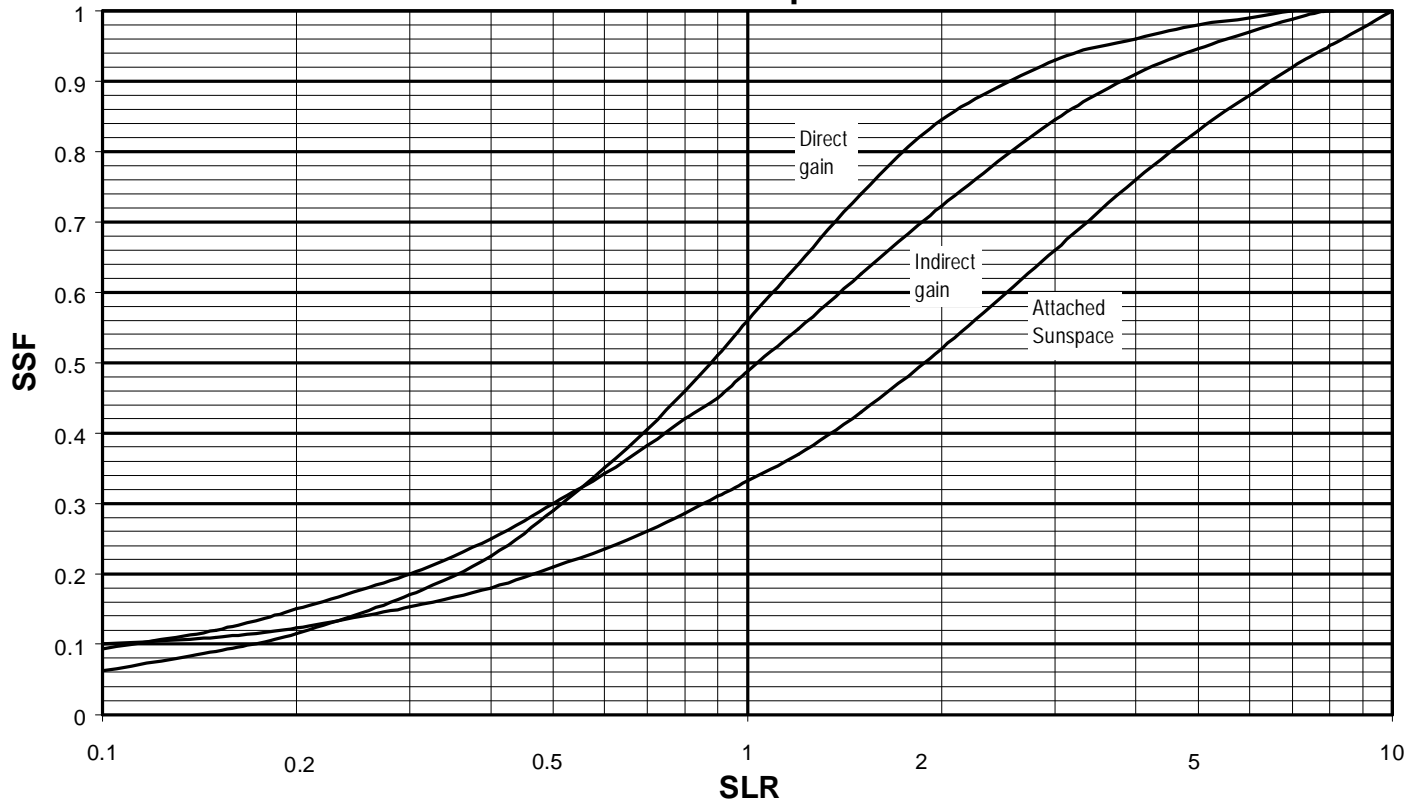
Tip speed ratio:

$$\mu = \frac{Speed\ of\ blade\ tip}{Wind\ speed} = \frac{\omega R}{V}$$

Solidity:

$$\frac{Total\ blade\ area}{Flow\ area\ swept\ by\ rotor} = \frac{A_b}{A}$$

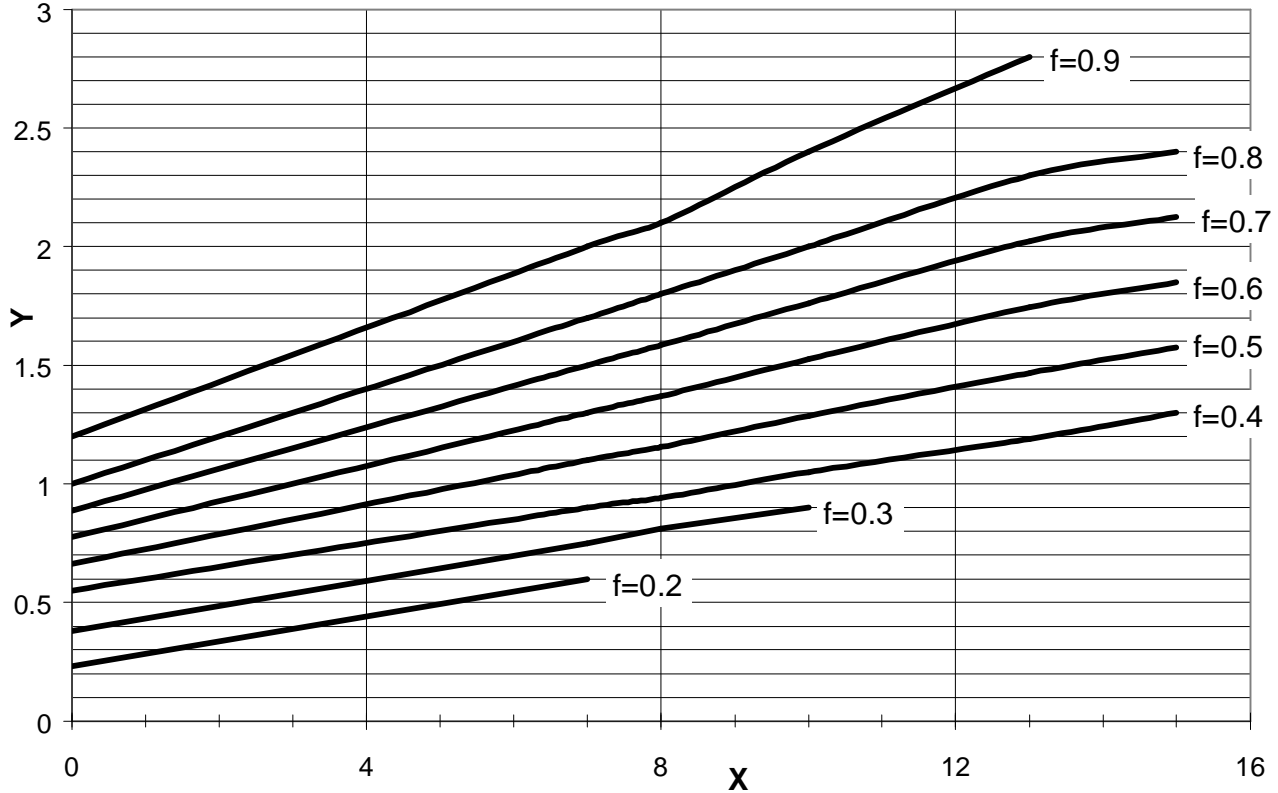
SLR/SSF Graph



f Chart

$$X = F_R \cdot U^1 \cdot \frac{F_R^1}{F_R} (T_{ref} - \bar{T}_a) \cdot N_S \cdot \frac{A}{L}$$

$$Y = F_R \cdot (\tau\alpha)_\eta \cdot \frac{F_R^1}{F_R} \cdot \frac{(\bar{\tau\alpha})}{(\bar{\tau\alpha})_n} \cdot \bar{H}_T \cdot N_D \cdot \frac{A}{L}$$



Sources

Alternative Fuels, E.M. Goodger, Macmillan Press Ltd., 1980.

Austrian Energy Agency

http://www.bioheat.info/pdf/kpn_wood_fuels_at.pdf

CODATA recommended values of the fundamental physical constants, P. J.

Mohr, B. N. Taylor,; 1998, Rev. Mod. Phys., 72, 351, 2000.

Combustion engineering, G. L. Borman and K. W. Ragland, McGraw Hill, 1998.

Energy Efficiency for Engineers and Technologists, T.D. Eastop, and D.R.

Croft, Longman, Harlow, 1990.

Explicit Equations for Pipe-Flow Problems, P.K. Swami, and A.K. Jaïne,

Journal of the Hydraulics Division, Proceedings of the ASCE, May 1976.

F-Chart Software EES, W. Beckman and S. Klein, Box 44042 Madison, WI

53744.

Fundamentals of fluid mechanics, B.R. Munson, D.F. Young, and T.H. Okiishi,

3rd ed., John Wiley and Sons, 1998.

Fundamentals of heat and mass transfer, F. P. Incropera and D. P. DeWitt, 2nd

Ed, John Wiley and Sons, 1985.

Gas Turbine Combustion, A. H. Lefebvre, Taylor and Francis, 1983.

Gas Turbine Fuels and Their Influence on Combustion, J. Odgers and D.

Kretschmer, Abacus Press, 1986.

Ground-Source Heat Pumps - Design of Geothermal Systems for Commercial

and Institutional Buildings, S.P. Kavanaugh; K. Rafferty ASHRAE, 1997.

Heat and mass transfer: a practical approach, Y. A. Cengel, 3rd ed., McGraw Hill, 2006.

Internal flow systems, Miller, D.S., 2nd edition, BHRA, Cranfield, 1990.

MechEng Calculators

<http://www.mechengcalculations.com/index.html>

Oak Ridge National Laboratory

http://www.ornl.gov/~wlj/hpdm/MARK_V_Initial_Doc_w_Refs.pdf

Thermodynamic and transport properties of fluids, G.F.C Rogers and Y.R.

Mayhew, Basil Blackwell, Oxford, 1980.

Thermophysical Properties of Matter, Y.S. Touloukian, et al. Vols. 3 and 11

IFI/Plenum, NY, 1970.

GENERAL INFORMATION

Useful data

Acceleration due to gravity	g	9.81 m s^{-2}
Avogadro constant	N_a	$6.022 \times 10^{26} \text{ kmol}^{-1}$
Boltzmann's constant:	k	$1.381 \times 10^{-23} \text{ JK}^{-1}$
Charge on electron:	e	$-1.602 \times 10^{-19} \text{ C}$
Molar gas constant	R_u	$8.314 \text{ kJ kmol}^{-1} \text{ K}^{-1}$
Molar volume of ideal gas (273.15 K, 100 kPa)	V_m	$22.4 \text{ m}^3 \text{ kmol}^{-1}$
Planck's constant:	h	$6.626 \times 10^{-34} \text{ Js}$
Speed of light in vacuum	c	$2.998 \times 10^8 \text{ m s}^{-1}$
Stefan-Boltzmann constant	σ	$56.7 \times 10^{-9} \text{ W m}^{-2} \text{ K}^{-4}$
Standard atmospheric pressure	p_a	101.325 kPa

Composition of air by volume

Nitrogen	N_2	78.084 %
Oxygen	O_2	20.9476 %
Argon	Ar	0.934 %
Carbon Dioxide	CO_2	0.0314 %

Just when you thought it was safe to get back into the compressed liquid water... along comes this extremely useful book of thermodynamic and fluid mechanics tables, formulæ and other vital information.

This compact tome will form a great companion for the rest of your engineering career.

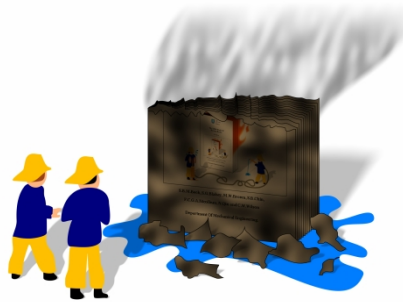
Some comments on previous editions :

“Before getting this, I used to lie awake worrying about the enthalpy of superheated R134a refrigerant - it has cured my insomnia”

“I can’t wait for the sequel”

“Just the right thickness to stop my desk rattling”

“If you enjoyed The DaVinci Code, you will love this; if you didn’t, you will still love it”



“Since the discovery of ink, nothing greater has ever been achieved”

“Crammed with equation upon exciting equation, this book has helped me to answer many of life’s big questions such as, ‘What’s the mass flow rate in the gutter outside my window?’ ”

“Last Christmas I purchased a copy for every member of my family. Never again will they forget the Ideal Gas Law. Thanks to the authors for saving their lives”

“You have enabled me to answer every question I have ever been asked”

This third edition promises to be still more exciting as it contains even more stuff. Big sections on oblique shock waves and solar and wind energy make this even better value.

Price: To you, two and a half quid.