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## Temperature-stable dielectric ceramics based on $\text{Na}_{0.5}\text{Bi}_{0.5}\text{TiO}_3$

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### ABSTRACT

Multiple ion substitutions to  $\text{Na}_{0.5}\text{Bi}_{0.5}\text{TiO}_3$  give rise to favourable dielectric properties over the technologically important temperature range  $-55\text{ }^\circ\text{C}$  to  $300\text{ }^\circ\text{C}$ . A relative permittivity,  $\epsilon_r = 1300 \pm 15\%$  was recorded, with low loss tangent,  $\tan\delta \leq 0.025$ , for temperatures from  $310\text{ }^\circ\text{C}$  to  $0\text{ }^\circ\text{C}$ ,  $\tan\delta$  increasing to 0.05 at  $-55\text{ }^\circ\text{C}$  (1 kHz) in the targeted solid solution  $(1-x)[0.85\text{Na}_{0.5}\text{Bi}_{0.5}\text{TiO}_3-0.15\text{Ba}_{0.8}\text{Ca}_{0.2}\text{Ti}_{1-y}\text{Zr}_y\text{O}_3]-x\text{NaNbO}_3$ :  $x = 0.3$ ,  $y = 0.2$ . The  $\epsilon_r$ -T plots for  $\text{NaNbO}_3$  contents  $x < 0.2$  exhibited a frequency-dependent inflection below the temperature of a broad dielectric peak. Higher levels of niobate substitution resulted in a single peak with frequency dispersion, typical of a normal relaxor ferroelectric. Experimental trends in properties suggest that the dielectric inflection is the true relaxor dielectric peak and appears as an inflection due to overlap with an independent broad dielectric peak. Process-related cation and oxygen vacancies and their possible contributions to dielectric properties are discussed.

### 1. Introduction

There is an ongoing drive to develop lead-free dielectrics for capacitors for use in electronic systems that can operate at temperatures well above  $200\text{ }^\circ\text{C}$  [1–19]. Applications include deep-well oil and gas exploration, defence and aerospace, and emerging power electronics technologies [1]. Most of these applications demand upper working temperatures between  $200$ – $300\text{ }^\circ\text{C}$ , with a lower operating temperature of  $-55\text{ }^\circ\text{C}$  [2,3]. High and stable relative permittivity combined with low dielectric loss tangent are basic requirements of the dielectric. Conventional core-shell ferroelectric-based barium titanate dielectrics with high and temperature-stable relative permittivity ( $\epsilon_r$ ), for use in Class II capacitors have upper operating temperatures of  $< 200\text{ }^\circ\text{C}$ . [3].

A number of lead-free dielectric ceramics with a temperature-stable relative permittivity (variation within  $\pm 15\%$ ) to temperatures in excess of  $200\text{ }^\circ\text{C}$  have been reported in recent years [3]. However the challenge of simultaneously extending performance to  $300\text{ }^\circ\text{C}$  whilst maintaining the Electronics Industries Alliance (EIA) specified minimum operating temperature of  $-55\text{ }^\circ\text{C}$ , in tandem with low dielectric loss and relative permittivity  $\epsilon_r$  values exceeding 1000, remains a major research challenge. The majority of the  $> 200\text{ }^\circ\text{C}$  dielectrics are based on relaxor ferroelectrics. In a classic relaxor ferroelectric such as  $\text{Pb}(\text{Mg}_{1/3}\text{Nb}_{2/3})\text{O}_3$ , compositional and charge disorder on the perovskite crystal lattice prevent the microscale electrostatic alignment of dipoles which occurs in a ferroelectric such as  $\text{BaTiO}_3$ . The concept of polar nanoregions is usually employed to account for the characteristic dielectric properties of a relaxor ferroelectric: a broad  $\epsilon_r$  peak with frequency dispersion arises from thermally induced changes to dipole

size and coupling dynamics. However it has been shown that multiple lattice substitution on the A and the B sites of the perovskite  $\text{ABO}_3$  lattice can suppress the relaxor dielectric peak. This enables  $\pm 15\%$  stability in  $\epsilon_r$  values to be achieved over wide temperature ranges, extending to high temperatures,  $> 200\text{ }^\circ\text{C}$  [3–24]. The new heavily disordered relaxors, with a near-flat  $\epsilon_r$ -T response, are referred to as ‘temperature-stable relaxors’ [3,6–10].

The properties of the majority of temperature stable relaxors can broadly be classified as: (a) materials which achieve high upper temperature limits of stable  $\epsilon_r$  (e.g.  $300$ – $500\text{ }^\circ\text{C}$ ) with mid value  $\epsilon_r$  ( $\epsilon_{r\text{ mid}}$ ) values of  $1000$ – $1200$  but with a minimum working temperature (e.g.  $50$ – $100\text{ }^\circ\text{C}$ ) well above the required EIA standard value of  $-55\text{ }^\circ\text{C}$ ; (b) materials which achieve stable  $\epsilon_r$  over the target  $-55\text{ }^\circ\text{C}$  to  $300\text{ }^\circ\text{C}$  temperature range but have a modest  $\epsilon_{r\text{ mid}}$  value of  $\sim 450$ – $500$ , which is detrimental to capacitor volumetric efficiency. Moreover, a number of materials have undesirably high dielectric loss tangents over at least part of the temperature range of stable  $\epsilon_r$  [3].

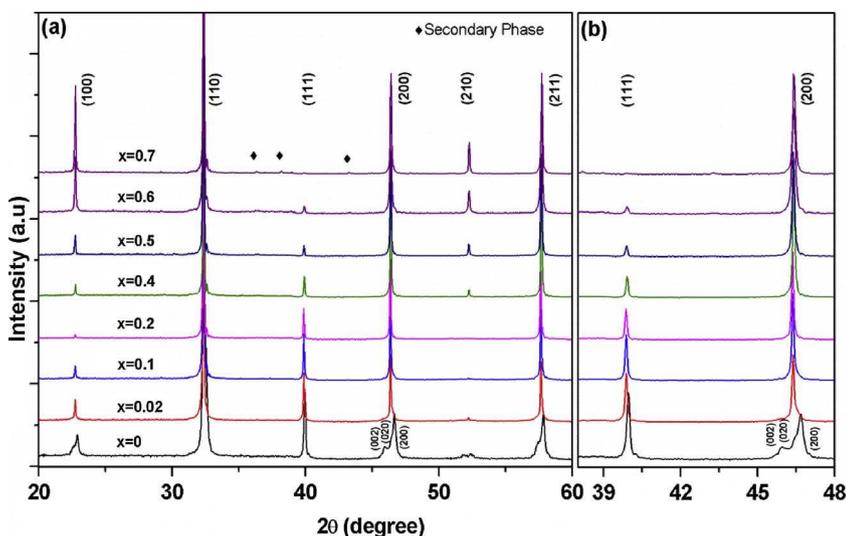
Against this background there is a requirement to discover new and improved compositions which achieve a temperature range of stable and high relative permittivity from  $-55\text{ }^\circ\text{C}$  to  $300\text{ }^\circ\text{C}$  and exhibit low dielectric losses across the full temperature range. Selecting  $\text{Na}_{0.5}\text{Bi}_{0.5}\text{TiO}_3$  as the parent relaxor material for developing a flattened  $\epsilon_r$ -T response by compositional engineering is a promising approach, given the high peak  $\epsilon_r$  values of  $\text{Na}_{0.5}\text{Bi}_{0.5}\text{TiO}_3$  [3–5,17–20]. Here we demonstrate that Zr-modification of a  $\text{Na}_{0.5}\text{Bi}_{0.5}\text{TiO}_3$ - $\text{Ba}_{0.8}\text{Ca}_{0.2}\text{TiO}_3$ - $\text{NaNbO}_3$  solid solution produces a material which satisfies the target  $-55$  to  $300\text{ }^\circ\text{C}$  temperature range of stability whilst possessing a moderately high  $\epsilon_{r\text{ mid}}$  value of 1300, with very promising values of dielectric loss.

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**Fig. 1.** (a) X-ray diffraction patterns of the ceramic series  $(1-x)[0.85\text{Na}_0.5\text{Bi}_0.5\text{TiO}_3-0.15\text{Ba}_0.8\text{Ca}_0.2\text{Ti}(\text{1-y})\text{Zr}_y\text{O}_3]-x\text{NaNbO}_3$ , ( $0 \leq x \leq 0.7$ ) (b) expanded scale showing  $\{111\}$  and  $\{200\}$  peaks. Diamond symbols indicate unidentified secondary phase(s) in  $x = 0.06$  and  $0.07$  samples.

## 2. Experimental procedure

Multiple lattice substitutions to  $\text{Na}_{0.5}\text{Bi}_{0.5}\text{TiO}_3$  involving Ca, Nb, and Zr were achieved in the solid solution system:  $(1-x)[0.85\text{Na}_{0.5}\text{Bi}_{0.5}\text{TiO}_3-0.15\text{Ba}_{0.8}\text{Ca}_{0.2}\text{Ti}(\text{1-y})\text{Zr}_y\text{O}_3]-0.3\text{NaNbO}_3$  ( $0 \leq x \leq 0.7$ ;  $y = 0$  or  $0.2$ ). The solid solution nomenclature is abbreviated to  $1-x(\text{NBT-BCT})-x\text{NN}$  for  $y = 0$  compositions (without Zr modification). This corresponds to the notional formula  $1-x(\text{Na}_{0.425}\text{Bi}_{0.425}\text{Ba}_{0.12}\text{Ca}_{0.03}\text{TiO}_3)-x(\text{NaNbO}_3)$ , but the results described below indicate the products deviate from this composition.

Ceramic samples were prepared by a mixed oxide route, using the following starting reagents:  $\text{BaCO}_3$  ( $\geq 99\%$  purity; Alpha Aesar, Ward Hill, MA);  $\text{Nb}_2\text{O}_5$  (99.9%, Alpha Aesar);  $\text{CaCO}_3$  ( $\geq 99\%$ ; Sigma Aldrich, St. Louis, MO);  $\text{Na}_2\text{CO}_3$  ( $\geq 99.5\%$ , Sigma Aldrich);  $\text{Bi}_2\text{O}_3$  (99.9%, Aldrich);  $\text{TiO}_2$  (99.9%, Aldrich) and  $\text{ZrO}_2$  (99%, Sigma Aldrich). The raw powders were dried overnight in an oven at  $\sim 200^\circ\text{C}$  prior to weighing in appropriate ratios, followed by ball milling in isopropanol for 24 h. The dried slurries were sieved through a 300  $\mu\text{m}$  nylon mesh and calcined at  $850^\circ\text{C}$  for 4 h (heating rate  $5^\circ\text{C}/\text{min}$ ). A binder (Ciba Glascol HA4; Ciba Speciality Chemicals, Bradford UK) was introduced and the powders were re-milled again for 24 h. These powders were uniaxially compacted in a steel die at  $\sim 70\text{MPa}$  followed by cold isostatic pressing at 200 MPa to produce disc-shaped pellets,  $\sim 10\text{mm}$  in diameter and  $\sim 1.5\text{mm}$  thickness. The pellets were embedded in a previously calcined powder of the same composition in an alumina crucible, and a lid fitted to minimise loss of volatile components during sintering, carried out at a temperature  $1160^\circ\text{C}$ , for 10 h (heating rate  $1^\circ\text{C}/\text{min}$  to  $550^\circ\text{C}$ , then  $5^\circ\text{C}/\text{min}$  to  $1160^\circ\text{C}$ ; cooling rate  $5^\circ\text{C}/\text{min}$ ).

Phase analysis of the sintered pellets was performed on crushed pellets using a X-ray diffractometer (Bruker; D8, Karlsruhe, Germany,  $\lambda_{\text{Cu-K}\alpha 1} = 1.5406\text{\AA}$ , scan speed  $1^\circ/\text{min}$ ): an external standard was used for calibration purposes prior to commencing the measurements. Microstructural analysis was carried out on fracture surfaces by scanning electron microscopy, SEM, which qualitatively indicated grain sizes of 2–6  $\mu\text{m}$ . Ion polished surfaces were also examined by SEM (LEO Gemini 1530 Oxford instruments) with energy dispersive X-ray analysis EDX facility. Phase quantification (% area) was obtained from SEM-EDX maps by processing energy dispersive X-ray (EDX) area maps using Image J software (v1.50i).

For dielectric measurements, the sintered ceramics were polished using 400 and 800 grade silicon carbide papers and electrodes applied using silver paint (Agar Scientific, Stansted, UK); pellets were fired at  $550^\circ\text{C}$  for 10 min to form the electrodes. Values of relative permittivity and loss tangent were measured as a function of temperature using an impedance analyser (HP Agilent 4192A, Hewlett Packard, Santa Clara,

CA). The influence of an electric bias field on the dielectric properties was determined by analysis of polarisation-electric field (P-E) loops using a field amplitude of  $1\text{ kV}/\text{mm}$ . The required time-dependent voltage waveforms were generated using a HP33120A function generator and then applied to the specimens by means of a high voltage amplifier (Chevin Research, Otley, UK). Values of dc resistance were measured using a Keithley 617 programmable electrometer (Cleveland, OH) in the temperature range  $250\text{--}550^\circ\text{C}$  at a fixed dc voltage of  $80\text{ V}$ .

## 3. Results and discussion

Room temperature X-ray powder diffraction patterns of crushed sintered pellets of  $1-x(\text{NBT-BCT})-x\text{NN}$  formulations (without Zr modification) are shown in Fig. 1. The crystal structure of the parent NBT compound is complex, being a distorted perovskite with extensive oxygen tilt systems: it is reported to be rhombohedral or monoclinic at room temperature becoming tetragonal at  $400^\circ\text{C}$  [26–29]. The lack of resolution in normal laboratory XRD data, Fig. 1, makes definitive phase analysis of NBT-BCT-NN challenging. The XRD patterns for compositions  $x > 0.02$  appear to be pseudocubic, whilst sample  $x = 0$  and possibly  $x = 0.02$  appear to be mixed tetragonal and pseudocubic. There was a low intensity peak ( $32.4^\circ 2\theta$ ) adjacent to the 110 main-phase perovskite peak in  $x \geq 0.1$  samples. This corresponds to the most intense reflection in the XRD pattern of  $\text{NaNbO}_3$  (ICDD 04-017-2917). Additional unidentified weak extra peaks appeared in  $x = 0.6$  and  $0.7$  samples. There was no significant variation in cubic lattice parameter with increasing  $\text{NaNbO}_3$  content, but the changes to dielectric data (Fig. 2) indicate that a change to the composition of the solid solution occurred with increasing  $x$ , consistent with  $\text{NaNbO}_3$  incorporation.

The  $\epsilon_r$ - $T$  plots for sample compositions,  $x = 0, 0.02, 0.05, 0.1$ , each showed an inflection below the temperature of a broad peak: these are labelled  $T_1$  and  $T_2$  respectively, Fig. 2. This type of dielectric plot with a broad peak and a frequency dependent inflection is similar to that reported for unmodified  $\text{Na}_{0.5}\text{Bi}_{0.5}\text{TiO}_3$  and for other  $\text{N}_{0.5}\text{Bi}_{0.5}\text{TiO}_3$  solid solutions such as the Pb-free piezoelectric material NBT-BT [3–5,17,18]. The  $T_1$  peak of the latter has been attributed in the literature to a depolarisation event, and  $T_2$  labelled as  $T_m$  implying it to be a normal relaxor ferroelectric peak. However, the broad peaks around temperature  $T_2$  in Fig. 2a–c showed negligible frequency dependence, unlike that of typical relaxors. Without  $\text{NaNbO}_3$  modification ( $x = 0$ ) the very broad  $T_2$  peak was centred at  $\sim 250^\circ\text{C}$ ; this reduced slightly to  $\sim 220^\circ\text{C}$  for all of the  $\text{NaNbO}_3$  modified compositions  $x = 0, 0.02, 0.05$  and  $0.1$ . The magnitude of the  $T_2$  dielectric peak decreased with increasing  $x$  for the  $x \leq 0.1$  compositional series and was barely detectable at composition  $x = 0.2$ , Fig. 2a–d. Because of the disappearance of

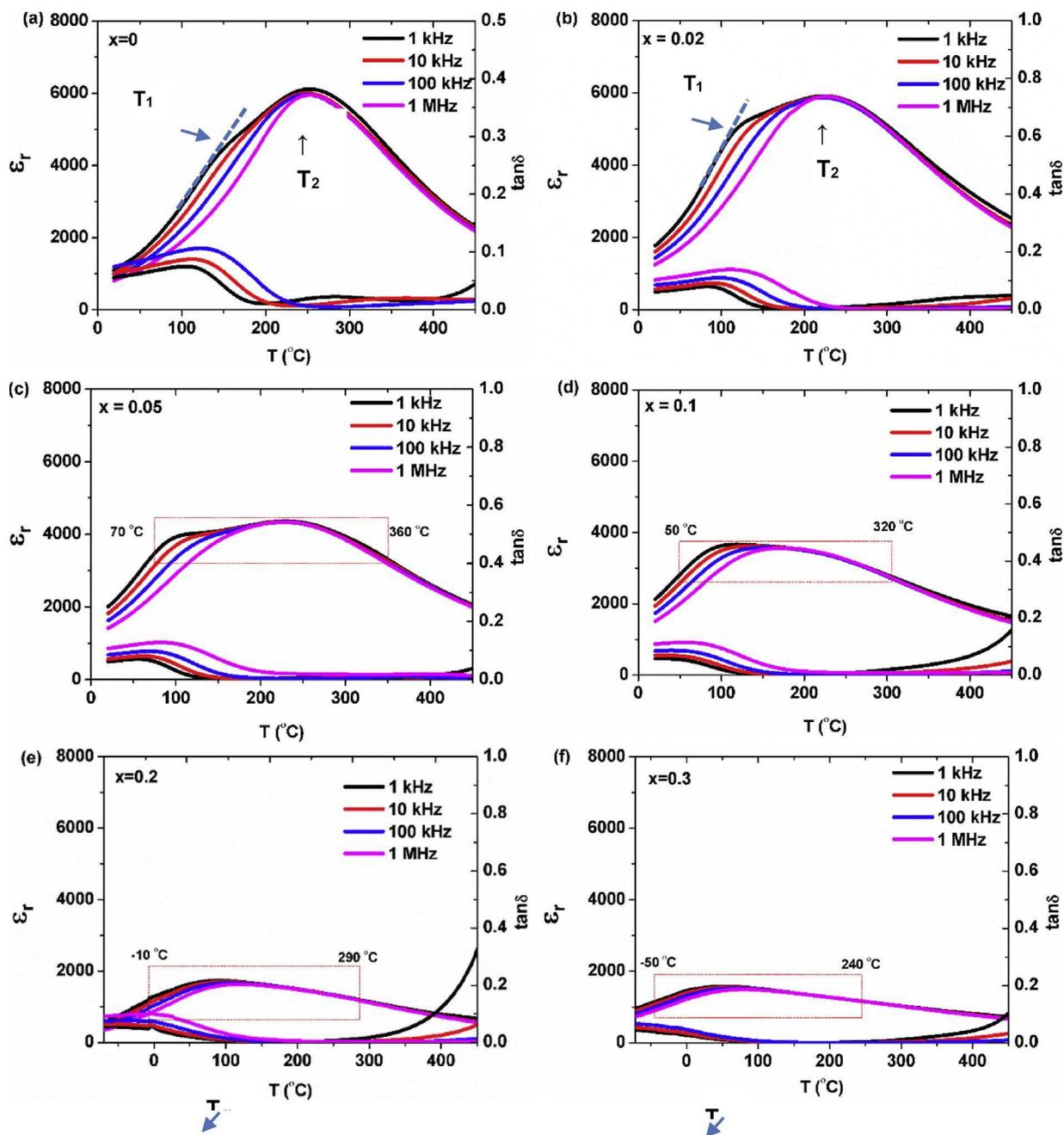


Fig. 2. Temperature-dependent relative permittivity,  $\epsilon_r$ , and loss tangent,  $\tan\delta$ , of  $(1-x)[\text{Na}_{0.85}\text{Bi}_{0.5}\text{TiO}_3-0.15\text{Ba}_{0.8}\text{Ca}_{0.2}\text{TiO}_3]-x\text{NaNbO}_3$ : (a)  $x = 0$  (expanded  $\tan\delta$  scale); (b)  $x = 0.02$ ; (c)  $x = 0.05$ ; (d)  $x = 0.1$ ; (e)  $x = 0.2$ , (f)  $x = 0.3$ . Boxes indicates temperature range of  $\pm 15\%$  stability in  $\epsilon_r$ . The ‘inflection’ and peak are labelled  $T_1$  and  $T_2$  (Fig. 3a, b).

**Table 1**  
Summary of the properties of  $(1-x)[\text{Na}_{0.5}\text{Bi}_{0.5}\text{TiO}_3-0.15\text{Ba}_{0.8}\text{Ca}_{0.2}\text{TiO}_3]-x[\text{NaNbO}_3]$  ( $0 \leq x \leq 0.5$ ) and Zr-modified ceramics,  $0.7[\text{Na}_{0.5}\text{Bi}_{0.5}\text{TiO}_3-0.15\text{Ba}_{0.8}\text{Ca}_{0.2}\text{TiO}_3\text{Zr}_{0.2}\text{O}_3]-0.3[\text{NaNbO}_3]$ , ‘ $x = 0.3, y = 0.2$ ’ (1 kHz). \*  $\epsilon_{r\text{mid}}$  refers to the median value in the T range quoted for  $\epsilon_r \pm 15\%$ .

x	$\epsilon_{r25^\circ\text{C}}$	$T_1, T_m$ (°C)	$T_2$ (°C)	$\epsilon_{r\text{max}}$	$\epsilon_{r\text{mid}}^*$	T-range (°C) $\epsilon_{r\text{mid}} \pm 15\%$	T-range (°C) $\tan\delta \leq 0.025$
0	1190	160	250	6120	–	–	170 to 410
0.02	1870	120	220	5690	–	–	140 to 310
0.05	2110	110	220	4360	3800	70 to 360	110 to 420
0.1	2230	100	220	3630	3190	50 to 320	100 to 310
0.2	1530	80	–	1720	1500	–10 to 290	50 to 310
0.3	1550	50	–	1580	1400	–50 to 240	20 to 340
0.4	1460	40	–	1480	1300	–70 to 210	–10 to 380
0.45	1280	30	–	1280	1100	–70 to 200	–40 to 300
0.5	1100	20	–	1100	950	–70 to 190	–50 to 290
$x = 0.3, y = 0.2$	1480	60	–	1530	1300	–55 to 330	0 to 310

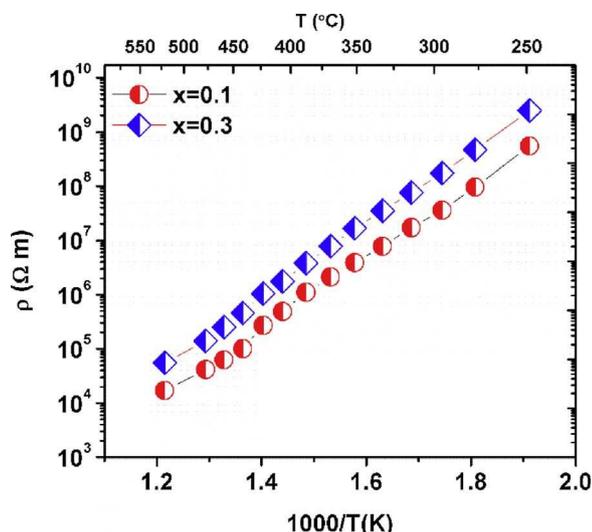


Fig. 3. dc resistivity versus reciprocal temperature for sample compositions  $x = 0.1$  and  $0.3$ .

the  $T_2$  peak, the dielectric plots for samples  $x \geq 0.2$  were similar to those of a normal relaxor with a single frequency-dependent peak, labelled  $T_m$ . The observation that  $\text{NaNbO}_3$  incorporation suppresses the magnitude of the  $T_2$  peak has been reported

The temperature ranges of  $\epsilon_r \pm 15\%$  stability are represented by outline boxes in Fig. 2, and listed in Table 1 along with other dielectric data. At composition  $x = 0.3$ ,  $\epsilon_r = 1400 \pm 15\%$  at temperatures between  $-50^\circ\text{C}$  and  $240^\circ\text{C}$ , with  $\tan\delta$  values  $\leq 0.025$  (1 kHz) for the temperature range  $20^\circ\text{C}$  to  $340^\circ\text{C}$ . None of these NBT-BCT-NN compositions satisfy the combination of basic dielectric properties required of a new generation of high temperature capacitor materials.

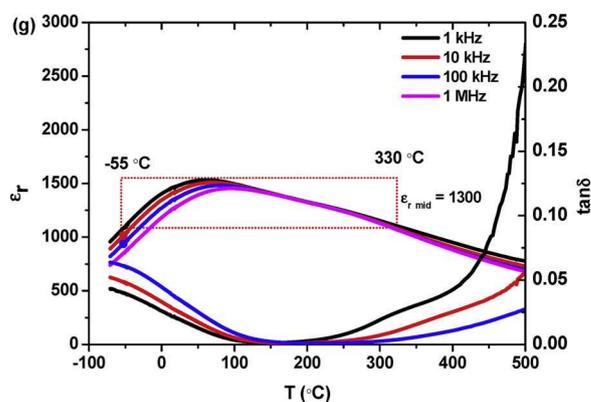


Fig. 5. Temperature-dependence of relative permittivity ( $\epsilon_r$ ) of Zr-modified samples,  $x = 0.3$ ,  $y = 0.2$  ceramics:  $0.7[0.85\text{Na}0.5\text{Bi}0.5\text{TiO}_3-0.15\text{Ba}0.8\text{Ca}0.2\text{Ti}_{0.8}\text{Zr}_{0.2}\text{O}_3]-0.3\text{NaNbO}_3$ . Dashed region indicates temperature range of  $\epsilon_r$  with  $\pm 15\%$  stability.

Values of d.c. resistivity were measured for sample  $x = 0.1$  (twin dielectric anomalies,  $T_1$  and  $T_2$ , but with a relatively small peak) and sample  $x = 0.3$  (single relaxor peak,  $T_m$ ). The plot of  $\rho$  vs.  $1/T$ , shown in Fig. 3, indicates an activation energy for conduction of  $0.5\text{--}0.6\text{ eV}$ , consistent with an oxide ion conduction mechanism. The  $x = 0.3$  sample showed higher resistivity; at  $300^\circ\text{C}$ ,  $\rho = 2 \times 10^7$  and  $1 \times 10^8\ \Omega\text{m}$  for  $x = 0.1$  and  $0.3$  respectively.

In order to further modify the solid solution composition NBT-BCT-NN with the aim of achieving improved dielectric performance, the effect of incorporating  $\text{Zr}^{4+}$  along with  $\text{Ti}^{4+}$  and  $\text{Nb}^{5+}$  ions on the B sites was investigated, selecting  $x = 0.3$  as the base composition. The formulation  $0.7[0.85\text{Na}_{0.5}\text{Bi}_{0.5}\text{TiO}_3-0.15\text{Ba}_{0.8}\text{Ca}_{0.2}\text{Ti}_{(1-y)}\text{Zr}_y\text{O}_3]-0.3\text{NaNbO}_3$  with  $y = 0.2$  was selected for study. Higher values of  $\text{NaNbO}_3$  content resulted in significant phase heterogeneity. Samples with  $x = 0.3$ ,  $y = 0.2$  were

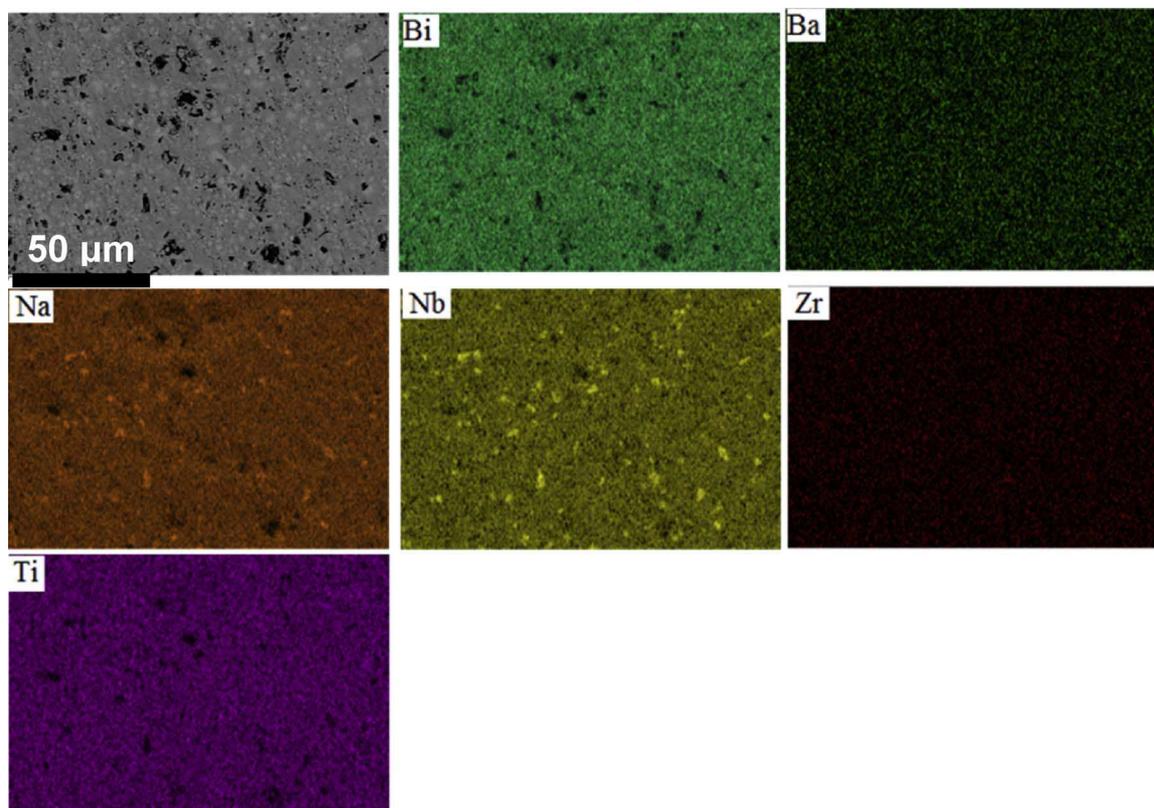


Fig. 4. SEM-EDX mapping of  $x = 0.3$ ,  $y = 0.2$  ceramic:  $0.7[0.85\text{Na}_{0.5}\text{Bi}_{0.5}\text{TiO}_3-0.15\text{Ba}_{0.8}\text{Ca}_{0.2}\text{Ti}_{(1-y)}\text{Zr}_y\text{O}_3]-0.3\text{NaNbO}_3$ , illustrating the occurrence of a Na- and Nb-rich phase for this composition.

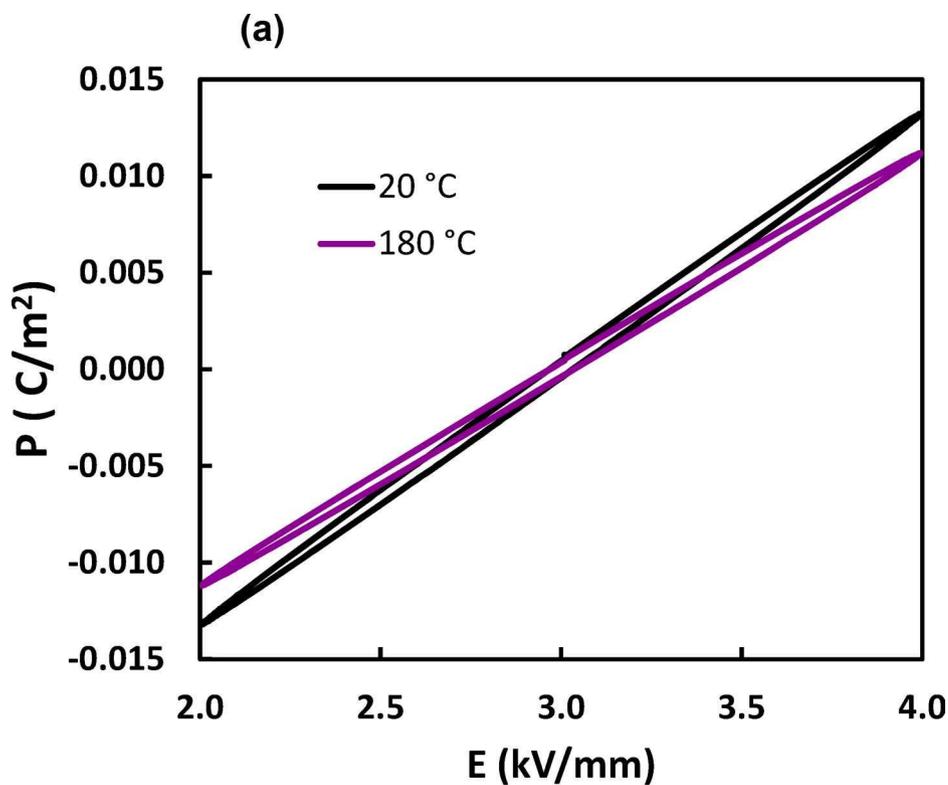
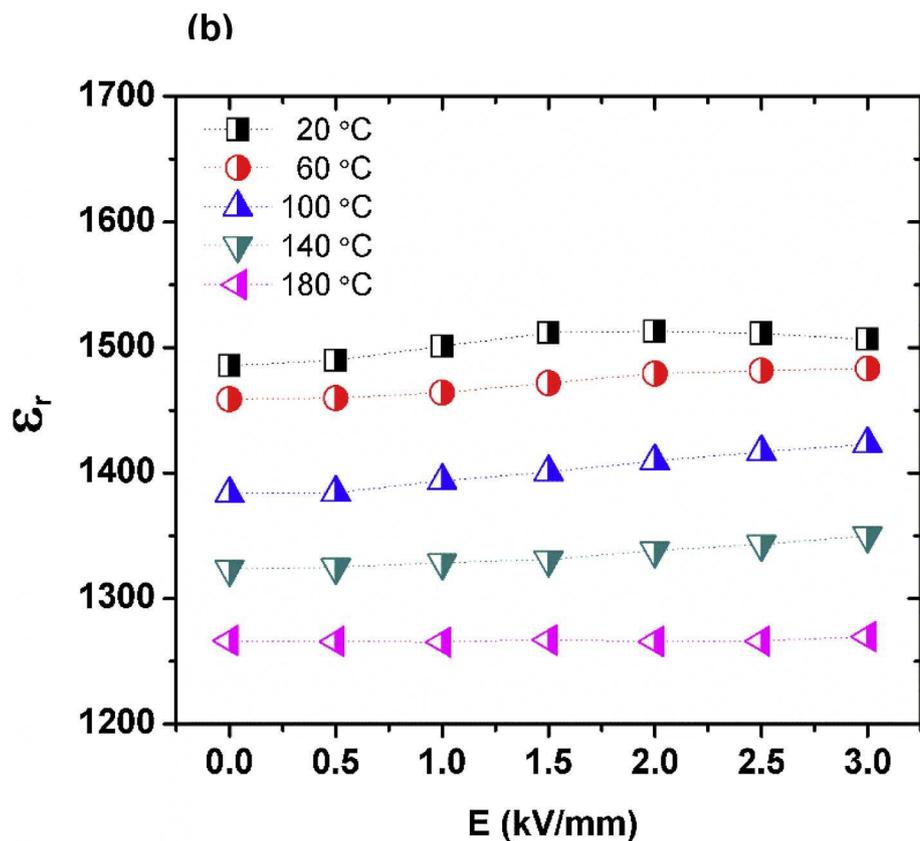


Fig. 6. (a) Examples of polarisation-electric field (P-E) loops used to obtain permittivity data at high fields; (b) variations in dielectric permittivity with increasing bias field for  $x = 0.3$ ,  $y = 0.2$ : electric field amplitude,  $E_0 = 1$  kV/mm, and frequency,  $f = 2$  Hz.



cubic by XRD, again showing evidence of a minor quantity of  $\text{NaNbO}_3$ , but with no other secondary peaks. However there was evidence from SEM-EDX of incomplete solid state reaction, in that grains of a Na- and Nb-rich phase were identified (Fig. 4). Image analysis of SEM-EDX maps indicated that this phase occupied  $\sim 10\%$  of the area. As a consequence, the matrix

will have a lower  $\text{NaNbO}_3$  content than that of the notional composition. It is reasonable to assume that this secondary phase may also have been present in the unmodified NBT-BCT-NN materials, which would support the assignment that the extra XRD peak at  $32.4^\circ 2\theta$  was due to  $\text{NaNbO}_3$  (Fig. 1).

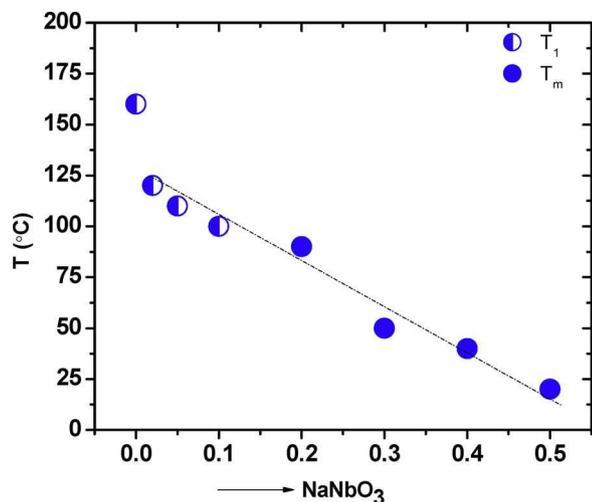


Fig. 7. Plot of  $T_1$  (for  $x < 0.2$ ) and  $T_m$  (for  $x \geq 0.2$ ) across the solid solution series  $(1-x)[0.85\text{Na}_0.5\text{Bi}_0.5\text{TiO}_3-0.15\text{Ba}_0.8\text{Ca}_0.2\text{TiO}_3]-x[\text{NaNbO}_3]$ . Estimated error in determining  $T_1$  or  $T_m$  is  $\pm 5^\circ\text{C}$  for compositions  $x = 0.02-0.5$ .

The  $\epsilon_r$ - $T$  plot for sample  $y = 0.2$  indicated  $\epsilon_{r\text{mid}}(150^\circ\text{C}) = 1300 \pm 15\%$  over the temperature range  $330^\circ\text{C}$  to  $-55^\circ\text{C}$  with low dielectric loss,  $\tan\delta < 0.025$ , from  $310^\circ\text{C}$  to  $0^\circ\text{C}$ , Fig. 5. Below  $0^\circ\text{C}$ ,  $\tan\delta$  progressively increased to 0.05 as the temperature fell to  $-55^\circ\text{C}$ . This combination of properties offers an improvement in temperature-stability relative to the NBT-BCT-NN series, indicating the benefit of Zr incorporation. A combination of wide temperature-stable range of  $\epsilon_r$ , encompassing the target  $-55^\circ\text{C}$  to  $300^\circ\text{C}$  span, reasonably high  $\epsilon_r$  values and low dielectric losses suggest that the  $x = 0.3$ ,  $y = 0.2$  composition is worthy of further development and testing as a high temperature capacitor material [3].

By way of property comparisons with related materials,  $\text{Na}_{0.5}\text{Bi}_{0.5}\text{TiO}_3\text{-BaTiO}_3\text{-NaTaO}_3$  achieves a relative permittivity of  $\sim 1500$  with good temperature-stability from  $-6^\circ\text{C}$  to  $312^\circ\text{C}$  (based on a  $\epsilon_{r\text{mid}}$  value at  $25^\circ\text{C}$ ) and  $\tan\delta = 0.31$  at  $25^\circ\text{C}$ ; the stability range is  $3^\circ\text{C}$  to  $284^\circ\text{C}$  for  $\epsilon_{r\text{mid}}$  of  $125^\circ\text{C}$  [30]. For NBT-NN ceramics, a temperature-stable range of  $\epsilon_r$  from  $-60^\circ\text{C}$  to  $400^\circ\text{C}$  is reported, but  $\tan\delta$  appeared to increase to 0.05 at  $\sim 200^\circ\text{C}$  and to  $> 0.1$  at  $\geq 250^\circ\text{C}$  (1 kHz); the loss values below room-temperature were not reported [18]. The system  $\text{Na}_{0.5}\text{Bi}_{0.5}\text{TiO}_3\text{-BaTiO}_3\text{-NaNbO}_3$  has also been studied and energy storage characteristics examined; the materials show an evolution in  $\epsilon_r$ - $T$  plots similar to that shown in Fig. 2 [17,19]. The  $\text{Na}_{0.5}\text{Bi}_{0.5}\text{TiO}_3\text{-Ba}_{0.85}\text{Ca}_{0.15}\text{Ti}_{0.9}\text{Zr}_{0.1}\text{O}_3$  system is reported to give stable  $\epsilon_r$  values from  $81^\circ\text{C}$  to  $330^\circ\text{C}$  [20]. Other reports of NBT based ‘high temperature’ dielectrics are reviewed in reference [3].

The mechanisms that suppress the dielectric peak in compositionally-complex relaxor ferroelectrics are uncertain. The lattice is expected to be composed of a variety of different  $\text{ABO}_3$  primary cell compositions, creating locally fluctuating electrostatic and strain fields where the length scales of fluctuations decrease with increases in concentration and multiplicity of substituents. It seems that this variability in nanostructure restricts correlated cation displacements to an extent that the normal rise in permittivity, which creates a strong dielectric peak in a typical relaxor ferroelectric, is suppressed. In the present work, the blocking effect of non-displaced Zr ions in  $\text{ZrO}_6$  octahedra is expected to further disrupt polar ordering in the Zr-modified material relative to NBT-BCT. The experimental results (Fig. 5) illustrate that this additional disruption to polar order is important in terms of targeting temperature-stable dielectric properties over the  $-55^\circ\text{C}$  to  $300^\circ\text{C}$  range. Furthermore, the NBT-BCT-NN materials are biphasic indicating only a proportion of the added NN is incorporated into the lattice. The role of displacements of  $\text{Bi}^{3+}$  ions in affecting the electrical properties of temperature stable relaxors is has yet to be established unequivocally

in this class of material. Mechanistic studies should include consideration of the role of cation and oxygen vacancy defects introduced during high temperature processing.

Because high temperature dielectric research programs are motivated by eventual use of the products as capacitor materials, which commonly take the form of thick films, a test of the stability in  $\epsilon_r$  values under high d.c. bias fields was conducted, yielding the results presented in Fig. 6. It was found that the permittivity values remained stable under high electric field levels, with the most significant reductions arising as a result of temperature variations, consistent with the low-field dielectric measurements reported in Fig. 5. A similar result was observed previously for BCT-BMT [40] suggesting resilience in  $\epsilon_r$  under d.c. bias is a valuable characteristic of temperature-stable relaxor ferroelectric ceramics.

The double temperature-dependent dielectric anomalies in NBT and NBT- $\text{BaTiO}_3$  ceramics are similar to those for NBT-BCT-NN:  $x < 0.2$ . Their origin has been the subject of much scientific debate in the literature relating to the two former compositions. The broad frequency-independent peak at  $T_2$  (Fig. 2) is often assigned to the true relaxor peak  $T_m$ , whilst the inflection at  $T_1$  has been suggested to relate to depolarisation linked to a non-ergodic to ergodic relaxor ferroelectric transition. Transmission electron microscopy indicates that nanoscale R3c and P4bm phases co-exist over a wide-temperature range [31]. Based on this finding, other authors have suggested that the two dielectric anomalies can be attributed to the thermal evolution of these two different types of polar nanoregion [25].

Although the primary motivation for this research was to investigate temperature-stability of  $\epsilon_r$  values as a function of composition in NBT-BCT-NN solid solutions, the observed experimental trends, together with an assessment of the data presented in previous reports, highlight the uncertainty over the origin of the double dielectric anomalies in NBT-based dielectrics. Fig. 7 shows how the inflection temperature,  $T_1$ , for samples with two dielectric anomalies ( $x < 0.02$ ), and  $T_m$ , for the normal relaxor ferroelectric compositions ( $x \geq 0.02$ ), change as a function of the increasing  $\text{NaNbO}_3$  content. A linear trend is observed, as reported for other relaxor ferroelectric solid solutions [7]. The linear correlation between  $T_1$  (for low  $\text{NaNbO}_3$  contents) and the unambiguously assigned  $T_m$  (for high  $\text{NaNbO}_3$  contents) supports the view that the frequency-dependent inflection observed at  $T_1$  represents the true relaxor ferroelectric peak. Further evidence that the inflection represents  $T_m$  lies in the position of the  $\tan\delta$  relaxation peak, which occurs at temperatures close to  $T_1$  (Fig. 2): the  $\tan\delta$  relaxation peak is expected to occur at  $T \sim T_m$  in a relaxor ferroelectric.

Very diffuse, non-frequency dependent peaks of the type presented in Fig. 2a-c for  $T_2$  can arise in a compositionally heterogeneous ferroelectric. However in NBT it appears that the gradation from an ergodic relaxor ferroelectric to a non-ergodic state occurs at or below the inflection temperature,  $T_1$ . Thus the  $T_2$  peak cannot be associated with a diffuse ferroelectric phase transition- unless it were to arise from a separate phase, for example due to compositional segregation. It may well be that the  $T_2$  peak somehow arises from evolution of two distinct polar nanoregions [25] and that by implication from Fig. 2 modification by  $\text{NaNbO}_3$  produces a monophasic polar nanostructure, but other factors are worthy of consideration. Given that partial loss of  $\text{Bi}_2\text{O}_3$  and  $\text{Na}_2\text{O}$  is very likely during high temperature ceramic processing there is the possibility that lattice defects (cation and oxygen vacancies) contribute to the unusual  $\epsilon_r$ - $T$  response of NBT-based ceramics.

It has been demonstrated that donor doping of NBT by Nb causes a diminution of the ‘ $T_2$ ’ peak, the extent of which depends on the level of Nb substitution [38,39]. Electrical conductivity in NBT originates from oxide ion conduction [38,39]. The effect of  $\text{Nb}^{5+}$  substitution for  $\text{Ti}^{4+}$  in NBT is to reduce the concentration of oxygen defects and reduce conductivity. The reasons for the similar dielectric and conductivity trends observed here for  $\text{NaNbO}_3$  modified NBT-BCT to those reported for donor doped NBT, for example suppression of the  $T_2$  dielectric peak and increase in resistivity, are not understood. The NBT-BCT-NN

ceramic products are not single phase which indicates they do not conform to the notional formula  $1-x(\text{Na}_{0.425}\text{Bi}_{0.425}\text{Ti}_{0.85}\text{Ba}_{0.12}\text{Ca}_{0.03}\text{Ti}_{0.15}\text{O}_3)-x(\text{NaNbO}_3)$ . The correlations in electrical properties to donor doping (Nb-NBT) may imply that the substitution of  $\text{Ti}^{4+}$  by  $\text{Nb}^{5+}$  occurs without sufficient complementary charge balance on A sites by the extra  $\text{Na}^+$  ions introduced from  $\text{NaNbO}_3$ . It has been reported there is a tendency for Na deficiency in NBT [41]. Moreover volatilisation losses are likely. Uncertainties over the Na (and Bi) contents may go some way to explaining the unexpected donor-like response of ceramics made from starting formulations containing extra  $\text{Na}_2\text{CO}_3$ , along with  $\text{Nb}_2\text{O}_5$ . As well as the possibility of differential volatilisation losses during prolonged high temperature sintering contributing to an apparent donor effect (from electrical property measurements), the thermodynamically stable solid solution formula may deviate from the assumed formula and therefore defect chemistry cannot be rationalised from the present set of results. Further work to identify if a single phase solid solution can be formed in the NBT-BCT-BCT 'ternary' system would help clarify this anomaly: even better dielectric properties may result from such an examination.

In terms of the double dielectric anomalies, short range displacements of oxygen ions, changes to octahedral tilt systems and/or defect pair association phenomena are all aspects that require further investigation given the likelihood of oxygen, bismuth and sodium ion vacancies being introduced during high temperature processing. Oxygen vacancies introduced in this manner are not susceptible to re-oxidation by oxygen-annealing in contrast to 'intrinsic' oxygen vacancies [32]. However donor doping by Nb can have a compensating effect as has already been proven for NBT. There is evidence in the perovskite ferroelectrics literature that oxygen vacancies and defect pairs involving oxygen vacancies give rise to dielectric peaks (usually with frequency-dependent relaxation) at temperatures in the range reported for the  $T_2$  peak in the NBT family [33–37]. Relatively little frequency-dependence in  $T_2$  was observed for NBT-BCT-NN ( $\sim 10^\circ\text{C}$  variation over the frequency range from 100 Hz to 1 MHz). A more notable dispersion was observed in weak  $\tan\delta$  anomalies at  $T \geq T_2$ . In the field of fluorite solid oxide electrolytes cation defect-oxygen ion vacancy pair formation is considered to be responsible for a break in slope of Arrhenius plots [42,43]. A cation vacancy–oxygen vacancy extrinsic defect pair in NBT-ceramics could in principle associate in a similar manner. It is noted that Arrhenius plots for NBT show a change in activation energy for oxide conduction at temperatures close to  $T_2$  [38,39]. Computational modelling has predicted the existence of  $(V_{\text{Bi}}^{\text{III}} - V_{\text{O}})$  associates and  $(\text{Mg}_{\text{Ti}}^{\text{II}} - V_{\text{O}})$  in Mg-modified NBT [44]. All of these observations confirm the many challenges faced in unravelling the complex structure-property relationships in the NBT family of dielectrics.

#### 4. Conclusions

A study of the dielectric properties of compositionally modified  $\text{Na}_{0.5}\text{Bi}_{0.5}\text{TiO}_3$  ceramics in the nominal solution system  $(1-x)[0.85\text{Na}_{0.5}\text{Bi}_{0.5}\text{TiO}_3-0.15\text{Ba}_{0.8}\text{Ca}_{0.2}\text{Ti}_{1-y}\text{Zr}_y\text{O}_3]-x\text{NaNbO}_3$  ( $0 \leq x \leq 0.8$ ,  $y = 0.2$ ) indicate that stable relative permittivity develops over a wide temperature range with increasing levels of lattice substitutions. For NBT-BCT-NN a temperature-stable relative permittivity  $\epsilon_r$  of  $1400 \pm 15\%$  was observed for temperatures between  $-50^\circ\text{C}$  and  $240^\circ\text{C}$  for the composition  $x = 0.3$ , but from a device point of view further substitution of  $\text{Ti}^{4+}$  by  $\text{Zr}^{4+}$  led to even better performance, extending the range of temperature stability to  $-55^\circ\text{C}$  to  $330^\circ\text{C}$ , with  $\epsilon_r = 1300 \pm 15\%$ , accompanied by relatively low dielectric losses. This combination of properties achieves the Electronics Industries Alliance  $-55^\circ\text{C}$  lower temperature specification of a capacitor material, with moderately high relative permittivity and low dielectric loss, notably from  $0^\circ\text{C}$  to  $300^\circ\text{C}$ . Compositional trends in relative permittivity-temperature plots and d.c. resistivity values suggested that a dielectric inflection is representative of a normal relaxor peak,  $T_m$ ,

whilst the higher temperature peak is an independent feature. The role of cation-oxygen vacancies to the characteristic dielectric response of NBT-based ceramics is discussed.

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