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Lag and mixing during sediment transfer across the Tian Shan piedmont caused by climate-driven aggradation-incision cycles Supplementary files

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8 1 Introduction

Details of the sampling and analytical methods are listed in the supplementary file. Most of it is 9 a description of the 20 post-IR IRSL samples collected by the Caltech-CAGS field mission to the 10 Chinese Tian Shan in June and July 2013 and analysed in the UCLA luminescence laboratory. The 11 detailed method for cosmogenic nuclide analysis is in Section 3. Information about the samples is 12 listed in Section 4. Each sample location is described in Figures 3 to 26 with a wide view of the 13 outcrop and a close-up view of the deposits. The photos are embedded at high-resolution in the 14 pdf. The analytical results are illustrated with a sensitivity plot and a radial plot of single-grain 15 equivalent dose D_e values. The UCLA lab number is indicated in brackets after the field number. 16 The final Figure 27 shows the details of the cosmogenic profile samples collected by the 2012 CRPG 17 Nancy mission on terrace T18 of the Anjihai River. 18

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²⁰ 2 Method for luminescence dating

21 2.1 Sample preparation, instrumentation, and measurement protocol

²² K-feldspar grains of 175-200 μ m were isolated from the sedimentary samples under dim amber ²³ LED light conditions. Subsamples were wet-sieved, treated with 3% HCl, separated by density ²⁴ with lithium metatungstate ($\rho < 2.565 \text{ g/cm}^3$; Rhodes, 2015), and treated with 10% HF for 10 ²⁵ minutes to remove the outer layer from the grains.

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²⁷ Luminescence measurements were carried out using a TL-DA-20 Risø automated reader equipped ²⁸ with a single-grain IR laser (830 nm, at 90% of 150 mW) and a 90 Sr/ 90 Y beta source. Measurements ²⁹ of scatter in D_e values for Risø calibration quartz suggest that source inhomogeneity causes 11% ³⁰ overdispersion. Emissions were detected through a Schott BG3-BG39 filter combination. Samples ³¹ were mounted on aluminium single-grain discs with 100 holes.

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The U and Th concentrations were measured with inductively-coupled plasma mass spectrometry (ICP-MS), and the K concentration (Table 2) was measured using inductively-coupled plasma

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³⁵ optical emission spectrometry (ICP-OES). These values were used to calculate the total beta dose-³⁶ rate contribution using the conversion factors of Adamiec and Aitken (1998). A value of $12.5 \pm$ ³⁷ 0.12 wt. % K content was used in calculating the internal dose rate (Huntley and Baril, 1997). ³⁸ Sediment samples were collected within each sample hole for water content measurement, and cos-³⁹ mic dose-rates were estimated following Prescott and Hutton (1994).

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⁴¹ A post-IR IRSL single-grain protocol (Buylaert et al., 2009) was used to measure equivalent ⁴² dose (D_e) values. Individual grains were stimulated first at 50 °C for 3 s, and then at 225 °C for 3 ⁴³ s to measure the more stable post-IR IRSL signal. Preheating at 250 °C for 60 s was used before ⁴⁴ natural and regenerative measurements, as well as a stimulation with the IR diodes at 290 °C for ⁴⁵ 40 s at the end of each single-aliquot regenerative-dose (SAR) cycle Wintle and Murray (2006).

46 2.2 Fading correction

Faded and unfaded ages of the samples are listed in Table 2. The stimulation temperature of 225 $^{\circ}$ C 47 for the post-IR IRSL measurement was chosen to minimise athermal fading while maximizing the 48 solar-bleaching rate (Li and Li, 2011; Kars et al., 2014). Nevertheless, post-IR IRSL signals exhibit a 49 range of fading values (Buylaert et al., 2009). To assess the stability of the measured signal at room 50 temperature, we measured the sensitivity-corrected luminescence following a beta dose of 70.7 Gy, 51 a preheat of 250 °C for 60 s and a pause ranging from 3270 s to 1.02×10^6 s (Huntley and Lamothe, 52 2001). These measurements were performed for two aliquots each of samples J0654, J0656, J0658, 53 and J0661. It has been shown that single aliquot fading measurements for density-separated K-54 feldspar sediments correspond to the fading values derived from the brightest individual grains of 55 a population (Brown et al., 2015). 56

The measured g-values for these samples were 3.60 ± 0.69 , 4.63 ± 0.94 , 4.34 ± 0.70 , and 4.95 ± 0.75 , giving a weighted mean value of 4.32 ± 0.38 % signal loss per decade with a time constant of 3349 s (Aitken, 1985, Appendix F). These values are abnormally high for a post-IR IRSL protocol measured in the blue wavelength (e.g., Thomsen et al., 2008), but also notably uniform. We applied this fading correction to the young samples using the 'Luminescence' package within **R** (Kreutzer et al., 2012).

For some of the older samples, the equivalent dose was beyond the linear portion of the dose-63 response curve, rendering the q-value correction of Huntley and Lamothe (2001) inappropriate. 64 In these cases, we followed the approach developed by Lamothe et al. (2003). A single, unfaded 65 dose-response curve for each sample was constructed using the approach of Kars et al. (2008); 66 the dimensionless recombination center density (ρ' ; Huntley, 2006) was estimated from laboratory 67 fading measurements as $2.98 \pm 0.38 \times 10^{-7}$. The summed luminescence intensities of each single-68 grain disc were used for the measured dose-response curves. The unfaded curve was then faded to 69 its natural level using the same q-value used for the young samples (equation 6 of Lamothe et al., 70 2003) and the corrected equivalent dose was calculated by mapping the natural intensity to the 71 approximated natural dose-response curve. 72

For Type C samples, two routines were used to determine ages: the Minimum Age model with three variables (MAM-3, Galbraith et al., 1999) and the DIscrete Minimum Model (DMM, Fuchs and Lang, 2001; Rhodes, 2015). Both methods compare well with 1σ overlap in most cases (Figure 1).



Figure 1: Results obtained using the Discrete Minimum Model (DMM; as described within the text, assuming an overdispersion of 25%) are compared against the Minimum Age Model with 3 variables (MAM-3). Note correspondence over a wide range of equivalent dose values.

Table 1:	Post-IR	IRSL	protocol	used	for 1	uminescei	ice d	lating	in thi	s study	y. T	his sing	gle-al	iquot
regenera	tive cycle	is rep	eated for	the n	atura	al dose an	d all	subse	quent	laborat	tory	doses.		

\mathbf{Step}	Treatment	Description
1	Irradiation for t s	Natural dose (i.e., do nothing) for first cycle,
		laboratory dose for subsequent cycles
2	Heat to 250° C for 60 s	Preheat
3	IR laser stimulation at 50° C for 3 s per grain	IRSL
4	IR laser stimulation at 50° C for 3 s per grain	post-IR IRSL, Lx
5	Irradiation for t s	Test dose (same dose every cycle)
6	Heat to 250° C for 60 s	Preheat
7	IR laser stimulation at 50° C for 3 s per grain	Test dose IRSL
8	IR laser stimulation at 50° C for 3 s per grain	Test dose post-IR IRSL, Tx
9	IR diode stimulation at 290°C for 40 s	Hot bleach to empty all traps

he	ne distribution types are described in Section 4.1.2 of the main article.										
	${f Field}$	\mathbf{Lab}		\mathbf{Th}	\mathbf{U}	\mathbf{Depth}	Total dose	Equivalent	$\mathbf{Dist.}$	Faded	Unfaded
	\mathbf{code}	code	% K	(ppm)	(ppm)	(m)	rate (Gy/ka)	dose (Gy)	\mathbf{type}	age (ka)	age (ka)
	TS13_37	J0645	2.4 ± 0.1	$10.6{\pm}0.5$	$2.6 {\pm} 0.13$	0.75	$4.324{\pm}0.206$	$5.4{\pm}1.1$	С	1.2 ± 0.3	1.7 ± 0.4
	$TS13_36$	J0646	2.4 ± 0.1	$10.3{\pm}0.5$	$2.85 {\pm} 0.14$	3.0	$4.398{\pm}0.212$	$9.7 {\pm} 0.8$	В	$2.2{\pm}0.2$	$3.3 {\pm} 0.3$
	$TS13_45$	J0647	2.4 ± 0.1	$8.5 {\pm} 0.4$	$2.28{\pm}0.11$	0.50	$4.266{\pm}0.211$	22 ± 2.4	\mathbf{C}	$5.2 {\pm} 0.6$	$7.7 {\pm} 1.0$
	$TS13_86$	J0648	2.1 ± 0.1	$8.6{\pm}0.4$	$2.61{\pm}0.13$	3.0	$3.897{\pm}0.184$	22.1 ± 1.3	В	$5.7 {\pm} 0.4$	$8.4 {\pm} 0.7$
	$TS13_{-}11$	J0650	2.3 ± 0.1	$10{\pm}0.5$	$3.63{\pm}0.18$	3.0	$4.386{\pm}0.205$	39.4 ± 3.4	\mathbf{C}	$9.4{\pm}1.0$	$13.4{\pm}1.6$
	$TS13_06$	J0651	2.1 ± 0.1	$9{\pm}0.5$	$2.67{\pm}0.13$	1.32	$4.109 {\pm} 0.193$	41.6 ± 3.6	\mathbf{C}	$9{\pm}0.9$	15.1 ± 1.7
	$TS13_01$	J0652	2.2 ± 0.1	$9.8{\pm}0.5$	$2.67{\pm}0.13$	38.2	$3.904{\pm}0.191$	$276.3{\pm}16.0$	А	$70.8 {\pm} 5.6$	$116.8 {\pm} 8.1$
	$TS13_03$	J0653	2.4 ± 0.1	$9.6{\pm}0.5$	$2.65{\pm}0.13$	7.5	$4.242{\pm}0.210$	$51.4 {\pm} 6.1$	В	12.1 ± 1.6	$18.3 {\pm} 2.6$
	$TS13_12$	J0654	2.4 ± 0.1	$8.6 {\pm} 0.4$	$2.32{\pm}0.12$	15	$4.105 {\pm} 0.209$	$433.7 {\pm} 28.7$	В	$105.7 {\pm} 9.1$	181 ± 13.0
	$TS13_08$	J0655	2.2 ± 0.1	$10.1{\pm}0.5$	$2.73 {\pm} 0.14$	100	$3.956{\pm}0.194$	$124.8 {\pm} 17.5$	А	$31.3 {\pm} 1.7$	$48.9 {\pm} 3.6$
	$TS13_07$	J0656	2.6 ± 0.1	$8.7 {\pm} 0.4$	$2.29{\pm}0.11$	100	$4.324{\pm}0.228$	$518.3 {\pm} 59.9$	В	$119.9 {\pm} 15.4$	$193.4{\pm}28.0$
	$TS13_{10}$	J0657	2.3 ± 0.1	$4.8 {\pm} 0.2$	$1.37{\pm}0.07$	200	$3.479 {\pm} 0.191$	$846.7 {\pm} 83.2$	В	$243.4{\pm}27.8$	$396.5 {\pm} 36.7$
	$TS13_09$	J0658	2.5 ± 0.1	$7.6 {\pm} 0.4$	$1.92{\pm}0.10$	200	$3.995{\pm}0.213$	$923.6 {\pm} 55.7$	В	$231.2{\pm}19.2$	$316.9 {\pm} 24.3$
	$TS13_02$	J0659	2.5 ± 0.1	$8.4{\pm}0.4$	$2.11 {\pm} 0.11$	200	$4.160{\pm}0.219$	839.2 ± 134.9	В	201.8 ± 34.4	$286.1 {\pm} 40.9$
	$TS13_19$	J0661	2.4 ± 0.1	$11.1{\pm}0.6$	$4.05 {\pm} 0.20$	1.0	$4.346{\pm}0.197$	$10.7 {\pm} 0.8$	\mathbf{C}	$2.5 {\pm} 0.2$	$3.6{\pm}0.3$
	$TS13_{-}35$	J0662	1.7 ± 0.1	$7.5 {\pm} 0.4$	$1.91{\pm}0.10$	10	$2.177 {\pm} 0.094$	53 ± 8.0	А	24.3 ± 3.9	$37.4{\pm}6.4$
	$TS13_14$	J0663	2.3 ± 0.1	$10{\pm}0.5$	$2.53{\pm}0.13$	0.80	$4.246{\pm}0.202$	$5.3 {\pm} 0.7$	\mathbf{C}	$1.2{\pm}0.2$	$1.7{\pm}0.3$
	$TS13_34$	J0664	1.5 ± 0.1	$5.7 {\pm} 0.3$	$1.68{\pm}0.08$	4.0	$3.017 {\pm} 0.137$	$489.2 {\pm} 58.9$	В	162.2 ± 21.1	$236.1 {\pm} 26.3$
	$TS13_{-}32$	J0665	2.2 ± 0.1	$10.4{\pm}0.5$	$3.55{\pm}0.18$	10	$4.087 {\pm} 0.190$	$319.3{\pm}14.4$	В	$78.1 {\pm} 5.3$	111 ± 7.0
	$TS13_{-}30$	J0668	1.8 ± 0.1	$5.2 {\pm} 0.3$	$3.51{\pm}0.18$	4.0	$3.642{\pm}0.168$	$188 {\pm} 15.0$	В	$51.6 {\pm} 4.9$	$81.3 {\pm} 9.0$
	$TS13_3$	J0669	2.2 ± 0.1	$9.5 {\pm} 0.5$	$3.57 {\pm} 0.18$	5.0	$4.039 {\pm} 0.187$	578.7 ± 62.1	В	$143.3{\pm}17.0$	$198.1 {\pm} 20.5$

Table 2: Detailed results of post-IR IRSL luminescence dating. 'Depth' indicates the position of the sample below the surface. The unfaded age is the final calculated age for each sample. The river acronyms are KTN (Kuitun), AJH (Anjihai), and MNS (Manas). The distribution types are described in Section 4.1.2 of the main article.

77 **3** Method for cosmogenic profile

78 3.1 Methods and parameters

Details of the sampling location and analytical results of sample TS12_ANJ_T1B are presented in
Figure 27. We infer the age of surface abandonment from the depth distribution of cosmogenic
isotope concentration (Dunai, 2010; Gosse and Phillips, 2001). To better account for the potential
deposit of loess and/or soil after terrace abandonment, we followed the approach of Braucher et al.
(2000) and Guralnik et al. (2011) and modified the general formulation of Lal (1991) as follow:

$$C(z,B) = -\overline{C_0} e^{\lambda x/B} + \sum_{i=n,m_1,m_2} \frac{P_i}{\frac{\rho B}{\Delta_i} + \lambda} e^{-\rho z/\Delta_i} \left(1 - e^{\frac{\lambda}{B} + \frac{\rho}{\Delta_i} z}\right)$$
(1)

Where B is a 'negative' denudation rate (Braucher et al., 2000) which represents the accumu-84 lation rate or burial rate since terrace abandon: t represents the time since initial exposure of the 85 surface (in this case, the abandonment of the terrace surface); C_0 is the average cosmogenic inher-86 itance (in atoms/g); λ is the decay constant of ¹⁰Be equal to $\ln(2)/T_{1/2}$ where $T_{1/2}$ is the half-life 87 of 1.387 Ma (Chmeleff et al., 2010; Korschinek et al., 2010); n, m_1 , and m_2 refer to the neutrons, 88 fast muons and slow muons, respectively; Δ is the respective attenuation length of neutrons, slow 89 muons and fast muons (~160, ~1500, ~4320 g/cm² respectively) from Braucher et al. (2011); P 90 is the respective local production rates (at g^{-1} yr⁻¹) for the neutrons, slow muons and fast muons; 91 and ρ is the soil density (g/cm³). This new formulation assumes that the few tens of centimeters 92 of loess covering the terraces accumulated at a constant rate since the terraces abandonment. The 93 exposure time of each sample is therefore dependent of its depth (t = z/B). 94

The local 10 Be production rates, P, for neutrons, fast muons and slow muons were scaled for 95 local latitude and altitude according to Stone (2000) and the local atmospheric pressures were 96 extracted from the ERA40 dataset (Uppala et al., 2005). In this study, we used the SLHL (see level 97 high latitude) production rate of 3.9 ± 0.1 at g^{-1} yr⁻¹ that was compiled by Balco et al. (2009) and 98 revised by Braucher et al. (2011) to include the slow and fast muons contribution. The slow and 99 fast muonic production rates (0.01 and 0.034 at g^{-1} yr⁻¹ respectively) were derived from Braucher 100 et al. (2011). Alluvium density was estimated by analyzing pictures of the outcrop in order to 101 determine first the relative proportions of grains larger than medium gravel ($\emptyset > 1-2$ cm) and of 102 sand-sized to medium gravel-sized grains. Bulk density was calculated by attributing densities of 103 2.7 ± 0.1 g/cm³ to coarser grains and 1.9 ± 0.1 g/cm³ to finer grains (Hancock et al., 1999). 104

105 3.2 Sample treatment

Quartz separation and isolation of pure beryllium oxide (BeO) was performed at CRPG (Nancy, 106 France). Samples were first crushed and sieved. The 200-800 μ m fraction was then processed 107 by magnetic separation and the non-magnetic fraction was dissolved in a mixture of H_2SiF_6 and 108 HCl. Quartz was then purified in three successive HF baths to remove atmospheric ¹⁰Be from 109 the quartz surfaces (Brown et al., 1991; Kohl and Nishiizumi, 1992). Next, the purified quartz 110 was completely dissolved in HF after addition of 200 μ l of an in-house 2.020 10⁻³ g/g ⁹Be carrier 111 solution. Purified BeO samples were obtained after subsequent purification by anion exchange, 112 cation exchange and alkaline precipitation. The ¹⁰Be/⁹Be ratios of the BeO samples were measured 113 at the ASTER (Accelerator for Earth Sciences, Environment and Risks) national AMS (Accelerator 114 Mass Spectrometer) facility, located at CEREGE in Aix en Provence, France. These concentrations 115

Sample	\mathbf{Depth}	Sampling	Pure Qz	10 Be/ 9 Be	$^{10}\mathbf{Be}$	$[^{10}\mathbf{Be}]$	error
name	(m)	${ m thickness}$	\mathbf{weight}	10^{-14}	counts	10^4	10^4
		(cm)	(\mathbf{g})			(at/g)	(at/g)
TS12_ANJ_T1B_P0a	0	5	10	3.7	476	9.59	0.5
TS12_ANJ_T1B_P0d	0	5	9.7	3.8	381	10.11	0.61
TS12_ANJ_T1B_P0e	0	5	25	8.9	1145	9.58	0.33
TS12_ANJ_T1B_P1	-0.3	5	4.2	2.5	248	14.84	1.09
TS12_ANJ_T1B_P2	-0.75	5	2.6	1.3	155	12.29	1.27
TS12_ANJ_T1B_P3	-1.1	5	5.9	2.5	204	10.77	0.85
TS12_ANJ_T1B_P4	-2.5	5	2.2	1.1	113	11.42	1.43

Table 3: Sample data set and cosmogenic results

are normalized to the ${}^{10}\text{Be}/{}^{9}\text{Be}$ SRM 4325 NIST reference material using an assigned value of 2.79 ± 0.03 · 10⁻¹¹ (Nishiizumi et al., 2007). This standardization is equivalent to 07KNSTD within rounding error. The mean ${}^{10}\text{Be}/{}^{9}\text{Be}$ ratio of 22 chemical blank samples is $1.7 \pm 0.7 \cdot 10^{-15}$. Blank corrections represent between 0.1% and 8% of the samples (average of 1.6%).

¹²⁰ 4 Sample locations and results

Grain size was surveyed at eight locations along the Kuitun River (Figure 2). The intermediate axes of >100 grains was surveyed on the surface of alluvial bars next to the active river channel in six locations along the Kuitun River (sampling sites I-VI) and on the dry bed of the small tributary Swallows' Canyon (sampling sites VII and VIII). The location of the sampling sites can be found in Figures 4 and 7 of the main article. Picking was done in an area of roughly 20 by 20 meters where the surveyors would walk at random and, at each step, pick the the sediment grain that their finger would first hit when reaching for the ground without looking (Wolman, 1954).



Figure 2: Grain size survey of the Kuitun River. Top: along stream evolution of the grain sizes on active banks of the Kuitun River. Bottom: cumulative fractions of grain sizes for each survey. See Figures 4 and 7 of the main article for location.



Figure 3: Location and details of sample **TS13_37** (**J0645**) = 1.7 ± 0.4 ka; Kuitun; abandonment. Sample taken in 0.8 m of fluvially reworked clayey fine sand to silt with few granules. The sample was collected 5 cm above the fluvial fill. The fluvial fill is 3.2 m thick and lies on a bedrock strath of T2. On 3.7.2013, the strath was 1.6 m above the water level. The general approach for analysis is to reject grains based on sensitivity and high outliers. The overdispersion is 0.54.



Figure 4: Location and details of sample $TS13_36$ (J0646) = 3.3 ± 0.3 ka; Kuitun; abandonment. Sample taken in the silt of a fluvially reworked 3.2 m thick series of loess and cross-bedded medium grained sand 20 cm above the top of the alluvial cobble conglomerate. The alluvial cobble conglomerate lies on the terrace strath and the sample constrains abandonment age. The general approach for analysis is to reject grains based on sensitivity. The overdispersion is 0.2.



Figure 5: Location and details of sample $TS13_45$ (J0647) = 7.7 ± 1.0 ka; Kuitun; abandonment. Sample taken in the middle of the 0.3 m thick silt horizon capping the 1.5 m thick cobble conglomerate that lies on the strath of T7. The silt horizon is covered by a layer of creeping colluvium. It was not possible to dissociate the colluvium from the capping silt unequivocally. But it is very likely that the silt constrains the abandonment age of terrace T7.



Figure 6: Location and details of sample $TS13_86 (J0648) = 8.4 \pm 0.7 \text{ ka}$; Kuitun; abandonment. The sample was taken in a silt horizon 20 cm above the fluvial deposit of the terrace and below a colluvium wedge. Although it appears from the pictures that the overlying coarse deposit might be fluvial and not colluvial. The sample would then reflect an aggradation age, not an abandonment.



Figure 7: Location and details of sample $TS13_1$ (J0650) = 13.4 ± 1.6 ka; Kuitun; abandonment. Sample taken in a silt lens at the base of the colluvium wedge covering the alluvial cover of the terrace T9. It constrains the abandonment of T9 and it is a repeat of sample KTN-09 (10±2 ka) of Poisson and Avouac (2004).



Figure 8: Location and details of sample $TS13_01 (J0652) = 116.8 \pm 8.1$ ka; Kuitun; aggradation. Sample is collected at the base of the conglomerate cliff cut after abandonment of terrace T2. Material is a thick silt lens of reworked loess and very fine sand. The sample constrains a phase of aggradation of the alluvial fan. The overdispersion is 0.50.



Figure 9: Location and details of sample $TS13_03 (J0653) = 18.3 \pm 2.6$ ka; Kuitun; aggradation. Sample is collected in the riser of T3 at the downstream end of the Kuitun. Material is taken from a thin lens of silt. The sample constrains a phase of aggradation of the alluvial fan. The overdispersion is 0.33.



Figure 10: Picture looking East and down in the Swallow Canyon. The Kuitun Canyon, flowing from right to left, is visible in the background.



Figure 11: Schematic profile of the tributary Swallow Canyon and location of the samples TS13_12 (J0654), TS13_08 (J0655), TS13_07 (J0656), TS13_10 (J0657), TS13_09 (J0658). The shading represents a possible stratigraphy.



Figure 12: Location and details of sample $TS13_12$ (J0654) = 181.0 ± 13.0 ka; Kuitun; aggradation. Sample taken in a 10-15 cm thick lens of reworked silt to medium sand 201 m above the river. The sample constrains a phase of aggradation of the alluvial fan. The overdispersion is 0.25.



Figure 13: Location and details of sample $TS13_08$ (J0655) = 48.9 ± 3.6 ka; Kuitun; aggradation. Sample taken in a thin lens of reworked silt 127 m above the river. The sample constrains a phase of aggradation of the alluvial fan. The overdispersion is 0.42.



Figure 14: Location and details of sample $TS13_07 (J0656) = 193.4 \pm 28.0$ ka; Kuitun; aggradation. Sample taken in a lens of reworked silt to fine sand 109 m above the river. The sample constrains a phase of aggradation of the alluvial fan. The overdispersion is 0.28.



Figure 15: Location and details of sample $TS13_10 (J0657) = 396.5 \pm 36.7$ ka; Kuitun; aggradation. Sample taken in a 10-15 cm thick lens of reworked silt to fine sand 74 m above the river. The sample constrains a phase of aggradation of the alluvial fan. The overdispersion is 0.22.



Figure 16: Location and details of sample $TS13_09 (J0658) = 316.9 \pm 24.3 \text{ ka}$; Kuitun; aggradation. Sample taken in a thin lens of reworked silt to medium sand 21 m above the river. The sample constrains a phase of aggradation of the alluvial fan. The overdispersion is 0.25.



Figure 17: Location and details of sample $TS13_02 (J0659) = 286.1 \pm 40.9 \text{ ka}$; Kuitun; aggradation. Sample is collected at the base of the Kuitun main conglomerate cliff that is cut by Holocene incision, >250 m below the alluvial fan surface. Material is taken from a 1-1.5m thick loess horizon. The overdispersion is 0.46.



Figure 18: Location and details of sample $TS13_19$ (J0661) = 3.6 ± 0.3 ka; Anjihai; abandonment. Sample taken in a fine sand bed capping the fluvial deposits of terrace T13. The sample should constrain the abandonment of T13.



Figure 19: Location and details of sample $TS13_14$ (J0663) = 1.7 ± 0.3 ka; Anjihai; sample taken in a lens of reworked silt to fine sand at 0.8 m depth in the alluvial fill under terrace T2. The sample will provide an age constrain on the Anjihai alluvial fan aggradation.



Figure 20: Location and details of sample TS13_35 (J0662) = 37.4 ± 6.4 ka; Toudao; abandonment. Sample taken in a silt horizon at the base of a ca. 10 m thick colluvial wedge, 5-10 cm above the top of the cobble conglomerate fill that defines the main terrace of the Toudao River. Sampling was done in a side wash cutting through the terrace. From this sample, we expect an abandonment constraint for the main terrace. The overdispersion is 0.



Figure 21: Stratigraphic relationship between **TS13_32 (J0665)** and **TS13_34 (J0664)**; Toudao; the samples are collected from silt lenses in an alluvial conglomerate that lies unconformable on Jurassic sandstone and is capped by colluvium.



Figure 22: Location and details of sample **TS13_34** (**J0664**) = **236.1** \pm **26.3** ka; Toudao; Sample collected above the Toudao River in a narrow silty sand lens less than 10 cm thick, with granules and then pebbles and cobbles conglomerates above and below. The sample lies 2-3 m above the bedrock and 3-4 m below sample TS13_32, the two constrain the age of the fluvial deposit on the strath. See Figure 21 for a sketch of the stratigraphic relationship with TS13_32 (J0665). The overdispersion is 0.



Figure 23: Location and details of sample $TS13_32$ (J0665) = 111.0 ± 7.0 ka; Toudao; abandonment. Sample taken in the first reworked silt lens above the massive fluvial cobble conglomerate and below a few thinner pebble conglomerate horizons. It represents the very last phase of aggradation that postdates the deposition of the main fill (cobble conglomerate) of this high terrace. The sample lies 3-4 m above TS13_34. See Figure 21 for a sketch of the stratigraphic relationship with TS13_34 (J0664). The overdispersion is 0.03.



Figure 24: Stratigraphic relationship between **TS13_30 (J0668)** and **TS13_33 (J0669)**. The samples are collected from silt lenses in a thick alluvial conglomerate that lies unconformable on Jurassic sandstone and is capped by colluvium.



Figure 25: Location and details of sample $TS13_30$ (J0668) = 81.3 ± 9.0 ka; Manas; abandonment. The sample is in front of Jiawei Pan in the left picture. The sample was collected in the clay to fine sand capping the fluvial cobble-pebble deposits of the main strath terrace in the Upper Manas). This bed is covered by angular to subangular cobble-pebble colluvium and soil. The sample should constrain the age of the Upper Manas strath terrace. See Figure 24 for a sketch of the stratigraphic relationship with TS13_33 (J0669). The overdispersion is 0.05.



Figure 26: Location and details of sample $TS13_33$ (J0669) = 198.1 ± 20.5 ka. Sample taken in a very small clayey silt in the boulder conglomerate of the main strath terrace of the Upper Manas. The sample lies 2.5 m above the strath. It is a good constraint on the creation of the strath (assuming that the boulder conglomerate present today is the original cover of the strath). See Figure 24 for a sketch of the stratigraphic relationship with TS13_30 (J0668). The overdispersion is 0.24.



Figure 27: Left: sampling site for the depth profile analysis of sample $TS12_ANJ_T1B = 5.1 \pm 1.7$ ka. Right: ¹⁰Be cosmogenic concentrations as a function of depth. The red line show the best fit model. Fine sediments (silt, loess, soil) are assumed to have a bulk density of 1.6 ± 0.2 g/cm³. The measured depths are converted to theoretical depths with the respective densities (blue ellipses).

Table 4: Supplementary Table Compilation of all published ages dating surfaces of the north alluvial piedmont of the Eastern Tian Shan. The map no. column lists the numbering used in the maps ("e" for external source). The relative height^{*} is the elevation of the sample above the river divided by the height of the fill terrace marking the incision onset. Easting and Northing are referenced in the UTM zone 45 T. The River acronyms are ANJ (Anjihai), ANJw (Anjihai windgap), HTB (Hutubi), JNG (Jingou), KTN (Kuitun), MNS (Manas), TDO (Toudao), TSH (Tashi), and URQ (Urumqi). The sources are 1: this study; 2: Poisson and Avouac (2004); 3: Poisson (2002); 4: Gong et al. (2014); 5: Lu et al. (2014);6: Lu et al. (2010); 7: Stockmeyer, in review; 8: Fu et al. (2017). * Combination of the surface F_2 samples following Lu et al. (2010, p. 348). [†] These samples are not included in Figures 13 and 14 because they only border a small ephemeral stream that crosses the windgap after it was abandonment by the Anjihai River. The coordinates for Fu et al. (2017) listed here are the mean positions of the samples that contribute to each age.

River	Map	Sample	Age	Height*	Lat.	Lon.	Method	
	code	no.	(ka)		(°N)	(°E)		
KTN	01	$TS13_01^1$	116.8 ± 8.1	0.10	44.3260	84.7793	p-IR IRSL	
KTN	02	$TS13_02^1$	286.1 ± 40.9	0.05	44.1408	84.7354	p-IR IRSL	
KTN	03	$TS13_03^1$	18.3 ± 2.6	0.67	44.3685	84.7927	p-IR IRSL	
KTN	07	$TS13_07^1$	$193.4{\pm}28.0$	0.44	44.2146	84.7740	p-IR IRSL	
KTN	08	$TS13_08^1$	48.9 ± 3.6	0.52	44.2150	84.7729	p-IR IRSL	
KTN	09	$TS13_09^1$	316.9 ± 24.3	0.09	44.2154	84.7806	p-IR IRSL	
KTN	10	$TS13_{-}10^{1}$	396.5 ± 36.7	0.30	44.2143	84.7771	p-IR IRSL	
KTN	11	$TS13_{-}11^{1}$	$13.4{\pm}1.6$	1.00	44.2123	84.7672	p-IR IRSL	
KTN	12	$TS13_{-}12^{1}$	$181{\pm}13.0$	0.82	44.2121	84.7669	p-IR IRSL	
ANJ	14	$TS13_{-}14^{1}$	1.7 ± 0.3	0.16	44.1008	85.0983	p-IR IRSL	
ANJ	19	$TS13_{-}19^{1}$	3.6 ± 0.3	0.88	44.0929	85.0986	p-IR IRSL	
MNS	30	$TS13_{-}30^{1}$	81.3 ± 9.0	0.95	43.8489	85.8011	p-IR IRSL	
TDO	32	$TS13_32^1$	111 ± 7.0	1.00	43.9734	85.1261	p-IR IRSL	
MNS	33	$TS13_3^1$	$198.1{\pm}20.5$	0.80	43.8489	85.8013	p-IR IRSL	
TDO	34	$TS13_34^1$	236.1 ± 26.3	1.00	43.9738	85.1255	p-IR IRSL	
TDO	35	$TS13_35^1$	37.4 ± 6.4	1.00	43.9794	85.1071	p-IR IRSL	
KTN	36	$TS13_{-}36^{1}$	3.3 ± 0.3	0.32	44.2919	84.7873	p-IR IRSL	
KTN	37	$TS13_37^1$	1.7 ± 0.4	0.02	44.2962	84.7885	p-IR IRSL	
KTN	45	$TS13_{-}45^{1}$	7.7 ± 1.0	0.76	44.2885	84.7819	p-IR IRSL	
KTN	86	$TS13_{-}86^{1}$	$8.4{\pm}0.7$	0.65	44.2900	84.7900	p-IR IRSL	
ANJ	1B	$TS12$ - ANJ - $T1B^1$	5.1 ± 1.7	1.00	44.1052	85.0973	TCN	
KTN	e1	$OSL-T2-1^2$	10 ± 1	0.92	44.2142	84.7725	OSL	
KTN	e2	$OSL-T2-2^2$	10.8 ± 2	0.92	44.2142	84.7725	OSL	
KTN	e3	$OSL-T4-1^2$	7.3 ± 1	0.65	44.3242	84.7728	OSL	
KTN	e4	$OSL-T4-2^2$	6.8 ± 0.5	0.65	44.3223	84.7735	OSL	
KTN	e5	$OSL-T4-3^2$	7.5 ± 1	0.65	44.3222	84.7738	OSL	
KTN	e6	$C-T5-1^{2}$	3.3 ± 0.1	0.32	44.3213	84.7789	^{14}C	
KTN	e7	$C-T5-2^{2}$	3.4 ± 0.2	0.32	44.2997	84.7811	¹⁴ C	
KTN	e8	KTN_01^3	35 ± 10	1.00	44.2713	84.7625	OSL	

e9	$ $ KTN_02 ³	86 ± 10	1.00	44.2894	84.7600	OSL
e10	T-6-loess-bottom ⁴	19.9 ± 1.5	1.00	44.1786	86.1401	p-IR IRSL
e11	T-5-loess-bottom ⁴	12.4 ± 0.8	0.83	44.1284	86.1064	p-IR IRSL
e12	T-4-loess-bottom ⁴	4 ± 0.4	0.58	44.1659	86.1172	p-IR IRSL
e13	T-3-loess-bottom ⁴	3.1 ± 0.3	0.44	44.1673	86.1155	p-IR IRSL
e14	T-2-loess-bottom ⁴	1.4 ± 0.3	0.22	44.1677	86.1139	p-IR IRSL
e15	$T-1-loess-bottom^4$	0.5 ± 0.1	0.11	44.1685	86.1114	p-IR IRSL
e16	$4 (T7)^5$	255 - 25/+15	1.00	43.4043	87.2149	OSL
e17	$2 (T5)^5$	142 ± 14	1.00	43.4867	87.3060	OSL
e18	$1 (T2)^5$	3.52 ± 0.04	0.73	43.5314	87.3304	$^{14}\mathrm{C}$
o10	$9.2.4.5(F_{1}(T_{1}))^{6*}$	205 +25	1.00			FCD
020	$1 (T_{2}(F_{2}))^{6}$	230 ± 20 1 8 ± 0.2	0.16	44 1576	86 3/16	OSI
021	$(I_3(I_3))$ 1 $(T_2(F_2))^6$	1.0 ± 0.2 26 ± 2.7	0.10	44.1570	86 3360	OSL
022	(13(13)) $(22(T_2(F_2))^6$	20 ± 2.7 28 7 ± 3	0.10	44.0122	85 4513	OSL
622 623	$3h (T_3(T_3))$	126 ± 13	0.80	44.1014	85 4513	OSL
025	55 (13(13))	12.0 ±1.0	0.31	44.1014	00.4010	
e24	$TGL-T4^7$	19.6 + 14.5 / -8.3	1.00	44.0649	86.3351	p-IR IRSL
e25	$TGL-T3^7$	42.8 + 18.2 - 12.7	1.00	44.0709	86.3280	p-IR IRSL
e26	$TGL-T2^7$	75.2 +31.7/-17.6	1.00	44.0647	86.3280	p-IR IRSL
e27	$TGL-T1^7$	188.8 + 62.8 / -47.1	1.00	44.0673	86.3138	p-IR IRSL
e28	$TGL-T0^7$	245.6 + 72.3 / -55.9	1.00	44.0686	86.3094	p-IR IRSL
e29	AJH-02-04 ^{8†}	3.6 ± 0.1	1.00	~ 44.27	~ 85.17	OSL & p-IR IRSL
e30	AJH-06.07.08 ^{8†}	9.0 ± 0.6	1.00	~ 44.27	$\sim\!85.18$	OSL & p-IR IRSL
e31	AJH-08,09,11,12 ⁸	53.3 ± 2.2	1.00	~ 44.26	$\sim\!85.19$	OSL & p-IR IRSL
	$\begin{array}{c} e9\\ e10\\ e11\\ e12\\ e13\\ e14\\ e15\\ e16\\ e17\\ e18\\ e19\\ e20\\ e21\\ e22\\ e23\\ e24\\ e25\\ e26\\ e27\\ e28\\ e29\\ e30\\ e31\\ \end{array}$	e9KTN_02^3e10T-6-loess-bottom ⁴ e11T-5-loess-bottom ⁴ e12T-4-loess-bottom ⁴ e13T-3-loess-bottom ⁴ e14T-2-loess-bottom ⁴ e15T-1-loess-bottom ⁴ e164 (T7) ⁵ e172 (T5) ⁵ e181 (T2) ⁵ e192-3-4-5 $(F_2(T_2))^{6*}$ e201 $(T_3(F_3))^6$ e211 $(T_3(F_3))^6$ e233b $(T_3(F_3))^6$ e24TGL-T4 ⁷ e25TGL-T3 ⁷ e26TGL-T1 ⁷ e28TGL-T0 ⁷ e29AJH-02-04 ^{8†} e30AJH-06,07,08 ^{8†} e31AJH-08,09,11,12 ⁸	e9KTN_02^386 ±10e10T-6-loess-bottom ⁴ 19.9 ±1.5e11T-5-loess-bottom ⁴ 12.4 ±0.8e12T-4-loess-bottom ⁴ 4 ±0.4e13T-3-loess-bottom ⁴ 3.1 ± 0.3 e14T-2-loess-bottom ⁴ 1.4 ± 0.3 e15T-1-loess-bottom ⁴ 0.5 ± 0.1 e164 (T7) ⁵ $255 \cdot 25/+15$ e172 (T5) ⁵ 142 ± 14 e181 (T2) ⁵ 255 ± 25 e201 (T_3(F_3))^6 26 ± 2.7 e211 (T_3(F_3))^6 26 ± 2.7 e23 $3b (T_3(F_3))^6$ 28.7 ± 3 e23 $3b (T_3(F_3))^6$ 12.6 ± 1.3 e24TGL-T4 ⁷ $19.6 + 14.5/-8.3$ e25TGL-T3 ⁷ $42.8 + 18.2 \cdot 12.7$ e26TGL-T0 ⁷ $245.6 + 72.3/-55.9$ e29AJH-02-04 ^{8†} 3.6 ± 0.1 e30AJH-06,07,08 ^{8†} 9.0 ± 0.6 e31AJH-08,09,11,12 ⁸ 53.3 ± 2.2	e9KTN_02386 ±101.00e10T-6-loess-bottom419.9 ±1.51.00e11T-5-loess-bottom412.4 ±0.80.83e12T-4-loess-bottom44 ±0.40.58e13T-3-loess-bottom43.1 ±0.30.44e14T-2-loess-bottom41.4 ±0.30.22e15T-1-loess-bottom40.5 ±0.10.11e164 (T7) ⁵ 255 -25/+151.00e172 (T5) ⁵ 142 ±141.00e181 (T2) ⁵ 3.52 ±0.040.73e192-3-4-5 (F ₂ (T ₂)) ^{6*} 295 ±251.00e201 (T ₃ (F ₃)) ⁶ 26 ±2.70.16e211 (T ₃ (F ₃)) ⁶ 28.7 ±30.80e233b (T ₃ (F ₃)) ⁶ 12.6 ±1.30.97e24TGL-T4 ⁷ 19.6 +14.5/-8.31.00e25TGL-T3 ⁷ 42.8 +18.2-12.71.00e26TGL-T0 ⁷ 188.8 +62.8/-47.11.00e27TGL-T1 ⁷ 188.8 +62.8/-47.11.00e28TGL-T0 ⁷ 245.6 +72.3/-55.91.00e29AJH-02-04 ^{8†} 3.6±0.11.00e30AJH-06,07,08 ^{8†} 9.0±0.61.00e31AJH-08,09,11,12 ⁸ 53.3±2.21.00	e9KTN_02 ³ 86 ±101.0044.2894e10T-6-loess-bottom ⁴ 19.9 ±1.51.0044.1786e11T-5-loess-bottom ⁴ 12.4 ±0.80.8344.1284e12T-4-loess-bottom ⁴ 4 ±0.40.5844.1659e13T-3-loess-bottom ⁴ 3.1 ±0.30.4444.1673e14T-2-loess-bottom ⁴ 1.4 ±0.30.2244.1677e15T-1-loess-bottom ⁴ 0.5 ±0.10.1143.4043e172 (T5) ⁵ 142 ±141.0043.4067e181 (T2) ⁵ 3.52 ±0.040.7343.5314e192-3-4-5 (F ₂ (T ₂)) ^{6*} 295 ±251.00e201 (T ₃ (F ₃)) ⁶ 26 ±2.70.1644.1576e111 (T ₃ (F ₃)) ⁶ 28.7 ±30.8044.1814e233b (T ₃ (F ₃)) ⁶ 28.7 ±30.9744.1814e24TGL-T4 ⁷ 19.6 +14.5/-8.31.0044.0649e25TGL-T3 ⁷ 42.8 +18.2-12.71.0044.0673e28TGL-T0 ⁷ 245.6 +72.3/-55.91.0044.0673e28AJH-02-04 ^{8†} 3.6±0.11.00~44.27e30AJH-06,07,08 ^{8†} 9.0±0.61.00~44.27e31AJH-08,09,11,12 ⁸ 53.3±2.21.00~44.26	e9KTN.02386 ±101.0044.289484.7600e10T-6-loess-bottom419.9 ±1.51.0044.178686.1401e11T-5-loess-bottom412.4 ±0.80.8344.128486.1064e12T-4-loess-bottom412.4 ±0.30.5844.165986.1172e13T-3-loess-bottom43.1 ±0.30.4444.167386.1155e14T-2-loess-bottom41.4 ±0.30.2244.167786.1139e15T-1-loess-bottom40.5 ±0.10.1144.168586.1114e164 (T7) ⁵ 255 -25/+151.0043.404387.2149e172 (T5) ⁵ 142 ±141.0043.486787.3060e181 (T2) ⁵ 3.52 ±0.040.7343.531487.3304e192-3-4-5 (F ₂ (T ₂)) ^{6*} 295 ±251.00e201 (T ₃ (F ₃)) ⁶ 28.7 ±30.8044.181485.4513e233b (T ₃ (F ₃)) ⁶ 28.7 ±30.9744.181485.4513e24TGL-T4 ⁷ 19.6 +14.5/-8.31.0044.064986.3351e25TGL-T1 ⁷ 18.8.8 +62.8/-47.11.0044.064786.3280e26TGL-T0 ⁷ 245.6 +72.3/-55.91.00e28TGL-T0 ⁷ 245.6 +72.3/-55.91.0044.064786.3138e28AJH-02.04 ^{8†} 3.6±0.11.00~44.27~85.18e31AJH-08,09,11,12 ⁸ 3.6±0.11.00~44.26~85.19

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