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Real World SI Vehicle Emissions in Low Speed Congested Traffic

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5th International Exhaust Emissions Symposium 2016, 19-20 May, 2016, BOSMAL, Bielsko-Biala, Poland

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Real Driving Emissions (RDE) - 1

The current appalling press regarding RDE shows a lack of understanding of the issue and an industry that has not got its voice across to the public.

The VW issue in the press has been more about vehicles with higher emissions in RDE than on test cycles, which has been the situation since emissions regulations came in and applies equally well to SI engines as diesel, as I will show in this lecture.

Whether VW have 'cheated' and made the RDE worse relative to the test cycle, is a separate issue, but the RDE would have been higher than on the test cycle irrespective of any RDE calibrations that were different to those on the test cycle.

It is my view that congested traffic is a key feature of RDE.

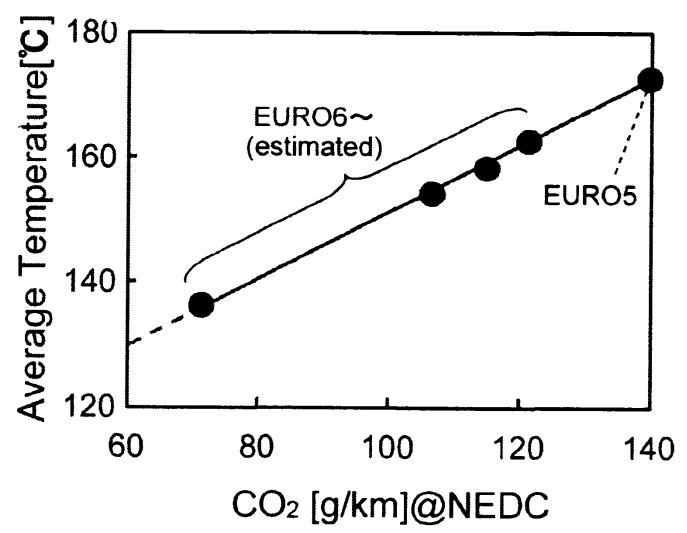
Real Driving Emissions (RDE) - 2

My research group on RDE at Leeds University have over the last 12 years published over 40 SAE papers on RDE and why they are higher than on test cycles.

RDE higher than on test cycles applies to all vehicles SI and diesel and for SI vehicles the RDE effect is closely related to longer cold start in RDE and higher acceleration rates and more stop/starts, as I will show in this presentation.

Modern Euro 6 diesels with particle filters have no real world issues with PM emissions and yet SI engines without a particle trap are now emitting more PM in RDE than diesels with particle traps fitted.

The major RDE effect for diesels is on NOx and CO_2 and with catalysts to control NOx, either NSR or Urea SCR, the catalyst has to be above about 200°C to be active and the lower temperatures of diesel exhausts make this difficult, as I will illustrate for a HDD truck RDE journey.



Future low CO₂ vehicles will have lower exhaust temperatures due to more TC and associated leaner diesel engine operation.

5

deNOx catalyst for lean burn require T>200°C for light off. RD temperatures are lower than on test cycles and so NOx emissions will be higher.

Tsukamoto, Y. et al., Development of new concept catalyst for low CO₂ emissions Diesel engine using NOx adsorption at low temperatures. Toyota. SAE 2012-01-0370

Prediction of Urban Air Quality in Europe -1

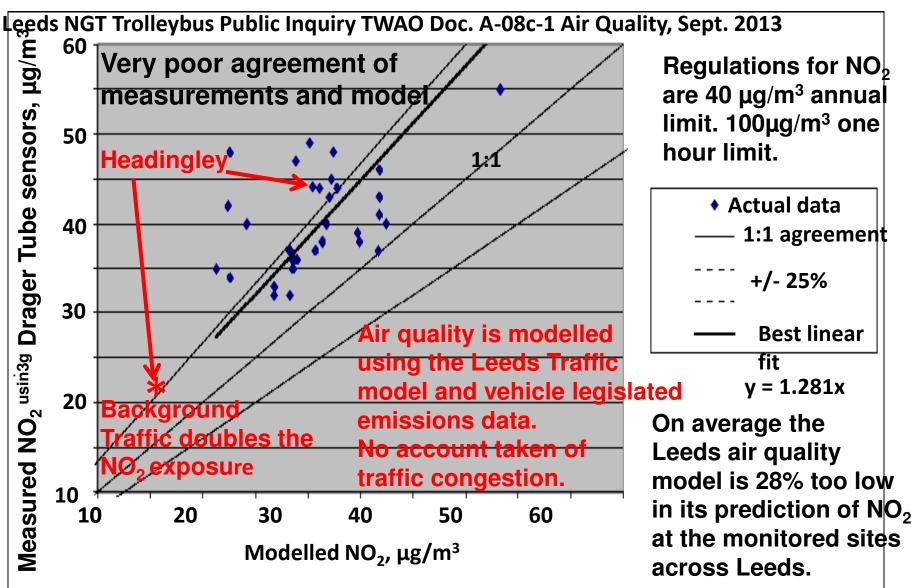
There are relatively few experimentally based air quality measurements in Europe and in UK cities. One per city is quite common.

In Leeds the entire Leeds air quality is measured by the official government funded site at ONE location in the centre of Leeds. This is about 20m from a busy slip road leading to the Leeds Inner Ring Road. Concentrations elsewhere are based on the Leeds air quality model.

The city council has additional roadside measurement locations and one of these is in Headingley on the A660, on the congested route used in this study. This is a site that frequently exceeds European regulations on NOx and PM and this study investigates the pollution from triffic passing this site using a probe vehicle in the traffic flow with PEMS.

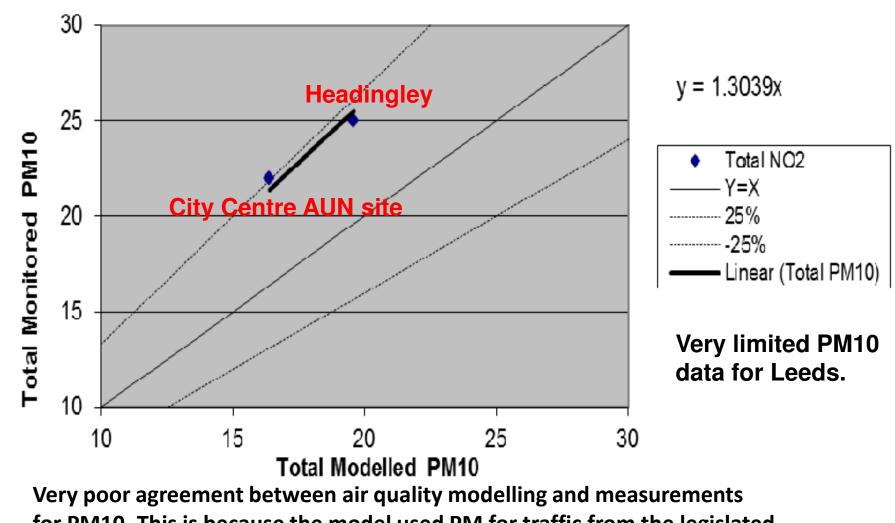
Predictions of air quality relating to traffic rely on three inputs:

- 1. Traffic modelling for traffic flows and mean travel time.
- 2. The UK national database for the age of registered vehicles in Leeds
- 3. The certified emissions per vehicle according to its age using the NEDC test cycle.
- 4. Although there is a procedure agreed in the UK to take into account cold start in situations where they may be significant, this is often ignored for Euro 3 onwards and was ignored in the Leeds model.



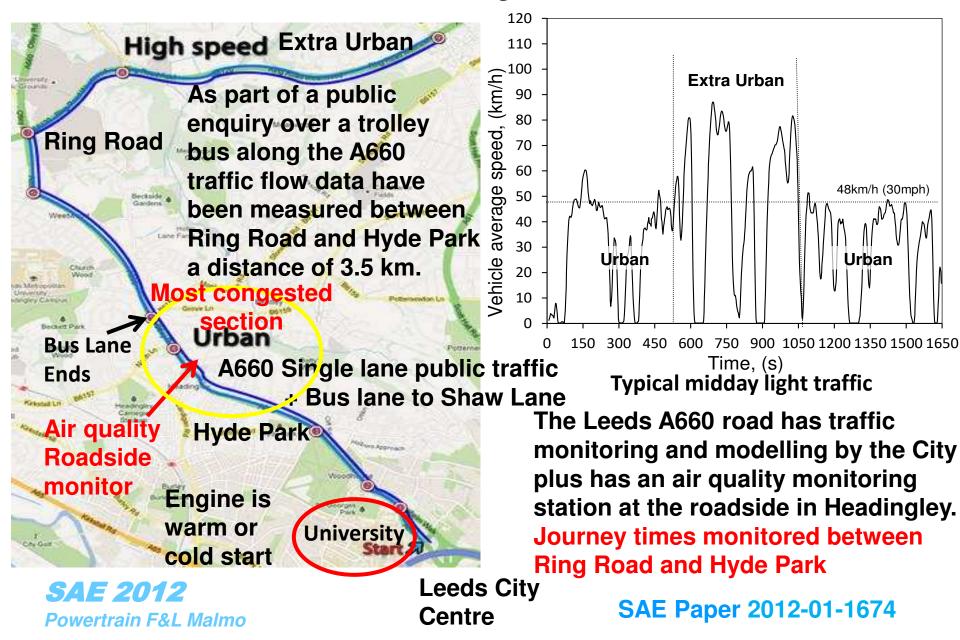
4th Int. Exhaust Emissions Symposium 22-23 May 2014, BOSMAL, Bielsko-Biala, Poland

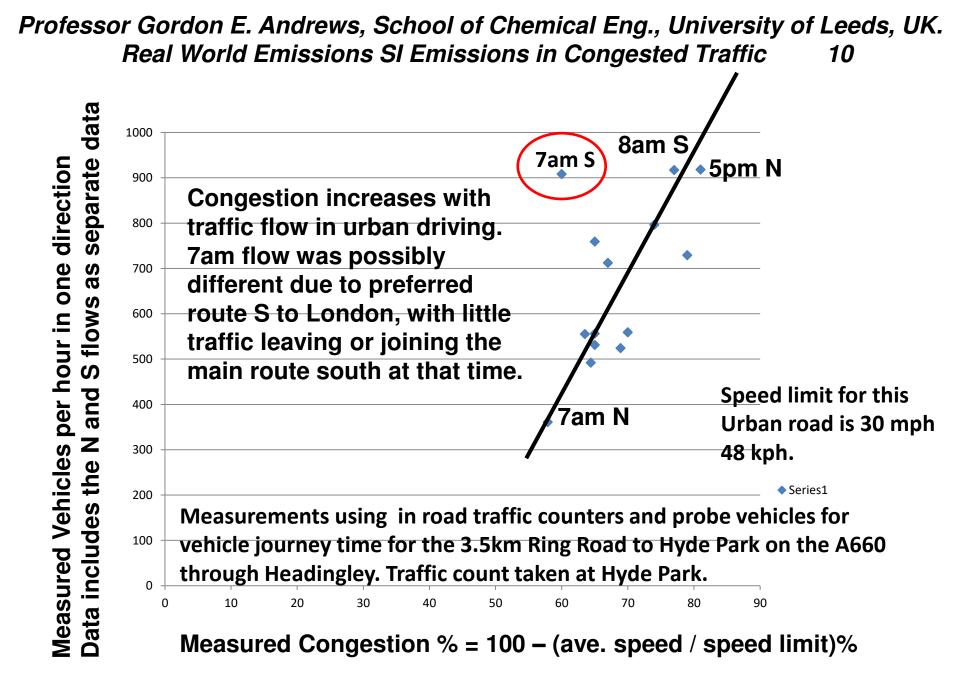
Leeds NGT Trolleybus Public Inquiry TWAO Doc. A-08c-1 Air Quality, Sept. 2013



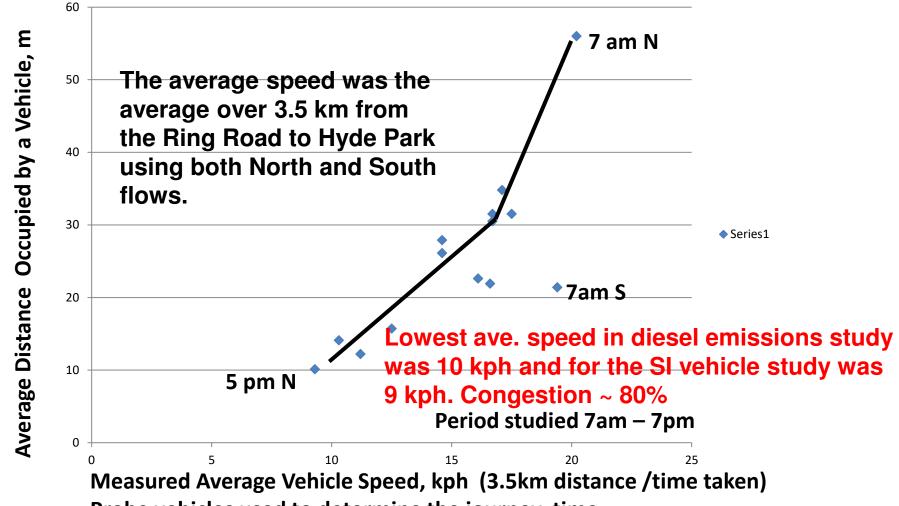
for PM10. This is because the model used PM for traffic from the legislated test cycles and emissions in congested traffic are higher.

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Probe vehicles used to determine the journey time.

Another definition of congestion is when the journey time is half the normal time congestion Is 100% and the above results show that the A660 is congested for all times of the day.

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Euro 3 Diesel Van SAE Paper 2012-01-1674 and SAE 2013-01-2528

	B100			Diesel				RDE x
	MEAN (5°C)	SD	SD/ MEAN	MEAN (13°C)	SD	SD/ MEAN	Euro 3 Limit	Euro Limit
CO ₂ , g/km	172.9	11.8	6.82%	173.6	5.9	3.37%	172*	
CO, g/km	0.067	0.01	16.59%	0.153	0.04	24.63%	0.8	0.2
THC+NOx, g/km	1.342	0.04	3.38%	2.004	0.59	29.61%	0.72	2.8
THC, g/km	0.194	0.03	17.29%	0.145	0.03	18.23%	0.07	2.1
NO _x , g/km	1.148	0.03	2.67%	1.858	0.57	30.51%	0.65	2.9
NO, g/km	0.695	0.04	6.46%	1.491	0.69	46.50%		
NO ₂ , g/km	0.454	0.07	14.35%	0.367	0.14	37.08%		
NO ₂ /NO	65%			25%				

Journey average emissions of the most congested part in units of g/km

SAE 2013-01	-2528								
	Diesel	Diesel	B50	B50	B100	B100	Euro 3	RDE	
Fuel	Run1	Run2	Run1	Run2	Run1	Run2	Limit	Factor	
CO, g/km	8.7	6.3	7.0	5.5	8.2	12.9	0.8	10.1	
THC, g/km	0.72	0.64	0.69	0.47	1.46	2.78	0.07	9.7 (D)	
NO _x , g/km	4.0	3.5	3.3	2.9	4.2	5.2	0.65	12.6	
CO ₂ , g/km	737	1189	579	543	789	942	172	3.7	
V _{mean} ,							17.2		
km/h	6.8	4.5	7.6	7.7	6.6	5.4	(Urban)		
In this nanor this most congested part of the route was									

In this paper this most congested part of the route was Investigated for a SI Vehicle – Euro4

Diesel Particulate and NOx Emissions 2015 Prof. Gordon E. Andrews, Energy Research Institute, U. Leeds, UK 14

Tim Johnson, Review of Vehicular Emissions Trends, SAE Int. J. Engines 7(3) 2015, Corning Inc. doi:10.4271/2015-01-0993 SAE Paper 2015-01-0993

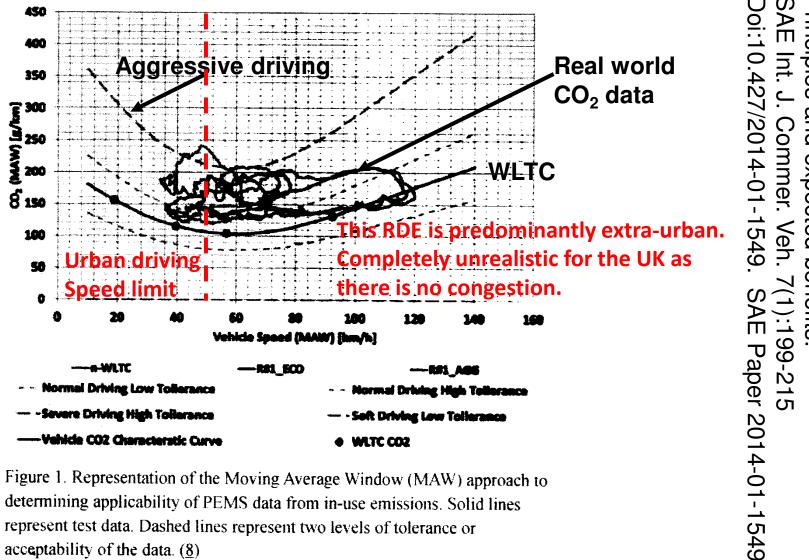


Figure 1. Representation of the Moving Average Window (MAW) approach to determining applicability of PEMS data from in-use emissions. Solid lines represent test data. Dashed lines represent two levels of tolerance or acceptability of the data. (8)

EMS rinciple **OISSI** lachos 5 the and eg current ቧ slation: expected <u>മ</u> . and SD Ď benefits VIEW emissions European vehicle underlying testing with

Comparison of congestion simulated in test cycles

This assumes a regulated speed of 30 mph or 48.3kph for urban driving

Test Cycle	NEDC	FTP	CAFE	JC09	WLTC	RDE	This work
Mean Vel. kph	33.6	31.5	52.3	24.4	46.5	30 - 110 ¹	5 – 26
Congestion	30%	34%	0%	49%	3%	0%	90% - 46%
Max. Acc. m/s ²	1.0	1.5		1.7	1.7	1.5 ²	2.2 – 2.8
Distance, km	11	12		8.2	23.3	~80-901	5
No. Acc. From Idle / km	1.3	1.5		1.5	0.4	~0.21	1.2 - 7

RDE in congested traffic involves lower speeds, higher accelerations and many more accelerations from idle than on any legislated test cycle WLTC will have lower emissions than NEDC due to higher speeds and proposals for RDE ignore congested driving completely

¹RDE Examples f rom S. Hausberger et al. TU Graz, 3rd Conf. RDE, Berlin, Oct. 2015.

²J. Merks et al. U. Poznaz, 3rd RDE, Berlin, Oct. 2015

The air quality exceedances for PM and NO₂ in cities is based on local monitoring stations close to roads with congested traffic e.g. Marylebone Road in London and Headingley in Leeds. It is the local congested traffic that is the problem and as I have shown, none of the test cycles or so called improved test cycles address this issue and it is totally ignored in the proposals for RDE testing.

In congested traffic the average speed is low, peak accelerations are high and the number of accelerations from idle/km is much higher than on any test cycle. These are the reasons for real world driving causing poor air quality in cities and these conditions are ignored in WLTC and RDE proposals. Thus these new test procedures will not address the issue of real world driving and poor urban air quality.

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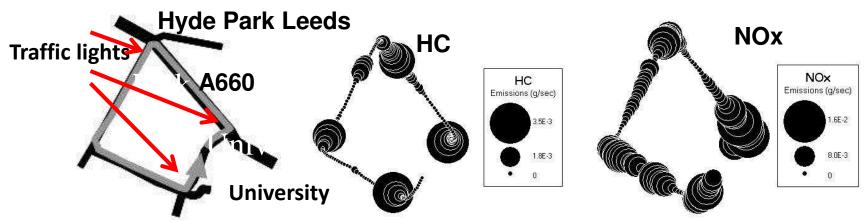
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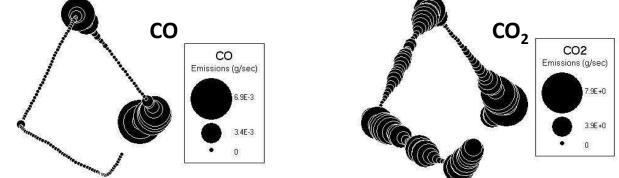
Factors that influence RDE – both SI and Diesel

- 1. Driver behaviour aggressive drivers high acc./decel
- 2. Ambient temperature affects catalyst light off and water and lube oil warm-up times, related to cold start.
- 3. Congested traffic in urban driving low average speed and more stop/starts influence of other drivers this is the main topic of this presentation.
- 4. Traffic lights and road junctions most emissions in urban areas occur at these real driving events.
- 5. Cold start in RDE is longer than on test cycles and often occurs in congested traffic.
- Diesels have an additional problem that the catalyst can cool down after it has lit off – cruise and reaching congested traffic after a period of high speed driving. This will be shown for SCR and has previously been shown for oxidation catalysts.

Example of emissions mapping using Horiba OBS g/s in a Ford Mondeo Euro 1 For Euro II – VI with lower emissions there are no significant emissions other than at junctions, so the effect of junctions is greater.

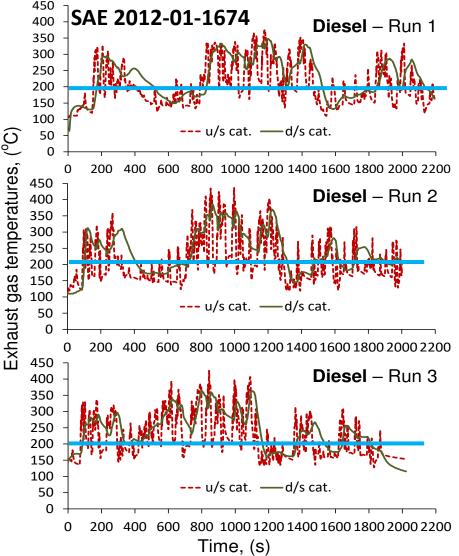


Pollution and CO₂ is predominantly at junctions for Euro 2 and increasingly so for Euro 4+



Junctions are the most important influence of congested traffic driving in urban locations. There are no junctions in the NEDC!

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The present work was not designed to include a cold start, the time at the start of the test while instruments and data loggers were set up was sufficiently long for catalyst cooling to occur. The low oxidation catalyst temperatures at the start of the test resulted in high CO and HC emissions during the subsequent warm up period. For most of the journeys the catalyst temperature was well above 200°C. However, there were times when the catalyst cooled down to around 150°C in congested traffic, where CO and HC increased.

This is a different catalyst behavior to that in SI vehicles operating at λ =1 as the exhaust temperature are higher and there is greater heat release at the catalyst due to CO and HC oxidation.

3rd International Conference on Real Driving Emissions 2015, 27 – 29 October 2015, Berlin, Germany

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PEMS – Temet FTIR (Gasmet) with Horiba OBS pitot tube exhaust mass flow measurements and gas sampling.

Racelogic GPS for velocity and acceleration measurements

Cold start and hot start emissions compared for the same test journey.

Congestion varied by testing at different times of the day with different traffic loadings.

29 hot start trips and 8 cold start – total journeys 37

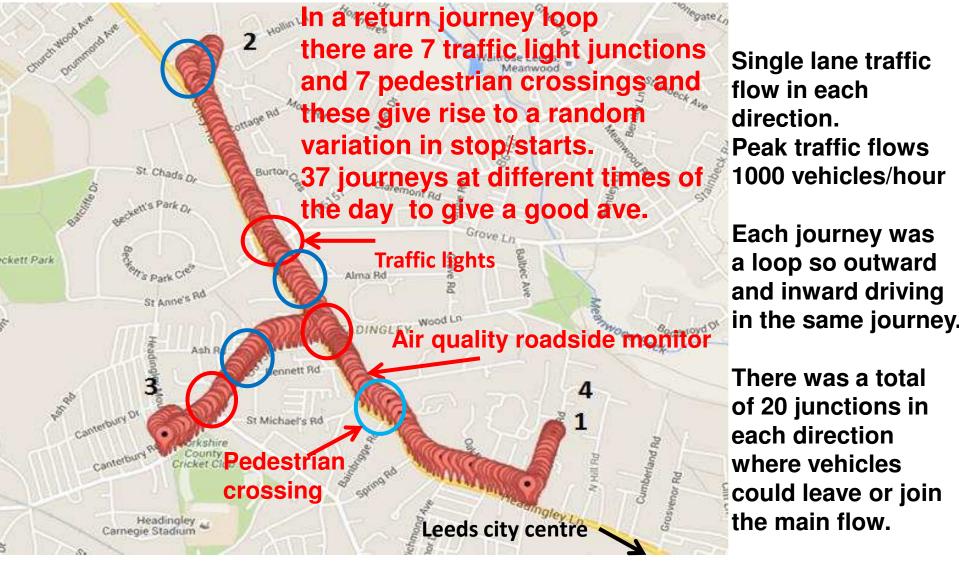
Same driver for all journeys.

Ford Mondeo Euro 4 vehicle

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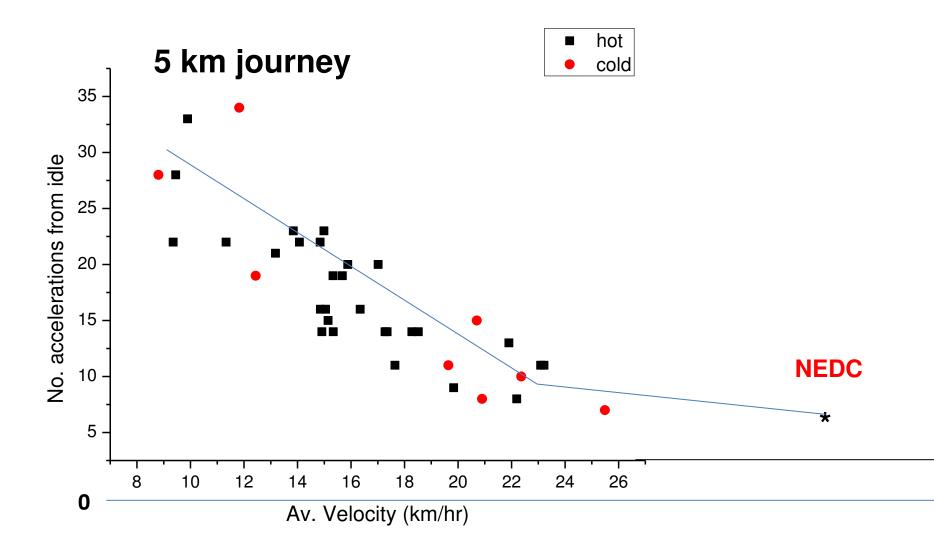
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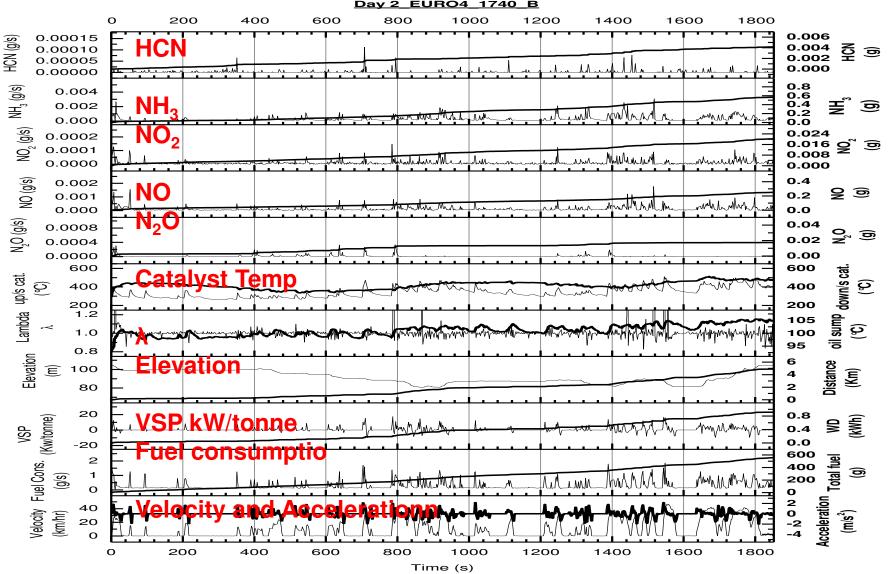
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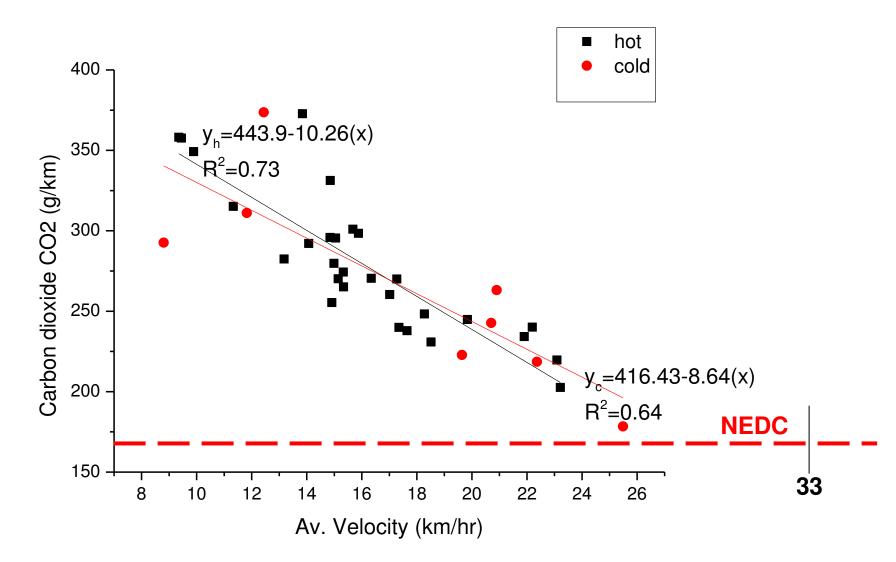
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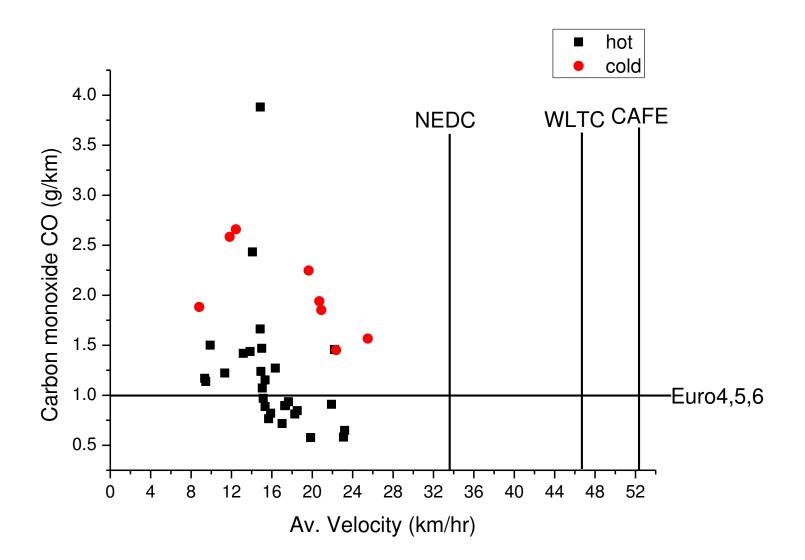
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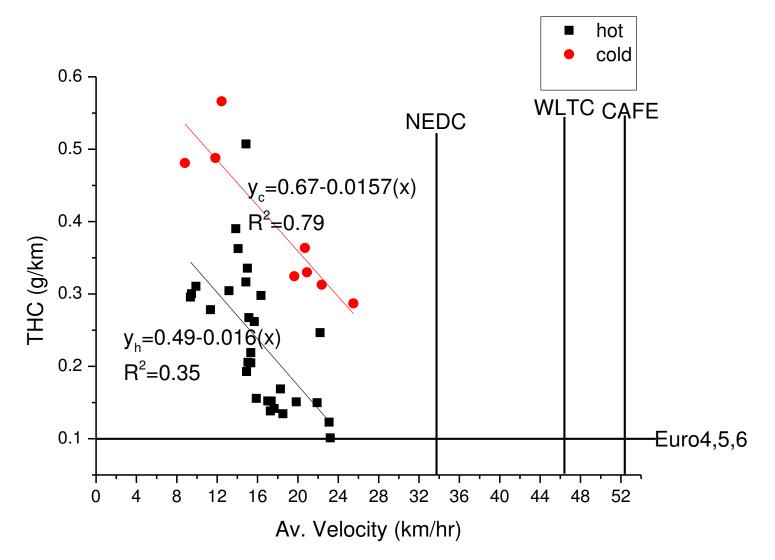


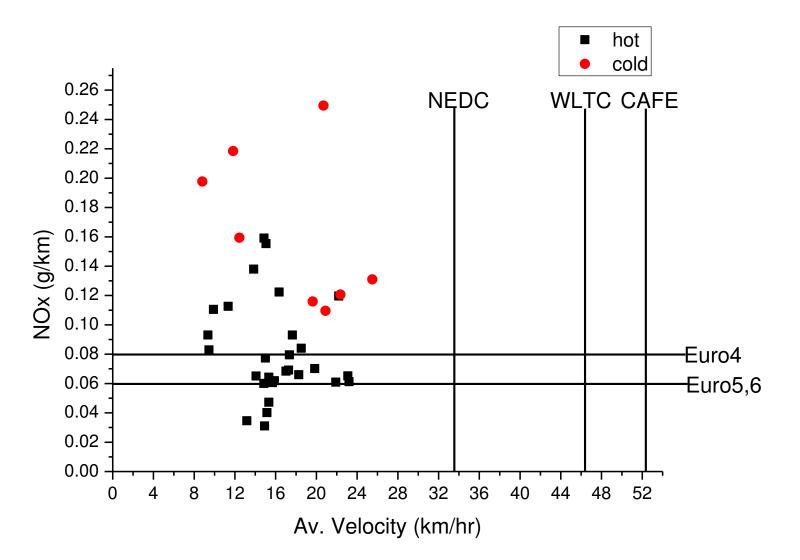
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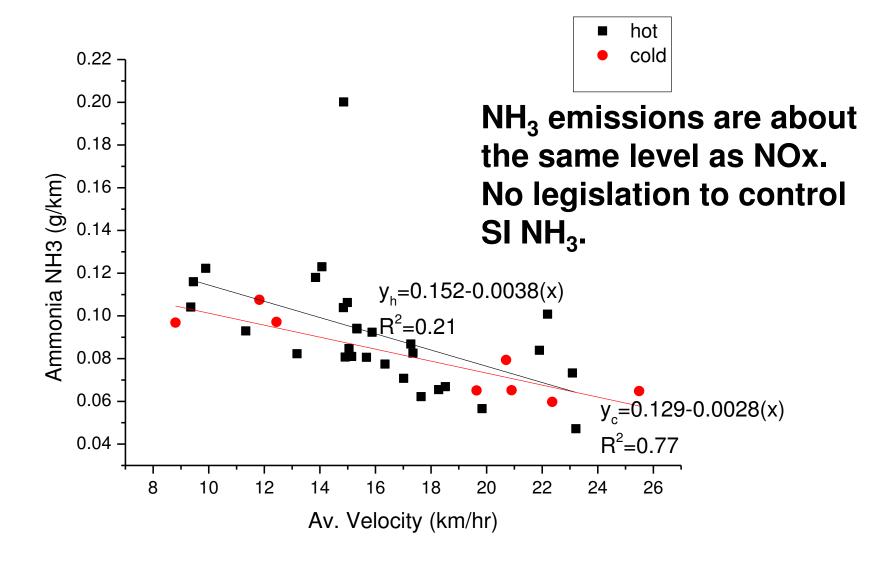
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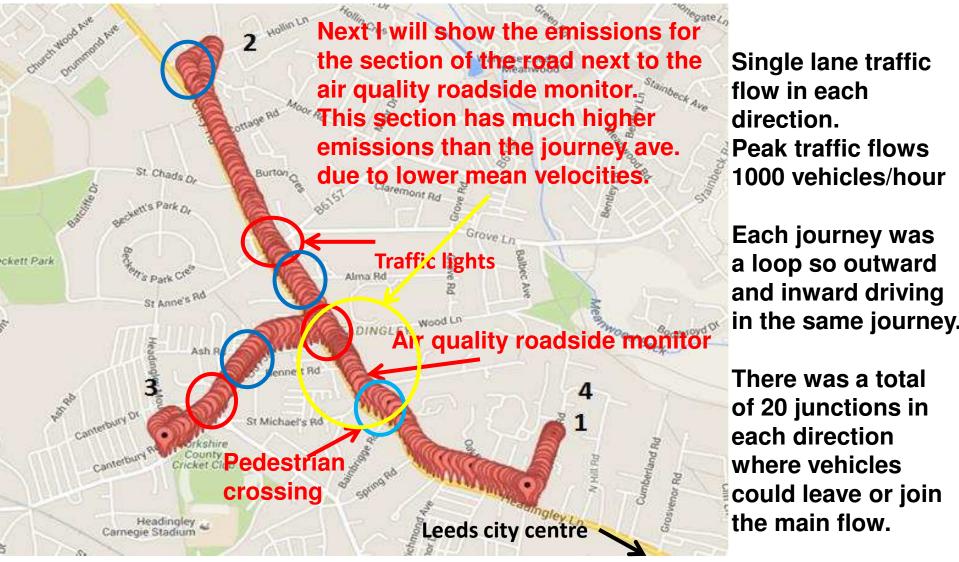


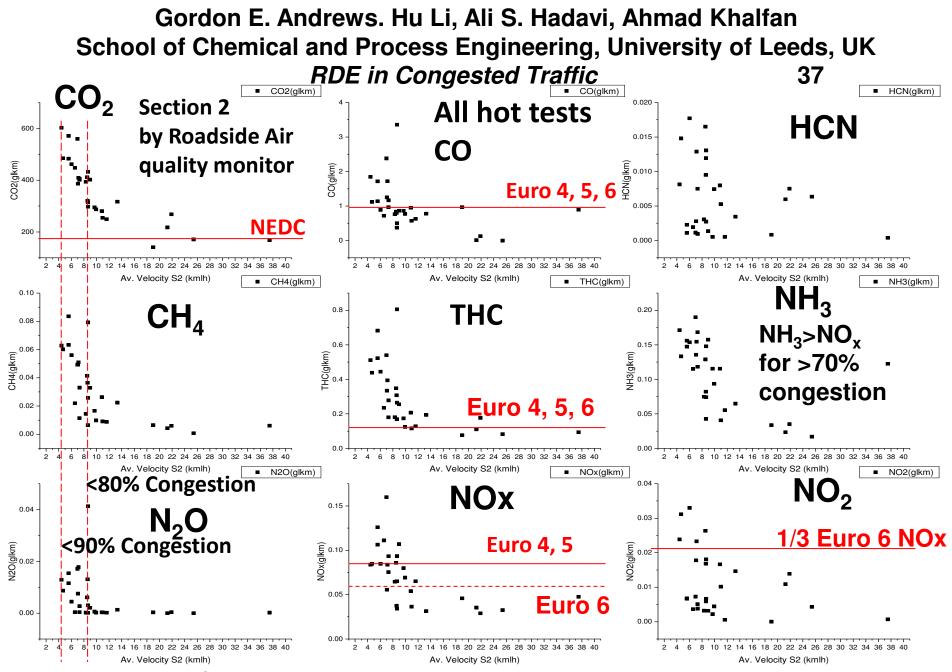




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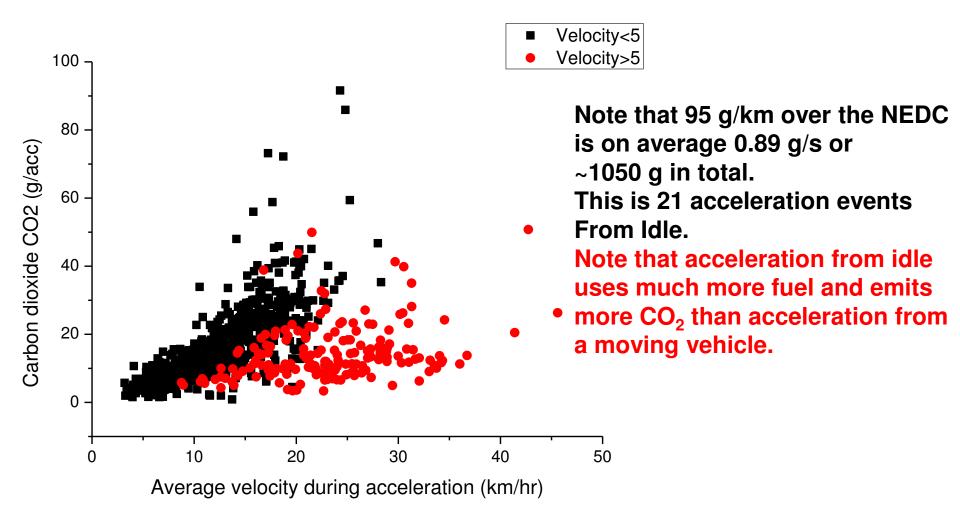
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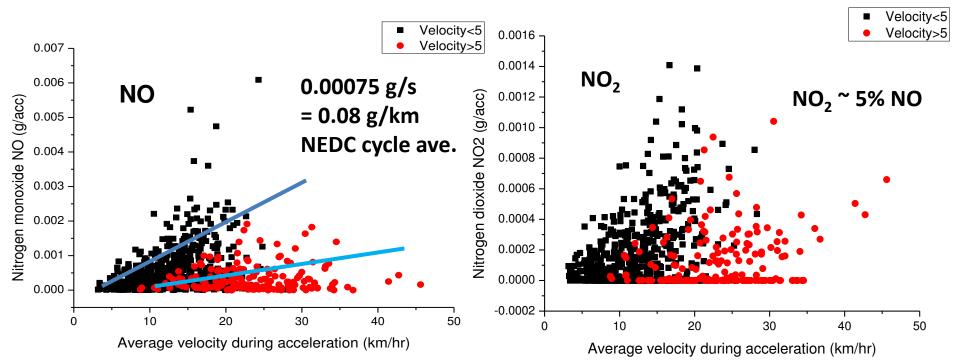




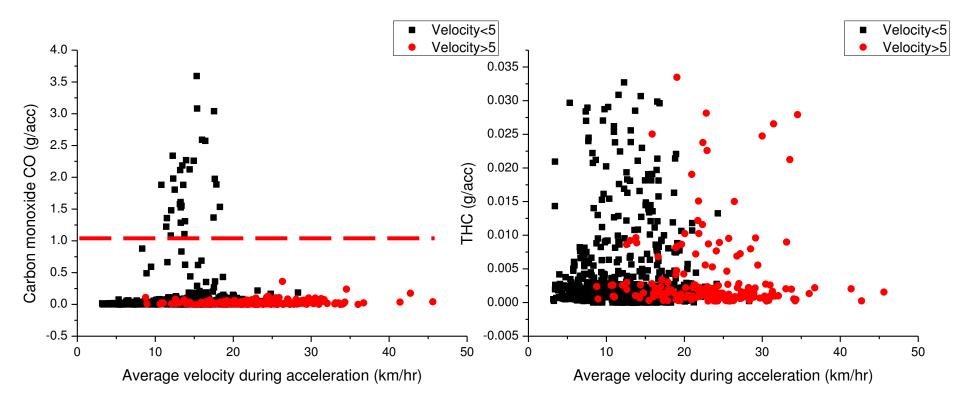
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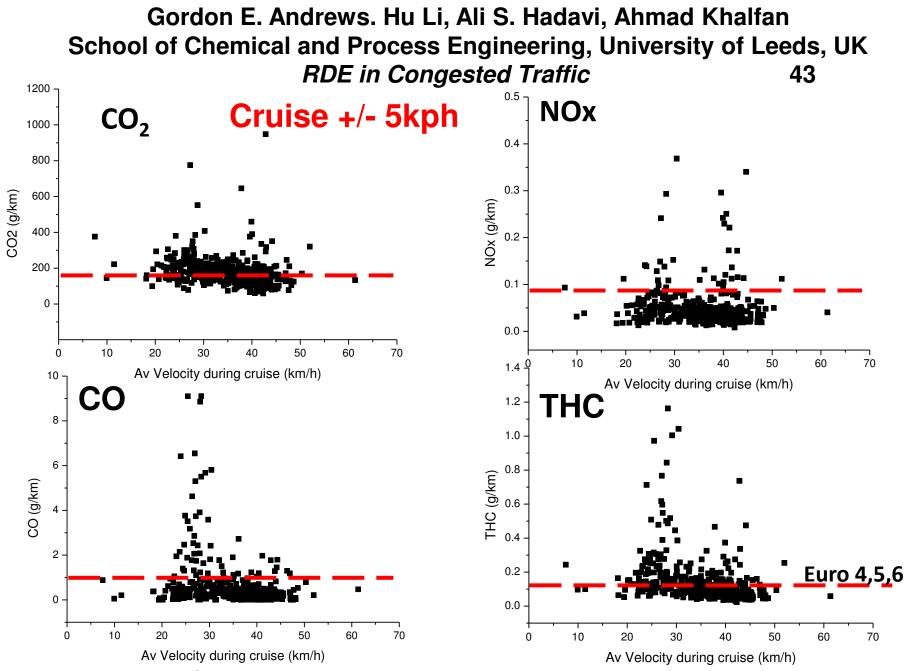
High acceleration has higher NOx emissions due to higher power used. Acceleration from idle has higher NOx due to higher power requirement. Congested traffic has a high number of acceleration events from idle. Variation in NOx emission rate for the same average velocity in the acceleration was very large ~ x10. It is possible to accelerate hard without generating large NOx emissions.



NEDC limit 1 g/km = 0.093 g/s averaged across the test cycle. X>10 of this rate has been measured In medium acceleration events. NEDC limit g/km = 0.0093 g/s ave. most acc. are below this but some are very high THC emissions.

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Cruise emissions at nominal constant velocity (cruise) scatter around the values for the NEDC.

- Cruise criteria is constant velocity at +/- 5kph for >8s
- CO₂ has much of the data above the NEDC value
- NOx and CO and mainly below the NEDC limit
- THC mainly above the NEDC limit.
- It may be that the +/- 5 kph is too large for the constant velocity assumption to be valid.

However, the wide variation in nominal constant velocity in a journey with no trend in emissions may indicate that the short duration cruise emissions are influenced by the preceding acceleration or deceleration

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- 1. Air quality exceedances in cities occur at local roadside mesurements stations.
- 2. Existing test cycles have low levels of congested driving and the WLTC and proposed RDE have even lower congestion than the NEDC
- 3. In congested traffic for diesels the lower temperature can cause the catalyst not to work. This is very significant for Urea SRC where the low average speed gives low temperatures and low activity of the NOx removal.
- 4. Congested traffic has a high number of accelerations from Idle and these stop/start event cause pollution.
- 5. In congested traffic emissions may be x ~10 of the limit.

Acknowledgements

We would like to thank the UK EPSRC for supporting the early stages of this research and for providing the heated FTIR. This was through two large grants

LANTERN and RETEMM 2001 - 2008

More recent work has been through PhD students.

The recent HDD vehicle RDE diesel work was through a UK Department for Transport and Technology Strategy Board for supporting the research element within the project "Environmental and Performance Impact of Direct use of used cooking oil in 44 tonne trucks under real world driving conditions" which is part of the Low Carbon Truck Demonstration Trial." Thanks go to United Biscuits Midland Distribution Centre for the provision of a truck and general support and collaboration in field tests. Thanks also go to Bioltec System GmbH for advice and permission to use some technical information and Convert2Green for the provision of Ultra Biofuels for the tests