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***Figures***

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**Published paper**

Jumahat, A., Soutis, C., Jones, F.R., Hodzic, A. (2009) *Fracture mechanisms and failure analysis of carbon fibre/toughened epoxy composites subjected to compressive loading*, Composite Structures, 92 (2), pp. 295-305  
<http://dx.doi.org/10.1016/j.compstruct.2009.08.010>

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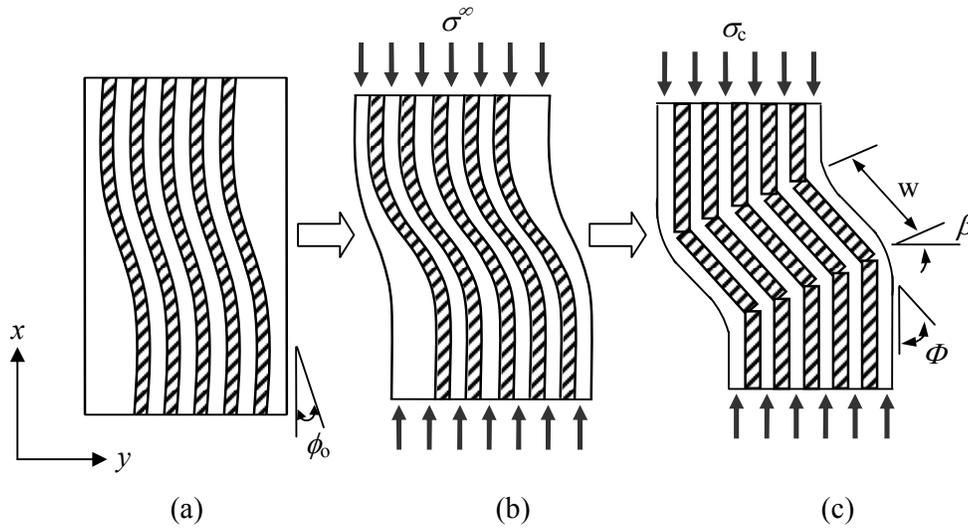


Fig. 1. The schematic diagram showing the formation of kinking failure mode and its geometry; (a) in plane buckling of  $0^\circ$  fibres with an initial fibre misalignment  $\phi_0$ , (b) deformation of  $0^\circ$  fibres via fibre microbuckling mechanism when it is loaded in compression  $\sigma^\infty$ , and (c) fibres kinking phenomena causing catastrophic fracture of the UD laminate. The kink band geometry:  $w$  = kink band width,  $\beta$  = boundary orientation and  $\Phi = \phi_0 + \gamma$  = inclination angle.

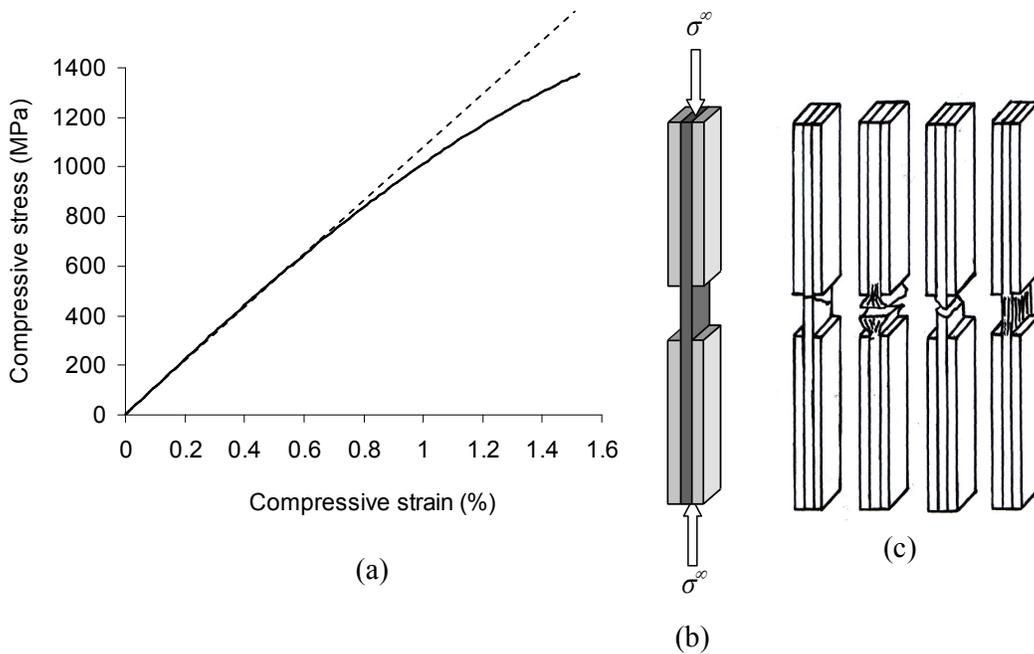


Fig. 2. (a) A typical compressive stress-strain response of a UD HTS40/977-2 laminate [20]; (b) schematic representation of UD specimen loaded in compression; and (c) schematic diagram of various types of failure specimens according to ASTM D3410 and D6641.

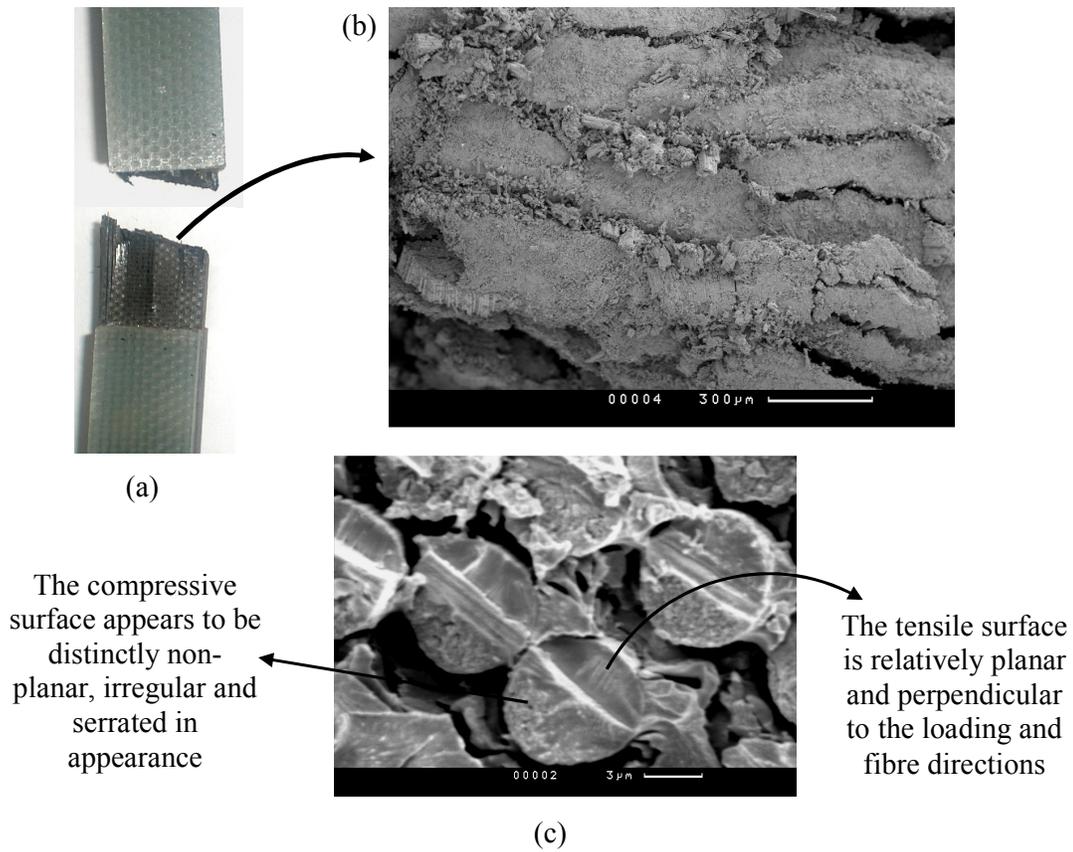


Fig. 3. Characteristics of fractured specimen; (a) the overall view of the actual fractured specimen of UD HTS40/977-2 composite laminate. Fracture surface is at an angle  $\beta=10^\circ$  to  $25^\circ$  which is called kink band inclination angle; (b) SEM micrograph of the fractured surface (top view); and (c) SEM micrograph illustrating tensile and compressive surfaces on an individual failed fibre due to microbuckling.

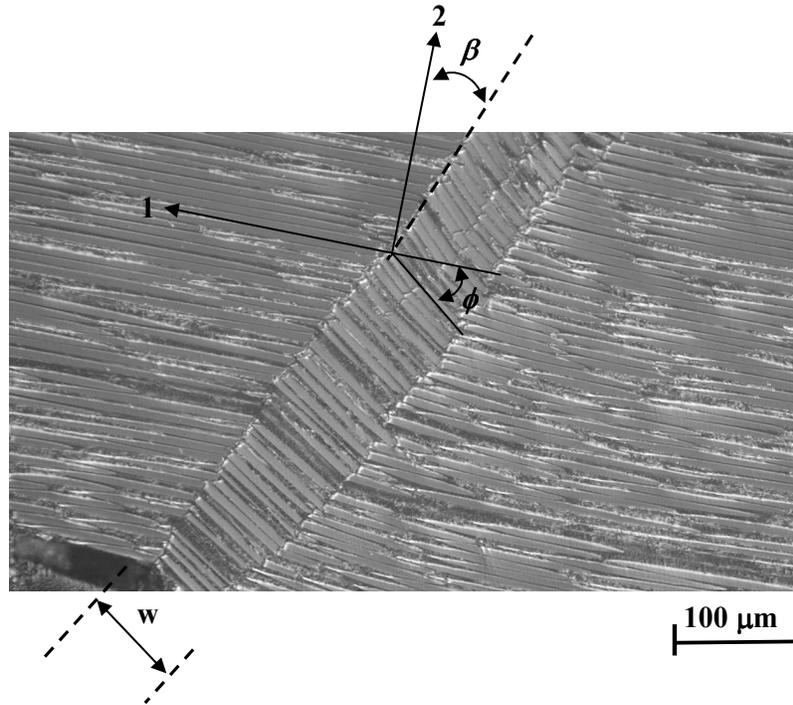
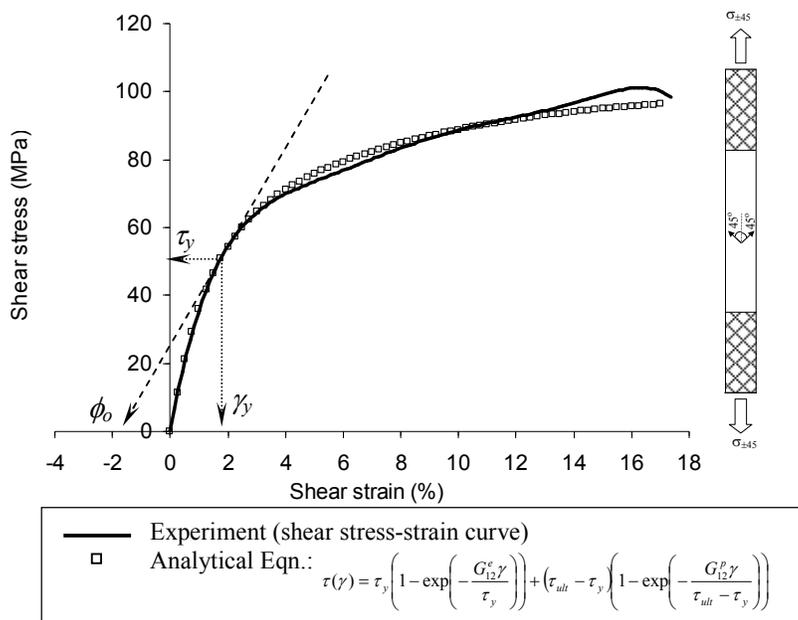


Fig. 4. Optical microscopic across width view (at 200x magnification) of UD HTS40/977-2 CFRP composite laminate. Kink band width,  $w = 60 \mu\text{m}$  to  $100 \mu\text{m}$  (or  $\approx 8$  to  $15$  fibre diameters) and kink band inclination angle,  $\beta = 10^\circ$  to  $25^\circ$ .



(a)



(b)

Fig. 5. (a) In-plane shear stress-strain response of a  $[\pm 45]_{2s}$  HTS40/977-2 composite laminate and (b) failed specimen.

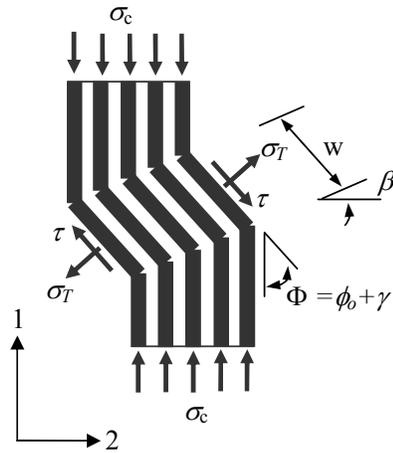


Fig. 6. Budiansky's fibre kinking model with schematic geometry of a kink band width,  $w$  oriented at an angle,  $\Phi$  to the 1-direction (fibre direction) and reaction forces of the material loaded in compression.

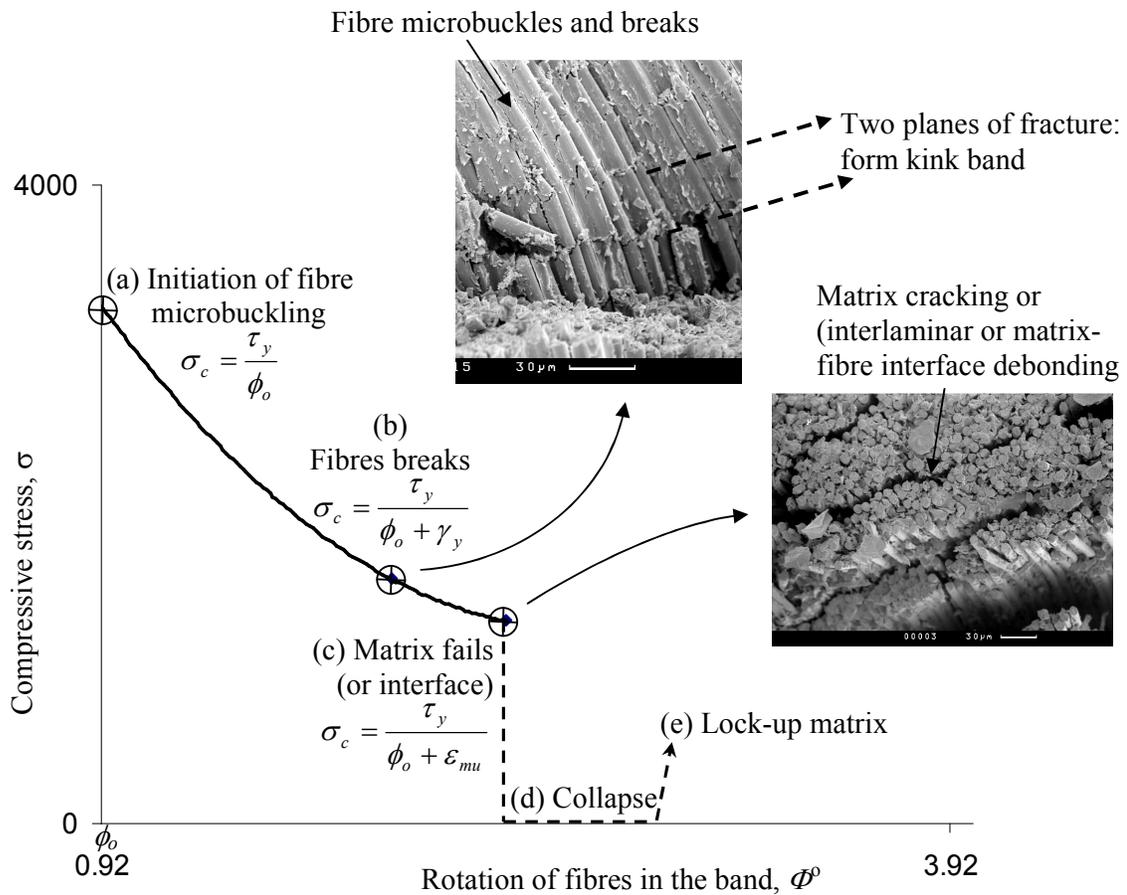


Fig. 7. Theoretical compressive stress-strain response of the UD HTS40/977-2 composite laminate after the initiation of fibre microbuckling.

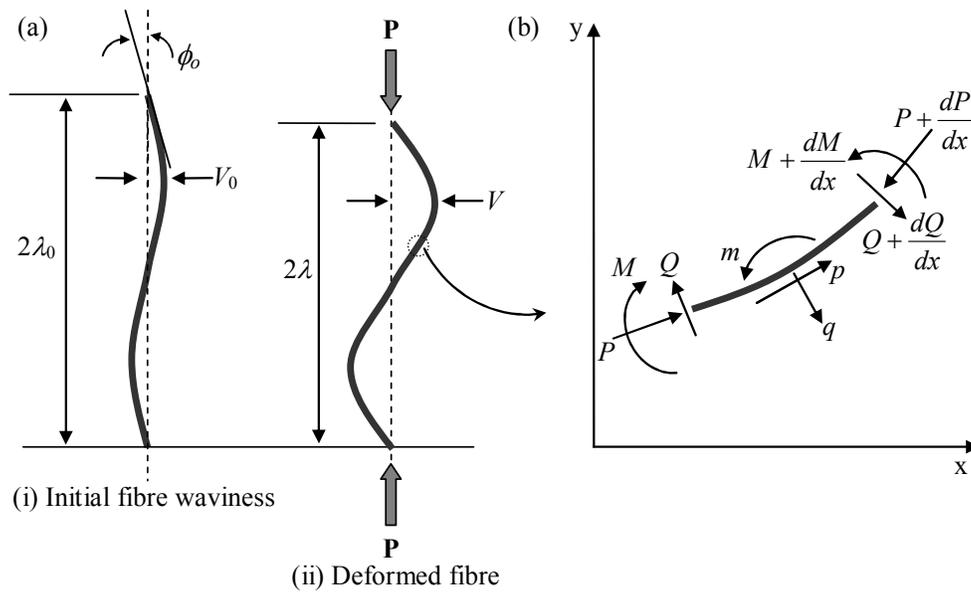


Fig. 8. (a) A schematic of fibre microbuckling mode [24] (b) Free body diagram for a fibre element [4].  $P$  = Axial compressive force,  $Q$  = Transverse shear,  $M$  = Bending moment,  $p$  = Applied distributed axial force,  $q$  = Applied distributed transverse force,  $m$  = Applied distributed bending moment.

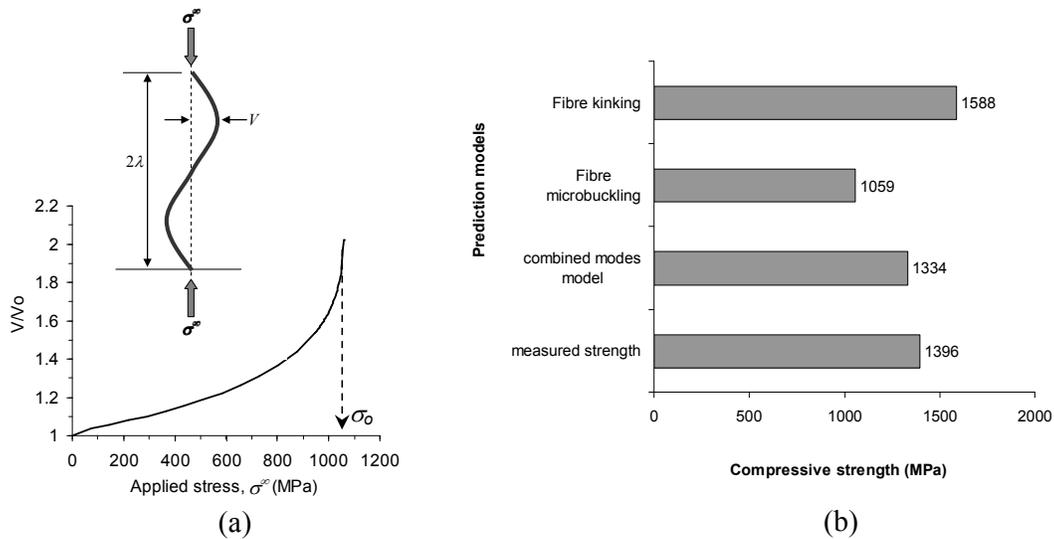


Fig. 9. (a) Fibre amplitude  $V$  normalised by initial fibre imperfection  $V_0$  versus applied compressive stress,  $\sigma^0$ . ( $\sigma_0 = 1059$  MPa, is the critical stress at which fibre microbuckling is triggered); and (b) compressive strength prediction using combined modes model and comparison between predicted and measured compressive failure strengths of the UD HTS40/977-2 CFRP composite laminate.

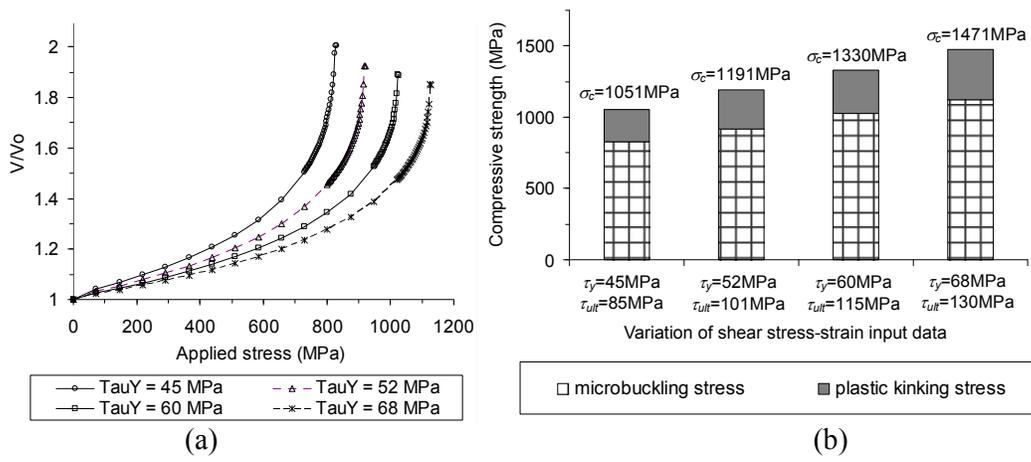


Figure 10: The effects of non-linear shear stress-strain ( $\tau - \gamma$ ) response on the compressive strength of the UD HTS40/977-2 composite laminate; (a) Variation of  $0^\circ$  fibre amplitude with applied stress of the UD HTS40/977-2 laminate (b) Compressive strength prediction using combined modes model.

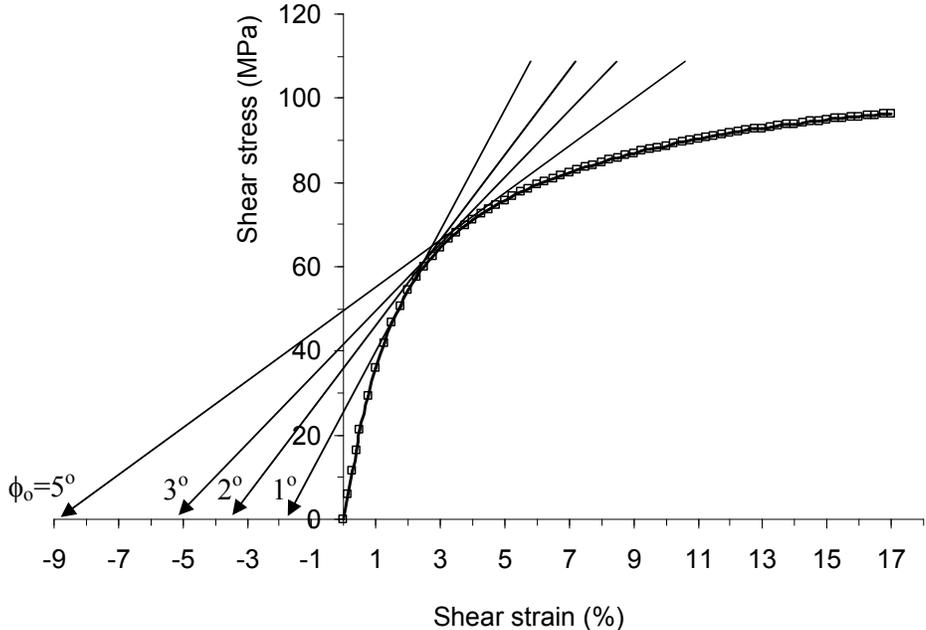


Figure 11: Measurement of shear yield stress and strain using nonlinear shear stress-strain diagram to study the effects of initial fibre misalignment on the compressive strength of the HTS40/977-2 UD composite laminate.

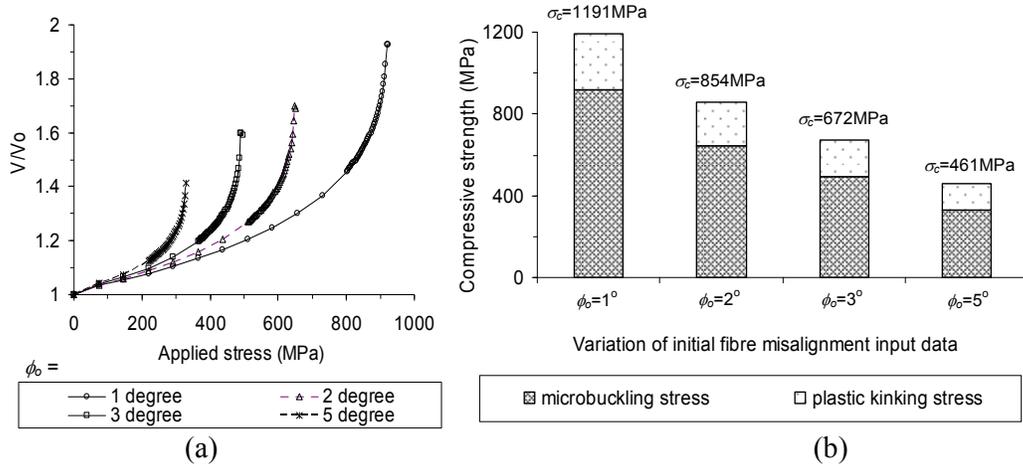


Figure 12: The effects of initial fibre misalignment on the compressive strength of the UD HTS40/977-2 composite laminates; (a) Variation of  $0^\circ$  fibre amplitude with applied stress on the UD HTS40/977-2 laminate (b) Compressive strength prediction using combined modes model.

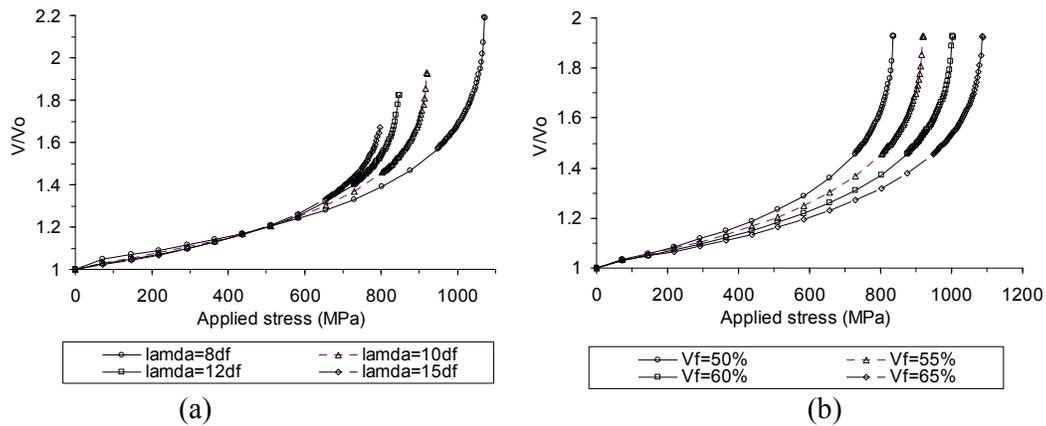


Figure 13: Variation of  $0^\circ$  fibre amplitude with applied stress on the UD HTS40/977-2 laminate at various (a) initial half-wavelengths of the fibre and (b) fibre volume fractions.

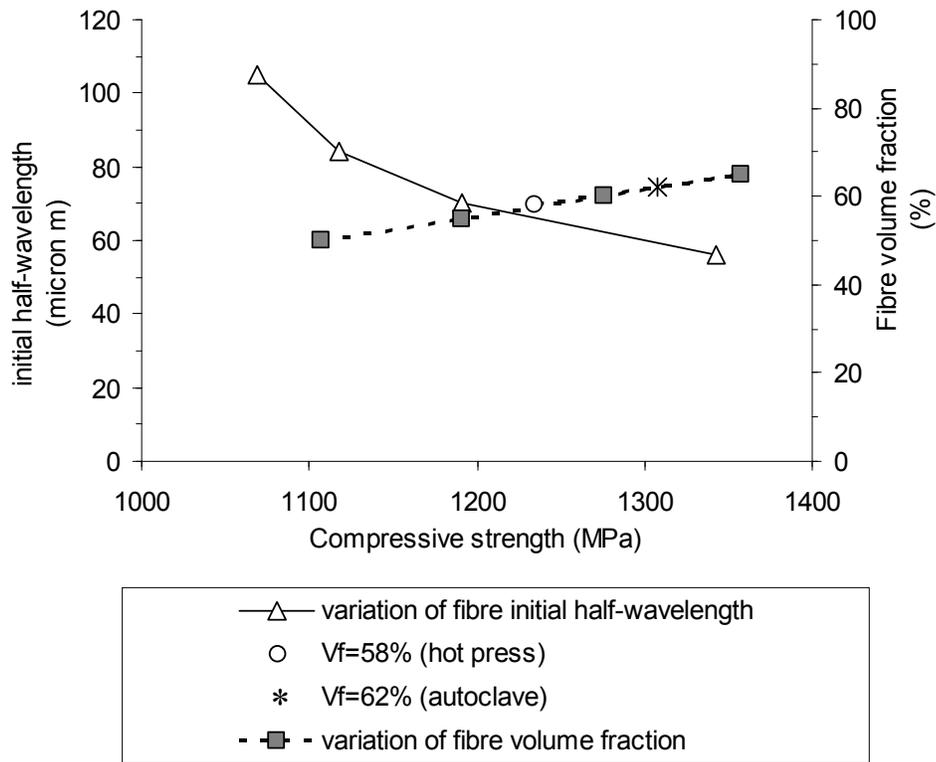


Figure 14: The effects of initial half-wavelength of the fibre and fibre volume fraction on the compressive strength of the UD HTS40/977-2 composite laminates.

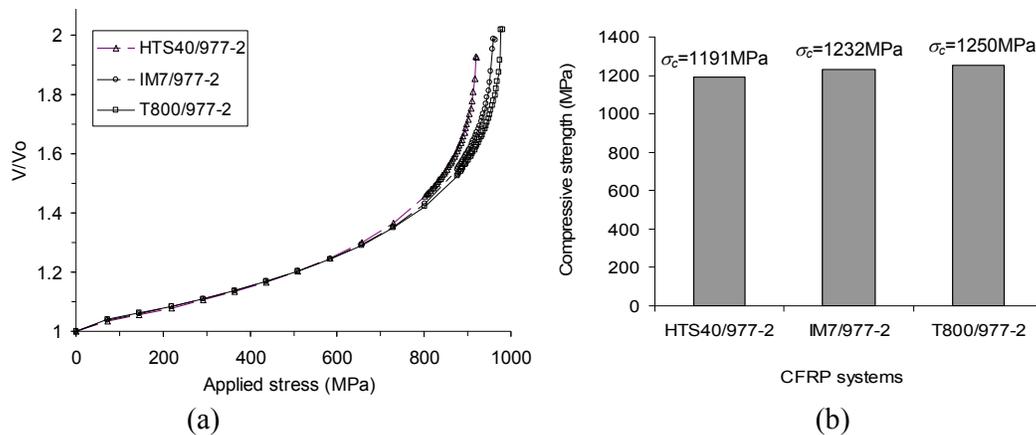


Figure 15: The effects of fibre types and properties on the compressive strength of the UD HTS40/977-2 composite laminate; (a) Variation of  $0^\circ$  fibre amplitude with applied stress on the UD HTS40/977-2 laminate (b) Compressive strength prediction using combined modes model.