



Critical factors for levulinic acid production from starch-rich food waste: Solvent effects, reaction pressure, and phase separation

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15

Abstract

A considerable amount of food waste generated globally could be upcycled to synthesise platform 16 chemicals to enhance environmental sustainability and help realise a circular economy. This study 17 investigates the catalytic production of the vital platform molecule levulinic acid (LA) from bread 18 waste, a typical stream of starch-rich food waste generated worldwide. Gamma-valerolactone 19 (GVL), isopropanol (IPA), and propylene carbonate (PC) were evaluated as bio-derived and CO₂-20 derived green co-solvents for LA synthesis. In-vessel pressure generated in PC/H₂O (1:1) solvent 21 was conducive to rapid LA production from bread waste compared to GVL/H₂O and IPA/H₂O. In 22 PC/H₂O, 72 mol% total soluble product yield was observed quickly within 1 min in moderate 23 reaction conditions (130°C, 0.5 M H₂SO₄), whereas ~15-20 mol% of LA could be obtained when 24 the reaction was prolonged for 10-20 min at 130°C. The yield of LA could be significantly 25 enhanced in GVL/H₂O through phase separation using NaCl (30 wt%_(aq)). LA yield increased up 26 to a maximum of ~2.5 times in the biphasic system (28 mol%, 150°C, 15 min) (representing a 27 theoretical yield of 66%) in GVL/H₂O (1:1) compared to the monophasic system (~11 mol%) 28 under the same reaction conditions. The partition coefficient for LA achieved was 4.2 in the 29 GVL/H₂O (1:1) biphasic medium, indicating that the system was efficient for simultaneous 30 production and extraction of LA. Biphasic GVL/H₂O facilitated selective LA production, which 31 could be optimised by tuning the reaction conditions. These new insights can foster the 32 development of high-performance LA production and sustainable biorefinery. 33

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Keywords: Waste recycling/management; Platform chemicals; Green solvents; Extractive
separation; Sustainably biorefinery; Circular economy.

37

38 Introduction

Appropriate and sustainable management of the growing amount of food waste is a big 39 issue in modern society. Approximately 931 million tonnes of food waste were globally generated 40 in the year of 2019 at the retail and consumer level (households and commercial food services). 41 excluding food loss during post-harvest to distribution in the food supply chain.¹ Such an enormous 42 amount of food waste requires proper handling to minimise pollution risks and be diverted from 43 landfill disposal.² Transforming food waste into platform chemicals offers a sustainable 44 opportunity to utilise the vast waste stream for biorefinery applications and pave the way forward 45 to realising a circular bioeconomy.³ 46

Levulinic acid (LA) is one of the top bio-derived platform chemicals with various 47 applications, e.g., pharmaceuticals, plasticisers, solvents, fuels, and personal care products.⁴⁻⁵ 48 Besides, LA serves as a building block for the production of various value-added derivatives such 49 as gamma-valerolactone (GVL),⁶ succinic acid, diphenolic acid,⁷⁻⁸ alkyl levulinates, 2-methyl-50 tetrahydrofuran, etc.⁵ Considering the low cost and high catalytic activity for tandem hydrolysis 51 52 and dehydration reactions, mineral acids such as H_2SO_4 and HCl are generally used for LA production from diverse biomass feedstock including food waste, paper waste, etc.⁹⁻¹⁰ Starch-rich 53 foods such as rice, bread, and potatoes are commonly consumed and constitute a significant 54 proportion of global food waste,¹¹ which can serve as a potential feedstock for biorefineries. Recent 55 studies demonstrated that catalytic production of sugars and platform chemicals could be an 56 effective technique for recycling/valorising a considerable amount of starch-rich food waste 57 generated globally.¹²⁻¹³ In this study, bread waste serves as the representative starch-rich feedstock 58 for the catalytic production of LA. 59

Appropriate reaction conditions and solvent selection are critical for selective and cost-60 effective LA production.¹⁴ As the greenest and environmentally benign solvent, water has been 61 used as a reaction medium for LA synthesis. However, harsh reaction conditions, i.e., high 62 temperature and acidity, are required when using water as the reaction medium resulting in an 63 energy-intensive process and high byproduct (humin) formation.¹⁵ The selection of a suitable 64 solvent is necessary, as it not only serves as a reaction medium, but also influences the catalytic 65 process through solvent-solute interactions, adjusting the reactivity of proton, suppressing the 66 byproduct formation, etc.^{13,16} Owing to the need for selective and high-efficiency chemical 67 synthesis, various organic solvents as reaction medium have been widely investigated, such as 68 dimethylsulfoxide (DMSO),⁹ tetrahydrofuran (THF), dimethylformamide (DMF),⁷ GVL, acetone, 69 etc.^{10,17} However, conventional organic solvents DMSO, DMF, THF, etc., are widely considered 70 "non-green" due to their direct or indirect detrimental effects on the natural environment and 71 human health and safety. Therefore, the use of alternative "green" solvents, and especially those 72 which are renewable and bio-derived (GVL, alcohols, etc.) or CO₂-derived (propylene carbonate 73 (PC), dimethyl carbonate (DMC), etc.), are recommended for future applications.¹⁸⁻¹⁹ Furthermore, 74 enhanced catalytic conversion of biowaste using these bio-derived and CO₂-derived solvents was 75 reported in recent studies,^{10,13,20} yet their influences should be evaluated in comparable conditions 76 to validate their efficiency and elucidate the critical factors for catalytic LA production. 77

Apart from using environmentally friendly and safe reaction systems, process intensification is indispensable to improve the final concentration of LA for scaling up at the industrial level.¹⁴ Efficient separation and purification of LA are necessary for the possible recovery of mineral acid catalyst and further conversion of LA to valuable derivatives such as GVL, which can be negatively affected by the presence of mineral acid.^{17,21} A viable strategy could Page 9 of 68

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be using the biphasic solvent system comprising two immiscible layers. The aqueous layer 83 contains the acid catalyst and serves as the reactive phase, while the organic layer acts as the 84 extractive phase, facilitating simultaneous production and extraction of LA, which might enhance 85 LA vield and selectivity.²¹⁻²² For instance, a recent study on the conversion of remnant algal 86 biomass reported a significant enhancement of hydroxymethylfurfural (HMF) and LA yield using 87 88 acidic ZSM-5 zeolite as a heterogeneous catalyst when utilising a biphasic solvent system composed of methyl isobutyl ketone (MIBK) and H₂O with NaCl as the phase modifier.²³ Another 89 study achieved a ~4 fold increase in LA yield from rice straw using a biphasic reaction medium 90 91 containing dichloromethane (DCM) and H₂O (DCM/H₂O, 1:1), in which the enhanced performance was attributed to the good extraction capability of DCM solvent.²⁴ However, there is 92 insufficient experimental evidence and limited understanding of critical impacts of the biphasic 93 system on LA production using the recommended green solvents. 94

This study examines LA production from bread waste using PC, GVL, and isopropanol 95 (IPA) as green co-solvent systems, i.e., PC/H₂O, GVL/H₂O, IPA/H₂O, catalysed by dilute H₂SO₄ 96 to investigate how and why an efficient yield of LA could be achieved at moderate reaction 97 conditions using these bio-derived and CO₂-derived green co-solvents. Water (100%) as the 98 greenest solvent was also evaluated as a baseline for comparison. Furthermore, this study explores 99 the application and tuning of the binary biphasic reaction medium to intensify the concentration of 100 101 the target product LA considering the potential advantages of phase separation for reactive LA 102 extraction.

103 Materials and methods

104 Bread waste and chemicals

105 Bread waste was collected from catering outlets in the Hong Kong International Airport (HKIA) and dried, ground, sieved through a 0.3 mm mesh, and stored in an airtight container for 106 further experimental use. The bread waste contains 72.6% available carbohydrates, 4.2% total 107 dietary fibre, 14.8% protein, 6.1% total fat, 2.3% ash, and 41.5% total organic carbon (TOC) on a 108 dry mass basis.¹³ Solvents were purchased as follows, PC (99%, Aladdin), IPA (99%, Honeywell), 109 and GVL (99%, Sigma-Aldrich). The standard chemical/compounds for calibration of the 110 analytical equipment and catalytic reaction included glucose (99%, UNI-chem, China); fructose 111 (≥99%) and maltose monohydrate (98%) (WAKO); levoglucosan (LG) (Fluorochem); LA (98%), 112 and formic acid (FA) (98%) (Alfa Aesar); furfural (99%) and HMF (≥99%, Sigma Aldrich); and 113 H₂SO₄ (98%, Honeywell Fluka). All standard chemicals were used as received. 114

115 Catalytic conversion

The catalytic conversion of bread waste substrate was performed under microwave heating 116 117 in a microwave reactor (Ethos Up Microwave Reactor, Milestone, maximum power of 1.9 kW) following the method reported in our recent studies.^{13,20} To perform catalytic tests using a 118 monophasic system, 0.5 g bread waste (5 wt/v%), a mixture of organic solvent (PC/GVL/IPA) and 119 water (total volume 10 ml; solvent ratio 1:1 for monophasic reaction), and 0.5 M H₂SO₄ were 120 loaded in Teflon vessel and sealed, then heated to reach the desired reaction temperature (110-121 150°C) following a constant ramp rate (32°C min⁻¹), followed by a holding stage for 1-20 min, and 122 cooling down for 20-30 min using mechanical ventilation. Each experimental run was conducted 123 in duplicates to ensure reliable analysis. The reaction conditions were selected based on the latest 124 studies on starch-rich food waste conversion^{11,13} and adjusted if necessary based on the 125

experimental observations. To substantiate the experimental results obtained in PC/H_2O solvent, additional tests under the selected conditions were conducted using propylene glycol (PG) and water (PG/H₂O, 1:1) for comparison.

After analysing the results obtained from different monophasic solvent systems, GVL/H₂O 129 and IPA/H₂O solvents were investigated for biphasic reactions. As GVL and IPA are completely 130 miscible in water, 30 wt%_(aq) NaCl was applied as a phase modifier to prepare the biphasic 131 system,^{21,25} and catalytic tests were conducted following the conditions mentioned above. It is 132 noted that the concentration of H₂SO₄ refers to the whole solvent system (i.e., consistent for all 133 experimental runs with different solvents, both monophasic and biphasic), whereas the 134 concentration of NaCl refers to the reaction phase only, which is denoted as $NaCl_{(aq)}$. To analyse 135 the influence of the reaction phase and extraction phase on catalytic performance in the biphasic 136 system, different ratios of water and organic solvent (1:1, 1:3, 3:1) were applied for the conversion. 137 Control runs without bread waste substrate were performed for solvent systems under the selected 138 conditions. Standard thermocouple and pressure data-logger were used during catalytic reactions 139 to monitor and record the in-vessel reaction temperature and autogenous pressure, respectively. 140

141 Analysis of samples

Soluble samples were obtained from each replicate, diluted with deionised water (DIW), and filtered through a membrane filter (0.45 μ m) before analysis. For biphasic reactions, samples were obtained from each layer and prepared separately for analysis after dilution in DIW. Highperformance liquid chromatography (HPLC) consisting of a Chromaster instrument equipped with Aminex HPX-87H column (Bio-Rad) and a refractive index detector (Hitachi, Japan) was used to analyse the soluble products; 0.01 M H₂SO₄ was used as the mobile phase at 0.5 ml min⁻¹ flow rate at 50 °C.^{10,26} To ensure reliable analysis, spiked samples with known concentrations of standard

compounds were injected before analysing the experimental samples. The yield of products was
calculated based on the carbon content (Eq. (1)) of the bread waste substrate.¹³

151
$$Product yield (C mol\%) = \frac{Conc_p (mg ml^{-1}) \times Vol (ml)/MW_p \times C_p}{C_s (mol)} \times 100 \quad (1)$$

Where $Conc_p$ denotes the concentration of products (including disaccharide, glucose, fructose, LG, HMF, LA, FA, and furfural); MW_p and C_p represent the molecular mass and number of carbons in the related product, respectively; C_s represents the total number of organic carbons in the substrate, which is 17.3 mmol for 0.5 g of bread waste. A volume loss of 5-15% (following various reaction duration) was recorded for PC/H₂O solvent, which was taken into account for calculating the soluble product yields. For biphasic systems, partition coefficients (R_x) for a particular product such as LA (R_{LA}) and FA (R_{FA}) were calculated following Eq. (2),

159 Partition coefficient
$$(R_x) = \frac{C \mod \% \text{ of product in the organic layer}}{C \mod \% \text{ of product in the aqueous layer}}$$
 (2)

160 Post-reaction solid residues were collected through centrifugation and decantation; washed with DIW three times and oven-dried for 48 h at 60°C and then ground as a powder for further 161 analysis using ¹³C nuclear magnetic resonance (NMR). Solid ¹³C NMR were recorded with bulk 162 powder samples on a Jeol JNM-ECZ500R MHz spectrometer operating at a resonance frequency 163 of 125 MHz. A commercial 3.2 mm magic-angle spinning (MAS) NMR probe was used with a 164 standard cross-polarisation MAS (CPMAS) pulse sequence. The MAS frequency was 10 kHz with 165 relaxation delay, scan times, and contact time at 5 s, 1200-2000, and 2 ms, respectively. Liquid 166 samples subjected to the selected reaction conditions were also analysed by ¹³C NMR using D₂O 167 solution. Chemical shifts (δ) were given in ppm and measured relative to tetramethylsilane (TMS) 168 as the internal standard. The solid residues were also characterised by X-ray diffraction (XRD) 169

- 170 (Rigaku Smatlab, 5° to 50° 2 θ , rate: 10° min⁻¹ at 45 kV and 200 mA) and the crystallinity index
- 171 (*CrI*) was calculated from XRD patterns following the method reported in the literature.²⁷

172 Results and discussion

173 Catalytic conversion of bread waste under bio-derived and CO₂-derived solvents

Facile conversion of bread waste was achieved under moderate reaction conditions, 174 obtaining 45-72 mol% total product yield at 130°C under bio-derived and CO₂-derived co-solvent 175 systems (Fig. 1a). For H₂O, PC/H₂O, and GVL/H₂O solvents, the maximum total sugars released 176 from bread waste were 64-70 mol% in a short reaction duration of 1 min (Fig. S1a). In contrast, 177 using IPA/H₂O, the total sugar yield after 1 min of reaction was 43.5 mol%, increasing up to 48.8 178 179 mol% when the reaction was prolonged for 20 min. Given the total sugar yield generated at 110°C (Fig. 1b), hydrolysis of bread waste was faster in GVL/H₂O (48.1 mol%) and PC/H₂O (53.7 mol%) 180 compared to H₂O (~30 mol%) and IPA/H₂O (9.4 mol%). With increasing reaction duration up to 181 182 20 min, sugar yield in H₂O and IPA/H₂O remained steady and generated an insignificant LA yield \sim 1.5 mol% after 20 min of reaction. In contrast, sugars were consumed, and LA vield increased 183 with increasing reaction duration gradually in GVL/H₂O (up to 4.8 mol%) and sharply in PC/H₂O 184 (up to 19.6 mol%) (Fig. 1a). ¹³C NMR spectra of reacted solutions (1 and 20 min reaction) (Fig. 185 2a) provided further evidence for the disparity in catalytic conversion under different solvent 186 systems. ¹³C NMR chemical shift (δ) at 95.8 ppm, attributed to glucose,²⁸ was observed for all 187 reactions. The highest intensity of glucose peak was observed for 1 min reacted solution in 188 189 PC/H₂O, which agrees with the maximum sugar yield measured by HPLC. In contrast, the lowest intensity of glucose peak and emerged LA peak (at 27.7, 37.6, 177 pm) along with an FA peak (at 190 165.45 ppm)²⁹ for 20 min reaction in PC/H₂O further prove the efficient tandem catalysis in 191 PC/H₂O. The characteristic peaks for LA and FA were not detectable in IPA/H₂O and H₂O, while 192

193 low-intensity peaks could be observed for GVL/H_2O . Besides, representative solvent peaks ²⁹ were 194 detected in the reacted solutions indicated in **Fig. 2a**.

The higher soluble product yields in PC/H₂O and GVL/H₂O (Fig. 1b) could be related to 195 the high reactivity of the Brønsted acid catalyst due to the availability of highly active proton in 196 the presence of aprotic co-solvents in the reaction system.^{13,30} The extent of proton stabilisation 197 influences the acid dissociation constant, and in water lowers the proton reactivity, which 198 subsequently elevates the required energy level for acid-catalysed biomass conversion reactions 199 such as hydrolysis and dehydration.³⁰ Therefore, reaction kinetics could be slower in H₂O (100%) 200 compared to a solvent system consisting of a polar aprotic solvent such as GVL and PC, which 201 might enhance the reaction rates owing to reactive proton and facile glycosidic bond cleavage.^{20,31} 202 For instance, a recent study reported a ten-fold increase in reaction rate for acid-catalysed 203 conversion of HMF to LA using GVL with 10% H₂O compared to 100% H₂O as solvent.³² Slower 204 conversion of bread waste was observable in the case of IPA/H₂O solvent (total sugar ~10 mol%, 205 at 110°C, 1 min) (Fig. 1b), where both co-solvents are protic and probably hamper the proton 206 reactivity during conversion. 207

208 The starch contained in the bread waste substrate represents a complex structure combining 209 linear amylose chains and highly branched amylopectin comprising $\alpha(1\rightarrow 4)$ and $\alpha(1\rightarrow 6)$ glycosidic bonds. ¹³C NMR spectra of solid residues (Fig. 2b) subjected to reaction under different 210 solvent systems (20 min) showed differences in chemical shifts than the untreated bread waste, 211 possibly related to the changes in starch structures.³³ The chemical shifts observed at resonance 212 values of 93-103, 74-85, 64-73, 55-60 ppm can be attributed to C1, C4, C2,3,5, and C6 of glucose 213 units, respectively.^{11,34} Resonance values attributed to C1 and C4 can be helpful to understand the 214 changes in the amorphous and highly ordered/crystalline state of starch. The C1 resonance for 215

post-reaction solid residues shifted toward 98-103 ppm, presenting comparatively sharp peaks 216 217 compared to the broad peak observed at 93-100 ppm for untreated bread waste. The broad shoulder observed around 95 ppm for untreated bread waste is characteristic of the amorphous domain of 218 C1. In contrast, a sharp peak observed around 100 ppm (C1) for solid residues might indicate a 219 decrease in amorphous content and a subsequent rise in relative crystallinity, which was previously 220 reported for acid-modified starch.³⁴⁻³⁵ In contrast, the resonance for C4 around 82 ppm was 221 observed for solid residues, characteristic of an amorphous state.³⁶ Different changes in chemical 222 shifts in different carbon regions can reflect varied transformations between amylose and 223 224 amylopectin within the starch structures. Amylose is mainly amorphous and more susceptible to acid hydrolysis than amylopectin, which comprises highly ordered/crystalline domain building 225 double-helical structures. However, initially during acid hydrolysis, amorphous amylose could be 226 partially transformed into double helices resistant to acid hydrolysis, and consequently, crystalline 227 content could be enhanced relative to amorphous content.³⁷⁻³⁸ The observed changes in solid 228 residues compared to untreated bread waste was substantiated by XRD analysis. The XRD pattern 229 of untreated bread waste (Fig. S2) showed a broad crystalline peak at $\sim 2\theta = 20^\circ$, and the calculated 230 CrI value was ~0.51, whereas solid residues in different solvent systems provided CrI values 231 ranging $\sim 0.73-0.78$. This also suggested the rapid decomposition of amorphous region of starch 232 granules during acid hydrolysis resulting in an increased relative crystallinity.²⁷ 233

234

235 LA yield enhanced by in-vessel high pressure generated in PC/H₂O

Comparing different co-solvent systems, PC/H2O was found to be the best for LA 236 production, generating 19.6 mol% after 20 min reaction at 130°C (Fig. 1a), which is promising 237 considering mild reaction conditions used in this study and the reported literature results under 238 comparable experimental conditions.^{9,39} Under GVL/H₂O solvent, sugars depleted gradually 239 during 3-20 min of reaction and generated 2-4.8 mol% LA. In contrast, in PC/H₂O solvent, sugars 240 started to deplete rapidly during 3-20 min of reaction, and 19.6 mol% LA yield was achieved after 241 20 min. A significant in-vessel pressure build-up was recorded during reaction in PC/H₂O, 242 reaching a maximum ~27 bar at 130°C, 20 min compared to reactions in other solvents (Fig. 3a). 243 Compared to the autogenous in-vessel pressure (~13 bar) generated in PC/H₂O during 1 min 244 reaction, the reaction pressure level almost doubled (~23-27 bar) during 3-20 min reaction (Fig. 245 **3b**), which was analogous to rapid sugar consumption and a sharp increase in LA yield (4-19.6 246 mol%) during 3-20 min. In acidic conditions, PC solvent could decompose into PG and CO₂ as 247 reported in the literature.^{13,40} Noticeably, ~5-15% solvent loss was recorded for reactions in 248 PC/H₂O (1-20 min), indicating that a fraction of the PC solvent was decomposed during the 249 reaction. Besides, ¹³C NMR spectra (Fig. 2a) for the reacted solutions under PC/H₂O (1 and 20 250 min) showed peaks at 66.4 and 67.7 ppm representing PG.²⁹ The PG peaks had comparatively 251 higher intensity after 20 min reaction than 1 min, suggesting that a higher fraction of PC was 252 253 decomposed to PG, which was consistent with higher CO₂ pressure recorded for more prolonged 254 reactions in PC/H₂O (Fig. 3b).

Apart from the aprotic nature of the PC solvent, significant pressure build-up resulting from CO₂ generation during catalytic conversion in PC/H_2O might enhance the LA production rate. Another influential factor could be the increased acidity due to carbonic acid derived from partial

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dissolution of CO_2 during the reaction, which might enhance sugar dehydration.⁴¹ Solution acidity can arise through *in situ* formation and dissociation of carbonic acid, as given in Eq. (3).⁴²

260

$$\rm CO_2 + 2H_2O \iff \rm HCO_3^- + H_3O^+$$

261 $HCO_3^- + H_2O \leftrightarrow CO_3^{2-} + H_3O^+$ (3)

The acidity (pH) associated with CO₂ generated during 3-20 min reaction in PC/H₂O was 262 estimated, following the scheme reported in the literature.⁴³⁻⁴⁴ The estimated CO₂-derived pH 263 value for specified reaction conditions was \sim 3.5, i.e., considerably higher than the H₂SO₄ derived 264 pH (~0.5) in this study. Therefore, CO₂-derived pH on its own might not be sufficient to catalyse 265 tandem reactions and significantly enhance LA yield. In other words, LA yield might be improved 266 267 probably by PC/H₂O generated CO₂ pressure more than CO₂-derived acidity during the catalytic conversion of bread waste. To testify this postulation, an additional test using PC/H₂O was 268 269 conducted, in which autogenous pressure developed due to PC degradation (~22 bar) was released 270 after 5 min reaction, and then the solution underwent reaction for another 15 min (Fig. 3c). Compared to continuous 20 min reaction in PC/H₂O (LA yield 19.6 mol%), only about half of LA 271 was produced (LA yield 11.2 mol%) when the pressure was released prematurely during the 272 reaction. After the pressure release, the autogenous pressure was \sim 4.2 bar from the beginning till 273 the end point of additional 15-min reaction. Moreover, supplementary tests using PG/H₂O only 274 275 generated ~3 mol% LA yield (130°C, 20 min) (Fig. 3d), which was insignificant compared to LA yield obtained in PC/H₂O, therefore disproving any favourable influences by PG solvent 276 277 (decomposed from PC) on the catalytic performance. These experimental evidences confirm the 278 crucial enhancement of reaction pressure on the catalytic LA production.

279 Intensification of LA yield through phase separation

Among co-solvent systems, PC/H₂O generated the highest LA yield 19.6 mol% at 130°C, and 280 ~9 mol% soluble sugar remained after a 20 min reaction. In contrast, ~47-49 mol% soluble sugar 281 was available after 20 min reaction in GVL/H₂O and IPA/H₂O (Fig. 1a), which could be further 282 converted to LA or other sugar derivatives. To improve the catalytic performance in GVL/H₂O 283 and IPA/H₂O, conversion of bread waste was conducted at 150°C for 1-20 min reaction duration 284 (Fig. 4a&b). As higher temperature provided more energy for the reaction, LA yield increased 285 gradually up to 16.4 mol% in GVL/H₂O (150°C, 20 min) (Fig. 4b), which was more than three 286 287 times higher than the maximum LA yield achieved at 130°C (4.8 mol%, 20 min). The maximum LA yield achieved in IPA/H₂O was only 6.6 mol% (150°C, 20 min) (Fig. 4a), notably lower than 288 GVL/H₂O system, corroborating the positive role of aprotic GVL solvent in enhancing proton 289 reactivity for less energy-intensive tandem catalysis.^{10,30} 290

The biphasic solvent systems (prepared using 30 wt% NaCl_(a0)) were further investigated 291 292 as an intensification scheme to improve the concentration of the target product LA in this study. 293 Promisingly, the concentration of LA at the end of the reaction (150°C, 20 min) increased ~1.6 294 times in both biphasic GVL/H₂O and IPA/H₂O systems (Fig. 4c) compared to analogous 295 monophasic systems. Though total soluble product yields were comparable in the two biphasic systems (~33-35 mol%) (Fig. S1b), the distributions of soluble products were distinctive between 296 GVL/H₂O and IPA/H₂O. While biphasic GVL/H₂O selectively generated LA as the main product 297 298 26.8 mol% yield and 4.4 mol% FA as co-product, IPA/H₂O biphasic contained 10.6 mol% LA, 2.6 mol% FA, ~7 mol% HMF, and 10.2 mol% remaining sugars (glucose and fructose) (Fig. 4c). A 299 considerable fraction of HMF present in both monophasic and biphasic IPA/H₂O indicated that 300 the solvent could hinder the HMF rehydration to LA. In comparison to DMSO, which is a widely 301

302	recommended solvent for HMF production, IPA can create a shielding effect around HMF that
303	helps to prevent its rehydration and suppress further conversion to byproducts such as insoluble
304	humins. ⁴⁵⁻⁴⁶ A recent study revealed that the rate constant for fructose to HMF was considerably
305	higher than that of HMF to degradation products when IPA was present in the solvent system, ⁴⁶
306	echoing the experimental observations in this study where low LA selectivity was obtained in
307	IPA/H ₂ O solvent system. In other words, IPA/H ₂ O could be considered as a potential solvent for
308	HMF production in future investigations. By contrast, in the presence of GVL solvent, $\mathrm{H_2SO_4}$
309	catalysed HMF production could be rapid and readily converted to LA at high acid strength. ⁴⁷
310	Considerable LA yield achieved in biphasic GVL/H ₂ O in this study (26.8 mol%, at 150°C, 20 min)
311	proves the high efficiency of $H_2SO_4/GVL/H_2O$ system for LA production.

As GVL/H₂O biphasic solvent was the most efficient for intensifying LA yield at moderate 312 conditions, a comprehensive investigation was conducted for bread waste conversion in the co-313 solvent system following varied reaction conditions (150°C, 10-20 min). In biphasic GVL/H₂O, 314 LA yield increased with increasing reaction duration (~19-28 mol% in 10-15 min) (GVL/H₂O, 315 1:1) (Fig. 5a). However, a slight decrease in LA yield was observed after 20 min, suggesting that 316 LA started to degrade with prolonged reaction. The major product in monophasic $GVL/H_2O(1:1,$ 317 15 min) was glucose (34.6 mol%), while the biphasic system selectively generated LA (~28 mol%) 318 319 as the major product. The LA yield increased up to ~2.5 times in the biphasic system compared to the monophasic one (~11 mol%) (150°C, 15 min), implying that phase separation could be 320 321 beneficial for intensive LA production and upscaling to industrial scale.

Essentially, to develop an efficient biphasic reaction medium, it is necessary to understand the contribution and influences of the reaction phase (H_2O) and the extraction phase (GVL) to optimise the yield of the target product. To tune the reaction and extraction phases in GVL/H_2O

biphasic system, catalytic tests were conducted with various ratios of GVL and H₂O (1:1, 1:3, and 325 3:1 of GVL/H₂O). The partition coefficient for LA (R_{LA}) in the GVL/H₂O biphasic solvent was 326 calculated to evaluate the effect of the extraction phase (GVL) in the system. The R_{LA} achieved for 327 10-15 min reaction was 4.2 when 1:1 GVL/H₂O was applied for reaction (Fig. 5b), indicating a 328 higher distribution of LA in the organic phase compared to the aqueous phase. Therefore, GVL 329 330 solvent can be considered highly effective for reactive LA extraction. The partitioning of LA obtained in this study (R_{LA} 4.2) is comparable to a previous study that reported R_{LA} ranging 3.7-4 331 using cellulose as feedstock.²¹ 332

The total yield of LA increased (27.4-32 mol%) when a higher fraction of H_2O (1:3, 333 334 GVL/H₂O) was applied during catalytic conversion, whereas the total LA yield decreased (14.5-17.1 mol%) when a lower fraction of H_2O (3:1, GVL/H_2O) was applied (Fig. 5b). Though the total 335 LA yield increased with a higher fraction of H₂O, the extraction of LA was found to be inefficient. 336 The partition coefficient achieved was only 1.1 (1:3, GVL/H₂O), indicating nearly even 337 distribution of produced LA in the reaction and extraction phases due to the lower fraction of GVL 338 applied. In comparison, ~97% of the total LA produced was extracted into the GVL phase when a 339 higher fraction of GVL (3:1, GVL/H₂O) was applied for reaction. However, a considerable 340 341 decrease in total LA yield was observed, possibly due to the lack of sufficient aqueous phase 342 available for reaction. These observations suggested the indispensable contribution of both reaction and extraction phases for an efficient biphasic system for LA production. Considering LA 343 yield (27.4 mol%) and R_{LA} (4.2), the 1:1 GVL/H₂O biphasic system (150°C, 15 min) provided the 344 345 best performance for intensive LA production.

To reflect further on the mechanism and roles of catalytic species in NaCl modified
GVL/H₂O biphasic system, additional tests were performed under the selected reaction conditions.

In the case of reaction conducted with only NaCl (30 wt%) without acid catalyst, only marginal 348 product yield was observed (Fig. 6a). When NaCl was applied together with H₂SO₄ for bread 349 waste conversion, an increase in LA yield was observed compared to the reaction in the presence 350 of H₂SO₄ without salt addition. These observations indicate that NaCl alone could not catalyse the 351 desired reaction yet it may act synergistically with H₂SO₄ enhancing the LA production in the 352 aqueous phase during biphasic conversion of bread waste. Product distributions in the aqueous and 353 GVL phases in the specified reaction conditions are provided in Fig. S3. The synergistic catalysis 354 by NaCl and H₂SO₄ together with simultaneous efficient extraction of LA into GVL could account 355 356 for the high LA yield obtained in the GVL/H₂O biphasic system.

357 Moreover, the recyclability of the aqueous phase containing H₂SO₄ was investigated. After the catalytic run (reaction and cooling), the reacted organic phase was removed and fresh GVL 358 and bread waste substrate were applied for another cycle of catalytic reaction (run-2) again while 359 360 retaining the aqueous phase from the previous run without adding extra H₂SO₄. Similarly, the third cycle of catalytic reaction (run-3) was conducted. In the 2nd and 3rd run (Fig. 6b), 15 mol% and 13 361 mol% LA was obtained, respectively, compared to the LA yield (28 mol%) obtained in the initial 362 run, which suggested that the acid catalyst could be retained in the aqueous phase and recycled for 363 further conversion, though a certain degree of decrease in LA yield was observed. Future studies 364 365 would be required for evaluating the biphasic system in a continuous reaction mode, which may be more efficient compared to the batch reaction mode. 366

Apart from LA as the target product, FA yield was analysed for bread waste conversion in monophasic and biphasic GVL/H₂O, as FA is often co-produced during biomass conversion.⁴⁸ Similar to LA, the FA yield was enhanced through phase separation with the yield from ~2-3 mol% in the monophasic system to a maximum 5.4 mol% FA yield in biphasic GVL/H₂O (150°C, 15 min, 1:3 solvent ratio) (**Fig. 5c**). Using 1:1 GVL/H₂O, FA partition coefficient (R_{FA}) obtained was ~2-3 (150°C, 10-20 min, solvent ratio 1:1) (**Fig. 5c**), indicating that FA could also be simultaneously extracted into the GVL layer during bread waste conversion. Besides, partition coefficients for LA, FA, and HMF were evaluated in IPA/H₂O solvent (150°C, 20 min, 1:1 solvent ratio), and the values were 6.6, 5.4, and 5.7, respectively (**Fig. S4**), corroborating an effective extraction of these compounds into the organic phase. Considering the low LA selectivity and total LA yield (10.6 mol% at 150°C, 20 min), further investigation was discontinued for IPA/H₂O.

378 Perspectives on LA production and solvent recycling

To evaluate the efficiency of the catalytic system for LA production, LA yield relative to 379 theoretical LA yield of bread waste substrate (considering total available carbohydrate and 380 possible maximum theoretical yield (64.5%)) was calculated and compared with the reported 381 achievements with commercially available starch substrates in the existing literature (Table 1). 382 383 For PC/H₂O (130°C, 20 min) and GVL/H₂O biphasic solvents (150°C, 15 min), 45.7% and 66% LA yield was achieved relative to theoretical yield, respectively. This is considered promising in 384 comparison to the reported LA yield (45.6-66.4%) from commercially available starch substrates 385 in previous studies⁴⁹⁻⁵⁰ where the conversion was conducted using comparatively harsh reaction 386 conditions. For other recent studies where no direct comparison is possible due to the lack of data 387 regarding relative LA yield,^{17,51} it should be noted that much longer reaction duration was required 388 to obtain the reported LA yield. 389

The recyclability of GVL/H_2O biphasic solvent was investigated and discussed in the previous section. For PC/H₂O solvent, despite partial decomposition of PC during acid catalysis, it offers various advantages as a solvent because a high product yield can be obtained with a moderate temperature and a short duration, which play a critical role in reducing the energy

consumption and reactor size. The production of PC from CO₂ is beneficial for process economy 394 and environmental sustainability in terms of CO₂ utilisation. In the application of PC solvent, the 395 derived CO₂ after reaction can be captured and recycled for PC production or other CO₂ based 396 biorefineries, which are conducive to fostering the circular economy. The spent organic solvents 397 can be recycled after separation and purification following commonly used techniques such as 398 399 fractional distillation. For instance, a comprehensive life cycle assessment (LCA) on solvent waste recovery⁵² demonstrated that implementing a solvent recovery system can reduce the 400 environmental footprint of the total solvent manufacturing, usage, and disposal process. The 401 402 energy requirements and emissions associated with the solvent recovery process have been recognised to be trivial in comparison to the emissions due to virgin solvent production and spent 403 solvent disposal by incineration. 404

405 **Conclusions**

This study provides comprehensive insights into the critical factors for intensive LA 406 production, which can be conducive to the technology scale-up. The bio-derived and CO₂-derived 407 co-solvents in this study, i.e., PC/H₂O, GVL/H₂O, IPA/H₂O, could facilitate H₂SO₄ catalysed 408 tandem reactions during bread waste conversion but demonstrated varied catalytic efficiency. 409 410 PC/H₂O solvent was the most efficient for LA production using moderate reaction conditions, which could be attributed to the CO₂ pressure generated *in situ* through solvent (PC) degradation. 411 Besides, catalytic performance could be significantly enhanced in GVL/H₂O and IPA/H₂O using 412 413 the biphasic system, facilitating reactive extraction of LA in the organic layer that intensified the final concentration of LA. GVL/H₂O biphasic solvent seems promising considering LA yield (28 414 mol%) and LA partitioning (R_{LA} 4.2) achieved in the study. The bio-derived and CO₂-derived 415

- 416 solvents applied in this study can be considered as emerging solvents and potential alternatives to
- 417 common industrial solvents in future biorefinery applications.

418

419 Supplementary information

420 The supplementary information is available online.

421

422 **Conflicts of interest**

423 The authors declare no conflict of interest.

424

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Critical factors for levulinic acid production from starch-rich food
waste: Solvent effects, reaction pressure, and phase separation
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Abstract

A considerable amount of food waste generated globally could be upcycled to synthesise platform 16 chemicals to enhance environmental sustainability and help realise a circular economy. This study 17 investigates the catalytic production of the vital platform molecule levulinic acid (LA) from bread 18 waste, a typical stream of starch-rich food waste generated worldwide. Gamma-valerolactone 19 20 (GVL), isopropanol (IPA), and propylene carbonate (PC) were evaluated as bio-derived and CO₂derived green co-solvents for LA synthesis. In-vessel pressure generated in PC/H₂O (1:1) solvent 21 was conducive to rapid LA production from bread waste compared to GVL/H₂O and IPA/H₂O. In 22 PC/H₂O, 72 mol% total soluble product yield was observed quickly within 1 min in moderate 23 reaction conditions (130°C, 0.5 M H₂SO₄), whereas ~15-20 mol% of LA could be obtained when 24 the reaction was prolonged for 10-20 min at 130°C. The yield of LA could be significantly 25 enhanced in GVL/H₂O through phase separation using NaCl (30 wt%_(aq)). LA yield increased up 26 to a maximum of ~2.5 times in the biphasic system (28 mol%, 150°C, 15 min) (representing a 27 28 theoretical yield of 66%) in GVL/H_2O (1:1) compared to the monophasic system (~11 mol%) under the same reaction conditions. The partition coefficient for LA achieved was 4.2 in the 29 GVL/H₂O (1:1) biphasic medium, indicating that the system was efficient for simultaneous 30 production and extraction of LA. Biphasic GVL/H₂O facilitated selective LA production, which 31 could be optimised by tuning the reaction conditions. These new insights can foster the 32 development of high-performance LA production and sustainable biorefinery. 33

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Keywords: Waste recycling/management; Platform chemicals; Green solvents; Extractive
separation; Sustainably biorefinery; Circular economy.

38 Introduction

Appropriate and sustainable management of the growing amount of food waste is a big 39 issue in modern society. Approximately 931 million tonnes of food waste were globally generated 40 in the year of 2019 at the retail and consumer level (households and commercial food services). 41 excluding food loss during post-harvest to distribution in the food supply chain.¹ Such an enormous 42 amount of food waste requires proper handling to minimise pollution risks and be diverted from 43 landfill disposal.² Transforming food waste into platform chemicals offers a sustainable 44 opportunity to utilise the vast waste stream for biorefinery applications and pave the way forward 45 to realising a circular bioeconomy.³ 46

Levulinic acid (LA) is one of the top bio-derived platform chemicals with various 47 applications, e.g., pharmaceuticals, plasticisers, solvents, fuels, and personal care products.⁴⁻⁵ 48 Besides, LA serves as a building block for the production of various value-added derivatives such 49 as gamma-valerolactone (GVL),⁶ succinic acid, diphenolic acid,⁷⁻⁸ alkyl levulinates, 2-methyl-50 tetrahydrofuran, etc.⁵ Considering the low cost and high catalytic activity for tandem hydrolysis 51 52 and dehydration reactions, mineral acids such as H_2SO_4 and HCl are generally used for LA production from diverse biomass feedstock including food waste, paper waste, etc.⁹⁻¹⁰ Starch-rich 53 foods such as rice, bread, and potatoes are commonly consumed and constitute a significant 54 proportion of global food waste,¹¹ which can serve as a potential feedstock for biorefineries. Recent 55 studies demonstrated that catalytic production of sugars and platform chemicals could be an 56 effective technique for recycling/valorising a considerable amount of starch-rich food waste 57 generated globally.¹²⁻¹³ In this study, bread waste serves as the representative starch-rich feedstock 58 for the catalytic production of LA. 59

Appropriate reaction conditions and solvent selection are critical for selective and cost-60 effective LA production.¹⁴ As the greenest and environmentally benign solvent, water has been 61 used as a reaction medium for LA synthesis. However, harsh reaction conditions, i.e., high 62 temperature and acidity, are required when using water as the reaction medium resulting in an 63 energy-intensive process and high byproduct (humin) formation.¹⁵ The selection of a suitable 64 solvent is necessary, as it not only serves as a reaction medium, but also influences the catalytic 65 process through solvent-solute interactions, adjusting the reactivity of proton, suppressing the 66 byproduct formation, etc.^{13,16} Owing to the need for selective and high-efficiency chemical 67 synthesis, various organic solvents as reaction medium have been widely investigated, such as 68 dimethylsulfoxide (DMSO),⁹ tetrahydrofuran (THF), dimethylformamide (DMF),⁷ GVL, acetone, 69 etc.^{10,17} However, conventional organic solvents DMSO, DMF, THF, etc., are widely considered 70 "non-green" due to their direct or indirect detrimental effects on the natural environment and 71 human health and safety. Therefore, the use of alternative "green" solvents, and especially those 72 which are renewable and bio-derived (GVL, alcohols, etc.) or CO₂-derived (propylene carbonate 73 (PC), dimethyl carbonate (DMC), etc.), are recommended for future applications.¹⁸⁻¹⁹ Furthermore, 74 enhanced catalytic conversion of biowaste using these bio-derived and CO₂-derived solvents was 75 reported in recent studies, ^{10,13,20} yet their influences should be evaluated in comparable conditions 76 to validate their efficiency and elucidate the critical factors for catalytic LA production. 77

Apart from using environmentally friendly and safe reaction systems, process intensification is indispensable to improve the final concentration of LA for scaling up at the industrial level.¹⁴ Efficient separation and purification of LA are necessary for the possible recovery of mineral acid catalyst and further conversion of LA to valuable derivatives such as GVL, which can be negatively affected by the presence of mineral acid.^{17,21} A viable strategy could

be using the biphasic solvent system comprising two immiscible layers. The aqueous layer 83 contains the acid catalyst and serves as the reactive phase, while the organic layer acts as the 84 extractive phase, facilitating simultaneous production and extraction of LA, which might enhance 85 LA vield and selectivity.²¹⁻²² For instance, a recent study on the conversion of remnant algal 86 biomass reported a significant enhancement of hydroxymethylfurfural (HMF) and LA yield using 87 88 acidic ZSM-5 zeolite as a heterogeneous catalyst when utilising a biphasic solvent system composed of methyl isobutyl ketone (MIBK) and H₂O with NaCl as the phase modifier.²³ Another 89 study achieved a ~4 fold increase in LA yield from rice straw using a biphasic reaction medium 90 91 containing dichloromethane (DCM) and H₂O (DCM/H₂O, 1:1), in which the enhanced performance was attributed to the good extraction capability of DCM solvent.²⁴ However, there is 92 insufficient experimental evidence and limited understanding of critical impacts of the biphasic 93 system on LA production using the recommended green solvents. 94

This study examines LA production from bread waste using PC, GVL, and isopropanol 95 (IPA) as green co-solvent systems, i.e., PC/H₂O, GVL/H₂O, IPA/H₂O, catalysed by dilute H₂SO₄ 96 to investigate how and why an efficient yield of LA could be achieved at moderate reaction 97 conditions using these bio-derived and CO₂-derived green co-solvents. Water (100%) as the 98 greenest solvent was also evaluated as a baseline for comparison. Furthermore, this study explores 99 the application and tuning of the binary biphasic reaction medium to intensify the concentration of 100 101 the target product LA considering the potential advantages of phase separation for reactive LA 102 extraction.

Materials and methods

104 Bread waste and chemicals

105 Bread waste was collected from catering outlets in the Hong Kong International Airport (HKIA) and dried, ground, sieved through a 0.3 mm mesh, and stored in an airtight container for 106 further experimental use. The bread waste contains 72.6% available carbohydrates, 4.2% total 107 dietary fibre, 14.8% protein, 6.1% total fat, 2.3% ash, and 41.5% total organic carbon (TOC) on a 108 dry mass basis.¹³ Solvents were purchased as follows, PC (99%, Aladdin), IPA (99%, Honeywell), 109 and GVL (99%, Sigma-Aldrich). The standard chemical/compounds for calibration of the 110 analytical equipment and catalytic reaction included glucose (99%, UNI-chem, China); fructose 111 (≥99%) and maltose monohydrate (98%) (WAKO); levoglucosan (LG) (Fluorochem); LA (98%), 112 and formic acid (FA) (98%) (Alfa Aesar); furfural (99%) and HMF (≥99%, Sigma Aldrich); and 113 H₂SO₄ (98%, Honeywell Fluka). All standard chemicals were used as received. 114

115 Catalytic conversion

The catalytic conversion of bread waste substrate was performed under microwave heating 116 117 in a microwave reactor (Ethos Up Microwave Reactor, Milestone, maximum power of 1.9 kW) following the method reported in our recent studies.^{13,20} To perform catalytic tests using a 118 monophasic system, 0.5 g bread waste (5 wt/v%), a mixture of organic solvent (PC/GVL/IPA) and 119 water (total volume 10 ml; solvent ratio 1:1 for monophasic reaction), and 0.5 M H₂SO₄ were 120 loaded in Teflon vessel and sealed, then heated to reach the desired reaction temperature (110-121 150°C) following a constant ramp rate (32°C min⁻¹), followed by a holding stage for 1-20 min, and 122 cooling down for 20-30 min using mechanical ventilation. Each experimental run was conducted 123 in duplicates to ensure reliable analysis. The reaction conditions were selected based on the latest 124 studies on starch-rich food waste conversion^{11,13} and adjusted if necessary based on the 125

experimental observations. To substantiate the experimental results obtained in PC/H_2O solvent, additional tests under the selected conditions were conducted using propylene glycol (PG) and water (PG/H₂O, 1:1) for comparison.

After analysing the results obtained from different monophasic solvent systems, GVL/H₂O 129 and IPA/H₂O solvents were investigated for biphasic reactions. As GVL and IPA are completely 130 miscible in water, 30 wt%_(aq) NaCl was applied as a phase modifier to prepare the biphasic 131 system,^{21,25} and catalytic tests were conducted following the conditions mentioned above. It is 132 noted that the concentration of H₂SO₄ refers to the whole solvent system (i.e., consistent for all 133 experimental runs with different solvents, both monophasic and biphasic), whereas the 134 135 concentration of NaCl refers to the reaction phase only, which is denoted as $NaCl_{(aq)}$. To analyse the influence of the reaction phase and extraction phase on catalytic performance in the biphasic 136 system, different ratios of water and organic solvent (1:1, 1:3, 3:1) were applied for the conversion. 137 Control runs without bread waste substrate were performed for solvent systems under the selected 138 conditions. Standard thermocouple and pressure data-logger were used during catalytic reactions 139 to monitor and record the in-vessel reaction temperature and autogenous pressure, respectively. 140

141 Analysis of samples

Soluble samples were obtained from each replicate, diluted with deionised water (DIW), and filtered through a membrane filter (0.45 μ m) before analysis. For biphasic reactions, samples were obtained from each layer and prepared separately for analysis after dilution in DIW. Highperformance liquid chromatography (HPLC) consisting of a Chromaster instrument equipped with Aminex HPX-87H column (Bio-Rad) and a refractive index detector (Hitachi, Japan) was used to analyse the soluble products; 0.01 M H₂SO₄ was used as the mobile phase at 0.5 ml min⁻¹ flow rate at 50 °C.^{10,26} To ensure reliable analysis, spiked samples with known concentrations of standard

compounds were injected before analysing the experimental samples. The yield of products was
calculated based on the carbon content (Eq. (1)) of the bread waste substrate.¹³

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$$Product yield (C mol\%) = \frac{Conc_p (mg ml^{-1}) \times Vol (ml)/MW_p \times C_p}{C_s (mol)} \times 100$$
(1)

Where $Conc_p$ denotes the concentration of products (including disaccharide, glucose, fructose, LG, HMF, LA, FA, and furfural); MW_p and C_p represent the molecular mass and number of carbons in the related product, respectively; C_s represents the total number of organic carbons in the substrate, which is 17.3 mmol for 0.5 g of bread waste. A volume loss of 5-15% (following various reaction duration) was recorded for PC/H₂O solvent, which was taken into account for calculating the soluble product yields. For biphasic systems, partition coefficients (R_x) for a particular product such as LA (R_{LA}) and FA (R_{FA}) were calculated following Eq. (2),

159 Partition coefficient
$$(R_x) = \frac{C \mod \% \text{ of product in the organic layer}}{C \mod \% \text{ of product in the aqueous layer}}$$
 (2)

160 Post-reaction solid residues were collected through centrifugation and decantation; washed with DIW three times and oven-dried for 48 h at 60°C and then ground as a powder for further 161 analysis using ¹³C nuclear magnetic resonance (NMR). Solid ¹³C NMR were recorded with bulk 162 powder samples on a Jeol JNM-ECZ500R MHz spectrometer operating at a resonance frequency 163 of 125 MHz. A commercial 3.2 mm magic-angle spinning (MAS) NMR probe was used with a 164 standard cross-polarisation MAS (CPMAS) pulse sequence. The MAS frequency was 10 kHz with 165 relaxation delay, scan times, and contact time at 5 s, 1200-2000, and 2 ms, respectively. Liquid 166 samples subjected to the selected reaction conditions were also analysed by ¹³C NMR using D₂O 167 solution. Chemical shifts (δ) were given in ppm and measured relative to tetramethylsilane (TMS) 168 as the internal standard. The solid residues were also characterised by X-ray diffraction (XRD) 169

- 170 (Rigaku Smatlab, 5° to 50° 2 θ , rate: 10° min⁻¹ at 45 kV and 200 mA) and the crystallinity index
- 171 (*CrI*) was calculated from XRD patterns following the method reported in the literature.²⁷

172 Results and discussion

173 Catalytic conversion of bread waste under bio-derived and CO₂-derived solvents

Facile conversion of bread waste was achieved under moderate reaction conditions, 174 obtaining 45-72 mol% total product yield at 130°C under bio-derived and CO₂-derived co-solvent 175 systems (Fig. 1a). For H₂O, PC/H₂O, and GVL/H₂O solvents, the maximum total sugars released 176 from bread waste were 64-70 mol% in a short reaction duration of 1 min (Fig. S1a). In contrast, 177 using IPA/H₂O, the total sugar yield after 1 min of reaction was 43.5 mol%, increasing up to 48.8 178 179 mol% when the reaction was prolonged for 20 min. Given the total sugar yield generated at 110°C (Fig. 1b), hydrolysis of bread waste was faster in GVL/H₂O (48.1 mol%) and PC/H₂O (53.7 mol%) 180 compared to H₂O (~30 mol%) and IPA/H₂O (9.4 mol%). With increasing reaction duration up to 181 182 20 min, sugar yield in H₂O and IPA/H₂O remained steady and generated an insignificant LA yield \sim 1.5 mol% after 20 min of reaction. In contrast, sugars were consumed, and LA vield increased 183 with increasing reaction duration gradually in GVL/H₂O (up to 4.8 mol%) and sharply in PC/H₂O 184 (up to 19.6 mol%) (Fig. 1a). ¹³C NMR spectra of reacted solutions (1 and 20 min reaction) (Fig. 185 2a) provided further evidence for the disparity in catalytic conversion under different solvent 186 systems. ¹³C NMR chemical shift (δ) at 95.8 ppm, attributed to glucose,²⁸ was observed for all 187 reactions. The highest intensity of glucose peak was observed for 1 min reacted solution in 188 189 PC/H₂O, which agrees with the maximum sugar yield measured by HPLC. In contrast, the lowest intensity of glucose peak and emerged LA peak (at 27.7, 37.6, 177 pm) along with an FA peak (at 190 165.45 ppm)²⁹ for 20 min reaction in PC/H₂O further prove the efficient tandem catalysis in 191 PC/H₂O. The characteristic peaks for LA and FA were not detectable in IPA/H₂O and H₂O, while 192

193 low-intensity peaks could be observed for GVL/H_2O . Besides, representative solvent peaks ²⁹ were 194 detected in the reacted solutions indicated in **Fig. 2a**.

The higher soluble product yields in PC/H₂O and GVL/H₂O (Fig. 1b) could be related to 195 the high reactivity of the Brønsted acid catalyst due to the availability of highly active proton in 196 the presence of aprotic co-solvents in the reaction system.^{13,30} The extent of proton stabilisation 197 influences the acid dissociation constant, and in water lowers the proton reactivity, which 198 subsequently elevates the required energy level for acid-catalysed biomass conversion reactions 199 such as hydrolysis and dehydration.³⁰ Therefore, reaction kinetics could be slower in H₂O (100%) 200 compared to a solvent system consisting of a polar aprotic solvent such as GVL and PC, which 201 might enhance the reaction rates owing to reactive proton and facile glycosidic bond cleavage.^{20,31} 202 For instance, a recent study reported a ten-fold increase in reaction rate for acid-catalysed 203 conversion of HMF to LA using GVL with 10% H₂O compared to 100% H₂O as solvent.³² Slower 204 conversion of bread waste was observable in the case of IPA/H₂O solvent (total sugar ~10 mol%, 205 at 110°C, 1 min) (Fig. 1b), where both co-solvents are protic and probably hamper the proton 206 reactivity during conversion. 207

208 The starch contained in the bread waste substrate represents a complex structure combining 209 linear amylose chains and highly branched amylopectin comprising $\alpha(1\rightarrow 4)$ and $\alpha(1\rightarrow 6)$ glycosidic bonds. ¹³C NMR spectra of solid residues (Fig. 2b) subjected to reaction under different 210 solvent systems (20 min) showed differences in chemical shifts than the untreated bread waste, 211 possibly related to the changes in starch structures.³³ The chemical shifts observed at resonance 212 values of 93-103, 74-85, 64-73, 55-60 ppm can be attributed to C1, C4, C2,3,5, and C6 of glucose 213 units, respectively.^{11,34} Resonance values attributed to C1 and C4 can be helpful to understand the 214 changes in the amorphous and highly ordered/crystalline state of starch. The C1 resonance for 215

post-reaction solid residues shifted toward 98-103 ppm, presenting comparatively sharp peaks 216 compared to the broad peak observed at 93-100 ppm for untreated bread waste. The broad shoulder 217 observed around 95 ppm for untreated bread waste is characteristic of the amorphous domain of 218 C1. In contrast, a sharp peak observed around 100 ppm (C1) for solid residues might indicate a 219 decrease in amorphous content and a subsequent rise in relative crystallinity, which was previously 220 reported for acid-modified starch.³⁴⁻³⁵ In contrast, the resonance for C4 around 82 ppm was 221 observed for solid residues, characteristic of an amorphous state.³⁶ Different changes in chemical 222 shifts in different carbon regions can reflect varied transformations between amylose and 223 224 amylopectin within the starch structures. Amylose is mainly amorphous and more susceptible to acid hydrolysis than amylopectin, which comprises highly ordered/crystalline domain building 225 double-helical structures. However, initially during acid hydrolysis, amorphous amylose could be 226 227 partially transformed into double helices resistant to acid hydrolysis, and consequently, crystalline content could be enhanced relative to amorphous content.³⁷⁻³⁸ The observed changes in solid 228 residues compared to untreated bread waste was substantiated by XRD analysis. The XRD pattern 229 of untreated bread waste (Fig. S2) showed a broad crystalline peak at $\sim 2\theta = 20^\circ$, and the calculated 230 CrI value was ~0.51, whereas solid residues in different solvent systems provided CrI values 231 ranging $\sim 0.73-0.78$. This also suggested the rapid decomposition of amorphous region of starch 232 granules during acid hydrolysis resulting in an increased relative crystallinity.²⁷ 233

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235 LA yield enhanced by in-vessel high pressure generated in PC/H₂O

Comparing different co-solvent systems, PC/H₂O was found to be the best for LA 236 production, generating 19.6 mol% after 20 min reaction at 130°C (Fig. 1a), which is promising 237 considering mild reaction conditions used in this study and the reported literature results under 238 comparable experimental conditions.^{9,39} Under GVL/H₂O solvent, sugars depleted gradually 239 during 3-20 min of reaction and generated 2-4.8 mol% LA. In contrast, in PC/H₂O solvent, sugars 240 started to deplete rapidly during 3-20 min of reaction, and 19.6 mol% LA yield was achieved after 241 20 min. A significant in-vessel pressure build-up was recorded during reaction in PC/H₂O, 242 reaching a maximum ~27 bar at 130°C, 20 min compared to reactions in other solvents (Fig. 3a). 243 Compared to the autogenous in-vessel pressure (~13 bar) generated in PC/H₂O during 1 min 244 reaction, the reaction pressure level almost doubled (~23-27 bar) during 3-20 min reaction (Fig. 245 **3b**), which was analogous to rapid sugar consumption and a sharp increase in LA yield (4-19.6 246 mol%) during 3-20 min. In acidic conditions, PC solvent could decompose into PG and CO₂ as 247 reported in the literature.^{13,40} Noticeably, ~5-15% solvent loss was recorded for reactions in 248 PC/H₂O (1-20 min), indicating that a fraction of the PC solvent was decomposed during the 249 reaction. Besides, ¹³C NMR spectra (Fig. 2a) for the reacted solutions under PC/H₂O (1 and 20 250 min) showed peaks at 66.4 and 67.7 ppm representing PG.²⁹ The PG peaks had comparatively 251 higher intensity after 20 min reaction than 1 min, suggesting that a higher fraction of PC was 252 decomposed to PG, which was consistent with higher CO₂ pressure recorded for more prolonged 253 254 reactions in PC/H₂O (Fig. 3b).

Apart from the aprotic nature of the PC solvent, significant pressure build-up resulting from CO₂ generation during catalytic conversion in PC/H_2O might enhance the LA production rate. Another influential factor could be the increased acidity due to carbonic acid derived from partial

dissolution of CO_2 during the reaction, which might enhance sugar dehydration.⁴¹ Solution acidity can arise through *in situ* formation and dissociation of carbonic acid, as given in Eq. (3).⁴²

260

$$\rm CO_2 + 2H_2O \iff \rm HCO_3^- + H_3O^+$$

261 $HCO_3^- + H_2O \leftrightarrow CO_3^{2-} + H_3O^+$ (3)

The acidity (pH) associated with CO₂ generated during 3-20 min reaction in PC/H₂O was 262 estimated, following the scheme reported in the literature.⁴³⁻⁴⁴ The estimated CO₂-derived pH 263 value for specified reaction conditions was \sim 3.5, i.e., considerably higher than the H₂SO₄ derived 264 pH (~0.5) in this study. Therefore, CO₂-derived pH on its own might not be sufficient to catalyse 265 tandem reactions and significantly enhance LA yield. In other words, LA yield might be improved 266 267 probably by PC/H₂O generated CO₂ pressure more than CO₂-derived acidity during the catalytic conversion of bread waste. To testify this postulation, an additional test using PC/H₂O was 268 269 conducted, in which autogenous pressure developed due to PC degradation (~22 bar) was released 270 after 5 min reaction, and then the solution underwent reaction for another 15 min (Fig. 3c). Compared to continuous 20 min reaction in PC/H₂O (LA yield 19.6 mol%), only about half of LA 271 was produced (LA yield 11.2 mol%) when the pressure was released prematurely during the 272 reaction. After the pressure release, the autogenous pressure was \sim 4.2 bar from the beginning till 273 the end point of additional 15-min reaction. Moreover, supplementary tests using PG/H₂O only 274 275 generated ~3 mol% LA yield (130°C, 20 min) (Fig. 3d), which was insignificant compared to LA yield obtained in PC/H₂O, therefore disproving any favourable influences by PG solvent 276 (decomposed from PC) on the catalytic performance. These experimental evidences confirm the 277 278 crucial enhancement of reaction pressure on the catalytic LA production.

279 Intensification of LA yield through phase separation

Among co-solvent systems, PC/H₂O generated the highest LA yield 19.6 mol% at 130°C, and 280 ~9 mol% soluble sugar remained after a 20 min reaction. In contrast, ~47-49 mol% soluble sugar 281 was available after 20 min reaction in GVL/H₂O and IPA/H₂O (Fig. 1a), which could be further 282 converted to LA or other sugar derivatives. To improve the catalytic performance in GVL/H₂O 283 and IPA/H₂O, conversion of bread waste was conducted at 150°C for 1-20 min reaction duration 284 (Fig. 4a&b). As higher temperature provided more energy for the reaction, LA yield increased 285 gradually up to 16.4 mol% in GVL/H₂O (150°C, 20 min) (Fig. 4b), which was more than three 286 287 times higher than the maximum LA yield achieved at 130°C (4.8 mol%, 20 min). The maximum LA yield achieved in IPA/H₂O was only 6.6 mol% (150°C, 20 min) (Fig. 4a), notably lower than 288 GVL/H₂O system, corroborating the positive role of aprotic GVL solvent in enhancing proton 289 reactivity for less energy-intensive tandem catalysis.^{10,30} 290

The biphasic solvent systems (prepared using 30 wt% NaCl_(a0)) were further investigated 291 292 as an intensification scheme to improve the concentration of the target product LA in this study. 293 Promisingly, the concentration of LA at the end of the reaction (150°C, 20 min) increased ~1.6 294 times in both biphasic GVL/H₂O and IPA/H₂O systems (Fig. 4c) compared to analogous 295 monophasic systems. Though total soluble product yields were comparable in the two biphasic systems (~33-35 mol%) (Fig. S1b), the distributions of soluble products were distinctive between 296 GVL/H₂O and IPA/H₂O. While biphasic GVL/H₂O selectively generated LA as the main product 297 298 26.8 mol% yield and 4.4 mol% FA as co-product, IPA/H₂O biphasic contained 10.6 mol% LA, 2.6 mol% FA, ~7 mol% HMF, and 10.2 mol% remaining sugars (glucose and fructose) (Fig. 4c). A 299 considerable fraction of HMF present in both monophasic and biphasic IPA/H₂O indicated that 300 the solvent could hinder the HMF rehydration to LA. In comparison to DMSO, which is a widely 301

recommended solvent for HMF production, IPA can create a shielding effect around HMF that 302 helps to prevent its rehydration and suppress further conversion to byproducts such as insoluble 303 humins.⁴⁵⁻⁴⁶ A recent study revealed that the rate constant for fructose to HMF was considerably 304 higher than that of HMF to degradation products when IPA was present in the solvent system.⁴⁶ 305 echoing the experimental observations in this study where low LA selectivity was obtained in 306 307 IPA/H₂O solvent system. In other words, IPA/H₂O could be considered as a potential solvent for HMF production in future investigations. By contrast, in the presence of GVL solvent, H₂SO₄ 308 catalysed HMF production could be rapid and readily converted to LA at high acid strength.⁴⁷ 309 310 Considerable LA yield achieved in biphasic GVL/H₂O in this study (26.8 mol%, at 150°C, 20 min) proves the high efficiency of H₂SO₄/GVL/H₂O system for LA production. 311 As GVL/H₂O biphasic solvent was the most efficient for intensifying LA yield at moderate 312 conditions, a comprehensive investigation was conducted for bread waste conversion in the co-313

solvent system following varied reaction conditions (150°C, 10-20 min). In biphasic GVL/H₂O, 314 LA yield increased with increasing reaction duration (~19-28 mol% in 10-15 min) (GVL/H₂O, 315 1:1) (Fig. 5a). However, a slight decrease in LA yield was observed after 20 min, suggesting that 316 LA started to degrade with prolonged reaction. The major product in monophasic $GVL/H_2O(1:1,$ 317 15 min) was glucose (34.6 mol%), while the biphasic system selectively generated LA (~28 mol%) 318 319 as the major product. The LA yield increased up to ~ 2.5 times in the biphasic system compared to the monophasic one (~11 mol%) (150°C, 15 min), implying that phase separation could be 320 321 beneficial for intensive LA production and upscaling to industrial scale.

Essentially, to develop an efficient biphasic reaction medium, it is necessary to understand the contribution and influences of the reaction phase (H_2O) and the extraction phase (GVL) to optimise the yield of the target product. To tune the reaction and extraction phases in GVL/H_2O

biphasic system, catalytic tests were conducted with various ratios of GVL and H₂O (1:1, 1:3, and 325 3:1 of GVL/H₂O). The partition coefficient for LA (R_{LA}) in the GVL/H₂O biphasic solvent was 326 calculated to evaluate the effect of the extraction phase (GVL) in the system. The R_{LA} achieved for 327 10-15 min reaction was 4.2 when 1:1 GVL/H₂O was applied for reaction (Fig. 5b), indicating a 328 higher distribution of LA in the organic phase compared to the aqueous phase. Therefore, GVL 329 330 solvent can be considered highly effective for reactive LA extraction. The partitioning of LA obtained in this study (R_{LA} 4.2) is comparable to a previous study that reported R_{LA} ranging 3.7-4 331 using cellulose as feedstock.²¹ 332

The total yield of LA increased (27.4-32 mol%) when a higher fraction of H_2O (1:3, 333 334 GVL/H₂O) was applied during catalytic conversion, whereas the total LA yield decreased (14.5-17.1 mol%) when a lower fraction of H_2O (3:1, GVL/H_2O) was applied (Fig. 5b). Though the total 335 LA yield increased with a higher fraction of H₂O, the extraction of LA was found to be inefficient. 336 337 The partition coefficient achieved was only 1.1 (1:3, GVL/H₂O), indicating nearly even distribution of produced LA in the reaction and extraction phases due to the lower fraction of GVL 338 applied. In comparison, ~97% of the total LA produced was extracted into the GVL phase when a 339 higher fraction of GVL (3:1, GVL/H₂O) was applied for reaction. However, a considerable 340 341 decrease in total LA yield was observed, possibly due to the lack of sufficient aqueous phase 342 available for reaction. These observations suggested the indispensable contribution of both reaction and extraction phases for an efficient biphasic system for LA production. Considering LA 343 yield (27.4 mol%) and R_{LA} (4.2), the 1:1 GVL/H₂O biphasic system (150°C, 15 min) provided the 344 345 best performance for intensive LA production.

To reflect further on the mechanism and roles of catalytic species in NaCl modified
 GVL/H₂O biphasic system, additional tests were performed under the selected reaction conditions.

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In the case of reaction conducted with only NaCl (30 wt%) without acid catalyst, only marginal 348 product yield was observed (Fig. 6a). When NaCl was applied together with H₂SO₄ for bread 349 waste conversion, an increase in LA yield was observed compared to the reaction in the presence 350 of H₂SO₄ without salt addition. These observations indicate that NaCl alone could not catalyse the 351 desired reaction yet it may act synergistically with H₂SO₄ enhancing the LA production in the 352 353 aqueous phase during biphasic conversion of bread waste. Product distributions in the aqueous and GVL phases in the specified reaction conditions are provided in Fig. S3. The synergistic catalysis 354 by NaCl and H₂SO₄ together with simultaneous efficient extraction of LA into GVL could account 355 356 for the high LA yield obtained in the GVL/H₂O biphasic system.

357 Moreover, the recyclability of the aqueous phase containing H₂SO₄ was investigated. After the catalytic run (reaction and cooling), the reacted organic phase was removed and fresh GVL 358 359 and bread waste substrate were applied for another cycle of catalytic reaction (run-2) again while 360 retaining the aqueous phase from the previous run without adding extra H₂SO₄. Similarly, the third cycle of catalytic reaction (run-3) was conducted. In the 2nd and 3rd run (Fig. 6b), 15 mol% and 13 361 mol% LA was obtained, respectively, compared to the LA yield (28 mol%) obtained in the initial 362 run, which suggested that the acid catalyst could be retained in the aqueous phase and recycled for 363 364 further conversion, though a certain degree of decrease in LA yield was observed. Future studies 365 would be required for evaluating the biphasic system in a continuous reaction mode, which may be more efficient compared to the batch reaction mode. 366

Apart from LA as the target product, FA yield was analysed for bread waste conversion in monophasic and biphasic GVL/H₂O, as FA is often co-produced during biomass conversion.⁴⁸ Similar to LA, the FA yield was enhanced through phase separation with the yield from ~2-3 mol% in the monophasic system to a maximum 5.4 mol% FA yield in biphasic GVL/H₂O (150°C, 15

min, 1:3 solvent ratio) (**Fig. 5c**). Using 1:1 GVL/H₂O, FA partition coefficient (R_{FA}) obtained was ~2-3 (150°C, 10-20 min, solvent ratio 1:1) (**Fig. 5c**), indicating that FA could also be simultaneously extracted into the GVL layer during bread waste conversion. Besides, partition coefficients for LA, FA, and HMF were evaluated in IPA/H₂O solvent (150°C, 20 min, 1:1 solvent ratio), and the values were 6.6, 5.4, and 5.7, respectively (**Fig. S4**), corroborating an effective extraction of these compounds into the organic phase. Considering the low LA selectivity and total LA yield (10.6 mol% at 150°C, 20 min), further investigation was discontinued for IPA/H₂O.

378 Perspectives on LA production and solvent recycling

To evaluate the efficiency of the catalytic system for LA production, LA yield relative to 379 theoretical LA yield of bread waste substrate (considering total available carbohydrate and 380 possible maximum theoretical yield (64.5%)) was calculated and compared with the reported 381 achievements with commercially available starch substrates in the existing literature (Table 1). 382 383 For PC/H₂O (130°C, 20 min) and GVL/H₂O biphasic solvents (150°C, 15 min), 45.7% and 66% LA yield was achieved relative to theoretical yield, respectively. This is considered promising in 384 comparison to the reported LA yield (45.6-66.4%) from commercially available starch substrates 385 in previous studies⁴⁹⁻⁵⁰ where the conversion was conducted using comparatively harsh reaction 386 conditions. For other recent studies where no direct comparison is possible due to the lack of data 387 regarding relative LA yield,^{17,51} it should be noted that much longer reaction duration was required 388 to obtain the reported LA yield. 389

The recyclability of GVL/H_2O biphasic solvent was investigated and discussed in the previous section. For PC/H₂O solvent, despite partial decomposition of PC during acid catalysis, it offers various advantages as a solvent because a high product yield can be obtained with a moderate temperature and a short duration, which play a critical role in reducing the energy

consumption and reactor size. The production of PC from CO₂ is beneficial for process economy 394 and environmental sustainability in terms of CO₂ utilisation. In the application of PC solvent, the 395 derived CO₂ after reaction can be captured and recycled for PC production or other CO₂ based 396 biorefineries, which are conducive to fostering the circular economy. The spent organic solvents 397 can be recycled after separation and purification following commonly used techniques such as 398 399 fractional distillation. For instance, a comprehensive life cycle assessment (LCA) on solvent waste recovery⁵² demonstrated that implementing a solvent recovery system can reduce the 400 environmental footprint of the total solvent manufacturing, usage, and disposal process. The 401 energy requirements and emissions associated with the solvent recovery process have been 402 recognised to be trivial in comparison to the emissions due to virgin solvent production and spent 403 solvent disposal by incineration. 404

405 **Conclusions**

This study provides comprehensive insights into the critical factors for intensive LA 406 production, which can be conducive to the technology scale-up. The bio-derived and CO₂-derived 407 co-solvents in this study, i.e., PC/H₂O, GVL/H₂O, IPA/H₂O, could facilitate H₂SO₄ catalysed 408 tandem reactions during bread waste conversion but demonstrated varied catalytic efficiency. 409 410 PC/H₂O solvent was the most efficient for LA production using moderate reaction conditions, which could be attributed to the CO₂ pressure generated *in situ* through solvent (PC) degradation. 411 Besides, catalytic performance could be significantly enhanced in GVL/H₂O and IPA/H₂O using 412 413 the biphasic system, facilitating reactive extraction of LA in the organic layer that intensified the final concentration of LA. GVL/H₂O biphasic solvent seems promising considering LA yield (28 414 mol%) and LA partitioning (R_{LA} 4.2) achieved in the study. The bio-derived and CO₂-derived 415

416	solvents applied in	this study can	be considered a	s emerging solvents a	and potential	alternatives to
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417 common industrial solvents in future biorefinery applications.

418

419 Supplementary information

420 The supplementary information is available online.

421

422 **Conflicts of interest**

423 The authors declare no conflict of interest.

424

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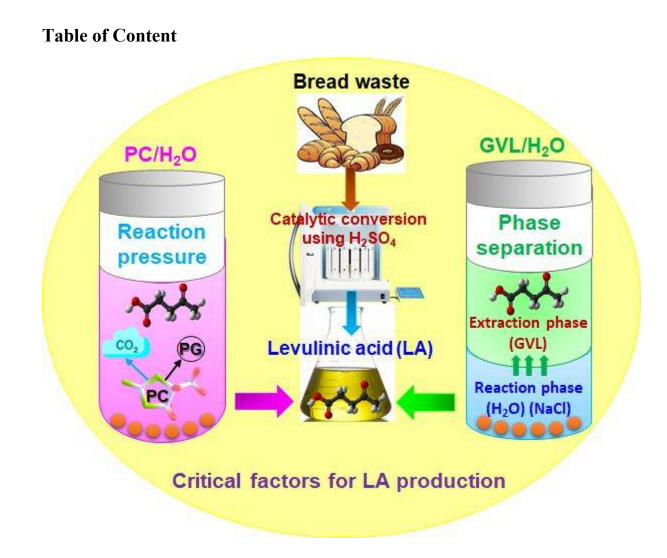
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Synopsis:

This study provides new and critical insights into sustainable catalytic conversion of food (bread) waste to platform chemicals for achieving sustainable development goals and fostering a circular economy.

Critical factors for levulinic acid production from starch-rich food waste:

Solvent effects, reaction pressure and phase separation

List of figures:

- **Fig. 1.** Total sugar yield and LA yield during the catalytic conversion of bread waste in different solvents (a) at 130°C, 1-20 min, (b) at 110°C, 1 min (Reaction conditions: 5 wt% substrate loading, 0.5 M H₂SO₄, 130°C, 1:1 solvent ratio).
- **Fig. 2.** (a) ¹³C NMR spectra of soluble samples obtained after bread waste conversion in different solvents (Reaction condition: 5 wt% substrate loading, 0.5 M H₂SO₄, 130°C, 1 min & 20 min, 1:1 solvent ratio), (b) ¹³C solid-state NMR spectra of untreated bread waste and solid residues collected after reaction under different solvent systems (Reaction conditions: 5 wt% substrate loading, 0.5 M H₂SO₄, 130°C, 20 min, 1:1 solvent ratio).
- Fig. 3. (a) Pressure profile during the catalytic conversion of bread waste in different solvents for 20 min reaction, (b) pressure profile in PC/H₂O for different reaction durations (1-20 min), (c) sugar and LA yield in PC/H₂O after 20 min and 5+15 min (pressure release after 5 min) reaction, (d) sugar and LA yield in PG/H₂O after 5 and 20 min reaction (Reaction conditions: 5 wt% substrate loading, 0.5 M H₂SO₄, 130°C, 1:1 solvent ratio).
- Fig. 4. Product yields during the catalytic conversion of bread waste at 150°C and 1-20 min reaction duration in (a) IPA/H₂O (monophasic) and (b) GVL/H₂O (monophasic); (c) comparative product yields in IPA/H₂O and GVL/H₂O monophasic and biphasic medium (30 wt% NaCl_(aq)) at 150°C, 20 min (Reaction conditions: 5 wt% substrate loading, 0.5 M H₂SO₄, 1:1 solvent ratio).
- Fig. 5. (a) Product yields during the catalytic conversion of bread waste in GVL/H₂O monophasic and biphasic medium comprising different solvent ratios; (b) LA and (c) FA distribution in the organic and aqueous phase and partition coefficients obtained for the catalytic conversion of bread waste in GVL/H₂O biphasic medium comprising different solvent ratios (Note: values for partition coefficient are not shown for solvent ratio 3:1 as ~97% of the total LA and ~92% of the total FA produced were extracted to the organic phase) (Reaction conditions: 5 wt% substrate loading, 0.5 M H₂SO₄, 30 wt% NaCl_(aq) 150°C, 10-20 min).
- Fig. 6. (a) LA yield and total product yield under different reaction conditions (Reaction conditions: 5 wt% substrate loading, 150°C), (b) LA yield and other product yields (sugar+HMF+furfural) in consecutive runs in GVL/H₂O biphasic system (Reaction conditions: 5 wt% substrate loading, 0.5 M H₂SO₄, 30 wt% NaCl_(aq) 150°C, 15 min, solvent ratio 1:1).

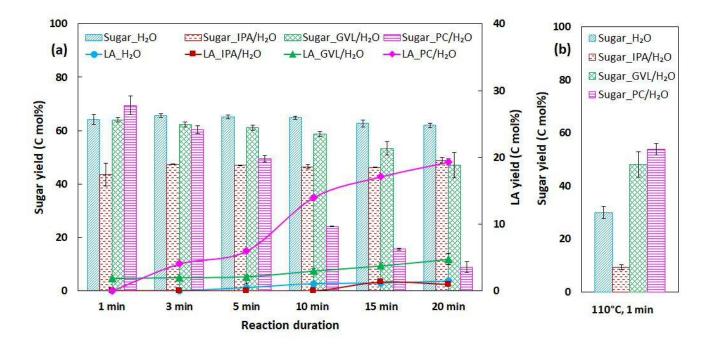


Fig. 1. Total sugar yield and LA yield during the catalytic conversion of bread waste in different solvents (a) at 130°C, 1-20 min, (b) at 110°C, 1 min (Reaction conditions: 5 wt% substrate loading, 0.5 M H₂SO₄, 130°C, 1:1 solvent ratio).

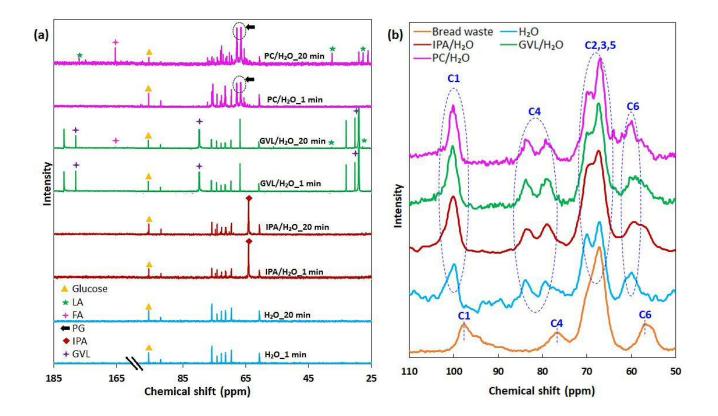


Fig. 2. (a) ¹³C NMR spectra of soluble samples obtained after bread waste conversion in different solvents (Reaction condition: 5 wt% substrate loading, 0.5 M H₂SO₄, 130°C, 1 min & 20 min, 1:1 solvent ratio), (b) ¹³C solid-state NMR spectra of untreated bread waste and solid residues collected after reaction under different solvent systems (Reaction conditions: 5 wt% substrate loading, 0.5 M H₂SO₄, 130°C, 20 min, 1:1 solvent ratio).

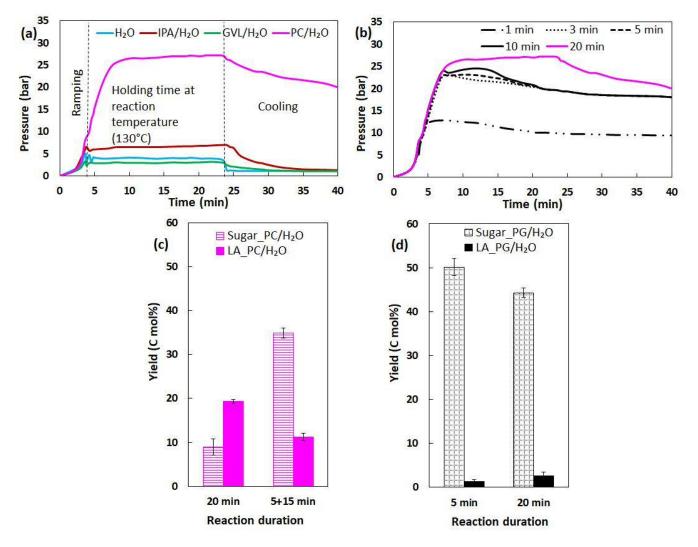


Fig. 3. (a) Pressure profile during the catalytic conversion of bread waste in different solvents for 20 min reaction, (b) pressure profile in PC/H₂O for different reaction durations (1-20 min), (c) sugar and LA yield in PC/H₂O after 20 min and 5+15 min (pressure release after 5 min) reaction, (d) sugar and LA yield in PG/H₂O after 5 and 20 min reaction (Reaction conditions: 5 wt% substrate loading, 0.5 M H₂SO₄, 130°C, 1:1 solvent ratio).

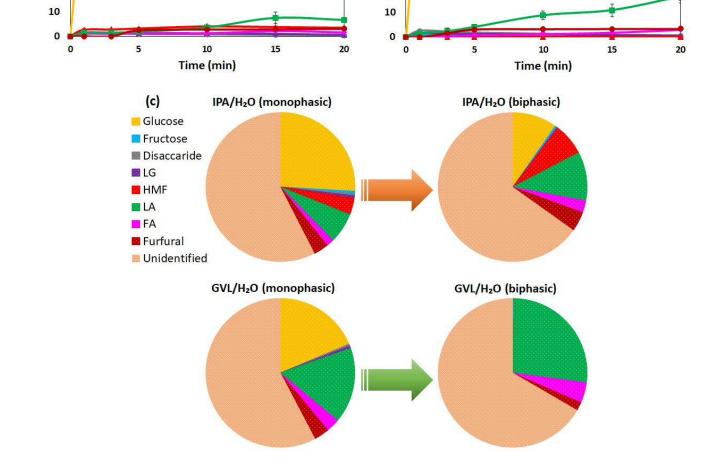


Fig. 4. Product yields during the catalytic conversion of bread waste at 150°C and 1-20 min reaction duration in (a) IPA/H₂O (monophasic) and (b) GVL/H₂O (monophasic); (c) comparative product yields in IPA/H₂O and GVL/H₂O monophasic and biphasic medium (30 wt% NaCl_(aq)) at 150°C, 20 min (Reaction conditions: 5 wt% substrate loading, 0.5 M H₂SO₄, 1:1 solvent ratio).

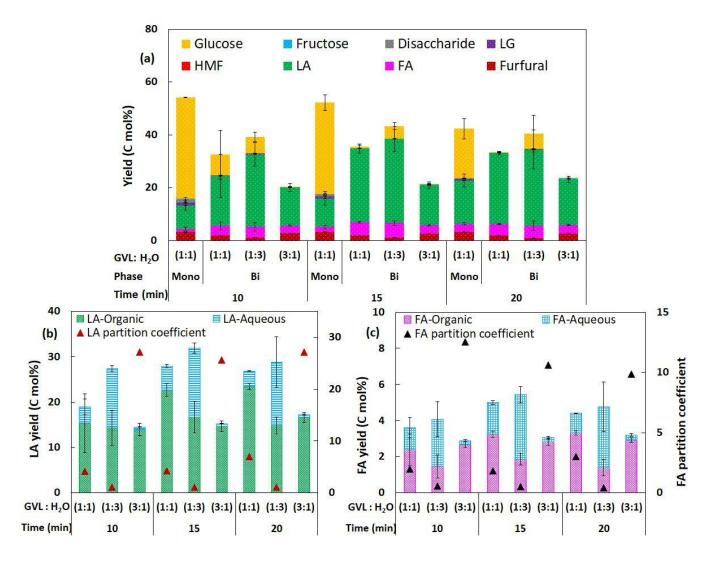


Fig. 5. (a) Product yields during the catalytic conversion of bread waste in GVL/H_2O monophasic and biphasic medium comprising different solvent ratios; (b) LA and (c) FA distribution in the organic and aqueous phase and partition coefficients obtained for the catalytic conversion of bread waste in GVL/H_2O biphasic medium comprising different solvent ratio (Reaction conditions: 5 wt% substrate loading, 0.5 M H_2SO_4 , 30 wt% NaCl_(aq) 150°C, 10-20 min).

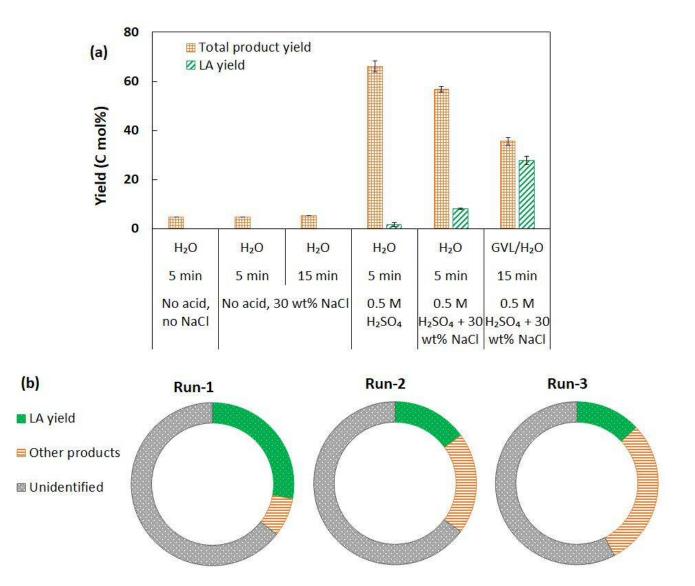


Fig. 6. (a) LA yield and total product yield under different reaction conditions (Reaction conditions: 5 wt% substrate loading, 150°C), (b) LA yield and other products (sugar+HMF+furfural) of consecutive runs in GVL/H₂O biphasic system (Reaction conditions: 5 wt% substrate loading, 0.5 M H₂SO₄, 30 wt% NaCl_(aq) 150°C, 15 min, solvent ratio 1:1).

Substrate	Reaction conditions	Catalyst	LA yield based on total organic carbon (mol%)	LA yield based on weight of substrate (%)	LA yiel to the yiel
	130°C, 20 min, H ₂ O	-	1.5	1.2	
-	130°C, 20 min, IPA/H ₂ O		1.0	0.8	
-	130°C, 20 min, GVL/H ₂ O		4.8	3.8	1
-	130°C, 20 min, PC/H ₂ O		19.6	15.5	4
David	150°C, 20 min, IPA/H ₂ O (mono)	0.5 M H ₂ SO ₄	6.6	5.3	1
Bread waste	150°C, 20 min, IPA/H ₂ O (bi)		10.6	8.5	2
-	150°C, 15 min, GVL/H ₂ O (mono)		10.9	8.8	2
-	150°C, 15 min, GVL/H ₂ O (bi)		27.9	22.4	6
-	150°C, 20 min, GVL/H ₂ O (mono)		16.4	13.2	3
-	150°C, 20 min, GVL/H ₂ O (bi)		26.8	21.6	6
Bread	130°C, 8 h	$\begin{array}{c} 1.5 \text{ ml } 5 \text{ M } \text{H}_2 \text{SO}_4 \\ \text{and } 10 \text{ ml } \text{GVL} \end{array}$	-	30.2	
Starch	165°C, 5 h	sulfonated hyperbranched poly (arylene oxindole)s	-	31.1	
Starch	200°C, 60 min	4% H ₂ SO ₄	-	47.5	6
Sorghum grain	200°C, 40 min	8% H ₂ SO ₄		32.6	4

Table 1. Comparative LA yield obtained from bread waste in this study and from starch substrates in the literatu

Supplementary Information

Critical factors for levulinic acid production from starch-rich food waste: Solvent effects, reaction pressure and phase separation

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- **Fig. S1.** Total product yields during the catalytic conversion of bread waste under different solvents at (a) at 130°C and (b) at 130°C and 150°C under GVL/H₂O and IPA/H₂O (Reaction conditions: 5 wt% substrate loading, 0.5 M H₂SO₄, 1-20 min, 1:1 solvent ratio).
- **Fig. S2.** XRD pattern of untreated bread waste and solid residues collected after reaction under different solvents (Reaction conditions: 5 wt% substrate loading, 0.5 M H₂SO₄, 130°C, 20 min, 1:1 solvent ratio).
- **Fig. S3.** Distribution of products in the aqueous phase and organic (GVL) phase during the catalytic conversion of bread waste in GVL/H₂O biphasic medium (Reaction conditions: 5 wt% substrate loading, 0.5 M H₂SO₄, 30 wt% NaCl_(aq) 150°C, 10-20 min, 1:1 solvent ratio).
- **Fig. S4.** LA, FA, and HMF distribution in the organic phase and the aqueous phase, and partition coefficients obtained for the catalytic conversion of bread waste in IPA/H₂O biphasic medium (Reaction conditions: 5 wt% substrate loading, 0.5 M H₂SO₄, 30 wt% NaCl_(aq) 150°C, 20 min).

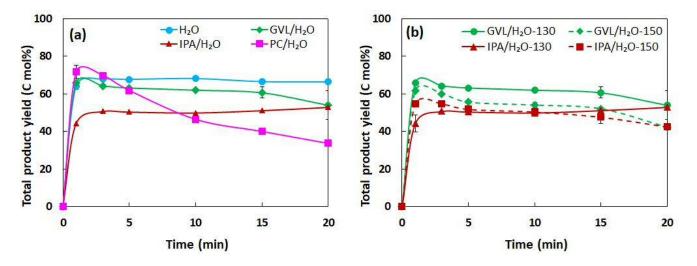


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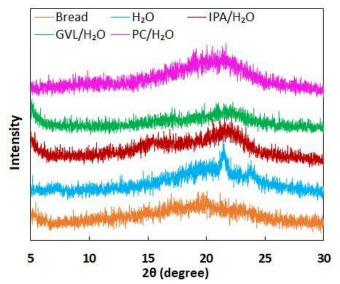


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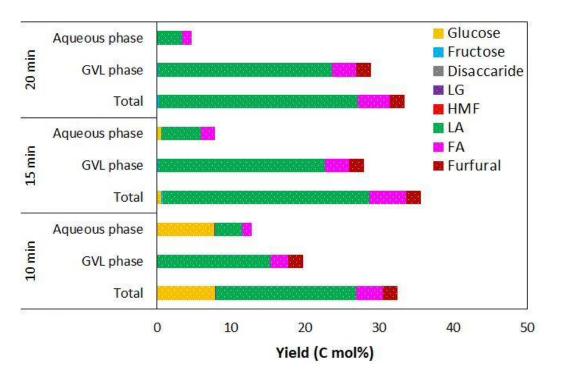


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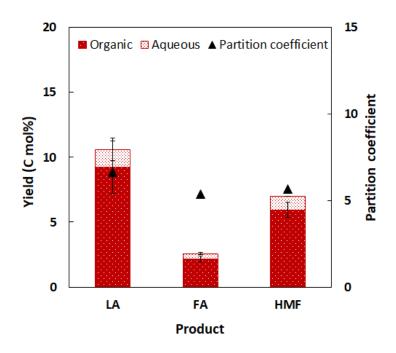


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