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# Efficient Mixing Enhancement by Orthogonal Injection of Shear-Thinning Fluids in a Micro Serpentine Channel at Low Reynolds Numbers

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## Abstract

Viscoelastic fluids have been recently proposed to promote mixing effect in microfluidic systems, where limited success has been obtained. However, the flow and mixing mechanism of a viscoelastic fluid is still poorly understood, particularly regarding the roles of injection on mixing at low Reynolds numbers. In this work, an efficient mixer by orthogonal injection into a primary flow is proposed. The mixing behaviors of shear-thinning fluids in a serpentine channel with an orthogonal injection were investigated experimentally. Dye visualization and concomitant statistical analysis were conducted to quantitatively characterize the mixing performance and to reveal the flow kinematics. Enhanced mixing is achieved just over a short effective mixing length. The probability distribution functions (PDFs) analysis shows that the mixing efficiency, defined by the normalized concentration of dye intensity[1], can be significantly improved from 22% for the Newtonian fluids to 69% and 76% by using a shear-thinning fluid with polymer concentrations of 25 and 50 ppm, respectively. The decay exponents of shear-thinning fluids plateau at -3.4 indicates the occurrence of elastic instability. The relative-change-ratio fluctuations illustrates that the observation area can generate sufficient elastic stress to induce flow instabilities, resulting in effective mixing in the channel.

**Keywords:** fluid-structure interactions, elastic turbulence, efficient mixing, microfluidics, non-Newtonian fluid dynamics

1 **Introduction.** Mixing is an ubiquitous phenomenon in nature and everyday life, and is of high importance  
2 to many applications[2] such as process intensification, enhanced oil recovery[3] and various chemical  
3 processes (i.e., chemical synthesis and micro/nano-particle production[4,5]). The mixing in microfluidics[6],  
4 which is essential for any lab-on-a-chip device (i.e., blood and saliva analysis[7], future drug diagnosis, and  
5 blood plasma mixing[8]), is especially challenging. It is widely accepted that the mixing achieved by a chaotic  
6 advection has a much higher efficiency than that purely induced by the molecular diffusion. At the macroscale,  
7 it is possible and relatively easy to induce hydrodynamic turbulence by directly increasing the Reynolds  
8 number, i.e.,  $Re = \rho V_a L / \eta$ , where  $\rho$  and  $\eta$  are the fluid density and viscosity, respectively,  $V_a$  is the mean  
9 velocity, and  $L$  is the characteristic length, via increasing the flow velocity. However at the microscale, the  
10 Reynolds number becomes very small due to the small value of the characteristic length, where the prevailing  
11 flow is in the laminar flow regime, resulting in a molecular diffusion dominated mixing behavior [9,10]. In  
12 addition, the increase of the surface-to-volume ratio at the microscale increases the capillary force, which  
13 dominates the interaction between the fluid flow and the channel geometry. To enhance mixing efficiency at  
14 the microscale, various approaches[9,11] have been proposed by fabricating complicated channel structures  
15 or micromixers[12,13] assisted by external drivers. These approaches, however, have not received practical  
16 applications as they still cannot successfully break through the limitation of laminar flow nature. An economic  
17 and convenient approach of efficient mixing at the microscale beyond the limitation of laminar flow will be  
18 of high value.

19 Although it is difficult to induce turbulence within the flow of Newtonian fluids in micro systems due to  
20 the limitation of laminar flow, a turbulent-like phenomenon with remarkable chaotic advection, which is  
21 known as elastic turbulence[14–21], does exist in the flow of a polymeric solution. With small amount of high-

1 molecular-weight polymer addition into a conventional Newtonian fluid, the fluid shows a non-Newtonian  
2 behavior that could exhibit both liquid and solid properties. There are two nonlinearities contribute to the flow  
3 instability, inertial nonlinearity and elastic nonlinearity, where the latter is ascribed to the polymer interaction  
4 with the primary flow[21]. The elastic stress within the fluids would exhibit a remarkable non-linear growth  
5 with shear rate with relaxation characteristics. The Weissenberg number,  $Wi = \lambda\dot{\gamma}$ , analogous to the definition  
6 of  $Re$ , is used to characterize the degree of elastic nonlinearity, where  $\lambda$  is the longest polymer relaxation time  
7 and  $\dot{\gamma}$  is the shear rate. Therefore, even at low  $Re$ , the flow could still transfer from a laminar state to a chaotic  
8 advection regime when the  $Wi$  exceeds a critical value, which could benefit the mixing performance.

9 However, the mechanisms of chaotic advection induced by the elastic instability and elastic turbulence, is  
10 still little known, especially during the transition from a stable to a chaotic state. Recently, a few theoretical  
11 and numerical investigations of effective enhancement of mixing by elastic instability/turbulence in micro  
12 channels have been conducted in various geometries[21–30], including serpentine channels[23,25,26,31] and  
13 abrupt contraction micro channels[1,32]. However, in the experiments conducted within serpentine channels,  
14 a relatively long mixing path at a moderate flow rate was still observed, which shows limited enhancement in  
15 the mixing [26,27]. Short mixing length was observed for flows in an abrupt contraction microchannel,  
16 however the channel structure is too complex and fragile for any practical applications. Additionally, the  
17 mixing performance is influenced by the injection even in a serpentine channel with a single semi-band, which  
18 is named VDP (Viscous Disk Pump) as illustrated in the dye visualization by Ligrani et al.[33,34]. Therefore,  
19 there is a strong need to investigate the influence of injection on the mixing performance along a serpentine  
20 channel.

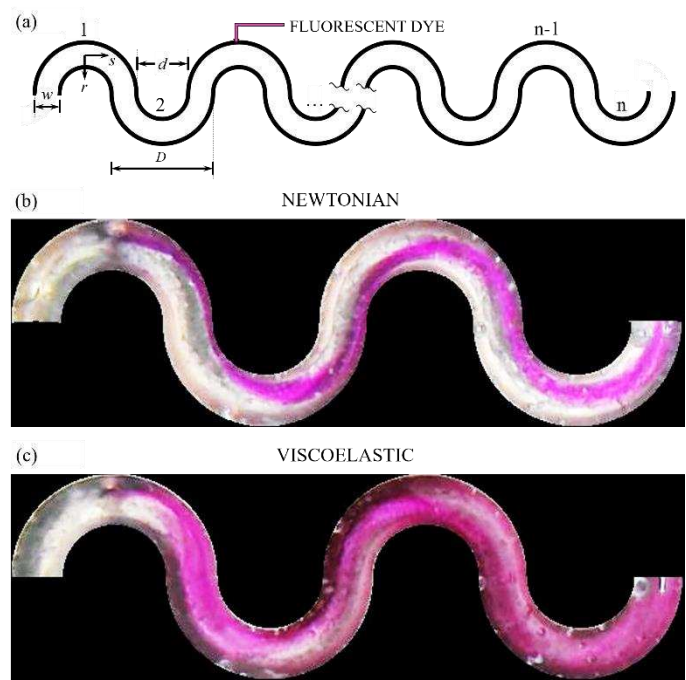
21 In order to show a strong non-Newtonian behavior[35], working fluids with orders of magnitude higher

1 viscosity than water were used in previous investigations, which brings a heavy penalty in pressure drop,  
2 especially for a high-throughput operation[9]. In addition, most of the working fluids used in these  
3 investigations are the Boger fluids, which have nearly constant viscosities in a log-log coordinate with low  
4 shear-thinning effects[36–39]. Hitherto, the effects of shear-thinning fluids on the introduction of elastic  
5 instability and turbulence have not been exploited effectively.

6 Addressing such limitations, we propose a new approach of enhancing mixing by combining the advantages  
7 of serpentine channel and abrupt contraction micro channel, i.e., a simple orthogonal injection into a micro  
8 serpentine channel, that results in a very short mixing length. Such an approach is similar to the work of Qin  
9 et al.[40] in the straight channel with a set of small cylinders at the entrance section. In this work, we prove  
10 experimentally that the orthogonal injection is a good bridge to connect the homogeneity on mixing wanted  
11 by the smallest scale fluctuation and the elastic instabilities, which is dominated by the large-scale fluctuations.  
12 [41]. Consequently, a rapid mixing is achieved within a shorted mixing path in the serpentine channel. To  
13 sufficiently decrease the effects of chemical additions (e.g. salt and antiseptic) on polymer, which is sensitive  
14 to salinity[42], aqueous solutions with a small amount of polyacrylamide are chosen as the working fluids. To  
15 reduce the influence of polymer additions on the other physical properties except the viscosity, polymeric  
16 solutions with extremely low concentration (25 ppm and 50 ppm) are used. The results provide experimental  
17 and theoretical proof of effective mixing due to chaotic flow, as shown by dye patterns, power spectra  
18 dependence and fluctuation of concentration variations, and derive a new criterion for predicting the onset of  
19 elastic instability with the incorporation of the geometry effects and shear-thinning effects.

20 **Methods.** In this manuscript, we investigated the flow of shear-thinning fluids with extremely low  
21 concentration in a serpentine channel at low Reynolds number  $Re$  using dye trajectory method and image

1 processing analysis. Dye trajectory method shows that remarkable bifurcations are generated within the flow  
 2 of viscoelastic fluids at low Reynolds number, while the flow of Newtonian fluids stays laminar. Systematic  
 3 image processing analysis based on the coupling of MATLAB and OpenCV was used to capture features of  
 4 perturbation within the flow. In addition, we study the statistical properties of mixing by quantitatively  
 5 analyzing the PDF of normalized dye concentrations, the power spectra and the decay exponents scaling of  
 6 the total normalized concentration in the observed area.



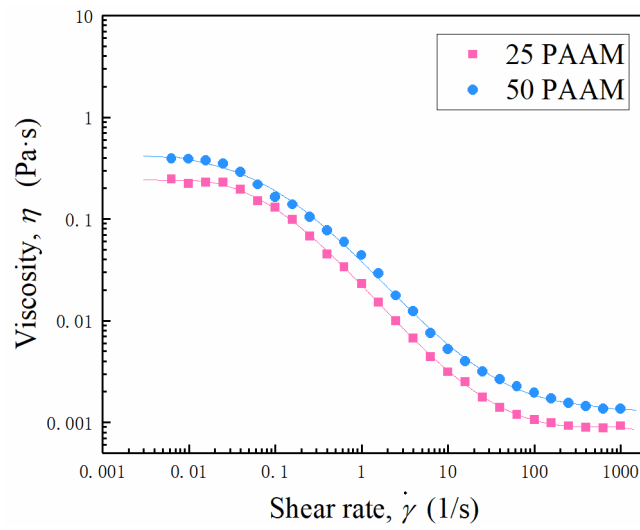
7  
 8 Fig. 1 (a) Schematic of the serpentine channel, showing the injecting point of dye, where  $n$  refers to the number of semi  
 9 C-shaped curved channel, where the definition of C-shaped channel is similar to Ligrani et al. [43], and example  
 10 dye patterns of (b) Newtonian fluids and (c) shear-thinning fluids with the concentration of 50 ppm, at bulk flowrate of  
 11  $V_b = 3500 \mu\text{l}/\text{min}$  ( $Wi = 5.89$ ).

12 Experiments were conducted using a serpentine channel with equal width and depth ( $W = H = 1\text{mm}$ ),  
 13 fabricated by polyethylene. The schematic view of the test section is shown in Fig.1a. The channel has 20  
 14 sections ( $n = 20$ ). The inner and outer diameters of curvatures are  $d = 1\text{mm}$  and  $D = 2\text{mm}$ , respectively. The

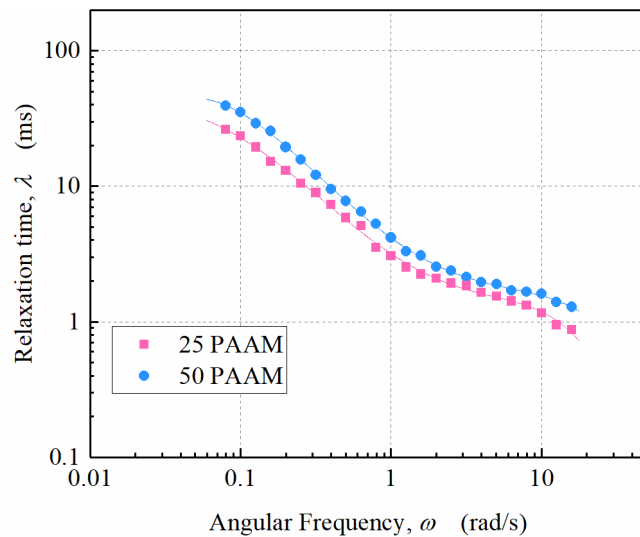
1 dye was injected from the center point of the outer semicircle of the third section in the serpentine channel. A  
2 syringe pump (KD Scientific, U.S.A) was used to control the bulk flow rates. The image acquisition system  
3 is the same as our previous work[44] and a highspeed camera (I-SPEED 720, U.K.) was used to capture the  
4 flow image. The dye was injected by another syringe pump through a syringe needle with a diameter of 0.3mm  
5 connected with the serpentine channel. These two syringe pumps are controlled by a synchronizer. The  
6 recorded images are digitally transferred (in TIF format) to a personal computer for further analysis (using  
7 MATLAB and OpenCV).

8 The polymeric solution was prepared by adding 25 ppm and 50 ppm of polyacrylamide (PAAM)  
9 ( $M_w=18\times 10^6$  Da) to the deionized water, respectively. For brevity, these two fluids are denoted as 25PAAM  
10 and 50PAAM, respectively. No other inorganic salt or sucrose have been added since that the viscosity of  
11 dilute polymer has an extremely sensitive reaction to the inorganic such as NaCl[42]. The Newtonian solvent,  
12 deionized water, which is denoted as WATER for brevity, has constant viscosity and was used as the base fluid.  
13 The Rhodamine B dye was seeded to the corresponding working fluids at a weight ratio of 0.05%. The  
14 properties of all working fluids are listed in Table 1. The rheological properties including viscosity and  
15 relaxation time of the working fluids were measured by a rheometer (TA Instruments AR100 N, U.S.A)  
16 controlled stress rheometer with a stainless-steel plate geometry (40 mm diameter). In this study, the shear  
17 viscosity,  $\eta$ , for all the polymer solutions against shear rate is schematically illustrated in Fig. 2. It is shown  
18 that the shear viscosity has a significant shear-thinning behavior. The Carreau-Yasuda model was adopted to  
19 fit the experimental viscosity as shown by the solid lines. In order to measure the relaxation time, small  
20 amplitude oscillatory shear stress (SAOS) tests conducted by the rheometer for the measurements of the  
21 storage modulus,  $G'$ , which represents the energy of elastic storage and the state of the structured materials,

1 and the loss modulus,  $G''$ , which represents viscous dissipation or loss of energy. Frequency sweeps were  
 2 conducted within linear viscoelastic region when the oscillation shear stress is kept constant at a low value  
 3 which is 0.01 here. Fig. 3 shows the dependence of polymer relaxation time on the angular frequency from  
 4 the measurements of SAOS for all the PAAM solutions used in this study. The value of the longest relaxation  
 5 time,  $\lambda$ , which is estimated in the limit of the angular velocity approaching to zero are summarized in Table  
 6 1 for all the non-Newtonian fluids utilized in the study.



7  
 8 Fig. 2 The viscosity of the shear-thinning fluids versus shear rates, including 25PAAM and 50PAAM.



9  
 10 Fig. 3 Relaxation time against the angular frequency obtained from small amplitude oscillatory shear stress measurements for  
 11 the PAAM solutions with the concentrations of 25 ppm and 50 ppm, respectively.

Throughout the overall study, the Reynolds number is ranging from 0.145 to 0.474, where  $Re = \rho UW / \eta$ , where  $U$  is the bulk flowrate,  $W$  is the channel width,  $\eta$  is the viscosity and  $\rho$  is the density of the working fluids. The relation of elastic stress and viscous stress is normalized by Weissenberg number,  $Wi$ , i.e.,  $Wi(\dot{\gamma}) = N_1(\dot{\gamma}) / 2\dot{\gamma}\eta_p(\dot{\gamma})$ , where  $\dot{\gamma} = U/W$  is the shear rate,  $N_1$  is the first normal stress difference and  $\eta_p(\dot{\gamma})$  is the polymeric viscosity which is calculated by  $\eta_p = \eta - \eta_s$  [27,45,46].  $Wi$  is ranging from 3.9 to 10.1 in this experiment. With reference to the main stream fluid, the other two dimensionless numbers  $El$  and  $Pe$  were also estimated. The Elastic number  $El$  and the Peclet number  $Pe$  are defined as  $El = Wi/Re$  and  $Pe = VW/D$ , respectively, where  $V$  is the flow velocity, and  $D$  is the diffusion coefficient, estimated to be  $D = 3.02 \times 10^{-12} \text{ m}^2/\text{s}$ , which has an inversely proportionality to the viscosity[1]. Additionally, the Dean number  $\kappa$ , defined by the ratio of the square root of the product of the inertia and centrifugal force to the viscous forces as  $\kappa = 2\delta^{1/2}Re$ , is also considered to evaluate the magnitude of secondary Dean flow in the curved serpentine channel, where  $\delta$  is the radius ratio determined by  $\delta = 4W/(D+d)$ . The Prandtl number  $Pr$  is defined by  $Pr = \nu/\alpha$ , where  $\alpha$  is the fluid thermal diffusivity defined as  $\alpha = k/(\rho c_p)$ , where  $k$  is the thermal conductivity coefficient and  $c_p$  is the specific heat.

Table 1 Fluid properties.

| Fluid  | Density<br>$\rho$ ( $\times 10^3 \text{ kg/m}^3$ ) | Longest relaxation time<br>$\lambda$ (s) |
|--------|--|--|
| WATER  | 0.995  | –  |
| 25PAAM | 0.995  | 0.067                                    |
| 50PAAM | 0.995  | 0.101                                    |

Table 2 Ranges of the dimensionless parameters

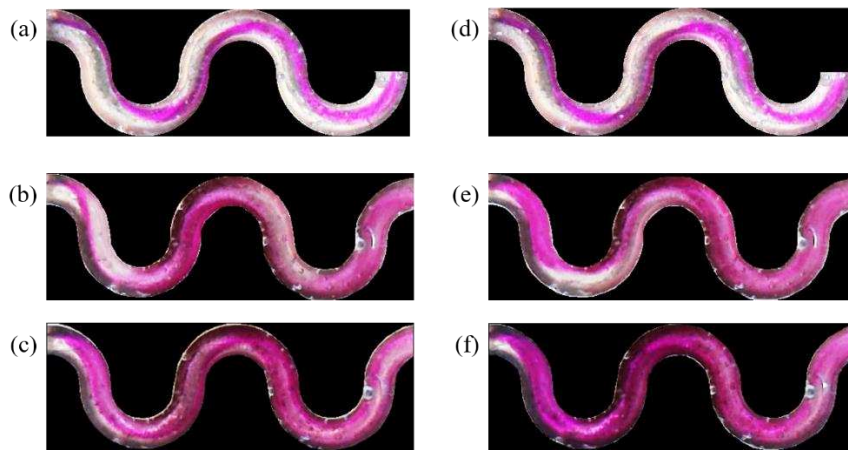
| Abb. | Dimensionless numbers | Expression             | Definition                                | Range (or Value) |
|------|-----------------------|------------------------|---|------------------|
| $Re$ | Reynolds              | $\rho UW / \eta$       | Inertia / Viscous                         | 0.15 – 0.48      |
| $Wi$ | Weissenberg           | $\lambda \dot{\gamma}$ | Polymer relaxation time / Shear rate time | 3.90 – 10.10     |
| $El$ | Elastic               | $Wi/Re$                | Elastic / Inertia                         | 21.31-26.90      |

|          |         |                    |   |   |
|----------|---------|--------------------|---|---|
| $Pe$     | Peclet  | $VW/D$             | Convective / Diffusive  | $19.40 \times 10^6 - 33.30 \times 10^6$     |
| $\kappa$ | Dean    | $2\delta^{1/2} Re$ | The ratio of the square root of the product of the inertia and centrifugal force to the viscous force | $0.75 \times 10^{-2} - 2.45 \times 10^{-2}$ |
| $Pr$     | Prandtl | $\nu/\alpha$       | Viscous / Thermal   | 1.47-2.80                                   |

1

2 **Results and Discussion**

3 **Dye pattern.** The investigation was conducted when the stable flow patterns formed after the main and dye  
4 streams of fluids were injected to the serpentine channel. The dye spreading patterns are observed far  
5 downstream in the visualized region (as shown in Fig. 1(a)) from the third section to the sixth section. Fig.  
6 1(b) and (c) show space time dye patterns of Newtonian fluids and shear-thinning fluids at a bulk flowrate  
7  $V_b = 3500 \mu\text{l}/\text{min}$ , respectively. For the Newtonian fluid, the profile shows typical laminar dye layer with  
8 minimal dye penetration into the undyed stream, except for the weak molecular diffusion effect. However  
9 when the Newtonian fluid is replaced by the shear-thinning fluid under the same experimental condition, as  
10 shown in Fig. 1 (c), irregular flow patterns with spikes of dye were penetrated into the undyed fluid stream,  
11 showing an enhanced mixing effect.



12

13 Fig. 4 Flow visualization images (a) (b) (c) WATER, 25PAAM and 50PAAM at a bulk flowrate of  $V_b = 3500 \text{ ul}/\text{min}$  (d)  
14 (e) (f) WATER, 25PPM and 50PPM at a bulk flowrate of  $V_b = 5500 \text{ ul}/\text{min}$ .

15 Flow visualization of WATER, 25PAAM and 50PAAM at  $V_b = 3500 \text{ ul}$  and  $V_b = 5500 \text{ ul}$ , respectively,

1 have been presented in Fig. 4. For cases of the Newtonian fluid, the dye streams are narrow with little distortion  
2 and the flow condition maintains laminar with insignificant mixing, dominated by molecular diffusion only.  
3 The interface between the main and dye streams is smooth, stable, and well defined with no penetration,  
4 overlapping, swinging, or encapsulating, as shown in Fig. 4 (a) and (d). With increased flowrates, the dye  
5 stream slightly moves down from the upper to the lower border with only minimal steady secondary flows  
6 presented accompanied by very little augmented mixing and slight movement of the flow direction in the  
7 central plane away from the center of curvature. The Newtonian fluid has negligible elasticity, and extremely  
8 low Reynolds number, so the corresponding elastic and inertial effects are insignificant while the viscous  
9 effects and the centrifugal effects play a dominant role in the flow. When that the aspect ratio is approximately  
10 near unity, an increase of velocity in the outer half of the bend and a decrease in the inner is induced in the  
11 curved channel. The orthogonal injection has strongly magnified the velocity difference between the inner and  
12 outer half of the curvature, which is responsible for the slight move of the dye trajectories. The mean shear  
13 stress is skewing by a transverse pressure gradient caused by the channel planform configuration of the  
14 orthogonal injection from the outer side[47]. Traditionally, in the channel flow with curvatures, the secondary  
15 flow is induced by inertia centrifugal effects, which is strongly influenced by the Dean number[48,49] and  
16 moderately by the radius ratio  $\delta$ . In other word, Dean number indicates the intensity of the secondary flow.  
17 However, in this study, the Dean number is still not large enough to generate a Dean vortex in the cross section  
18 of the serpentine channel as shown by the visualization results of deionized water. Therefore, one can find that  
19 the secondary flow is too weak to induce the following strong instabilities in the polymeric solutions.

20 However, for the case of shear-thinning fluids, which are 25PAAM (as shown in Fig. 4 (b) and (e)) and 50  
21 PAAM (as shown in Fig. 4 (c) and (f)), respectively, the mixing and flow behavior are dramatically different

1 from those of the Newtonian fluid. At the upstream of the channel, the moderate swinging, very weak agitation  
2 and oscillation with small amplitudes and low frequencies are observed due to the interaction of the enhanced  
3 elastic stress and the skewing secondary flow induced by the orthogonal injection. At the downstream,  
4 significant and continuous mixing is observed especially in the serpentine channel accompanied by significant  
5 oscillation, salient penetration and intermittent overlapping between the two streams, which are the remarkable  
6 characteristics of elastic instability. Such elastic stress gradient leads to initial polymer distortion and agitation,  
7 and increased unstable polymer stretching at both the circumferential and normal direction due to the long  
8 relaxation time of the long-chain polymers. This significant and sharp mixing within the four bends indicates  
9 a very short mixing path within the polymeric flow. The shortened mixing path is ascribed to two factors. First,  
10 the balance between the centrifugal force and the normal elastic force leads to the significant oscillation of  
11 normal velocity component at the normal direction, resulting in elastic instability related to the enhancement  
12 of mixing performance. When the  $Wi$  exceeds the critical Weissenberg number, a small finite-size perturbation  
13 caused by such oscillation could induce a secondary flow as analyzed theoretically by Morozov and  
14 Saarloos[50], who claimed that the nonlinear subcritical instability comparing with the induction of Hopf  
15 bifurcation is an inherent characteristic in such flow of polymeric solutions. In such Hopf bifurcation, elasto-  
16 inertial traveling wave solutions which is corresponding to the transition from the linear to non-linear  
17 instability will be created from a laminar state in a pipe/channel flow of viscoelastic fluids which has been  
18 theoretically proved its existence recently by Garg et al. [51]. Second, the strong shear-thinning effect exists  
19 in the polymeric flow, which is benefit for the induction of bifurcation instability and chaotic flow in the  
20 working fluid with extremely low polymer concentration. The polymeric solutions with moderate shear-  
21 thinning occurs elastic instability beyond the critical Weissenberg number due to the important normal stress

1 gradient existing near the wall. This elasticity significantly enhance the shear rate at the wall and homogenizes  
2 the viscosity profiles which leading to a perfect mixing as reported by Bodiguel et al. [52]. In regard to the  
3 secondary flow, the coupling of analogous Dean vortices and the shear-thinning effects in the viscoelastic  
4 flows cause the augment of mixing performance since that in the viscoelastic flows, the analogous viscoelastic  
5 secondary flow can be generated even at lower Dean numbers, as presented by Poole and his co-workers[53–  
6 55] in a serpentine channel.

7 With higher polymer concentrations and flowrates, the valid mixing is induced earlier in the channel. This  
8 result indicates that the enhanced polymer concentration contributes to the effective mixing due to the  
9 enhanced elastic instability by the incremental non-linear elastic stress gradient, originated from the stronger  
10 polymer stretching, roiling, twining and spiraling in dilute polymer solutions.

11 The phenomenon unexpected here is that, at the fourth semi-section, dyed streams in the flow of water tend  
12 to be closer to the upper border while that of the viscoelastic fluid tend to be closer to the lower one at the  
13 corresponding section. The trend direction of the viscoelastic fluids is opposite to that of the centrifugal force.  
14 This unique, anti-physical and unstable phenomenon might be originated from the interaction of the curvature  
15 of the serpentine channel with the significant first normal stress difference existing in the flow of polymeric  
16 fluids. The enhanced normal stress beyond the centrifugal force in the polymeric solutions tends to stretch the  
17 polymer inside and cause this inverse behavior.

18 ***Probability density function.*** Quantitative mixing performance is evaluated using the probability density  
19 function (PDF) of the intensity images normalized by its overall average value, which is resemble to the  
20 method used by Gan et al.[1]. The magnitude of mixing is evaluated by the PDFs of the normalized dye  
21 concentrations based on the image sequences. During each experimental group, a data sequence including

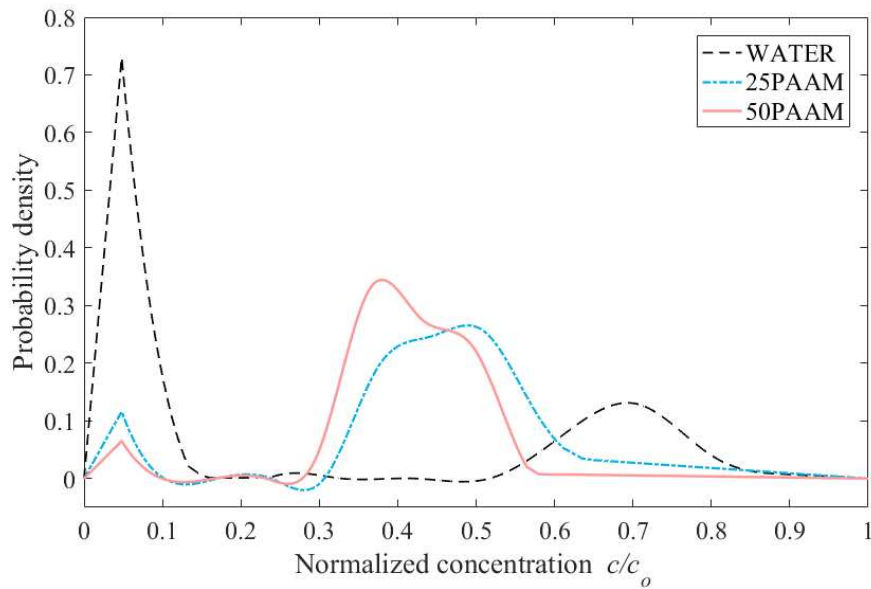
1 more than 8000 data points is obtained with a time interval of 30 fps (frames per second). And then the data  
 2 is statistically analyzed using the discrete distribution of the normalized concentrations over the ROI area of  
 3 the channel by splitting the range from 0 to 1 to more than 50 bins equally. In this condition, a function with  
 4 two respective peaks at the low and high normalized concentrations means that the fluids of the main stream  
 5 and the dye stream are not mixed effectively, while a smooth PDF gathered in the middle range with nearly  
 6 one peak indicates that the two streams are entirely mixed by the induced chaotic flow. Fig. 5 shows the PDFs  
 7 of the flows of shear-thinning fluids and Newtonian fluid within the ROI regime (i.e., region of interest, which  
 8 refers to the fourth dyed bend as shown in Fig. 4) at the flow rate of  $V_b=5000$  ul/min. The PDF of WATER  
 9 has two significant lathy peaks at the extremely low concentration and near the highest concentration,  
 10 indicating deficient mixing while that of 25PAAM or 50PAAM has a negligible peak at low concentrations  
 11 and a significant platform peaking in the mid-range which indicates effective mixing. In comparison with  
 12 25PAAM, the median of 50PAAM is much closer to the perfect mixing since the increased polymer  
 13 concentration causing elastic stress enhancement. Therefore, effective mixing was achieved in shear-thinning  
 14 fluids with extremely low concentrations which has a very low Reynolds number and a very large Peclet  
 15 number.

16 After normalization of the dye intensity ranging from 0 to 1, the mixing efficiency  $\sigma$  can be quantified  
 17 based on the following function. The mixing efficiency  $\sigma$  is defined quantitatively as follows with the  
 18 normalized concentration of dye intensity ranging from 0 to 1[1]:

$$\sigma = \left[ 1 - \frac{\sum_{i=0}^{i=1} |C_i - C_\infty| P(C_i)}{C_\infty} \right] \%$$

20 where  $C_i$  is the observed concentration normalized,  $C_\infty$  is the concentration normalized for fully mixing,  
 21 and  $P(C_i)$  is the probability density. In our study,  $C_\infty$  is estimated to be 0.4 for perfect mixing by calculating

1 the average normalized concentration of the completely mixed regimes. With this definition,  $\sigma = 0$  means  
 2 no mixing while  $\sigma = 1$  means fully mixing. Thus, the mixing efficiency  $\sigma$  was found to be 0.21 in the flow  
 3 of WATER and 0.69 and 0.76 in the flow of 25PAAM and 50PAAM, indicating that the addition of small  
 4 amount of polymer only dissolving into the Newtonian fluids has significantly improved the mixing  
 5 performance.

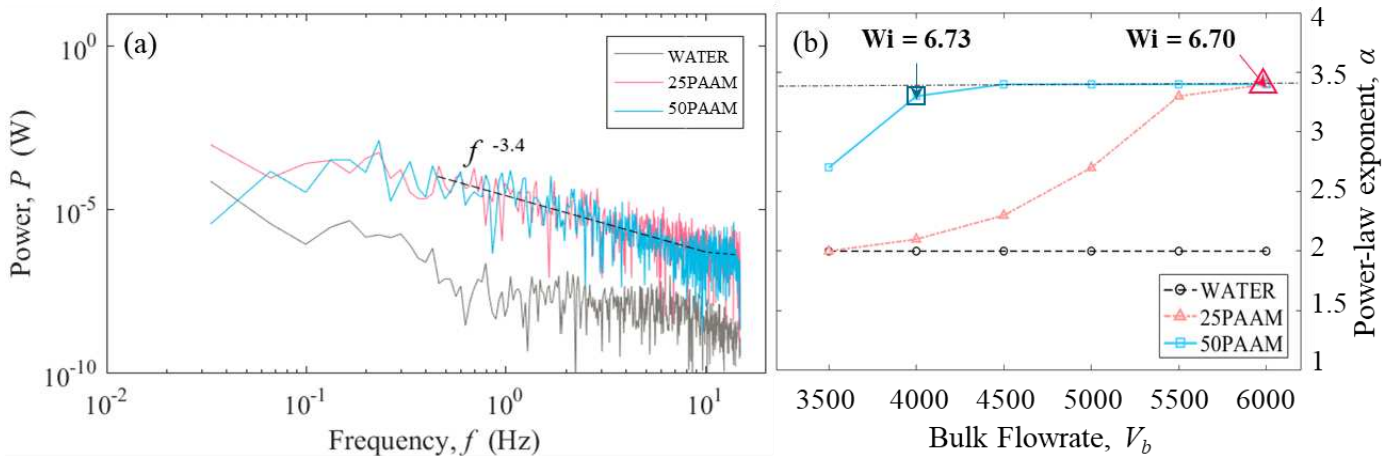


6  
 7 Fig. 5 Probability density function (PDF) of normalized concentration of the dye within the ROI area of the channel of WATER,  
 8 25PAAM and 50PAAM, respectively, at the flowrate of  $V_b=5000\text{ul} / \text{min}$ .

9 **Power spectrum.** Power spectra shows the power law behavior of a flow. The power-law exponent is a  
 10 quantitative way to characterize the existence of the chaotic flow motion. For example, the lower absolute  
 11 power-law exponent keeping constant means that the main stream and the dye stream are not mixed and the  
 12 instability and chaotic flow are not induced. A high power-law exponent higher than 3 means effective mixing  
 13 and inducement of chaotic flow. The fluctuation of normalized concentration is nonperiodic and obviously has  
 14 power law decay, which indicates that the mixing is induced in various time scales. In this study, the Power  
 15 Spectra Distribution (PSD) of the time series of fluctuations of normalized concentration is calculated by the

1 Fast-Flourier Transform (FFT) method in MATLAB based on 8000 data points. As shown in Fig. 6 (a), the  
2 power-law exponent of the shear-thinning solutions is approximately 3.4. The spectra do not exhibit  
3 remarkable peaks and have broad region of power law decay, which is typical for turbulent flow[27]. We  
4 observed that the power law decay is dependent on the flowrates and has non-monotonic behavior. Such decay  
5 has been interpreted as the evidence of elastic turbulence. In comparison, for the case of Newtonian fluids, the  
6 power spectrum is extremely flat corresponding with noise. We believe that such chaotic flow leads to the  
7 enhanced effective mixing due to the enhancement of non-linear elastic stress gradient. The absolute power-  
8 law exponent of Newtonian fluids stays around 2, closely related to the laminar flow as illustrated in Fig. 6  
9 (b). Adversely, the absolute power-law exponent of polymeric solutions gradually increases with the bulk  
10 flowrates and reaches a platform at 3.4 at the value of  $V_b$  around  $4000 \mu\text{l}$  and  $6000 \mu\text{l}$  for 25PAAM and  
11 50PAAM, respectively, which indicates that the flow is fully chaotic. This saturated exponent is independent  
12 on the polymer concentration and have been investigated in our previous studies [42]. When the polymer  
13 solutions are normalized by the relaxation time, the transition point of the fully chaotic regime are similar  
14 around  $Wi=6.7$  for both concentrations as shown in Fig. 6. In this present work, the differences of polymer  
15 contribution to the viscosity between those polymer solutions are insignificant due to the much dilute  
16 concentration. Therefore, the critical  $Wi$  is in same level for both polymer solutions. In addition, the absolute  
17 power-law exponent plateaus more quickly at a lower flowrate in the polymeric solution with a slightly higher  
18 polymer concentration. The changes in the exponent observed here can be explained by the different driving  
19 mechanisms of the processes of mixing, of which the Newtonian fluid is molecular diffusion purely and the  
20 shear-thinning fluid is driven by the induced chaotic flow. The dramatically growth of the absolute exponent  
21 proves that the flow condition transferring from laminar to elastic instability. We believe that the slightly more

1 polymer addition into the Newtonian fluids leads to the stronger polymer stretching, resulting in the  
 2 enhancement of normal elastic stress gradient and the corresponding non-linear flow instability[14]. The  
 3 power law spectra of the normalized concentration show a high frequency oscillation. Contrary to general  
 4 case, where the power-law decay of the normalized concentration corresponding to elastic turbulence  
 5 commences at  $f = -1$ , the mixing in such orthogonal flows cause the power-law spectra start to decay at lower  
 6 frequencies as shown in the figure, perhaps due to the high frequency oscillations.



7 Fig. 6 Power spectra of the total normalized concentration in the dyed area at the flowrate  $V_b = 5000 \mu\text{l}/\text{min}$  (b) Absolute  
 8 power-law exponent versus flowrates from  $V_b = 3500 \mu\text{l}/\text{min}$  to  $V_b = 6000 \mu\text{l}/\text{min}$ .

10 **Fluctuations.** The increase in mixing is closely associated with the onset of fluctuations of the relative  
 11 change ratio of the total normalized concentration (Fig. 7) which is defined as follows:

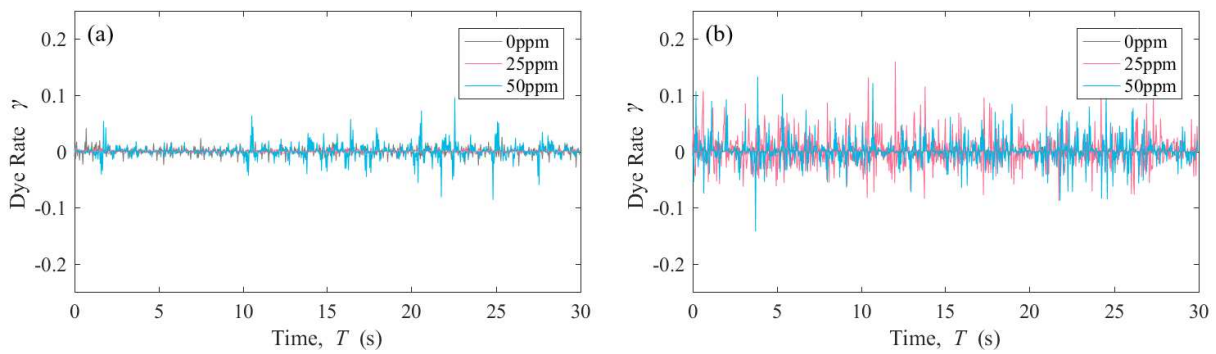
$$\gamma(i) = \frac{I_{i+1} - I_i}{I_i} \times 100\%$$

13 where  $I_i$  is the relative change ratio of the total normalized concentration in the dyed area,  $i$  is the series of  
 14 images captured by a frequency of 30Hz, which has been reported as a suitable frequency to capture the flow  
 15 characteristics of elastic instability and elastic turbulence[56]. We observe a clear increase in the fluctuations  
 16 of the relative change ratio of the total normalized concentration in the dyed area. Fig. 7 (a) shows the evolution

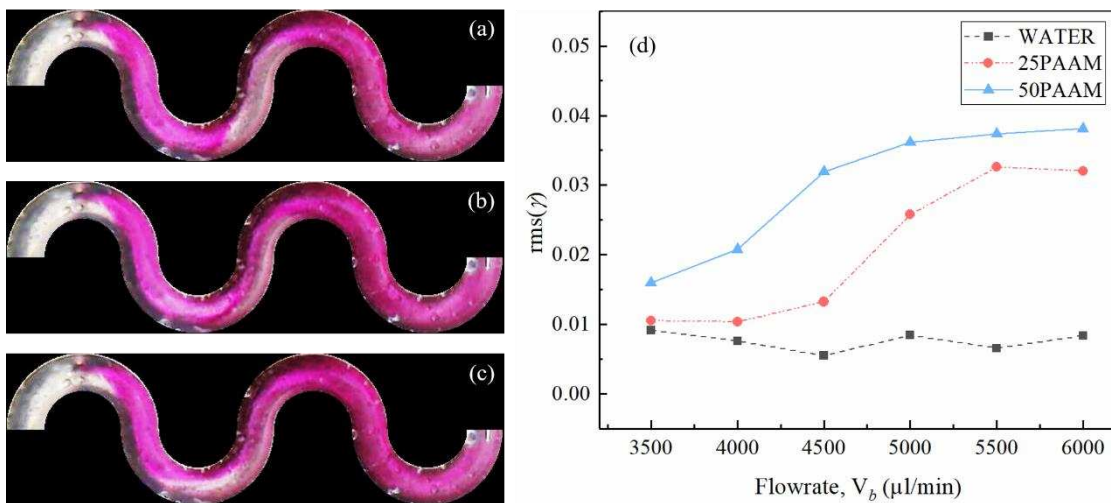
1 of such fluctuations within the sampling time. We illustrate the time dependent flow by showing a series of  
2 dye advection images in Fig. 8 (a)-(c). In the flow of polymeric solutions, the interfaces between the dyed and  
3 undyed fluids becomes unclear and oscillates with time, while in the flow of Newtonian fluids, the interface  
4 is sharp and steady. This indicates that a three-dimensional chaotic flow is induced here and becomes very  
5 complex which is comparable with the phenomenon shown by Arratia et al.[57] in the flow within a cross-  
6 channel flow.

7 Fig. 8(d) shows root-mean-square (rms) values of the relative-change-ratio fluctuations of both Newtonian  
8 and two shear-thinning fluids, respectively, as a function of flowrates. For the Newtonian fluid, the relative-  
9 change-ratio fluctuation remains small and steady, nearly independent of flowrate; the negligibly small  
10 increase in the fluctuation may be due to insignificant molecular diffusion. For polymer solutions, the rms  
11 values significant departure from the stable case of none polymer additions and shows a remarkable  
12 enhancement with increased flowrates accompanied by more irregular, more frequent, and stronger fluctuations  
13 until the secondary flow looks fully turbulent-like[58]. With the increase of polymer concentrations, the values  
14 of rms separate and plateau earlier at a lower flowrate which indicates that the transitions from laminar to  
15 subcritical instability and to chaotic flows with significant bifurcation instability occurs earlier, respectively.  
16 The amplitude of the fluctuation is not very large, and the signal jumps from the low dye rate to the high one  
17 frequently which is strongly benefit for the achievement of effective mixing as illustrated in Fig. 8. These  
18 results strongly indicate that a time-dependent flow can be created and sustained even with a very small  
19 amount of polymer addition when the flowrates exceeding a critical number. The relative-change-ratio of the  
20 concentrations is strongly fluctuating and its time dependence has well expressed chaotic advections. The  
21 chaotic performance is confirmed by the analysis of the root-mean-square (rms) of the relative-change-ratio

1 of the concentrations. These trends agree relatively well with the relative-change-ratio fluctuations and the  
 2 bifurcation instability observed in the flow visualization. Since that now the fluctuation of the relative-change-  
 3 ratio of the concentrations from the dyed space-time patterns (as examples in Fig. 4 shows) is available, it is  
 4 convenient to investigate the rule of flow state transitions for viscoelastic channel flows from the rms  
 5 development. Traditionally, for Newtonian fluids, the rms keeps small with negligible variations and  
 6 independent on the Weissenberg number. In what follows for polymeric solutions, we proposed that the rms  
 7 relative-change-ratio fluctuations is a good method to quantitatively scales the degree of elastic instability and  
 8 the transition from linear instability to a bifurcation instability and corresponding mixing performance.



9  
 10 Fig. 7 Fluctuations of the relative change ratio of the total normalized concentration of the dyed area versus time with solutions  
 11 of Water, 25PAAM and 50PAAM, respectively. (a) At the flowrate  $V_b = 3500 \mu\text{l}/\text{min}$ . (b) At the flowrate  $V_b = 5000 \mu\text{l}/\text{min}$ .



12  
 13 Fig. 8 (a)-(c) Dye advection patterns for the polymer solution with the concentration of 25 ppm in the time dependent regime

1 ( $V_b = 6000 \mu\text{l}/\text{min}$ ) at 3s intervals. (d) Root-mean-square (rms) of the fluctuations of the relative change ratio of the total  
2 normalized concentration of the dyed area as a function of flowrate for WATER, 25PAAM and 50PAAM.

3 **Conclusion.** In summary, a novel and effective micro mixer with orthogonal injection in the serpentine  
4 channel is proposed in this study. We have compared mixing behavior between the Newtonian fluid and shear-  
5 thinning fluids with low polymer concentrations in a micro serpentine channel with negligible inertial effect  
6 (low Re), and demonstrated that the orthogonal injection could boost the induction of elastic instability and  
7 promote effective mixing due to the augment of the interaction between the first normal stress difference and  
8 curvatures. A much earlier induced elastic instability is observed along the serpentine channel. Effective  
9 mixing is induced by the unstable chaotic flow via a nonlinear subcritical instability for finite perturbations.  
10 Even extremely small perturbations generated from the increased normal elastic stress gradient in the flow  
11 have the capability to induce significant mixing. The following conclusions can be drawn:

- 12 1. The progress of effective mixing and flow trajectories are developed over a short distance within the micro  
13 serpentine channel as proved by the dye visualization. Based on the new method, the main and dye streams  
14 of fluids can be easily mixed at a very short mixing length by using shear-thinning fluids with extremely  
15 low polymer concentrations. With the increase of flowrate and polymer concentration, flow instability  
16 transits from weak bifurcation instabilities to dramatically chaotic turbulence.
- 17 2. Effective mixing with a short mixing path is quantitatively characterized by statistical analysis.  
18 Probability Density Function (PDF) of normalized dye concentrations of the fluids indicates that the  
19 mixing efficiency can be significantly increased from 22% for the Newtonian fluids to 69% and 76% for  
20 the 25 and 50 PAAM respectively. The decay exponents of shear-thinning fluids plateau at -3.4 indicates  
21 the onset of elastic instability and chaotic flow. The relative-change-ratio fluctuations illustrated in the

1 observation area can generate sufficient normal elastic stress gradients to sustain the flow instabilities,  
2 resulting in effective mixing in the channel flow.

3 Our results show strong evidence for the “instability upon an instability” mechanism mentioned by Qin et  
4 al.[40] and provide a new method and device for the simplest mixing enhancement in micro channels without  
5 plenty of additions. We prove experimentally that the orthogonal injection is beneficial to achieve efficient  
6 mixing within a shorted mixing path. This work, provide a simple approach, by exploiting viscoelastic flow  
7 instability affected by shear-thinning effects, to enhance mixing in micro channels over a very short distance.  
8 Further studies are being undertaken to establish the velocity fields by using micro-PIV.

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