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Xiao, X orcid.org/0000-0003-0718-2591, Jia, H, Pervaiz, S orcid.org/0000-0002-6861-9374 et al. (1 more author) (2020) Molten Salt/Metal Foam/Graphene Nanoparticle Phase Change Composites for Thermal Energy Storage. ACS Applied Nano Materials, 3 (6). pp. 5240-5251. ISSN 2574-0970

https://doi.org/10.1021/acsanm.0c00648

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¹ Molten Salt/Metal Foam/Graphene Nanoparticle

² Phase Change Composites for Thermal Energy

3 Storage

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9 **ABSTRACT:** The binary and ternary mixtures of nitrates are desirable phase change materials 10 (PCMs) as latent heat thermal energy storage media for solar energy applications. In this study, 11 graphene oxide was synthesized with graphite powder firstly, then it was doped into HITEC salt 12 or solar salt solvent with sonication using two-step methods. Metal foams including nickel and 13 copper ones were impregnated with the salt seeded with graphene (nanocomposite) finally. The 14 morphologies of the synthesized composites were analyzed extensively, while the thermo-physical 15 properties of the composites were both theoretically predicted and experimentally investigated. 16 The results indicated that metal foam was compatible with nanocomposite, and the thermal 17 stabilities of the composite PCMs were good regarding the thermal cycle characteristics. The

1 effective thermal conductivities of the salt/graphene/metal foam composites were distinctly 2 enhanced, while the latent heats of the present composite PCMs were smaller than that of pure salt 3 to some extent. Furthermore, the phase change temperatures shifted slightly in the presence of 4 porous metal foam and graphene, while the addition of graphene could compensate for the 5 reduction of specific heats of the composite PCMs caused by metal foam. Finally, it was found 6 that the thermal effusivities of the salt/graphene/metal foam composites were larger than those of 7 pure salt, indicating the increments of 110~270% in solid state and 150~360% in liquid state, 8 respectively. The fundamental information of the nanocomposites with porous media could 9 broaden their application in thermal energy storage system.

KEYWORDS: molten salt; graphene; metal foam; morphological characteristics; thermal
 characterization

12 **1. INTRODUCTION**

13 Nowadays, renewable energy as one source of energy has drawn much attention due to the 14 increasing environmental problems such as global warming, COx emissions, depletion of zone 15 layer, etc. Solar energy as the clean and almost endless source of renewable energy is considered 16 as accessibility to energy resources in most countries in the world. However, energy system 17 integrated with solar energy is short of stability and reliability, which is caused by the intermittence 18 and instability of solar energy, as various regions with different climates. To overcome the 19 inevitable barriers of the imbalance between energy supply and requirement, energy storage is 20 proposed to address the time-dependant limitation essentially [1-2]. There are three different 21 methods for energy storage, including sensible heat storage, latent heat storage and chemical heat storage. Among them, latent heat thermal energy storage (LHTES) can provide a much higher
 energy storage density with a smaller temperature variation [3-4].

3 Molten salts as the phase change materials (PCMs), with relatively low cost and no 4 flammability, are widely used as the storage media of LHTES system among the temperature range 5 of 100-500 °C. It is difficult to directly use molten salts in real systems, as their weak thermal 6 stability and low thermal conductivity lead to low charging/discharging rates of the LHTES system. 7 It should be noted that many techniques related to heat transfer enhancement are adopted to 8 improve the thermo-physical properties of PCMs, and composite PCMs have received increasing 9 research interests. One of the effective methods is to impregnate PCMs into porous media such as 10 graphite foam and metal foam, which can significantly increase the thermal conductivities of the 11 PCMs [6-9]. Kholmanov et al. [6] fabricated carbon nanotube (CNT) network inside continuous 12 ultrathin graphite foam (UGF), then impregnated erythritol into the hybrid structure of UGF-CNT. The results indicated that the thermal conductivity increased to 4.1 W m⁻¹K⁻¹ and the sub-cooling 13 14 of erythritol was apparently suppressed. Wang et al. [7] synthesized cetyl palmitate/nickel foam 15 composites via melting infiltration method. It was found that the thermal conductivities of the composites fabricated with nickel foam of the pore sizes of 70, 90, 110 PPI were 0.6465, 0.6942, 16 1.6687 W m⁻¹K⁻¹, respectively, compared to that of pure cetyl palmitate of 0.3432 W m⁻¹K⁻¹. Xiao 17 18 et al. [8] synthesized the composite PCMs with paraffin and copper/nickel foams of different 19 porosities and pore sizes under vacuum impregnation method. The highest effective thermal conductivity in the results was 16.01 W m⁻¹K⁻¹, which was fabricated with copper foam of 89.0% 20 21 porosity and 1.0 mm pore size. Additionally, it was found that the pore size hardly affected the 22 effective thermal conductivity of the composite PCM. Feng et al. [9] experimentally and theoretically studied the effects of the porosity and pore density of the foam on the freezing rate, 23

which was conducted in a water/copper foam system with unidirectional freezing. They pointed out that the pore size slightly affected the freezing rate, and the local thermal equilibrium was verified with the temperature measurements of the foam skeleton and pore. However, majority of the studies indicated that the addition of metal foam would decrease the latent heat and specific heat of the composite PCM to some extent.

6 In other words, nanoparticles such as Al₂O₃, SiO₂, Fe₂O₃, TiO₂, CuO, MgO and CNT are with 7 exceptional thermal properties, and the utilization of those materials is one of the key effective 8 methods to improve the thermo-physical properties of pure PCMs [10-11]. Moreover, 9 nanoparticles have been recently proposed to mitigate the issue of low specific heats of molten 10 salts, i.e., keep and increase the specific heats of the nanocomposites [12-15]. Tiznobaik et al. [12] 11 studied the enhancements of specific heat of molten salt (Li₂CO₃:K₂CO₃=62:38) with the addition 12 of magnesium oxide nanoparticle. It was found that a semi-solid layer of dendritic shaped phase 13 was formed, contributing to the enhancement of the specific heats. Riazi et al. [13] experimentally 14 investigated the effects of the morphology and dispersion of particle on the specific heat of nano-15 salts fabricated by solar salt and silica nanoparticle, and stable dispersion could induce the 16 enhancement of the specific heat by 17.6%. Song et al. [14] investigated the specific heat of the 17 nanofluids made of Ca(NO₃)₂·4H₂O-KNO₃-NaNO₃-LiNO₃ and 1.0 wt.% SiO₂ nanoparticle with the size of 20 nm. The maximum specific heat increased by 17.0% when the nanofluid was 18 19 prepared under the condition of 750 rpm (stirring rate) and 15 min (mixing time). An enhancement 20 of 34.0% in the specific heat of binary carbonate salt was obtained by Zhang et al. [15], while the 21 salt was microencapsulated with silica shell. Graphene is with large specific surface area and stable 22 chemical characteristics, and extensively studied recently [16-23]. Yang et al. [20] synthesized the 23 composite PCMs made of polyethylene glycol (PEG) and hybrid graphene aerogels (HGA) via

1 vacuum impregnation, where HGA was composited of graphene oxide (GO) and graphene 2 nanoplatelets (GNP). It was found that the PEG/HGA composite presented high thermal 3 conductivity and good shape stabilization, e.g., the composite (0.45 wt.% GO, 1.8 wt.% GNP) had the thermal conductivity of 1.43 W m⁻¹K⁻¹, while that of pure PEG was 0.31 W m⁻¹K⁻¹. Chen et al. 4 [21] synthesized mePCMs with graphene oxide and octadecylamine (GO-ODA) via in-situ 5 6 polymerization. It was found that the supercooling of n-octadecane could be retrieved, and the 7 thermal conductivity and energy storage ability were substantially enhanced. Kant et al. [22] 8 numerically investigated the melting characteristics of an aluminum square cavity, which was 9 encapsulated with Capric Acid, CaCl₂·6H₂O, or n-octadecane mixed with graphene nanoparticles 10 in three different volumetric ratios (1%, 3%, and 5%). It was found that the graphene improved 11 the melting characteristics, but considerably degraded its natural convection heat transfer 12 efficiency. Yuan et al. [23] investigated the influences of the surface functionalization of graphene 13 on the properties of the polyethylene glycol/graphene composites with MD simulations. It was 14 found that the graphene increased the phase change temperature and specific heat. But these studies 15 indicated that the heat transfer enhancement with the addition of nanoparticles is very limit.

16 The integration of metal foam and nanoparticles together to enhance the thermo-physical 17 properties of pure salt can fill the research gap between thermal conductivity and thermal storage 18 capacity. However, the research on doping nanoparticles into molten salt/metal foam composite is 19 very few. The investigations of thermo-physical properties of the salt/graphene nanocomposites 20 and salt/graphene/metal foam composites are of vital importance. Based on the research 21 background of the storage of solar energy and geothermal energy within the temperature range of 22 100~300 °C for electricity generation, this research will be focused on preparation and 23 characterization of the salt/graphene/metal foam composites so as to see how the thermo-physical

1 properties of pure salt are affected by additives. Considering the suitable phase change 2 temperatures and moderate melting enthalpies [24-25], HITEC salt (40 wt.% NaNO₂, 7 wt.% 3 NaNO₃ and 53 wt.% KNO₃) and solar salt (60 wt.% NaNO₃ and 40 wt.% KNO₃) were employed 4 as the PCMs. Graphene oxide synthesized with several chemical processes were doped into salt 5 solvent with two-step method firstly, and metal foam was impregnated with graphene seeded salt 6 finally. The morphologies of the materials were analyzed by Scanning Electron Microscope (SEM), 7 Fourier Transform Infrared Spectrometer (FTIR) and X-ray diffraction (XRD), and the thermal 8 conductivities of the composite PCMs were theoretically predicted based on the correlations and 9 models of the porous media. The thermal behaviors of all the materials were analyzed with DSC 10 (differential scanning calorimeter), and the thermal stabilities and thermal effusivities were studied 11 subsequently. It is highly indispensable to study the thermo-physical properties of the composite 12 PCMs, which largely determine the performance and applicability of the LHTES system. And the 13 LHTES system can be integrated into solar energy and geothermal energy utilization systems.

14

2. PREPARATION AND THERMAL CHARACTERIZATION

15 2.1. Graphene oxide and composite PCMs

The graphene oxide was produced from graphite powder involving several chemical processes by adopting the modified Hummer's method [26-27], which was done in controlled environment. Graphite powder ($<20 \mu$ m, Sigma Aldrich, UK) was considered as the starting material. Sulphuric acid (H₂SO₄, concentration: 95%, VWR Chemicals, UK) and nitric acid (HNO₃, concentration: 69%, VWR Chemicals, UK) were used to oxidize graphite powder in water solution. As a typical synthesis procedure shown in **Figure 1 (a)**, 12 g of graphite powder was mixed with 100 mL H₂SO₄ and 50 mL HNO₃ in a conical flask, and the solution was kept on stirring for 24 h at a hot

1 plate of about 50 °C. The reactants were synthesized with the addition of 100 mL of Deionized 2 (DI) water, which were continuously magnetic stirring in a whole day. Then 12 g of potassium 3 permanganate (KMnO₄, concentration: 99%, Sigma-Aldrich, UK) was slowly added to the above 4 solution, and stirred in an ice bath of 0 °C for 5 h. 60 mL of hydrogen peroxide (H₂O₂, 5 concentration: 36%, Sigma-Aldrich, UK) was added, and the suspension was stirred overnight, 6 which was conducted in the ice bath to keep the temperature low. Subsequently a filter paper 7 (Whatman #42) was used to filter the resultant suspension. Then the filtrate from the solution was 8 successively washed three times with hydrochloric acid (HCl, concentration: 10%, Sigma-Aldrich, 9 UK) and DI water, which was then centrifuged with Heraeus Megafuge 16R (ThermoFisher 10 Scientific, UK) at 13000 rpm for 1 h. After discarding the supernatant, the remaining material was 11 then vacuum-dried overnight at 40 °C. Finally the graphene oxide nano-sheets were obtained.

12 NaNO₃ (Honeywell Fluka, UK), KNO₃ (Acros Organics, UK) and NaNO₂ (Honeywell Fluka, 13 UK) were used as the base PCM, and the previous graphene and metal foam (Suzhou Longde 14 Metal Foam Electronics Co. Ltd., CN; Porosity: 95.0%; Pore size: 10 pores per inch) were applied 15 to enhance the thermo-physical properties of pure salt. Table 1 lists the thermo-physical properties 16 of HITEC salt, solar salt, graphene (subscript np), and metal foam [28-30]. Figure 1 (b) shows the 17 synthesis process of the salt/graphene/metal foam composites, which was similar to that of the 18 salt/Al₂O₃ nanopowder/metal foam composites in a previous research [31]. Firstly, NaNO₂, 19 NaNO₃ and KNO₃ with mass ratios of 40:7:53 named HITEC salt was prepared and dissolved into 20 DI water. Graphene with different mass fractions (1%, 2% or 3%) was suspended in the solution, 21 respectively, which was then sonicated for 1 h (FB15057 ultrasonicator), so as to make good 22 dispersion. Then the immersion of metal foam in a metal disc filled with the solution was carried 23 out, which was sonicated with 10 mins to evacuate the air. The metal disc with the solution was

heated inside an eurotherm oven manufactured by Carbolite Sheffield at 200 °C for 30 mins, then the salt/graphene/metal foam composite PCMs were obtained after naturally cooled. A similar method was used to synthesize the solar salt/graphene/metal foam composites, while NaNO₃ and KNO₃ with a mass ratio of 60:40 and a heating temperature of 250 °C were used instead. Series morphological and thermal characterization of the composites were addressed subsequently.

6 2.2. Morphological analysis

TEM (Transmission electron microscopy, FEI Tecnai TF20, Oxford Instruments, UK) was used to reveal the size of the synthesized graphene, so as to check whether the nanoparticles prepared are in nanoscale or not. Tabletop Microscope TM3030Plus (SEM, Hitachi High-Technology, Japan) was used to measure the surface characteristics of the composites on an uneven area, the modes of BSE and EDX were applied.

12 FTIR and XRD which investigates the functional groups presented in a specimen can analyze chemical bonding and molecular structure of the specimens. In the present study, Nicolet IS10 FT-13 IR spectrometer (ThermoFisher Scientific, UK) with a resolution of 4 cm⁻¹ covers wavelength 14 range of 400~4000 cm⁻¹, and gives the spectra of all the specimens at room temperature. The lab-15 16 based XRD used was a D8 powder diffractometer (Bruker, UK) with a Vantec detector (Cu-Ka 17 source, 1.540 Å). The reflections of X-Rays was conducted by crystallographic atomic planes, and 18 the operational voltage and applied current for the instrument were maintained at 40 kV and 40 19 mA, respectively. The specimen of about 0.5 g was prepared and filled in a shallow and circular 20 holder, which was with the diameter of 4 cm and the depth of 1.5 cm. During the experiments, the 21 total scanning time was 45 mins considering a step size of 0.035 ° and a scanning range of 10-60 22 ^o, then the data were analyzed using X'Pert HighScore Plus software.

1 **2.3.** Techniques of thermal characterization

2 **2.3.1.** Characterization of effective thermal conductivity

Graphene used in the present study are with the density and thermal conductivity of 2200 kg m⁻³ and 5000 W m⁻¹K⁻¹, respectively [22], and the densities of the nanocomposites are shown in Supporting Information (**Table S1**). Nanoparticles can affect the thermal conductivity of the nanocomposite, which can be estimated with the theoretical models. The effective thermal conductivity of the nanocomposite (λ_{nc}) was calculated with the modified Maxwell-Garnett model [32-33], which considered the Brownian motion and nanoparticles aggregation and shown as follows:

10
$$\frac{\lambda_{nc}}{\lambda_{PCM}} = \frac{\lambda_{np} + 2\lambda_{PCM} - 2\Phi(\lambda_{PCM} - \lambda_{np})}{\lambda_{np} + 2\lambda_{PCM} + \Phi(\lambda_{PCM} - \lambda_{np})} + \frac{\rho_{np}\Phi c_{p-np}}{2\lambda_{PCM}}\sqrt{\frac{2K_BT_{nc}}{3\pi d_{np}\mu_{PCM}}}$$
(1)

where K_B is Boltzmann constant, d_{np} is nanoparticle size, which is 350 nm in the present study [34]. 11 12 T_{nc} is the temperature of nanocomposite, and μ_{PCM} is the viscosity of pure salt. Based on the 13 comparisons between the experimental measurements with steady state method and the theoretical 14 predictions with models in the previous research [8], it has been proven that the models can 15 accurately predict the thermal conductivities of the composite PCMs fabricated by metal foam. 16 Thus the thermal conductivities of the salt/graphene/metal foam composites were theoretically 17 predicted in the present study, due to the lack of steady state test device. A series of structural models were chosen based on the previous comparisons [35-37], as listed in Table S2. 18

19 **2.3.2.** Characterization of thermal behavior

The phase change behaviours of pure salt and composite PCMs were conducted with a MettlerToledo DSC (DSC1, Mettler Toledo Ltd., Leicester, UK), with the accuracy of temperature

1 measurement of ±0.02 °C. The specimen was weighted using an Ultra-microbalance Mettler-2 Toledo balance (UMX2, Mettler Toledo, Leicester, UK) with an uncertainty of ±0.001 mg, and 3 half of the crucible was filled to avoid the overflow issue. A standard aluminum crucible with 100 4 μ L as the sample crucible was encapsulated with about 20.0~30.0 mg specimen, then the sample 5 crucible and an empty crucible considered as the reference were symmetrically put into a platinum-6 iridium furnace. The heating method for HITEC salt and its composites was maintained at 50 °C 7 for 10 mins, ramped from 50 °C to 200 °C at a rate of 5 °C min⁻¹, then kept isothermally for 10 8 mins at 200 °C. While the cooling method was similar and ramped from 200 °C to 50 °C at a rate 9 of -5 °C min⁻¹, and the phase change of the specimens were characterized by both the extrapolated 10 onset and peak temperatures. The thermal cycle for solar salt and its composites was similar, while 11 the only difference was the temperature ranged from 100 °C to 300 °C.

The present DSC was also used to measure the specific heat of pure salt and its composites both in solid phase and liquid phase. The method followed to calculate the specific heat was the three-step procedure [38]. Firstly, the baseline heat flux (q_0) was recorded from two empty crucibles. Secondly, the heat flux $(q_{sapphire})$ was recorded from one crucible sealed with the standard sapphire and one empty one. Thirdly, the heat flux of the specimen was recorded (q_s) , where one crucible sealed with the specimen was used instead of the sapphire crucible. The specific heat of the specimen $(c_{p, s})$ can be calculated as follows:

19
$$c_{p,s} = c_{p, \text{sapphire}} \frac{\Delta q_s / m_s}{\Delta q_{\text{sapphire}} / m_{\text{sapphire}}}$$
(2)

In the present study, the salt and its composites were subjected to the same thermal procedure, that is, heated from 100 °C to 300 °C at 25.0 °C min⁻¹ and isothermal at 100 °C and 300 °C for 10 mins, respectively.

1 2.3.3. Thermo-gravimetric analysis and thermal effusivity

The weight of a specimen will be positively or negatively affected by the physical or chemical changes. Mettler-Toledo TGA (DSC1, Mettler Toledo Ltd., Leicester, UK) was used to detect the variation of mass correlated to temperature, and the operating temperature ranged from 40 °C to 5 850 °C at 10 °C min⁻¹ in the present study. The ceramic crucibles were selected to adapt the materials and temperatures of the experiments, and about 5.00 to 10.00 mg specimens were loaded into the crucibles. Nitrogen purge gas with the purity of 99.99% was worked as carrier under a flow rate of 50 mL min⁻¹, which was controlled by a gas controller GC100.

9 The thermal effusivity of a material illustrates the capability of a material to exchange thermal 10 energy with its surroundings [30, 38]. The thermal effusivity (*e*) is defined in Eq. (3).

11
$$e = \sqrt{\rho c_p \lambda}$$
(3)

The thermal effusivity consists of the heat capacity and heat transfer rate of the material, and is a critical physical quantity and a controlling parameter in describing the heat transfer performance in a number of industrial applications. In the present study, the thermal effusivities in both solid and liquid states were calculated respectively. For the calculation of thermal conductivity, 25 °C was considered in Eq. (1) in solid state, while 200 °C for HITEC salt and 250 °C for solar salt were considered in liquid state.

18 **3. RESULTS AND DISCUSSION**

19 **3.1. Morphologies of composite PCMs**

Figure 2 shows the morphologies of the graphene and composite PCMs characterized by TEM and SEM. The graphene shown in Figure 2 (a) is with the size of hundred nanometers, consists of

1 porous-like flakes. The SEM pictures of the salt/graphene nanocomposites are shown in Figure 2 2 (b). It can be found that the sample shows a smooth appearance in large scale, and a granular 3 appearance partially in the SEM pictures. As a result, distinguishing the nanoparticle (graphene) 4 from salt becomes difficult. Figure 2 (c) and (d) shows the samples of the salt/graphene/metal 5 foam composites. It can be seen that there is no separation between the nanocomposite and metal 6 foam, and the existence of the elements Cu, Na, K, N has been verified in the EDS spectrum. In 7 addition, a dimensionless parameter α [39] is employed to evaluate the compatibility between the 8 nanocomposite and metal foam, where the parameter reflects the ratio of the actual mass to the 9 ideal one of the nanocomposite impregnated into the porous metal foam. It was found that the 10 impregnation ratio can reach above 90.0% in the present study.

11 Figure 3 (a) shows FT-IR absorption spectra of pure salts, the salt/graphene nanocomposites and 12 salt/graphene/metal foam composites. The peaks in FTIR spectra (Figure 3 (a-I)) for HITEC salt and its composite PCMs are observed at 835 cm⁻¹, 1228 cm⁻¹, 1370 cm⁻¹, 1763 cm⁻¹ and 2396 13 cm⁻¹, while the peaks in FTIR spectra (Figure 3 (a-II)) for solar salt and its composite PCMs are 14 observed at 834 cm⁻¹, 1345 cm⁻¹, 1763 cm⁻¹, 1789 cm⁻¹ and 2428 cm⁻¹. The difference should be 15 16 attributed to the element of sodium nitrite (NaNO₂) in HITEC salt. It can be seen that no apparent 17 difference of FT-IR absorption spectra are found for all the specimens fabricated by the same salt, 18 indicating that the physical bonding of graphene with nitrate or nitrite exist does not interrupt the 19 chemical structure interaction. Thus graphene can mix well with salt, similarly to other 20 nanoparticles [40]. In addition, FT-IR absorption spectra also indicate that the salt/graphene/metal 21 foam composite has no occurrence of new structure.

Figure 3 (b) presents XRD patterns of pure salts, the salt/graphene nanocomposites and salt/graphene/metal foam composites. It can be seen from the pattern of HITEC salt that,

characteristic peaks appear at 19.35°, 23.86°, 29.72°, 32.30°, 34.11°, 41.45°, 44.77° and 51.41°. 1 While characteristic peaks appear at 23.94°, 29.52°, 32.14°, 39.19° and 48.13° from the pattern of 2 3 solar salt. The appearance and disappearance of peaks correspond to the relevant elements. Other 4 characteristic diffraction peaks of the composite PCMs are nearly the same as those of pure salt. It 5 can be concluded that the salt remains intact in the metal foam without chemical reaction, and is 6 also not greatly affected by graphene. As a result, all combinations are formed by physical action. 7 However, it can be seen from Figure 3 (b) that new peaks marked in rectangular regions appear at 8 around 26~28° in the patterns of the salt/graphene/metal foam composites. Those peaks should be 9 an indication of the appearance of nickel or copper element.

10 **3.2.** Thermal characterization of composite PCMs

11 **3.2.1.** Effective thermal conductivities of composite PCMs

Figure 4 shows the calculations of the effective thermal conductivities of the composite PCMs, 12 which were considered in solid state (T=25 °C). It is shown that the effective thermal conductivities 13 of the salt/graphene nanocomposites increase slightly. The effective thermal conductivities of 14 HITEC salt/graphene nanocomposites are 1.045 W m⁻¹K⁻¹, 1.091 W m⁻¹K⁻¹ and 1.137 W m⁻¹K⁻¹ 15 16 with the addition of 1 wt.%, 2 wt.% and 3 wt.% graphene, respectively, while those of solar salt/graphene nanocomposites are 1.049 W m⁻¹K⁻¹, 1.099 W m⁻¹K⁻¹ and 1.150 W m⁻¹K⁻¹. The 17 18 phenomenon is a little higher than those in the literature [40-41], e.g., the thermal conductivity of solar salt/1 wt.% Fe₂O₃ nanocomposite is 0.828 W m⁻¹K⁻¹ [40], while the thermal conductivity of 19 solar salt/0.5 wt.% MgO nanocomposite is 0.853 W m⁻¹K⁻¹ [41]. The reason is that the thermal 20 21 conductivities of the iron oxide and magesium oxide are slightly lower than that of graphene. 22 Similarly, the addition of 1~3 wt.% graphene slightly increases the effective thermal conductivities

1 of the salt/metal foam composites, i.e., the effective thermal conductivities of the salt/nickel foam 2 composites and salt/copper foam composites can be enhanced by 8~16% and 26~49%, 3 respectively. Moreover, the effective thermal conductivities of the salt/graphene/metal foam 4 composites are greatly enhanced, e.g., the effective thermal conductivity of HITEC salt/3 wt.% 5 graphene/copper foam composite can reach approximate 8.7 W m⁻¹K⁻¹, indicating about 1140% increment in comparison with HITEC salt; While that of HITEC salt/3 wt.% graphene/nickel foam 6 7 composite can reach approximate 3.0 W m⁻¹K⁻¹, indicating about 330% increment in comparison with 8 HITEC salt. Therefore, there are apparent difference between the effective thermal conductivities 9 of the salt/graphene/copper foam composites and those of the salt/graphene/nickel foam 10 composites, which is caused by the higher thermal conductivity of copper skeleton, as listed in 11 **Table 1**. However, because of corrosion issue of copper induced by salt, the balance related to the 12 thermal conductivity and thermal stability should be considered in practical application. It can be 13 concluded that the composite PCMs with good thermal characteristics can be the effective media 14 in the application of LHTES system, given that metal foam provides conductive paths for heat 15 transfer. In addition, in a preliminary pilot test, it is found that the time-duration of solar salt/2 wt.% 16 graphene/copper foam composite for heat storage is considerably reduced by about 75.0%, in 17 comparison with that of pure solar salt, which verifies the large thermal conductivity of the composite 18 PCMs.

19 **3.2.2.** Phase change behaviors of composite PCMs

The phase change temperatures and latent heats of pure salts, the salt/graphene nanocomposites and salt/graphene/metal foam composites were obtained with DSC. **Figure 5** shows the values of the phase change temperatures of pure salts and composite PCMs. With the addition of graphene, the extrapolated onset melting temperatures and onset freezing temperatures of pure salts can be

1 slightly decreased and increased, respectively, e.g., for HITEC salt/3 wt.% graphene 2 nanocomposite, the extrapolated onset melting temperature and onset freezing temperature shift 3 from 138.67 °C and 141.79 °C to 137.27 °C and 142.08 °C, respectively, in comparison with those 4 of HITEC salt; While for solar salt/3 wt.% graphene nanocomposite, the extrapolated onset melting 5 temperature and onset freezing temperature shift from 220.82 °C and 227.29 °C to 219.31 °C and 6 227.45 °C, respectively, in comparison with those of solar salt. The early occurrence of phase 7 change is mainly because of the good combination and dispersion performance of the salt and 8 nanoparticles [38], as depicted in Figure 2 (b). The combined effects of metal foam and graphene 9 induce the variations of phase change temperatures of the salt/graphene/metal foam composites to 10 some extent. It can be seen that for HITEC salt, the melting/freezing phase change temperatures 11 of the salt/graphene/copper foam composites deviate from 1.11 °C maximumly, whereas that of 12 the salt/graphene/nickel foam composites is about 0.69 °C. For solar salt, the melting/freezing 13 phase change temperatures of the salt/graphene/copper foam composites deviate from 4.13 °C 14 maximumly, whereas that of the salt/graphene/nickel foam composites is about 4.96 °C.

15 Figure 6 shows the variations of latent heats for pure salts and the composite PCMs. Three 16 measurements were done to ensure the repeatability and accuracy of the results. The latent heats 17 of the salt/metal foam composites decrease significantly as metal skeleton does not undergo the 18 phase change process, e.g., the latent heat of HITEC salt/nickel foam composite decreases from 60.62 kJ kg⁻¹ to 48.37 kJ kg⁻¹, while that of solar salt/nickel foam composite decreases from 108.39 19 kJ kg⁻¹ to 77.47 kJ kg⁻¹, in comparison with that of pure salt. The addition of graphene can slightly 20 21 affect the latent heats of the salt and salt/metal foam composites, e.g., the latent heats of HITEC salt and HITEC salt/nickel foam composite decrease to 57.59 kJ kg⁻¹ and 46.32 kJ kg⁻¹ with the 22 23 addition of 3 wt.% graphene, respectively; while those of solar salt and solar salt/nickel foam composite decrease to 104.59 kJ kg⁻¹ and 74.53 kJ kg⁻¹ with the addition of 3 wt.% graphene, respectively. The phenomenon of the slight decrease of latent heat can be attributed to the two reasons. On one hand, the mass fraction of graphene is very small and within 3%, which should reduce the latent heat slightly. On the other hand, the increase of the interfacial thermal resistance caused by the interface between the salt and graphene might affect the latent heat to some extent [42]. A compromise between the metal foam and graphene should be considered to get the suitable thermo-physical properties of the composite PCMs in practical application.

8 **3.2.3. Specific heats of composite PCMs**

9 Table 2 lists the mean specific heats of HITEC salt, the salt/graphene nanocomposites and 10 salt/graphene/metal foam composites. The specific heats in solid and liquid states were calculated 11 within the temperature range of 105~110 °C and 180~290 °C, respectively. It can be seen that with the addition of graphene, the specific heats of the nanocomposites are enhanced both in solid 12 and liquid states, e.g., the specific heats of HITEC salt/3 wt.% graphene nanocomposite are 1.463 13 kJ kg⁻¹K⁻¹ and 1.601 kJ kg⁻¹K⁻¹ in solid and liquid states, compared to those of HITEC salt of 14 1.415 kJ kg⁻¹K⁻¹ and 1.562 kJ kg⁻¹K⁻¹, respectively. It can be summaried that the enhancements 15 16 are about 0.80~3.39% in solid state, and -1.43~2.47% in liquid state with the graphene 17 concentration of 1~3 wt.%. Furthermore, the specific heat enhancements are compared with those 18 in the literature [43], as listed in **Table S3**. The enhancements are a little lower than those in the 19 relevant work, which is mainly due to the type, size and concentration of the nanoparticles. In 20 contrast, the specific heats of the salt/graphene/metal foam composites decrease, in comparison 21 with that of HITEC salt, which is due to the inclusion of metal foam. It is found that the 22 weaknesses of specific heat are about 0~12.01% in solid state, and 0.80~11.61% in liquid state 23 totally.

1 Table 3 lists the mean specific heats of solar salt, the salt/graphene nanocomposites and 2 salt/graphene/metal foam composites. The specific heats in solid and liquid states were calculated 3 within the temperature range of 150~200 °C and 260~290 °C, respectively. It can be seen that 4 with the addition of graphene, the specific heats of the nanocomposites are also slightly enhanced 5 in solid state, e.g., the specific heat of solar salt/3 wt.% graphene composite is $1.843 \text{ kJ kg}^{-1}\text{K}^{-1}$ in solid state, compared to that of solar salt of 1.830 kJ kg⁻¹K⁻¹. It can be seen that the enhancements 6 7 are about $0.05 \sim 2.45\%$ in solid state with graphene concentration of $1 \sim 3$ wt.%, which are lower to 8 be -7.46~-0.27% in liquid state. Similarly, Table S3 lists the comparisons of specific heat 9 enhancements with those in the literature [13, 40, 41, 44-47]. As different types, sizes and 10 concentrations of the nanoparticles were used by the researchers, diverse enhancements are 11 presented accordingly. The specific heat enhancements in the present study show general 12 agreement with the relevant works. Additionally, the same tendency is found between current 13 study and the study of Awad et al. [40], that is, the specific heat enhancements become lower in 14 liquid state than those in solid state. On the contrary, the specific heats of the salt/graphene/metal 15 foam composites decrease similarly, compared to that of solar salt, due to the inclusion of metal 16 foam. It is found that the weaknesses of specific heat are about 3.81~19.48% in solid state, and 17 5.56~18.81% in liquid state.

The phenomenon of the increase of specific heats for the salt/graphene nanocomposites can be attributed to the following reasons. Graphene nanoparticles strongly interact with the molten salt molecules around, and contribute to form the nanostructure named compressed layer with extremely large specific surface area [13, 42, 48-49]. This different structural characteristics cause large intermolecular force together with the increased surface energy, and induce the enhancement of the effective specific heat subsequently. Additionally, the interfacial thermal

resistance of the nanostructure between the salt and graphene will increase with the increased
 surface area to some extent [42], but it will not affect the total thermal resistance of the composite
 PCMs. Further molecular dynamics simulation and heat transfer analysis are needed to clarify the
 mechanism of the enhancement of specific heat.

5 3.2.4. Thermo-gravimetric analyses of composite PCMs

6 Figure 7 shows the thermo-gravimetric analyses of pure salts and salt/graphene/metal foam 7 composites. It can be seen that the tendency of two type of salts and their composites are similar. 8 There is no mass descending until 300 °C, indicating that the samples are totally dry for the 9 experiments. HITEC salt is stable up to about 540 °C, then rapid degradation of the salt appears, 10 as shown in Figure 7 (a). It can be seen that nearly 60% of the mass loses between 550°C and 11 800°C. The mass remain percentage at 800 °C for HITEC salt, HITEC salt/1 wt.% graphene, HITEC salt/2 wt.% graphene and HITEC salt/3 wt.% graphene are 41.39%, 44.40%, 48.19% and 12 13 53.27%, respectively. The larger percentages of HITEC salt/graphene composites might be due to 14 the inclusion of graphene, which can exist over 800 °C. A solid stable compound may be produced as the mass slightly changes above 800°C, e.g., the mass remain percentage of HITEC salt at 850 15 16 °C is 39.74%. Because all the TGA tests were conducted under the atmosphere of nitrogen to avoid 17 oxidation, and most of the mass loss happens through the release of nitrogen and oxygen gases. 18 The remain mass in the crucible might be a mixture of sodium and potassium oxide. Furthermore, 19 the salt/graphene/metal foam composites show larger mass left at the final stage, as the metal 20 skeleton (nickel or copper) can be kept over 850 °C [50-51].

It can be seen from Figure 7 (b) that solar salt is also stable up to about 590 °C, then rapid
degradation appears. Similarly, the salt/graphene nanocomposites are with larger percentages of

mass at 800 °C, in comparison with that of pure solar salt. The salt/graphene/metal foam composites show larger mass left finally because of the metal skeleton (nickel or copper), almost 65.0% and 75.0% for the salt/3 wt.% graphene/nickel foam composite and the salt/3 wt.% graphene/copper foam composites. However, it can be seen from Figure 7 that the mass remain percentages of the salt/graphene composites below 600 °C are slightly lower than that of pure salt, which might be caused by the tolerance of the experiments.

7 3.2.5. Thermal stabilities of composite PCMs

8 The stabilities of the salt/3 wt.% graphene/metal foam composites were determined with DSC, 9 which were performed similarly to section 3.2.2 of thermal behaviour characterization. Figure S1 10 shows examples of the curves of fifty thermal cycles, and it can be seen that the peaks belongs to 11 solid-solid phase change are obvious in several thermal curves at the beginning, but those peaks 12 degrade in the following thermal cycles. However, the solid-liquid phase change can be kept well 13 with the thermal cycles, and slight changes are found after the circulations. It is found that the 14 phase change temperatures together with latent heats of the composite PCMs after fifty thermal 15 cycles are almost the same as those shown in **Figures 5** and **6**, indicating that the samples are with 16 good stabilities. Furthermore, the morphologies of the sample before and after thermal cycles 17 indicates that slightly separation between graphene and salt appears after fifty cycles. A 18 preliminary pilot test shows that the temperature evolutions appear almost no difference after 19 several heat storage/retrieval processes.

20 **3.3. Thermal effusivities of composite PCMs**

The effusivities of pure salts, the salt/graphene nanocomposites and salt/graphene/metal foam composites are calculated, and the results both in solid and liquid states are listed in **Tables 2** and

1 **3**. Here, only the thermal conductivities calculated with the model of Calmidi and Mahajan were 2 considered [35]. Generally, because of the good thermo-physical properties of graphene, the 3 present effusivities of the nanocomposites are slightly larger than those in the literature, e.g., the effusivities of the solar salt/1 wt.% Fe₂O₃ nanocomposite are 1.636 kJ m⁻²K⁻¹s^{-1/2} and 1.301 kJ m⁻ 4 2 K ${}^{-1}$ s ${}^{-1/2}$ in solid and liquid states [40], in comparison with those of the solar salt/1 wt.% graphene 5 nanocomposite of 2.023 kJ m⁻²K⁻¹s^{-1/2} and 1.794 kJ m⁻²K⁻¹s^{-1/2}, respectively. It can be seen that the 6 7 effusivities of the composite PCMs are larger than those of pure salt, e.g., the effusivities of HITEC salt/3 wt.% graphene/copper foam composite are 5.11 kJ m⁻²K⁻¹s^{-1/2} in solid state and 5.27 kJ m⁻ 8 2 K⁻¹s^{-1/2} in liquid state, while those of HITEC salt are 1.43 kJ m⁻²K⁻ s^{-1/2} and 1.15 kJ m⁻²K⁻¹s^{-1/2} in 9 10 solid and liquid states, respectively. It is due to the reason that although the specific heats of the 11 salt/graphene nanocomposites and salt/metal foam composites decrease slightly, the thermal 12 conductivities of those composite PCMs increase. It can be concluded that the effusivities of the 13 salt/graphene/metal foam composites can be increased by 110~270% in solid state and 150~360% 14 in liquid state, respectively. Furthermore, as the inclusion of metal foam greatly increases the 15 thermal conductivities of pure salts (shown in Figure 4), the thermal effusivities of the 16 salt/graphene/metal foam composites are larger than those of the salt/graphene nanocomposites, 17 which benefits heat storage. The potential application of the salt/graphene/metal foam composites 18 can increase the heat storage/retrieval rates of the LHTES system, inducing the high power and 19 energy efficiency of the system.

It can be seen from **Table 2** that the thermal effusivities of HITEC salt and its composite PCMs are almost the same in solid and liquid states, which is because that the density and thermal conductivity of HITEC salt are larger in solid state than those in liquid state, but the specific heat of HITEC salt is lower in solid state than that in liquid state. However, **Table 3** show that the thermal effusivities of solar salt and its composite PCMs are very different between solid and liquid states, which is because that the density, thermal conductivity and specific heat of solar salt are larger in solid state than those in liquid state. Therefore, the characteristics of different thermal effusivities in solid and liquid states should be considered in the selection of PCMs used in the real temperature range. Moreover, the addition of graphene and metal foam can restrict the flow of liquid salt, and retrieve the issue of the leakage accordingly, which provides a new strategy for obtaining shape-stabilized PCMs applied for thermal energy storage.

8 4. CONCLUSIONS

9 In the present study, HITEC salt and solar salt were used as the pure PCMs, and graphene and 10 metal foam were combined to enhance pure salts. The composite PCMs were synethesized and 11 morphologically and thermally characterized, and the conclusions can be drawn as follows:

12 (1) The salt/graphene nanocomposite is totally compatible with metal foam, and no obvious 13 changes of wavelength peaks are found with FT-IR analyses. Small peaks appear in XRD 14 pattern of the salt/graphene/metal foam composites due to the addition of metal elements. 15 (2) The effective thermal conductivities of the salt/graphene/metal foam composites are greatly 16 enhanced, while those of the salt/graphene nanocomposites are slightly enhanced, in 17 comparison with that of pure salt. A preliminary pilot test indicates that the time-duration of 18 solar salt/2 wt.% graphene/copper foam composite for heat storage can be considerably 19 reduced by about 75.0%, in comparison with that of pure solar salt.

(3) With the addition of graphene, the extrapolated onset melting temperatures and onset freezing
 temperatures of pure salts can be slightly decreased and increased, respectively. The maximum
 deviation of the melting/freezing phase change temperatures of the HITEC

salt/graphene/copper foam composites is 1.11 °C, whereas that of the solar
 salt/graphene/copper foam composites is 4.13 °C. The specific heats of the salt/graphene
 nanocomposites are enhanced with the addition of graphene in solid state.

(4) Thermo-gravimetric analyses indicate that HITEC salt and solar salt are stable up to about 540
°C and 595 °C, respectively. Slight changes of phase change temperature and latent heat are
found after the composite PCMs underwent fifty melting-freezing cycles, indicating the good
stabilities of the composites. The effusivities of the salt/graphene/metal foam composites are
larger than those of pure salt, indicating the increments of 110~270% in solid state and
150~360% in liquid state, respectively.

10 Consequently, the investigations of thermo-physical properties of the nanocomposites with porous 11 media will lead to guide the design and model of the thermal energy storage system and improve 12 the performance of the system accordingly. In other words, it will extend the application of 13 nanoparticles in thermal energy storage.

14 ASSOCIATED CONTENT

15 Supporting Information

16 The following files:

17 Densities and volume fractions of the salt/graphene nanocomposites; Correlations and models of 18 effective thermal conductivities of the composite PCMs; Comparisons of specific heats with the 19 results in the literature; Repeated DSC curves of the salt/graphene/metal foam composites (PDF)

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- 8 Notes
- 9 The authors declare no competing financial interest.

10 ACKNOWLEDGMENT

11 The authors would like to acknowledge the support of EU Marie Sklodowska-Curie International

- 12 Incoming Fellowship (Project reference: 706788) and the European Research Council
- 13 Consolidator Grant (ERC2014-CoG, Project reference: 648375).

14 **REFERENCES**

- [1] Pelay, U.; Luo, L.; Fan, Y. L.; Stitou, D.; Rood, M. Thermal energy storage systems for
 concentrated solar power plants. *Renew. Sustain. Energy Rev.* 2017, 79, 82–100.
- 17 [2] Kuravi, S.; Trahan, J.; Goswami, D. Y.; Rahman, M. M.; Stefanakos, E K. Thermal energy
- 18 storage technologies and systems for concentrating solar power plants. *Prog. Energy Combust.*
- 19 *Sci.* **2013**, 39, 285–319.

1 [3]	Zhang, P.; Xiao, X.; Ma, Z. W. A review of the composite phase change materials: Fabrication,
2	characterization, mathematical modeling and application to performance enhancement. Appl.
3	<i>Energy</i> 2016 , 165, 472–510.
4 [4]	Zhu, S. L.; Nguyen, M. T.; Tokunaga, T.; Yonezawa, T. Size-tunable alumina-encapsulated
5	Sn-based phase change materials for thermal energy storage. ACS Appl. Nano Mater. 2019, 2,
6	3752–3760.
7 [5]	Liu, M. L.; Ma, Y. Y.; Wu, H. W.; Robert Y. Wang, R. Y. Metal matrix-metal nanoparticle
8	composites with tunable melting temperature and high thermal conductivity for phase-change
9	thermal storage. ACS Nano 2015, 9, 1341-1351.
10 [6]	Kholmanov, I.; Kim, J. Y.; Ou, E.; Ruoff, R. S.; Shi, L. Continuous carbon nanotube-ultrathin
11	graphite hybrid foams for increased thermal conductivity and suppressed subcooling in
12	composite phase change materials. ACS Nano 2015, 9, 11699–11707.
13 [7]	Wang, C. M.; Wang, T. J.; Hu, Z. J.; Cai, Z. Y. Facile synthesis and thermal performance of
14	cety palmitate/nickel foam composite phase change materials for thermal energy storage. J.
15	Energy Storage 2020 , 28, 101179.
16 [8]	Xiao, X.; Zhang, P.; Li, M. Effective thermal conductivity of open-cell metal foams
17	impregnated with pure paraffin for latent heat storage. Int. J. Therm. Sci. 2014, 81, 94–105.
18 [9]	Feng, S. S.; Zhang, Y.; Shi, M.; Wen, T.; Lu, T. J. Unidirectional freezing of phase change
19	materials saturated in open-cell metal foams. Appl. Therm. Eng. 2015, 88, 315-321.
20 [10]Riazi, H.; Murphy, T.; Webber, G. B.; Atkin, R.; Tehrani, S. S. M.; Taylor, R. A. Specific heat
21	control of nanofluids: a critical review. Int. J. Therm. Sci. 2016, 107, 25-38.

1	[11]Tran, N.; Zhao, W. Y.; Carlson, F.; Davidson, J. H.; Stein, A. Metal nanoparticle-carbon
2	matrix composites with tunable melting temperature as phase-change materials for thermal
3	energy storage. ACS Appl. Nano Mater. 2018, 1, 1894–1903.
4	[12] Tiznobaik, H.; Banerjee, D.; Shin, D. Effect of formation of "long range" secondary dendritic
5	nanostructures in molten salt nanofluids on the values of specific heat capacity. Int. J. Heat
6	Mass Transf. 2015, 91, 342–346.
7	[13]Riazi, H.; Mesgari, S.; Ahmed, N. A.; Taylor, R. A. The effect of nanoparticle morphology on
8	the specific heat of nanosalts. Int. J. Heat Mass Transf. 2016, 94, 254-261.
9	[14]Song, W. L.; Lu, Y. W.; Wu, Y. T.; Ma, C. F. Effect of SiO ₂ nanoparticles on specific heat
10	capacity of low-melting-point eutectic quaternary nitrate salt. Sol. Energy Mater. Sol. Cells
11	2018 , 179, 66–71.
12	[15]Zhang, H. F.; Shin, D. Y.; Santhanagopalan, S. Microencapsulated binary carbonate salt
13	mixture in silica shell with enhanced effective heat capacity for high temperature latent heat
14	storage. Renew. Energy 2019, 134, 1156–1162.
15	[16]Choi, H. J.; Jung, S. M.; Seo J. M.; Chang, D. W.; Dai, L. M.; Baek, J. B. Graphene for energy
16	conversion and storage in fuel cells and supercapacitors. <i>Nano Energy</i> 2012 , 1, 534–551.
17	[17]Pop, E.; Varshney, V.; Roy, A. K. Thermal properties of graphene: Fundamentals and
18	applications. MRS Bull. 2012, 37, 1273.
19	[18]Allahbakhsh, A.; Arjmand, M. Graphene-based phase change composites for energy
20	harvesting and storage: State of the art and future prospects. <i>Carbon</i> 2019 , 148, 441–480.

1	[19]Liu, Y. J.; Zhang, D. Effect of covalent functionalization and phase change matrix on heat
2	transfer across graphene/phase change material interfaces. Appl. Therm. Eng. 2019, 151, 38-
3	45.
4	[20] Yang, J.; Qi, G. Q.; Liu, Y.; Bao, R. Y.; Liu, Z. Y.; Yang, W.; Xie, B. H.; Yang, M. B. Hybrid
5	graphene aerogels/phase change material composites: Thermal conductivity, shape-
6	stabilization and light-to-thermal energy storage. Carbon 2016, 100, 693–702.
7	[21] Chen, D. Z.; Qin, S. Y.; Tsui, G. C. P.; Tang, C. Y.; Ouyang, X.; Liu, J. H.; Tang, J. N.; Zuo,
8	J. D. Fabrication, morphology and thermal properties of octadecylamine-grafted graphene
9	oxide-modified phase-change microcapsules for thermal energy storage. Composites Part B
10	2019 , 157, 239–247.
11	[22]Kant, K.; Shukla, A.; Sharma, A.; Biwole, P. H. Heat transfer study of phase change materials
12	with graphene nanoparticle for thermal energy storage. Sol. Energy 2017, 146, 453–463.
13	[23] Yuan, P.; Zhang, P.; Liang, T.; Zhai, S. P. Effects of surface functionalization on thermal and
14	mechanical properties of graphene/polyethylene glycol composite phase change materials.
15	Appl. Surf. Sci. 2019, 485, 402–412.
16	[24]Ho, M. X.; Pan, C. Experimental investigation of heat transfer performance of molten HITEC
17	salt flow with alumina nanoparticles. Int. J. Heat Mass Transf. 2017, 107, 1094-1103.
18	[25]Loo, K.V.; Lapauw, T.; Ozalp, N.; Strom, E.; Lambrinou, K.; Vleugels, J. Compatibility of
19	SiCand MAX phase-based ceramics with a KNO3-NaNO3 molten solar salt. Sol. Energy
20	Mater. Sol. Cells 2019, 195, 228-240.

1	[26] Hummers, Jr. W. S.; Offeman, R. E. Preparation of graphitic oxide. J Am. Chem. Soc. 195	8,
2	80, 1339.	

3	[27] Abdelkader, A. M.; Valles, C.; Cooper, A. J.; Kinloch, I. A.; Dryfe, R. A. W. Alkali reduction
4	of graphene oxide in molten halide salts: production of corrugated graphene derivatives for
5	high-performance supercapacitors. ACS Nano 2014, 8, 11225–11233.
6	[28] Janz, G.; Krebs, U.; Siegenthaler, H.; Tomkins, R. Molten salts: volume 3 nitrates, nitrites,
7	and mixtures: electrical conductance, density, viscosity, and surface tension data. J. Phys.
8	<i>Chem. Ref. Data</i> 1972 , 1, 581–746.
9	[29]Zhang P, Xiao X, Meng Z N, Li M. Heat transfer characteristics of a molten-salt thermal
10	energy storage unit with and without heat transfer enhancement. Appl. Energy 2015, 137, 758-
11	772.
12	[30] Yang, S. M.; Tao W. Q. Heat transfer. 3rd ed. Beijing: Higher Education Press; 2002.

[31]Xiao, X.; Jia, H. W.; Wen, D. S.; Zhao, X. D. Thermal performance analysis of a solar energy
 storage unit encapsulated with HITEC salt/copper foam/nanoparticles composite. *Energy* 2020, 192, 116593.

[32]Xuan, Y. M.; Li, Q.; Hu, W. F. Aggregation structure and thermal conductivity of nanofluids.
 AIChE J. 2003, 49, 1039–1043.

[33] Jouybari, H. J.; Saedodin, S.; Zamzamian, A.; Nimvari, M. E.; Wongwises, S. Effects of
porous material and nanoparticles on the thermal performance of a flat plate solar collector:
An experimental study. *Renew. Energy* 2017, 114, 1407–1418.

1	[34] Xiao, X.; Zhang, G.; Ding, Y. L.; Wen, D. S. Rheological characteristics of molten salt seeded
2	with Al ₂ O ₃ nanopowder and graphene. <i>Energies</i> 2019 , 12, 467.
3	[35]Calmidi, V. V.; Mahajan, R. L. The effective thermal conductivity of high porosity fibrous
4	metal foams. ASME J. Heat Transfer 1999, 121, 466-471.
5	[36] Dul'nev, G. N. Heat transfer through solid disperse systems. J. Eng. Phys. Thermophys. 1965,
6	9, 399–404.
7	[37]Singh, R.; Kasana, H. S. Computational aspects of effective thermal conductivity of highly
8	porous metal foams. Appl. Therm. Eng. 2004, 24, 1841–1849.
9	[38]Xiao, X.; Zhang, P. Morphologies and thermal characterization of paraffin/carbon foam
10	composite phase change material. Sol. Energy Mater. Sol. Cells 2013, 117, 451-461.
11	[39]Xiao, X.; Zhang, P.; Li, M. Preparation and thermal characterization of paraffin/metal foam
12	composite phase change material. Appl. Energy 2013, 112, 1357–1366.
13	[40] Awad, A.; Navarro, H.; Ding, Y. L.; Wen, D. S. Thermal-physical properties of nanoparticle-
14	seeded nitrate molten salts. Renew. Energy 2018, 120, 275.
15	[41]Saranprabhu, M. K.; Rajan, K. S. Magnesium oxide nanoparticles dispersed solar salt with
16	improved solid phase thermal conductivity and specific heat for latent heat thermal energy
17	storage. Renew. Energy 2019, 141, 451–459.
18	[42]Hu, Y. W.; He, Y. R.; Zhang, Z. D.; Wen, D. S. Effect of Al ₂ O ₃ nanoparticle dispersion on
19	the specific heat capacity of a eutectic binary nitrate salt for solar power applications. <i>Energy</i>
20	Convers. Manage. 2017, 142, 366–373.

1	[43]Ho, M. X.; Pan, C. Optimal concentration of alumina nanoparticles in molten Hitec salt to
2	maximize its specific heat capacity. Int. J. Heat Mass Transf. 2014, 70, 174-184.
3	[44]Dudda, B.; Shin, D. Effect of nanoparticle dispersion on specific heat capacity of a binary
4	nitrate salt eutectic for concentrated solar power applications. Int. J. Therm. Sci. 2013, 69, 37-
5	42.
6	[45]Chieruzzi, M.; Cerritelli, G. F.; Miliozzi, A.; Kenny, J. M. Effect of nanoparticles on heat
7	capacity of nanoflfluids based on molten salts as PCM for thermal energy storage. Nanoscale
8	Res. Lett. 2013, 8, 448.
9	[46]Lu, M. C.; Huang, C. H. Specific heat capacity of molten salt-based. Nanoscale Res. Lett.
10	2013 , 8, 292.
11	[47] Andreu-Cabedo, P.; Mondragon, R.; Hernandez, L.; Martinez-Cuenca, R.; Cabedo, L.; Julia,
12	J. E. Increment of specific heat capacity of solar salt with SiO ₂ nanoparticles. <i>Nanoscale Res.</i>
13	<i>Lett.</i> 2014 , 9, 582.
14	[48]Seo, J. H.; Shin, D. H. Size effect of nanoparticle on specific heat in a ternary nitrate (LiNO ₃ -
15	NaNO ₃ -KNO ₃) salt eutectic for thermal energy storage. Appl. Therm. Eng. 2016, 102, 144-
16	148.
17	[49] Yuan, F.; Li, M. J.; Qiu, Y.; Ma, Z.; Li, M. J. Specific heat capacity improvement of molten
18	salt for solar energy applications using charged single-walled carbon nanotubes. Appl. Energy
19	2019 , 250, 1481–1490.
20	[50]Lasfargues, M. Nitrate based high temperature nano-heat-transfer-fluids: formulation &
21	characterisation. PhD dissertation. University of Leeds, 2014.

1	[51]Stern, H. K. High temperature properties and decomposition of inorganic salts nitrates and
2	nitrites. J. Phys. Chem. Ref. Data 1972, 1, 747–772.
3	
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6	

7 **Table 1** Thermo-physical properties of pure salt, metal foam and graphene used in the present

study

8

		HITEC	Solar	Graphene [[22]		Metal foam	
		salt [28]	salt [28-				Nickel	Copper
			29]				foam [30]	foam [30]
Density	Solid	2065.5	2079.0	Density	2200	Porosity	95%	95%
(kg m ⁻³)	Liquid	1936.0	1884.0	(kg m ⁻³)				
Melting point	: (°C)	140~142	218~228	Thermal conductivity (W m ⁻¹ K ⁻¹)	5000	Pore size	10 PPI	10 PPI
Thermal	Solid	0.70	0.705	Specific	0.79	Skeleton	8900	8930
conductivity	Liquid	0.4366	0.478	heat		density		
$(W m^{-1}K^{-1})$				(kJ kg ⁻¹ K ⁻¹)		(kg m ⁻³)		
Dynamic visc	osity	0.00787	0.00506			Skeleton	91.4	398
(kg m ⁻¹ s ⁻¹)						thermal		
						conductivity		
						$(W m^{-1}K^{-1})$		

9

10

Table 2 Specific heats and thermal effusivities of pure HITEC salt, salt/graphene nanocomposites and salt/graphene/metal foam composites

	c _{ps} (kJ kg ⁻¹ K ⁻¹) (105-110 °C)	c _{pl} (kJ kg ⁻¹ K ⁻¹) (180-290 °C)	e_s (kJ m ⁻² K ⁻¹ s ^{-1/2})	e_l (kJ m ⁻² K ⁻¹ s ^{-1/2})
Pure HITEC salt	1.415	1.562	1.430	1.149
HITEC salt/1 wt.% graphene	1.440	1.540	1.763	1.777
HITEC salt/2 wt.% graphene	1.426	1.563	1.794	1.841
HITEC salt/3 wt.% graphene	1.463	1.601	1.855	1.913
HITEC salt/1 wt.%	1.274	1.422	3.003	3.099
graphene/nickel foam				
HITEC salt/2 wt.%	1.422	1.554	3.202	3.275
graphene/nickel foam				
HITEC salt/3 wt.%	1.303	1.427	3.094	3.180
graphene/nickel foam				
HITEC salt/1 wt.%	1.336	1.495	5.262	5.428
graphene/copper foam				
HITEC salt/2 wt.%	1.270	1.391	5.149	5.261
graphene/copper foam				
HITEC salt/3 wt.%	1.245	1.381	5.115	5.266
graphene/copper foam				

5 Table 3 Specific heats and thermal effusivities of pure solar salt, salt/graphene nanocomposites
6 and salt/graphene/metal foam composites

	c _{ps} (kJ kg ⁻¹ K ⁻¹) (150-200 °C)	c _{pl} (kJ kg ⁻¹ K ⁻¹) (260-290 °C)	e_s (kJ m ⁻² K ⁻¹ s ^{-1/2})	e_l (kJ m ⁻² K ⁻¹ s ^{-1/2})
Pure solar salt	1.830	1.677	1.638	1.229
Solar salt/0.5 wt.% Fe ₂ O ₃ ^a	1.570	1.394	1.819	1.583
Solar salt/0.5 wt.% CuO ^a	1.530	1.377	1.693	1.425
Solar salt/1 wt.% graphene	1.875	1.605	2.023	1.794
Solar salt/1 wt.% Fe ₂ O ₃ ^a	1.560	1.400	1.636	1.301
Solar salt/1 wt.% CuO ^a	1.520	1.343	1.151	1.203
Solar salt/2 wt.% graphene	1.831	1.551	2.047	1.817
Solar salt/3 wt.% graphene	1.843	1.672	2.101	1.940
Solar salt/1 wt.%	1.760	1.583	3.542	3.238
graphene/nickel foam				
Solar salt/2 wt.%	1.591	1.430	3.402	3.117
graphene/nickel foam				
Solar salt/3 wt.%	1.729	1.553	3.582	3.291
graphene/nickel foam				
Solar salt/1 wt.%	1.474	1.371	5.543	5.145
graphene/copper foam				
Solar salt/2 wt.%	1.715	1.510	6.001	5.426
graphene/copper foam				
Solar salt/3 wt.%	1.515	1.361	5.663	5.177
graphene/copper foam				

7 ^a The results from Awad et al. [40] are also included for comparison, which clearly indicates that

8 the thermal effusivities of the composite PCMs in the present study are improved significantly.





Figure 1. Schematic diagram of the synthesis processes. (a) graphene (b) salt/graphene/metal foam composites.



(a)

(c-I) (d-I) (d-II) (c-II)

Figure 2. TEM and SEM pictures of graphene (a), salt/3 wt.% graphene nanocomposites (b) salt/3 wt.% graphene/nickel foam composites (c) and salt/3 wt.% graphene/copper foam composites (d) (I: HITEC salt, II: solar salt).

1763 1370 835 1228 Salt/3 wt.% graphene/copper foam Salt/2 wt.% graphene/copper foam Transmittance (%)Salt/1 wt.% graphene/copper foam Salt/3 wt.% graphene/nickel foam Salt/2 wt.% graphene/nickel foam Salt/1 wt.% graphene/nickel foam Salt/3 wt.% graphene HITEC salt

1

2

3

4

5

1000 1500 2000 2500 3000 3500 Wave length (cm⁻¹)

2396

(a-I)



(a-II)





Figure 3. FT-IR (a) and XRD (b) curves of pure salt, salt/graphene nanocomposites and salt/graphene/metal foam composites. (I: HITEC salt, II: solar salt)





Figure 4. Effective thermal conductivities of salt/graphene nanocomposites and salt/graphene/metal foam composites. (a) HITEC salt (b) solar salt. (T=25 °C)







Figure 5. DSC curves of pure salt and salt/graphene/metal foam composites. (a) HITEC salt (b) solar salt.



(b)

Figure 6. Comparison of latent heats for pure salt and salt/graphene/metal foam composites. (a) HITEC salt (b) solar salt.



(b)

Figure 7. Thermo-gravimetric analyses of pure salt and salt/graphene/metal foam composites. (a) HITEC salt (b) solar salt.