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## Original Article

## New high temperature dielectrics: Bi-free tungsten bronze ceramics with stable permittivity over a very wide temperature range

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### ABSTRACT

High relative permittivity,  $\epsilon_r$ , over a very wide temperature range,  $-65\text{ }^\circ\text{C}$  to  $325\text{ }^\circ\text{C}$ , is presented for ceramics designed to be compatible with base metal electrode multilayer capacitor manufacturing processes. We report a  $\geq 300\text{ }^\circ\text{C}$  potential Class II capacitor material free from Bi or Pb ions, developed by doping  $\text{Sr}_2\text{NaNb}_5\text{O}_{15}$  with  $\text{Ca}^{2+}$ ,  $\text{Y}^{3+}$  and  $\text{Zr}^{4+}$  ions, according to the formulation  $\text{Sr}_{2-2z}\text{Ca}_z\text{Y}_z\text{NaNb}_{5-z}\text{Zr}_z\text{O}_{15}$ . For sample composition  $z = 0.025$ ,  $\epsilon_r$  values are  $1565 \pm 15\%$  (1 kHz) from  $-65\text{ }^\circ\text{C}$  to  $325\text{ }^\circ\text{C}$ . At a slightly higher level of doping,  $z = 0.05$ ,  $\epsilon_r$  values are  $1310 \pm 10\%$  from  $-65\text{ }^\circ\text{C}$  to  $300\text{ }^\circ\text{C}$ . Values of the dielectric loss tangent,  $\tan\delta$  are  $\leq 0.025$  from  $-60\text{ }^\circ\text{C}$  to  $290\text{ }^\circ\text{C}$ , for  $z = 0.025$ , with  $\tan\delta$  increasing to 0.035 at  $325\text{ }^\circ\text{C}$ . Microstructural analyses exclude core-shell mechanisms being responsible for the flattening of the  $\epsilon_r$ -T response.

### 1. Introduction

Commercially available Class II high volumetric efficiency ceramic capacitors based on ferroelectric  $\text{BaTiO}_3$  ceramics are specified from  $-55\text{ }^\circ\text{C}$  to  $125\text{ }^\circ\text{C}$  –  $175\text{ }^\circ\text{C}$  for materials referred to by the Electronics Industries Alliance (EIA) codes as X7R-X9R (where R signifies stability in capacitance within  $\pm 15\%$  of the room temperature value). For emerging power electronics applications relevant to the energy transition, an upper operating temperature ceiling of  $< 200\text{ }^\circ\text{C}$  is insufficient [1]. High voltage power electronics for renewable energy generation and distribution require passive components that can operate alongside wide bandgap semiconductors at junction temperatures of  $250\text{ }^\circ\text{C}$  –  $300\text{ }^\circ\text{C}$  [2]. There are also a number of other applications where new Class II capacitors must maintain stable performance to  $\geq 300\text{ }^\circ\text{C}$ , for example distributed engine control systems for aerospace applications to reduce fuel consumption and improve reliability; and for drill-bit feedback systems in deep-well geothermal energy exploration [3]. Potential applications also arise in electric and hybrid vehicles.

In a bid to address these strategically important technological requirements, compositionally complex relaxor ferroelectrics with the perovskite  $\text{ABO}_3$  crystal structure have been researched by many academic groups, recently with a focus on energy storage density measurements of multilayer samples [1–12]. Unfortunately, all of these materi-

als contain bismuth oxide (or lead oxide). This prevents their application in base metal (Ni) electrode multilayer ceramic capacitors (MLCCs) – the main market. Bismuth or lead containing oxide ceramics are thermodynamically incompatible with metallic nickel electrode materials under the high temperature, chemically-reducing conditions used to co-fire base metal electrodes and the ceramic layers [13]. Hence most reports of MLCCs made with Bi or Pb containing ceramic dielectrics use expensive precious metal electrodes, at best Ag/Pd. The mainstream multilayer capacitor industry replaced precious metal electrodes with nickel, and to a lesser extent copper, many years ago on cost and security of supply consideration. For Bi-containing ceramic dielectrics co-fired with Cu there is a restricted processing window. Thermodynamic calculations indicate multilayers would have to be co-fired at temperatures  $< 940\text{ }^\circ\text{C}$ , and oxygen partial pressures,  $P_{\text{O}_2} < 10^{-7}\text{ atm}$ . [14]. By adding a series of liquid forming sintering fluxes to a  $\text{Na}_{0.5}\text{Bi}_{0.5}\text{TiO}_3$  – based piezoceramic formulation, it proved possible to reduce the sintering temperature from  $1150\text{ }^\circ\text{C}$  to  $900\text{ }^\circ\text{C}$ , thereby enabling Cu electrodes to be demonstrated, but dielectric losses were higher than for samples fired in air [14]. A further issue of Bi-ceramic dielectrics relates to loss of volatile bismuth oxide during ceramic processing. Our interest in researching Pb, Bi-free high temperature dielectrics stems from industrial translation challenges of existing materials for applications in mass market Ni-electrode MLCCs.

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The best of the bismuth containing relaxor high temperature dielectrics are based on  $\text{Na}_{0.5}\text{Bi}_{0.5}\text{TiO}_3$ . For example, formulations in the  $\text{Na}_{0.5}\text{Bi}_{0.5}\text{TiO}_3\text{-Ba}_{0.8}\text{Ca}_{0.2}\text{Ti}_{1-y}\text{Zr}_y\text{O}_3\text{-NaNbO}_3$  system developed in our laboratory have  $\epsilon_r$  values of  $1300 \pm 15\%$  from  $-55^\circ\text{C}$  to  $300^\circ\text{C}$  [8]. In other temperature-stable relaxors, such as  $(\text{Ba,Ca})\text{TiO}_3\text{-BiMg}_{0.5}\text{Ti}_{0.5}\text{O}_3$  or  $\text{BaTiO}_3\text{-BiZn}_{0.5}\text{Ti}_{0.5}\text{O}_3$  solid solutions [7], the range of stable dielectric permittivity extends to upper temperatures exceeding  $300^\circ\text{C}$  ( $\sim 500^\circ\text{C}$  in some materials) but the lower limit is well above the Electronic Industries Appliance 'X' specified lower working temperature of  $-55^\circ\text{C}$ . Moreover, in many cases dielectric loss tangent values are relatively high, at least over part of the temperature span.

The need to discover alternative materials that avoid the use of heavy metal oxides so enabling integration with (Ni) base metal electrode MLCCs motivated us to shift the focus of research away from perovskite ferroelectrics. The criteria was to find a parent ferroelectric with dielectric anomalies at higher temperatures than for  $\text{BaTiO}_3$  - the starting point for X7R capacitor materials.  $\text{BaTiO}_3$  materials are limited to modest upper operating temperatures due to a Curie peak temperature of  $\sim 130^\circ\text{C}$ . Our criteria for designing new Bi-free next generation Class II dielectrics that could operate at significantly higher temperatures was to first select a parent ferroelectric with a higher Curie point,  $T_C$ , than  $\text{BaTiO}_3$  and with a high  $\epsilon_{r\text{max}}$  value at  $T_C$ , such that even after compositionally engineering a suppression of the permittivity peak, high Class II levels of permittivity were retained over an extended temperature range. This led us to the tungsten bronze ferroelectric and non-linear optics literature. The material we selected,  $\text{Sr}_4\text{Na}_2\text{Nb}_{10}\text{O}_{30}$ , not only satisfied this selection criteria in terms of Curie point ( $305^\circ\text{C}$ ) and  $\epsilon_{r\text{max}}$  value ( $\sim 1400$ ), it also displayed a second, lower temperature permittivity peak at  $-15^\circ\text{C}$  [15,16]. We considered that this would be of value in helping achieve stable permittivity to  $-55^\circ\text{C}$ , the EIA 'X' standard lower working temperature for a Class II capacitor. Relative permittivity varies by more than  $\pm 20\%$  across the temperature range  $-55^\circ\text{C}$  to  $300^\circ\text{C}$  for  $\text{Sr}_4\text{Na}_2\text{Nb}_{10}\text{O}_{30}$ .

The tungsten bronze crystal structure involves corner sharing of  $\text{BO}_6$  octahedra in two crystallographic orientations (here  $\text{B} = \text{Nb}^{5+}$ ) leaving three types of distinct crystallographic sites available for lower valence cations, labelled A2, A1 and C, in the generic formula  $(\text{A}2)_4(\text{A}1)_2(\text{C})_4(\text{B}1)_2(\text{B}2)_8\text{O}_{30}$  [15–21[32]], with co-ordination numbers 15, 12 and 9 for A2, A1 and C sites, respectively. The primary cell is tetragonal, but due to the existence of superstructures, either commensurate or incommensurate that involves modulation of the oxygen sublattice, the true symmetry may be orthorhombic with a much larger unit cell. A schematic of the tetragonal primary cell and its relationship to the larger orthorhombic unit cell is shown in Fig. 1. When viewed along the [001] direction, the A2 sites are visible as pentagonal channels, and the A1 square and C triangular channels. Our selection,  $\text{Sr}_4\text{Na}_2\text{Nb}_{10}\text{O}_{30}$  is an example of a 'filled' tungsten bronze, so called because all A sites are occupied (although the C sites are empty). An early crystallographic study of a closely related tungsten bronze,  $\text{Ba}_4\text{Na}_2\text{Nb}_{10}\text{O}_{30}$  was reported by researchers at Bell Telephone Laboratories [17]. However,  $\text{Sr}_4\text{Na}_2\text{Nb}_{10}\text{O}_{30}$  is less widely reported, although some crystallographic information is available from a combination of X-ray and electron diffraction [15,16].

In  $\text{Sr}_4\text{Na}_2\text{Nb}_{10}\text{O}_{30}$  tungsten bronze ferroelectrics a change from paraelectric to ferroelectric occurs with no change in crystal system: electrical properties may be strongly influenced by subtle changes to octahedral tilt systems, defect structures and crystal superstructures [15–21[32]]. Structure-property correlations have been less widely studied than for perovskite ferroelectrics and there is still much to learn. The results reported below will provide added stimulus for future wide-ranging studies to understand the fundamental structure-property relationships for this exciting new type of high temperature dielectric.

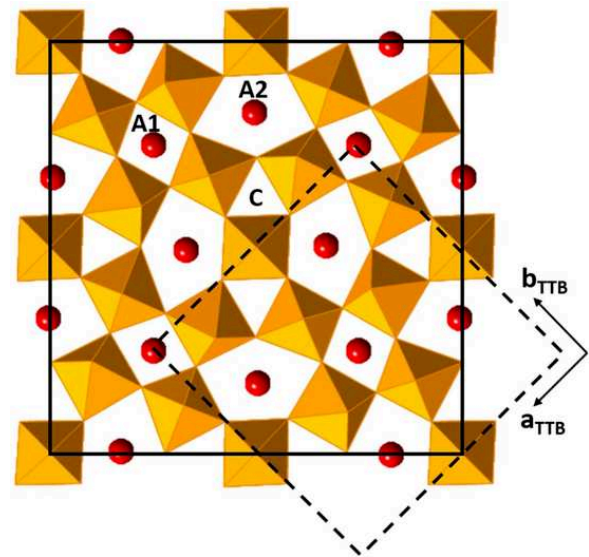


Fig. 1. Pseudocubic tetragonal primary cell of tungsten bronze structure (dashed lines) viewed along the [001] direction and its spatial relationship to a larger orthorhombic unit cell arising from by a superstructure (solid lines; after Ref [20]). In  $\text{Sr}_4\text{Na}_2\text{Nb}_{10}\text{O}_{30}$   $\text{Sr}^{2+}$  and  $\text{Na}^+$  ions are distributed over the A1 and A2 sites (red) formed by corner sharing  $\text{NbO}_6$  octahedra (orange).

## 2. Experimental

For convenience, the chemical formula of the parent niobate phase ( $\text{Sr}_4\text{Na}_2\text{Nb}_{10}\text{O}_{30}$ ) is expressed as  $\text{Sr}_2\text{NaNb}_5\text{O}_{15}$  (SNN) in the remainder of the text. The substituted compositions are expressed assuming a solid solution formula  $\text{Sr}_{2-2z}\text{Ca}_z\text{Y}_z\text{NaNb}_{5-z}\text{Zr}_z\text{O}_{15}$ . The assumption is that  $\text{Ca}^{2+}$  and  $\text{Y}^{3+}$  substituents will occupy A1/A2 sites and  $\text{Zr}^{4+}$  the  $\text{Nb}^{5+}$  (B) sites; C sites will remain empty. Sample formulations with  $z = 0, 0.025$  and  $0.05$  were prepared using the mixed oxide route. The compositions correspond to a very low level of substitution. Only 1.25 at.% of the  $\text{Sr}^{2+}$  (A) sites are substituted by  $\text{Y}^{3+}$  in composition  $z = 0.025$ , and 2.5 at.% in  $z = 0.05$ . For B sites, the  $\text{Zr}^{4+}$  for  $\text{Nb}^{5+}$  levels are 0.5 at.% and 1 at.% for compositions  $z = 0.025$  and  $0.05$  respectively.

Starting reagents of: strontium carbonate (Aldrich, 99.9 %); calcium carbonate (Aldrich, >99 %); sodium carbonate (Sigma-Aldrich, 99.95 %); niobium oxide (Alfa Aesar, 99.9 %); yttrium oxide (Alfa Aesar, 99.9 %) and zirconium oxide (Alfa Aesar, 99.7 %). Powders were mixed in appropriate ratios before ball-milling for up to 24 h in isopropanol using stabilised zirconia grinding media. Dried powders were calcined at  $1200^\circ\text{C}$  for 6 h (heating rate  $5^\circ\text{C}/\text{min}$ ) in high purity alumina crucibles. The calcined powders with the addition of 2 wt.% of binder (Optapix AC112, Zschimmer & Schwarz) were ball milled in water for 24 h, dried and passed through a  $300\ \mu\text{m}$  mesh nylon sieve, before pressing uniaxially at 100 MPa (for 90 s) in a 1 cm diameter steel die. After uniaxial pressing, the green pellets were isopressed (200 MPa for 5 min) in an isostatic press (Stanstead fluid power, Essex, UK). Binder burn-out was performed at a heating rate of  $1^\circ\text{C}/\text{min}$  to a dwell temperature of  $550^\circ\text{C}$  and held for 5 h. Sintering was carried out after embedding the pellets in a powder of the same composition. Maximum densities were obtained at a sintering temperature of  $1300^\circ\text{C}$  or  $1350^\circ\text{C}$ ; dwell times were 4–5 h. Sintered ceramic densities were measured from measured pellet dimensions and mass; the theoretical density was estimated from the nominal unit cell contents and measured lattice parameters.

Phase analysis by powder X-ray diffraction (XRD) was carried out using a Bruker D8 X-ray powder diffractometer. Unit cell lattice parameters of an adopted pseudo-tetragonal structure were obtained by full pattern Rietveld refinement using TOPAS 5.0 software (Bruker AXS,

Karlsruhe, Germany). In the refinement analysis, the peak shape function was determined by the fundamental parameters of the X-ray diffractometer geometry. The refined parameters are background function coefficient, lattice constant, scale factor, and atomic coordination.

In order to prepare specimens for microstructural characterisation by scanning electron microscopy, ceramic pellets were mounted in epoxy resin (Epothin, Buehler) and ground with P240, P600 and P2500 silicon carbide paper. Subsequent sequential polishing was carried out using Texmet P microcloths with MetaDi 2 diamond suspensions of decreasing particle size: 9  $\mu\text{m}$ , 3  $\mu\text{m}$  and 1  $\mu\text{m}$ . A final polish was carried out with ChemoMet and MasterMet 0.06  $\mu\text{m}$  colloidal silica on a Buehler EcoMet 300 grinder/polisher. Chemical etching was carried out with a 2:1 ratio of hydrofluoric acid and concentrated nitric acid for 90 s at room temperature.

Scanning electron microscopy (SEM) was performed using a Hitachi SU8230 high performance cold field emission instrument fitted with an Oxford Instruments Aztec energy dispersive X-ray analysis (EDX) system with 80 mm<sup>2</sup> X-Max SD detector and analysis software. For transmission electron microscopy (TEM), thin sample lamellae were prepared via the in-situ lift-out method using a FEI Helios G4 CX Dual Beam - High resolution monochromated, field emission gun, scanning electron microscope (FEG-SEM) with precise Focused Ion Beam (FIB). In the Dual Beam microscope, 500 nm of platinum (Pt) was electron beam deposited (at 5 kV, 6.4 nA for the electron source) onto the surface of the target area. This was followed by a second Pt layer (1  $\mu\text{m}$ ) using the FIB (at 30 kV, 80 pA for the liquid Ga ion source). An initial lamella was cut (by the FIB at 30 kV, 47 nA), before a final cut-out was performed (at 30 kV, 79 nA). Final thinning and polishing of the lamellae to electron transparency was performed with a low energy ion beam (5 kV, 41 pA). The lamellae were attached, using ion beam deposited Pt onto a copper FIB lift-out grid (Omniprobe, USA) mounted within the SEM chamber (in-situ) ready for transfer to the TEM. The lamellae were imaged using a FEI Titan Themis<sup>3</sup> 300 kV TEM fitted with a SuperX EDX system and Velox processing software.

For electrical measurements, silver electrodes were applied to opposite pellet faces (Sun Chemical, Gwent Electronic Materials). Relative permittivity,  $\epsilon_r$ , and loss tangent,  $\tan\delta$ , were measured at low-field as a function of temperature at fixed frequencies using a Hewlett Packard HP4284 LCR analyser. An environmental chamber was used for lower temperatures down to -65 °C (TJR; Tenney Environmental-SPX, White Deer, CA). Ferroelectric hysteresis measurements were carried out using a HP33120A function generator in combination with a HVA1B high voltage amplifier (Chevin Research, Otley, UK), using a sinusoidal electric field waveform with a frequency of 2 Hz. The measured electric field-time and current-time waveforms were processed to yield polarisation-electric field ( $P$ - $E$ ) loops and effective complex permittivity values using the method described previously [23].

### 3. Results and discussion

Full-pattern refinements of X-ray powder diffraction data for crushed sintered pellets are shown in Fig. 2. Secondary phase  $\text{NaNbO}_3$  was present in all three samples as has been reported by others for SNN [20,21]. In the present work, increasing the calcination and sintering times failed to eliminate the extra phase. Therefore, even for unmodified SNN the notional formula  $\text{Sr}_2\text{NaNb}_5\text{O}_{15}$  may be inaccurate: for example, the Na rich secondary phase may be due to  $\text{Sr}^{2+}$  occupancy of a fraction of the perceived  $\text{Na}^+$  sites, giving a formula  $\text{Sr}_{2+x}\text{Na}_{1-2x}\text{Nb}_5\text{O}_{15}$  [24]. Monoclinic  $\text{ZrO}_2$  secondary phase was identified only in the  $z = 0.05$  sample. All phases were included in the Rietveld refinements.

We found no convincing evidence from XRD of weak extra superlattice reflections reported at around  $20^\circ 2\theta$  or  $37^\circ 2\theta$  which others have observed with the aid of electron diffraction, and attributed to an orthorhombic unit cell (Space Group  $\text{Im}2a$ ). These reports relate to SNN

samples which had been fabricated by sintering for 2 days at 1250 °C, followed by rapid quenching to room temperature [20]. Some workers have assigned SNN to a different orthorhombic space group,  $\text{Cmm}2$  [25]. However the lack of any distinct supercell reflections in our XRD patterns prompted us to index on tetragonal axes, and to refine the data on the basis of space group  $P4bm$ . This tetragonal space group has been used in the past to index SNN samples obtained by calcining mixed oxide powders at 1150 °C for 12 h in an oxygen atmosphere [26]. The ambiguity in the literature as to space groups for SNN may in part relate to structural variations associated with different synthesis conditions. In a further example of the uncertainties in indexing diffraction patterns, a recent study of  $\text{Ca}^{2+}$  modified SNN reports a tetragonal phase for SNN with no  $\text{Ca}^{2+}$  substitution, changing to orthorhombic with increasing levels of  $\text{Ca}^{2+}$  substitution [24,27]. Verification of the true crystal system of SNN produced in our laboratory must await a detailed future study using electron and neutron diffraction. The emphasis of the present communication is to report microstructures and electrical properties of a new potential high temperature capacitor material.

Crystallographic data refined on  $P4bm$  are summarised in Table 1. The modifications by  $\text{Ca}^{2+}$ ,  $\text{Y}^{3+}$ ,  $\text{Zr}^{4+}$  produced a slight contraction in cell volume, consistent with solid solution formation.

Scanning electron micrographs of polished and etched sections of  $z = 0$  and  $z = 0.05$  are shown in Fig. 3. Observed grain sizes were similar ( $< 10 \mu\text{m}$ ) for both compositions. Densities were 92–93 % of estimated theoretical values. The possibility of elemental segregation within the grains was investigated by SEM-EDX and TEM-EDX. For X7R  $\text{BaTiO}_3$  based capacitor materials, a core-shell grain structure brought about by a variety of additive oxides is responsible for inducing a temperature stable permittivity response (from -55 °C to 125 °C). Thus it was important to establish if a comparable microstructure-strain mechanism was responsible for flattening the  $\epsilon_r$ - $T$  response of SNN. The SEM-EDX analysis for  $z = 0.05$  showed no elemental gradation within grains, Fig. 4. The existence of secondary grains of sodium niobate and zirconia identified in XRD patterns (Fig. 1) with grain sizes of  $\sim 5 \mu\text{m}$  and  $\sim 1 \mu\text{m}$  respectively was confirmed by the SEM-EDX analysis; there was also some evidence from EDX for the presence of Sr in the sodium niobate grains. More detailed analysis using TEM-EDX confirmed an absence of core-shell grain structures, or indeed any form of elemental gradation within individual grains, Fig. 5.

The relative permittivity-temperature,  $\epsilon_r$ - $T$  response of the parent tungsten bronze  $\text{Sr}_2\text{NaNb}_5\text{O}_{15}$  ceramic (SNN) is presented in Fig. 6a. The higher temperature dielectric peak at 305 °C is denoted  $T_2$ . For other tungsten bronzes, this dielectric anomaly is reported to correspond to the formation, on cooling, of a supercell which induces ferroelectric behaviour: hence  $T_2$  represents the Curie point [16]. Structural correlations are less well understood in the context of the lower temperature dielectric peak  $T_1$ , which occurs at -14 °C in SNN (1 kHz) and shows frequency dispersion similar to a relaxor ferroelectric. An accompanying change in thermal expansion coefficient for related tungsten bronzes implies that the  $T_1$  peak corresponds to a ferroelastic transition, but no associated structural deviations have been detected [18]. For  $z = 0$  (SNN), the 'standard' dielectric peaks created a variation in  $\epsilon_r$  of  $\pm 22$  % across the important temperature range, -55 °C to 300 °C, Fig. 6a. This is well outside the R-type  $\pm 15$  % stability level required of a Class II capacitor material. Consequently partial substitution of  $\text{Sr}^{2+}$  by  $\text{Ca}^{2+}$  was investigated for  $\text{Sr}_{2-x}\text{Ca}_x\text{NaNb}_5\text{O}_{15}$   $x < 0.1$ . The  $\epsilon_r$ - $T$  responses of SNN and Ca-SNN ceramics of comparable densities were generally similar. This finding is consistent with other reports [27]. Further chemical modifications, involving co-substitution of  $\text{Ca}^{2+}$ ,  $\text{Y}^{3+}$  for  $\text{Sr}^{2+}$  and  $\text{Zr}^{4+}$  for  $\text{Nb}^{5+}$  were investigated in an attempt to suppress the temperature variability in permittivity and attain R-type performance.

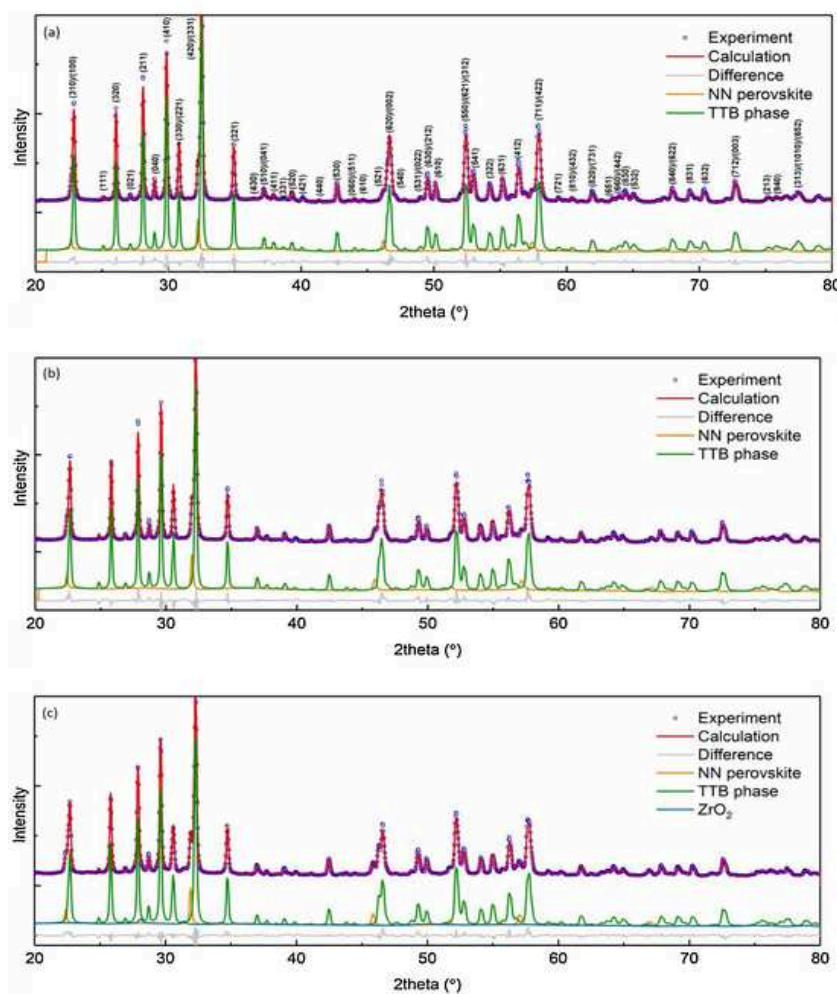


Fig. 2. Full pattern Rietveld refinements for  $\text{Sr}_{2-2z}\text{Ca}_2\text{Y}_2\text{NaNb}_{5-z}\text{Zr}_x\text{O}_{15}$ : a)  $z = 0$ ; b)  $z = 0.025$ ; c)  $z = 0.05$ . The terms NN and TTB in the legends refer to a sodium niobate type perovskite secondary phase and the pseudo-tetragonal tungsten bronze main phase respectively.

Table 1

Summary of (pseudo) tetragonal lattice parameters, goodness of fit,  $R_{\text{wp}}$  and phase fractions from Rietveld analysis for  $\text{Sr}_{2-2z}\text{Ca}_2\text{Y}_2\text{NaNb}_{5-z}\text{Zr}_x\text{O}_{15}$ .

Composition	a (Å)	c (Å)	V (Å <sup>3</sup> )	$R_{\text{wp}}\%$	%NaNbO <sub>3</sub>
$z = 0$	12.365(90)	3.8958(2)	595.73(3)	4.58	5.0
$z = 0.025$	12.362(9)	3.8920(1)	594.84(9)	4.99	7.4
$z = 0.05$	12.363(0)	3.8861(1)	593.97(3)	4.27	7.3

(+ 2.5 ZrO<sub>2</sub>)

For the  $\text{Ca}^{2+}$ ,  $\text{Y}^{3+}$ ,  $\text{Zr}^{4+}$  modified SNN sample composition  $z = 0.025$ , which had a very similar phase content to undoped SNN, the  $T_2$  peak temperature increased to 345 °C, from a value of 305 °C in unmodified SNN (at 1 kHz); there was also a decline in the  $\epsilon_r$  max value due to increased broadening, Fig. 6b. For the lower temperature peak, there was very little change in peak temperature  $T_1$  with substituent doping (−18 °C compared to −14 °C for SNN  $z = 0$ ), but there was an increase in frequency dispersion. For sample composition  $z = 0.025$  the difference in temperature,  $\Delta T$ , of  $\epsilon_r$  max temperatures ( $T_m$ ) between frequencies 1 kHz and 1 MHz was 25 °C, compared to 10 °C for unmodified SNN,  $z = 0$ .

For a higher level of chemical substitution,  $z = 0.05$ , the  $T_2$  anomaly was now displaced to 255 °C, some 90 °C below the  $T_2$  peak for  $z = 0.025$ , Fig. 6c. This non-monotonic shift of  $T_2$  with  $z$  indicates a

complex interplay between dopant level and temperature of the dielectric anomalies which may well relate to alterations in defect structures (possibly affecting  $\text{NbO}_6$  tilts in the case of  $T_2$ ). The  $T_2$  anomaly also became significantly more diffuse as the level of substitution increased. As a result, the  $\epsilon_r$  max value at  $T_2$  was approximately 60 % of that observed for unmodified SNN,  $z = 0$ . There was also an increase in broadening of the  $T_1$  peak, Fig. 6c, but less so than for  $T_2$ . The presence of zirconia secondary phase in the microstructure may at least in-part account for the drop in  $\epsilon_r$  25°C value compared to  $z = 0.025$ , but matrix strain effects consequent on transformation from tetragonal to monoclinic zirconia (on cooling from sintering temperatures) are thought unlikely, given the non-optimised sample density (92–93% theoretical).

The net effect of these chemical modifications on peak temperatures and peak profiles was to achieve the requisite  $\epsilon_r \pm 15\%$ , R-type consistency in  $\epsilon_r$  over very wide ranges of temperature. For  $z = 0.025$  the measured variation in the  $\epsilon_r$  data was within  $\pm 15\%$  of a median value of 1565 for temperatures extending from −65 °C to 325 °C (the median  $\epsilon_r$  value occurred at  $\sim 105$  °C). A further improvement in temperature-stability was achieved for higher levels of  $\text{Ca}^{2+}$ ,  $\text{Y}^{3+}$  and  $\text{Zr}^{4+}$  substitution. The  $z = 0.05$ , sample composition gave a median value of  $\epsilon_r = 1310$  with a  $\pm 10\%$  variation from temperatures of −65 °C to 300 °C. Very relevant to consideration as a capacitor material, the median value of  $\epsilon_r$  in  $z = 0.05$  ceramics occurred at 25 °C. Comparisons of

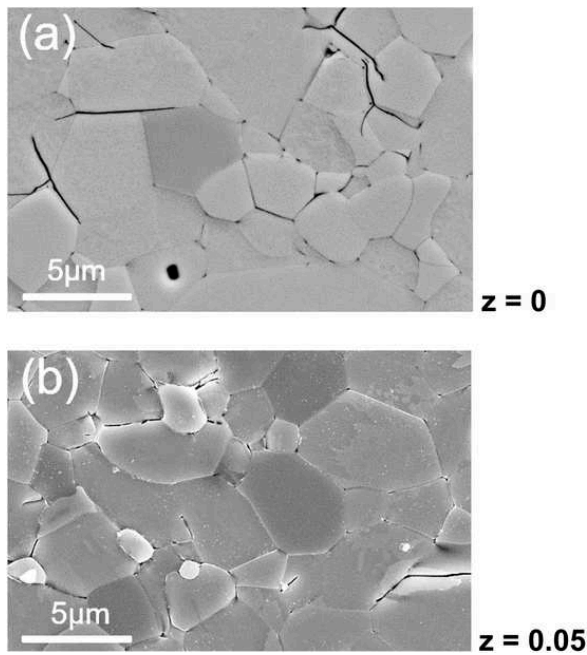


Fig. 3. SEM micrographs of  $\text{Sr}_{2-2z}\text{Ca}_2\text{Y}_z\text{NaNb}_{5-z}\text{Zr}_2\text{O}_{15}$ : (a)  $z = 0$  and (b)  $z = 0.05$  (sintered for 4 h at 1300 °C).

the 1 kHz  $\epsilon_r$ -T plots for  $z = 0$ ,  $z = 0.025$  and 0.05 are shown in Fig. 7 to highlight the development of temperature stable permittivity.

The low-field dielectric loss tangent values at 1 kHz were  $\leq 0.035$  from  $-65$  °C to 320 °C ( $\tan\delta \leq 0.025$  from  $-60$  °C to 290 °C) for  $z = 0.025$ . Losses were slightly higher in the  $z = 0.05$  sample, with  $\tan\delta < 0.04$ . Dielectric data for these 92–93 % dense samples are summarised in Table 2.

Phase stability and electrical properties of SNN have been reported for only a limited number of other cation substitutions, and no specific discussion of temperature stability of permittivity has been presented. Substitution of  $\text{Sb}^{5+}$  for  $\text{Nb}^{5+}$  produced a change from orthorhombic  $Ccm2$  to tetragonal  $P4bm$  Space Group, and shifted  $T_C$  to lower temperatures [28]. An evolution from orthorhombic to tetragonal crystal system was also induced by  $\text{Eu}^{3+}$ , and there was some indication from  $\epsilon_r$ -T. The same research group also examined  $\text{Sm}^{3+}$  substitution in relation to thermal luminescent properties [29,30].

The P-E hysteresis loops for all of the compositions studied were generally similar in appearance and showed clear evidence of ferroelectric character, as illustrated in Fig. 8a. The maximum polarisation (initially around 13  $\mu\text{C}\cdot\text{cm}^{-2}$ ) was reduced and the switching range around the coercive field became wider as  $z$  increased from 0 to 0.05. Significant dielectric nonlinearity and loss were evident in the sub-coercive field range, as illustrated in Fig. 8b. For example, the effective  $\tan\delta$  value at an electric field amplitude of 4  $\text{kV}\cdot\text{cm}^{-1}$  was determined as 0.154 for the undoped SNN, reducing to 0.081 and 0.060 for  $z = 0.025$  and 0.05, respectively.

Nonlinearity was also apparent in the real and imaginary parts of the complex dielectric permittivity, as shown in Fig. 9. The observed behaviour generally departs from the classical Rayleigh Law (linear  $\epsilon_r$ - $E_{\text{max}}$  relation) [23], tending towards a quadratic response in the field range up to 15  $\text{kV}\cdot\text{cm}^{-1}$ . The degree of nonlinearity was strongly suppressed for  $z = 0.05$ , indicating reduced contributions to the electric field-induced polarisation from domain switching mechanisms, consistent with increasing disorder.

In summary, the primary dielectric parameters of Bi-free and Pb-free dielectric ceramics produced by very low levels of chemical substitution of a tungsten bronze  $\text{Sr}_2\text{NaNb}_5\text{O}_{15}$  ferroelectric with  $\text{Ca}^{2+}$ ,  $\text{Y}^{3+}$ ,

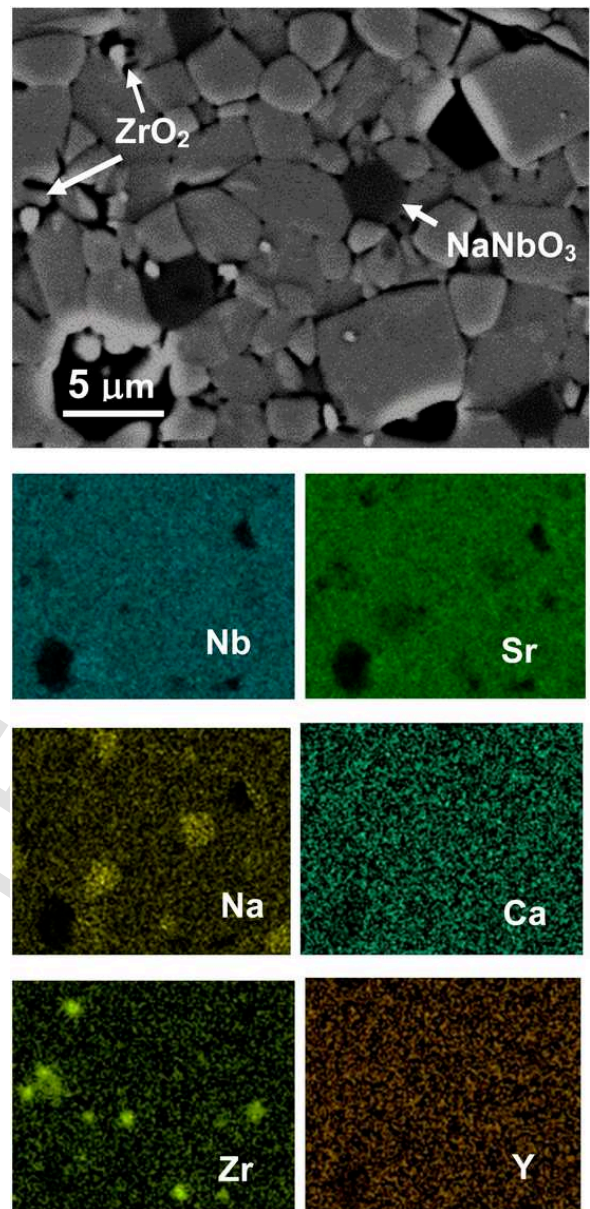


Fig. 4. SEM-EDX images of sample composition  $z = 0.05$  showing a secondary Na-rich phase, consistent with the  $\text{NaNbO}_3$  phase identified by XRD, and  $\text{ZrO}_2$  grains (sintered at 1300 °C for 4 h).

$\text{Zr}^{4+}$  are class leading and very significant in the quest to develop base metal electrode Class II capacitor materials capable of operating over very wide temperature ranges. Future fundamental studies of crystal structure and defect chemistry will be required to elucidate the reasons why such low levels of compositional modification by  $\text{Ca}^{2+}$ ,  $\text{Y}^{3+}$  and  $\text{Zr}^{4+}$  bring about such a dramatic change in the permittivity response. However, even at this early stage it is possible to exclude core-shell microstructural mechanisms, of the type which convert perovskite  $\text{BaTiO}_3$  into a X7R temperature stable dielectric. Moreover, the concentrations of  $\text{Ca}^{2+}$ ,  $\text{Y}^{3+}$ ,  $\text{Zr}^{4+}$  required to flatten the permittivity response of SNN are far below those required to produce significant broadening of Curie peaks in perovskites due to compositional heterogeneity effects. It is anticipated that this first report of a novel high temperature dielectric with intriguing composition-property relationships will generate a range of follow-on research encompassing microstructural, compositional, phase stability and fundamental mechanistic studies.

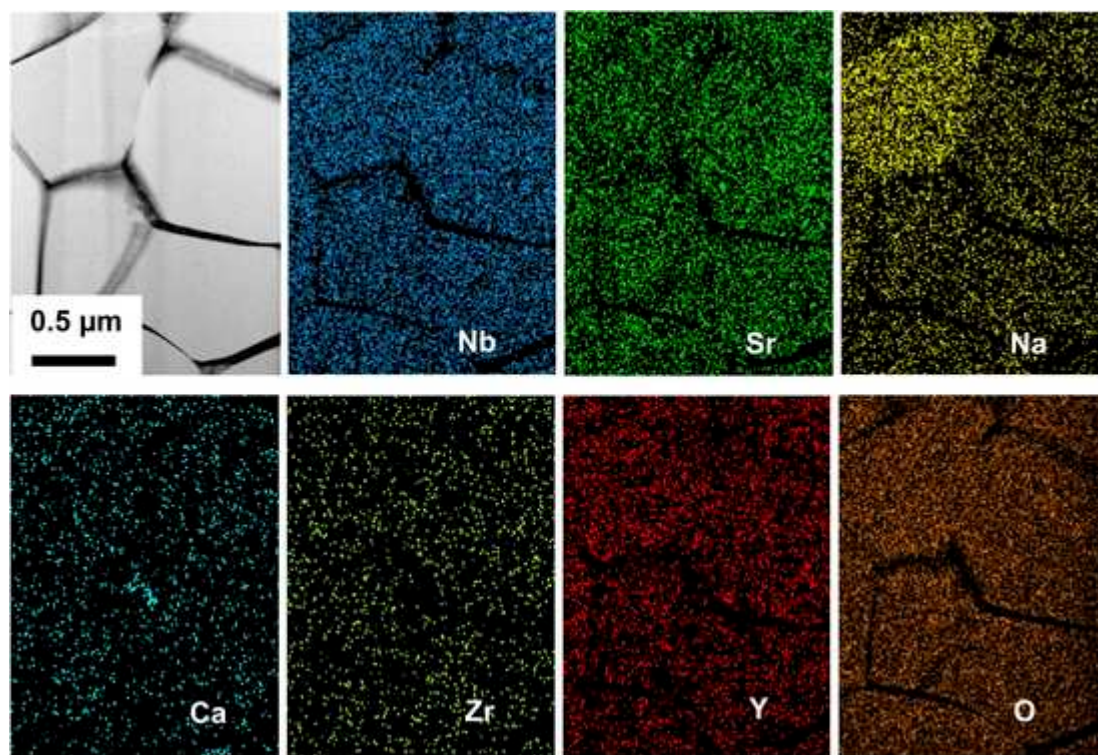


Fig. 5. Scanning TEM-EDX images confirming a lack of any detectable elemental gradation across grains - in contrast to conventional perovskite BaTiO<sub>3</sub> X7R temperature-stable dielectrics. Striations in HAADF\* image (top left) are a 'curtaining' artefact of the FIB-SEM thinning method used to prepare the TEM specimen. \* HAADF = high angle annular dark-field.

#### 4. Conclusions

A high permittivity Class II ceramic dielectric that offers stable permittivity to > 300 °C and which does not contain problematic bismuth or lead oxides is demonstrated. Chemical substitution of Sr<sub>2</sub>NaNb<sub>5</sub>O<sub>15</sub> by Ca<sup>2+</sup>, Y<sup>3+</sup> and Zr<sup>4+</sup> ions results in a material which more than satisfies the technologically important -55 °C to 300 °C temperature range of stable capacitance required for next generation power capacitor materials. For the formulation Sr<sub>2-2z</sub>Ca<sub>z</sub>Y<sub>z</sub>NaNb<sub>5-z</sub>Zr<sub>z</sub>O<sub>15</sub>, z = 0.025, values of  $\epsilon_r$  lie in the range 1565 ± 15 % for temperatures from -65 °C to 325 °C. At a higher dopant content, z = 0.05, the twin dielectric peaks become even more diffuse, giving  $\epsilon_r$  values of 1310 ± 10 % from temperatures of -65 °C to 300 °C. Dielectric loss tangent values are ≤ 0.035 (1 kHz) across the full temperature range of stable permittivity for sample composition, z = 0.025, and tanδ ≤ 0.025 from -60 °C to 290 °C. Limiting dielectric losses were slightly higher, tanδ ≤ 0.04, for z = 0.05 samples. These primary dielectric properties are of high impact given the growing demands for next generation Class II capacitors that can operate at temperatures well beyond the limit of existing market-leading BaTiO<sub>3</sub> based capacitors (under 200 °C). The absence of any volatile bismuth oxide component is highly advantageous in the search

for industrially-relevant dielectrics for future base metal electrode high temperature multilayer ceramic capacitors.

#### Declaration of Competing Interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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#### Appendix A. Supplementary data

Supplementary material related to this article can be found, in the online version, at doi:<https://doi.org/10.1016/j.jeurceramsoc.2020.10.034>.

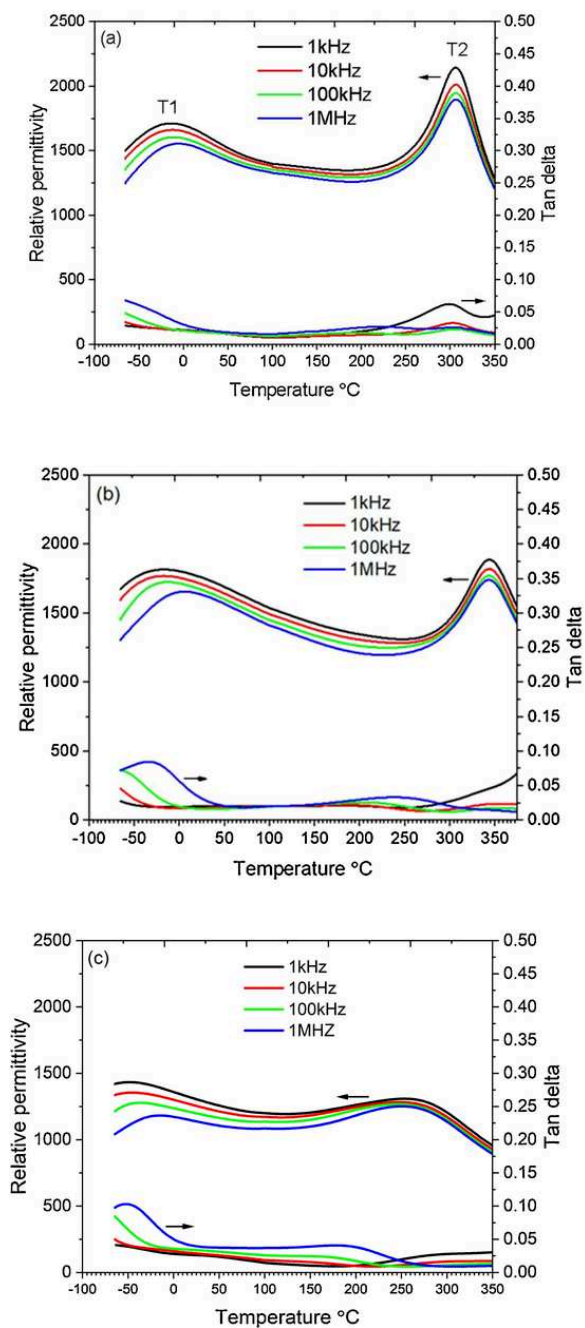


Fig. 6. Relative permittivity-temperature and loss tangent-temperature responses for  $\text{Sr}_{2-2z}\text{Ca}_z\text{Y}_z\text{NaNb}_{5-z}\text{Zr}_z\text{O}_{15}$ : a) SNN  $z = 0$ ; b)  $z = 0.025$ ; c)  $z = 0.05$ .

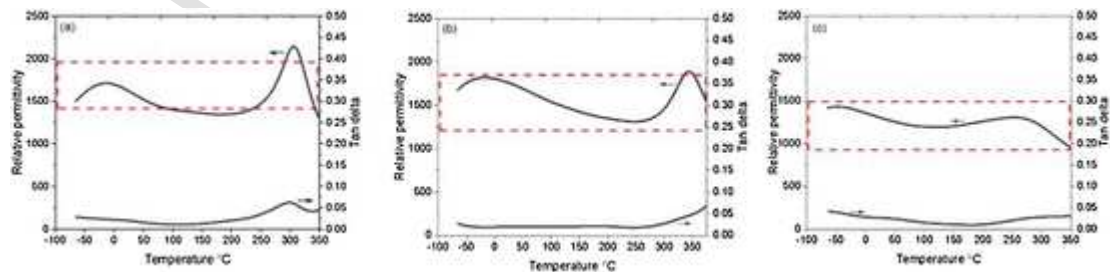


Fig. 7. Comparisons of the 1 kHz relative permittivity, highlighting the stability in  $\epsilon_r$  values from  $-65^\circ\text{C}$  to  $\geq 300^\circ\text{C}$  in  $\text{Sr}_{2-2z}\text{Ca}_z\text{Y}_z\text{NaNb}_{5-z}\text{Zr}_z\text{O}_{15}$ : (a)  $z = 0$ ; (b)  $z = 0.025$ ; (c)  $z = 0.05$ . The dashed outline indicates the  $\pm 15\%$  limits required by the EIA. Dielectric loss tangent plots are also shown.



**Table 2**  
Summary of dielectric data of 92-93 % dense  $\text{Sr}_{2-2z}\text{Ca}_z\text{Y}_z\text{NaNb}_{5-z}\text{Zr}_z\text{O}_{15}$  ceramics (1 kHz data).

Sample Code	Intended Product Composition	$\epsilon_r$ median (T)	$\pm$ % $\epsilon_r$ T range	T range	tan $\delta$ $\leq$ 0.03	tan $\delta$ $\leq$ 0.025
				$\leq$ 0.035		
z = 0	$\text{Sr}_{2.0}\text{Na}_{1.0}\text{Nb}_{5.0}\text{O}_{15}$	1733 (277 °C)	22 % -65 °C to 300 °C	-65 °C to 249 °C	-65 °C to 238 °C	-32 °C to 223 °C
z = 0.025	$\text{Sr}_{1.95}\text{Ca}_{0.025}\text{Na}_{1.0}\text{Y}_{0.025}\text{Zr}_{0.025}\text{Nb}_{4.975}\text{O}_{15}$	1565 (110 °C)	15 % -65 °C to 325 °C	-65 °C to 320 °C	-65 °C to 310 °C	-60 °C to 290 °C
z = 0.05	$\text{Sr}_{1.90}\text{Ca}_{0.05}\text{Na}_{1.0}\text{Y}_{0.05}\text{Zr}_{0.05}\text{Nb}_{4.95}\text{O}_{15}$	1310 (25 °C)	10 % -65 °C to 300 °C	-40 °C to 370 °C*	-20 °C to 320 °C	+20 °C to 270 °C

\*for z = 0.05, tan $\delta$  increased to 0.04 between -40 °C and -65 °C.

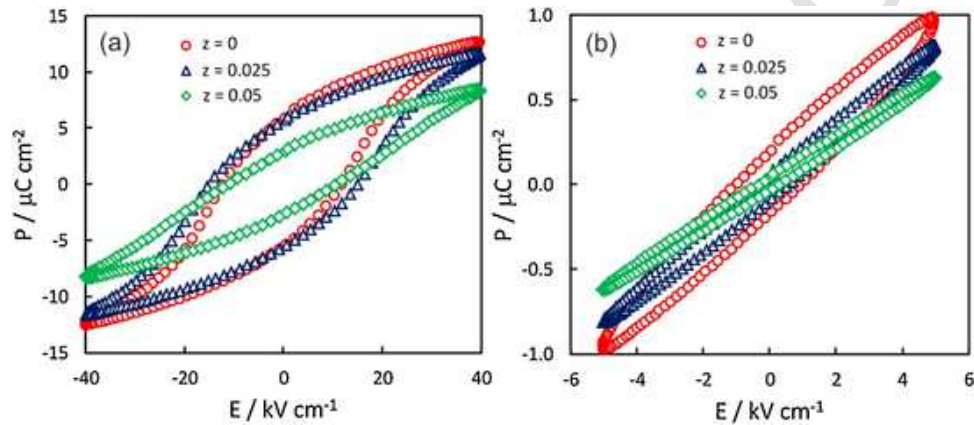


Fig. 8. Comparison of P-E loops for (a)  $E_{\text{max}} = 40 \text{ kV}\cdot\text{cm}^{-1}$  and (b)  $E_{\text{max}} = 5 \text{ kV}\cdot\text{cm}^{-1}$ .

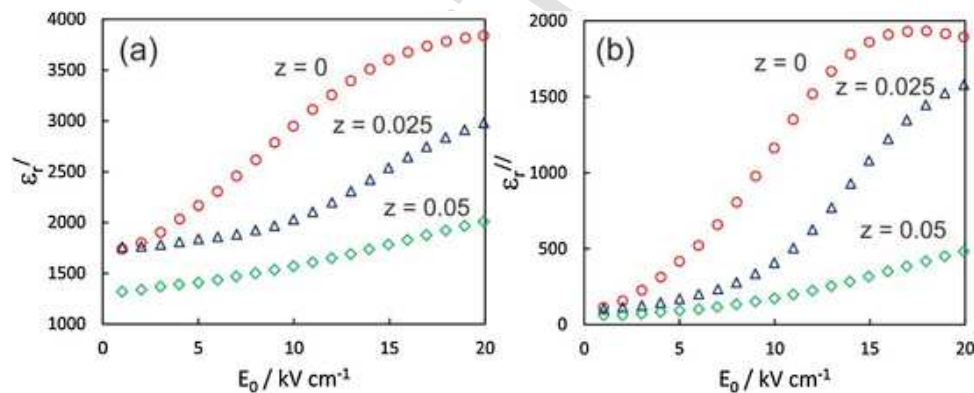


Fig. 9. Variations in (a) real and (b) imaginary parts of relative permittivity as a function of increasing electric field amplitude.

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