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Can we relate the surface expression of dike-induced normal 1 faults to subsurface dike geometry? 2 3 Craig Magee¹ and Christopher A-L Jackson² 4 5 ¹School of Earth Science and Environment, University of Leeds, Leeds, LS2 9JT, UK 6 ²Basins Research Group (BRG), Department of Earth Science and Engineering, Imperial 7 8 College, London, SW7 2BP, UK 9 Many igneous dikes do not reach the surface, instead triggering normal faulting and graben 10 11 formation in overlying rock. The surface expression of these dike-induced faults provides important records of active and ancient diking. For example, surface measurements of graben

12 half-widths have been used to estimate dike upper tip depths by projecting faults straight 13 14 down-dip, whereas extension measured at-surface across dike-induced fault pairs (i.e. their cumulative heave) is considered a proxy for dike thickness. We use 3D seismic reflection 15 data to test how the surface expression of two buried, dike-induced faults relates to dike 16 geometry. The dike-induced faults are non-planar, suggesting fault dips should not be 17 18 assumed constant when using graben half-widths to estimate dike depth. Multiple 19 displacement maxima occur across the dike-induced faults, but rarely at their lower or upper tips, suggesting they formed through linkage of isolated faults that nucleated *between* the dike 20 and free surface. Fault heave is greatest where these subsurface displacement maxima occur, 21 22 meaning the cumulative heave of the dike-induced fault pair measured at the syn-faulting free surface underestimates their total extension and poorly reflects dike thickness. Our results 23 24 imply that at-surface analyses of dike-induced fault geometry cannot be used to estimate key

dike parameters without *a priori* knowledge of fault structure and kinematics, or host rock
lithological variations.

27

28 INTRODUCTION

Dike intrusion can induce normal faulting of overlying rock (e.g., Pollard et al., 1983; Rubin 29 and Pollard, 1988; Rubin, 1992; Xu et al., 2016). Dike-induced normal faults form pairs that 30 dip towards underlying dikes and bound dike-parallel graben (Fig. 1) (e.g., Mastin and 31 Pollard, 1988; Trippanera et al., 2015a; Trippanera et al., 2015b). Faulting occurs because 32 33 dike dilation concentrates tensile stress in two lobes above the dike upper tip and in two zones at the free surface, within which related shear stresses instigate failure (Fig. 1) (e.g., 34 Pollard et al., 1983; Rubin and Pollard, 1988; Rubin, 1992; Gudmundsson, 2003; Koehn et 35 36 al., 2019). Because diking drives stress changes promoting faulting, dike emplacement and 37 shape impact fault growth and geometry (e.g., Trippanera et al., 2015a; Dumont et al., 2017). Our understanding of these dike and dike-induced fault relationships has been driven by 38 physical, numerical, and analytical modelling (e.g., Pollard et al., 1983; Mastin and Pollard, 39 1988; Trippanera et al., 2015b; Hardy, 2016; Bazargan and Gudmundsson, 2019; Koehn et 40 al., 2019). These models help us invert the surface expression of dike-induced faults to: (i) 41 track intruding dikes (e.g., Pallister et al., 2010); (ii) estimate dike volumes (e.g., Wilson and 42 Head, 2002); and (iii) examine how diking controls the morphology of Earth and other 43 44 planetary bodies (e.g., Wilson and Head, 2002; Carbotte et al., 2006; Ruch et al., 2016). However, few outcrops expose the geometry of both dikes and overlying dike-induced faults 45 (e.g., Gudmundsson, 2003; Von Hagke et al., 2019). Without access to the 3D structure of 46 47 natural dike and dike-induced fault systems, we cannot test models that underpin how we invert surface deformation to estimate dike geometry (e.g., thickness and depth). 48

49 We use seismic reflection images of the Exmouth Dyke Swarm, offshore NW Australia (Magee and Jackson, 2020), to quantify the 3D structure of a natural dike and dike-50 induced fault system. We test: (i) whether graben half-width can be used to predict dike upper 51 52 tip depths (e.g., Wilson and Head, 2002; Trippanera et al., 2015b; Hjartardóttir et al., 2016); and (ii) if extension across dike-induced fault pairs measured at the syn-faulting free surface 53 can be considered a proxy for dike thickness (e.g., Rubin and Pollard, 1988; Rubin, 1992; 54 Trippanera et al., 2015b). Our data also informs the debate regarding whether dike-induced 55 faults nucleate: (i) as near-surface vertical fractures (Fig. 1A) (e.g., Trippanera et al., 2015a; 56 57 Trippanera et al., 2015b; Al Shehri and Gudmundsson, 2018; Von Hagke et al., 2019); (ii) at dike tips (Fig. 1B) (e.g., Rubin, 1992; Xu et al., 2016; Koehn et al., 2019); (iii) a combination 58 of (i) and (ii) (Fig. 1C) (Tentler, 2005; Rowland et al., 2007); or (iv) between the dike tip and 59 60 surface (Fig. 1D) (Mastin and Pollard, 1988; Koehn et al., 2019). These fault growth models 61 can be used to predict diagnostic displacement-depth profiles, if we assume displacement is greatest where faults nucleated (Fig. 1) (e.g., Pollard and Segall, 1987; Trippanera et al., 62 63 2015b). Measuring displacement patterns across dike-induced faults may thus reveal their kinematics, which could relate to dike thickness changes and emplacement mechanics. By 64 unravelling how diking translates into faulting, we provide insights into the inversion of dike 65 geometry from surface-based analyses of dike-induced faults. 66

67

68 EXMOUTH DYKE SWARM AND STUDY AREA

Dikes manifest in the seismic reflection data as ~NNE-trending, sub-vertical, low-amplitude zones that disrupt stratigraphic reflections (e.g., Figs 2A and B). These dike-related zones are >100 m wide (Fig. 2A), but borehole data suggests dike thicknesses may only be 10's of metres (Magee and Jackson, 2020); i.e. the width of a dikes seismic expression may not capture its true thickness. The radial geometry of the swarm suggests dikes propagated

laterally northwards (Fig. 2A) (Magee and Jackson, 2020). Above and parallel to the dikes
are graben bound by normal faults that converge on the upper tips of underlying dikes (Figs
2B and C). The faults displace a ~1 km of Triassic-to-Jurassic strata (Fig. 2B), which locally
comprises interbedded claystones, siltstones, and sandstones (Ellis, 2011). At their upper tips,
dike-induced faults offset the ~148 Myr Base Cretaceous unconformity (horizon HK; Fig.
2B), which marks the syn-faulting free surface and indicates diking occurred during minor
Tithonian rifting (Magee and Jackson, 2020).

We examine an ~18 km long section of a graben bound by faults EF1 and EF2, and 81 82 underlain by Dike E, imaged in the time-migrated Chandon 3D seismic reflection survey (Fig. 2). Both EF1 and EF2 are continuous along-strike and rarely intersect pre-existing 83 tectonic normal faults (Fig. 2C). Using velocity data from four boreholes and dominant 84 85 frequency measurements, extracted from the seismic data, we (Supplementary Files 3-5): (i) convert the data from depth in time to metres; and (ii) estimate the limits of separability 86 $(\sim 20\pm 4 \text{ m})$ and visibility $(\sim 3\pm 1 \text{ m})$, which define the data's spatial resolution. We map 11 87 seismic horizons (HA-HK; Fig. 2B) and identify their hanging wall and footwall fault cut-88 offs along 121 transects spaced 125 m apart and oriented orthogonal to EF1 and EF2 89 90 (Supplementary Files 6 and 7). For each cut-off pair we measure fault throw and heave, which we use to calculate fault dip and displacement (Supplementary Files 6-8). Along 60 of 91 92 the transects, spaced 250 m apart, we also measure graben half-width at horizon HF, dike 93 upper tip depth beneath horizon HF, and the width of Dike E's seismic expression at ~4 km depth (Supplementary Files 6-8). 94

95

96 GRABEN HALF-WIDTH AND DIKE DEPTH

97 Graben half-widths (*HW*) measured at the surface are often used to predict dike upper tip

98 depths (D') by assuming fault dip (α) remains constant with depth (i.e. D' = HW tan α) (e.g.,

Pollard et al., 1983; Trippanera et al., 2015b; Hjartardóttir et al., 2016). We show HW along
horizon HF is $366\pm18-728\pm36$ m (Fig. 3A). Using HW and by projecting both faults straight
down-dip at an angle of HF α (i.e. the average dip on horizon HF for EF1 and EF2), we
predict D' is $343\pm51-803\pm121$ m (Fig. 3B). We also measure the depth of Dike E's upper tip
beneath horizon HF (D), showing it is $493\pm80-896\pm134$ m (Fig. B). HW and D are broadly
positively correlated, with our data showing that D typically exceeds $(D': D < 1)$ but is locally
equal ($D':D = 0.9-1.1$) or less ($D':D = >1.1$) than D' (Figs 3B and C).
The discrepancies between D and D' (Figs 3B and C) may relate to the: (i) true
location of Dike E's upper tip being shallower than resolved, such that our measurements
overestimate <i>D</i> ; and/or (ii) down dip variations in α (Fig. 3D). Where <i>D</i> ': <i>D</i> is <0.9, α for EF1
and EF2 broadly decreases below horizon HF and the faults display concave-up (listric)
geometries (Figs 3C and E). Conversely, where α remains constant with depth or increases
below horizon HF (i.e. faults are convex-up), D':D is >0.9 (Figs 3C and E). The variation in
α across EF1 and EF2 may reflect modification of dike-induced stresses by stresses related to
pre-existing tectonic faults (e.g., Fig. 3A), and/or heterogeneity in the mechanical properties
of the layered, sedimentary host rock (e.g., Schöpfer et al., 2006; Bazargan and
Gudmundsson, 2019). Our results imply graben half-width cannot be used to accurately
predict dike upper tip depths without information on subsurface fault structure and host rock
lithological variation (cf. Wilson and Head, 2002; Trippanera et al., 2015b; Hjartardóttir et
al., 2016).

120 DIKE-INDUCED FAULT DISPLACEMENTS AND KINEMATICS

121 Dike-induced fault displacement is intrinsically linked to dike dilation, implying the at-

122 surface 'cumulative heave' (extension) of dike-induced fault pairs can be related to dike

thickness (e.g., Rubin and Pollard, 1988; Rubin, 1992; Trippanera et al., 2015b). However,

fault heave is also dependent on variations in fault dip and displacement. We measure the
cumulative heave of EF1 and EF2 at the syn-faulting free surface (i.e. horizon HK; Magee
and Jackson, 2020), and determine their 'total extension'; i.e. the sum of maximum heave
values for both faults measured at *any* structural level on each transect (Supplementary File
7). By comparing these measurements to fault dip, displacement distribution, and the width of
Dike E's expression, we test whether at-surface cumulative heave measurements reflect dike
thickness.

We show fault dip and displacement vary across EF1 and EF2, with both faults 131 132 displaying zones of elevated displacement (e.g., EF2 segments 1–3) (Figs 3B and 4A). Displacement maxima measured on each transect ($\sim 78\pm12$ m on EF1; $\sim 101\pm15$ m on EF2) 133 occur at various structural levels (Fig. 4A); i.e. displacement-depth profiles are more complex 134 135 than hypothetical models predict (cf. Figs 1 and 4B). Overall, displacement broadly decreases 136 northwards (Fig. 4A). The total extension accommodated by the dike-induced faults mimics the displacement distribution and broadly decreases northwards (Fig. 4C). This northwards 137 decrease in displacement and total extension coincides with a reduction in the width of Dike 138 E's seismic expression (Figs 4A and B). In contrast, the distribution of cumulative heave 139 across horizon HK does not correlate with variations in the total extension or Dike E width, 140 showing no clear northwards decrease (Fig. 4B). There is also no correlation between fault 141 dip, cumulative heave, or total extension (Fig. 4C; Supplementary File 9). 142

Assuming the northwards reduction in the width of Dike E's seismic expression relates to changes in its true thickness (Magee and Jackson, 2020), the coincident northwards decrease in total extension (and displacement) may be considered a proxy for dike thickness (Fig. 4B). Local variations in total extension and displacement superimposed onto this northwards decrease, which do not relate to changes in fault dip, could reflect processes controlling dike thickness *during* or *after* emplacement (e.g., thermal wall rock erosion; Fig.

149	4D) (e.g., Delaney and Pollard, 1981; Gudmundsson, 1983; Kavanagh and Sparks, 2011;
150	Gudmundsson et al., 2012; Rivalta et al., 2015; Vachon and Hieronymus, 2017). An
151	alternative interpretation is that the zones of elevated displacement and total extension
152	correspond to fault nucleation sites (e.g., Pollard and Segall, 1987; Trippanera et al., 2015b;
153	Deng et al., 2017), with the distribution of these zones across EF1 and EF2 suggesting (Figs
154	4A-C and E): (i) isolated fault segments nucleated and eventually linked (e.g., Willemse et
155	al., 1996), perhaps due to cyclical phases of dike propagation and stalling (e.g., Woods et al.,
156	2019); and (ii) segment nucleation primarily occurred between the dike upper tip and
157	contemporaneous surface (e.g., Mastin and Pollard, 1988; Koehn et al., 2019), with few
158	nucleating at the dike upper tip (cf. Rubin, 1992; Xu et al., 2016; Koehn et al., 2019) or the
159	syn-faulting free surface (cf. Trippanera et al., 2015a; Trippanera et al., 2015b; Al Shehri and
160	Gudmundsson, 2018). Similar to controls on fault dip variation, fault displacement
161	distribution may have been influenced by the mechanically layered stratigraphy and/or
162	stresses related to pre-existing tectonic faults (e.g., Schöpfer et al., 2006).
163	Our results show cumulative heave measured at the syn-faulting free surface (i.e.
164	horizon HK) does not equal or mimic the total extension across EF1 and EF2, nor does it
165	reflect the broad northwards decrease in the width of Dike E's expression (Fig. 4B), implying
166	it is not a proxy for dike thickness (cf. Rubin and Pollard, 1988; Rubin, 1992; Trippanera et
167	al., 2015b). The lack of correlation between fault dip and cumulative heave suggests, instead,
168	that the latter is likely controlled by the vertical distribution of displacement during fault
169	linkage and/or dike thickening-related fault slip (Figs 4D and 4E).
170	

171 CONCLUSIONS

We use 3D seismic reflection data to image graben-bounding, dike-induced faults that extenddownwards from the syn-faulting free surface to converge on the upper tip of a dike. Our

174 results demonstrate predicted dike upper tip depths, calculated from graben half-width and assuming faults are planar, consistently underestimates measured dike upper tip depths. This 175 disparity between predicted and measured dike upper tip depths occurs because fault dip 176 varies down-dip, which possibly reflects heterogeneity in the mechanical properties of the 177 sedimentary host rock and/or stresses around pre-existing tectonic faults. We also show 178 displacement varies across the dike-induced faults, defining zones of elevated displacement. 179 If these zones of elevated displacement correspond to fault nucleation sites, their distribution 180 implies most fault segments nucleated between the dike upper tip and free surface. Because 181 182 the displacement maxima rarely occur at the fault upper tips, our measurements of fault heave along the syn-faulting surface do not approximate dike thickness. Accurately constraining 183 dike parameters (e.g., thickness and depth) from the surface expression of dike-induced faults 184 185 requires knowledge of fault geometry and kinematics in 3D. Reflection seismology is a powerful tool for studying how faults grow above dikes, and we anticipate future seismic-186 based studies will improve our understanding of how diking translates into surface 187 deformation. 188

189

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195

196 FIGURE CAPTIONS

197 Figure 1: Half-space schematics showing dike-induced fault growth models (based on

198 Mastin and Pollard, 1988; Rubin and Pollard, 1988; Tentler, 2005; Trippanera et al., 2015b;

199 Koehn et al., 2019). We predict displacement-depth profiles for each model assuming

displacement is greatest where faults nucleate (e.g., Pollard and Segall, 1987; Deng et al.,

- 201 2017). Horizontal stress patterns above an intruding dike, showing concentrated tensile stress
- at the surface (i) and above the dike tip (ii), are included (Rubin and Pollard, 1988).

203

Figure 2: (A) Root-mean squared (RMS) amplitude extraction across a 0.2 km high window
centred at 4 km depth showing dike A–I traces. Four boreholes shown are: 1=Chandon-1;
2=Chandon-2; 3=Chandon-3; 4=Yellowglen-1. Inset: Location map of the Chandon 3D
survey and Exmouth Dyke Swarm. (B) Interpreted depth-converted seismic section; see (C)
for location, Supplementary File 1 for uninterpreted version, and Supplementary File 2 for a
data video. (C) Horizon HF structure map showing dike-induced faults, underlying dike
traces, and tectonic faults.

211

Figure 3: (A) RMS amplitude map and graph showing variations in graben half-width (HW) 212 along-strike at horizon HF. Dip variations of both faults at HF (HF α) are highlighted. Error 213 bars for HW are $\pm 5\%$ (see Supplementary File 6 for explanation of error sources). (B) Plot 214 comparing measured (D) and predicted (D') dike upper tip depths below HF. Error envelopes 215 for D and D' are $\pm 15\%$. (C) Variation in the ratio of D':D along the graben related to fault 216 dip, where: (i) D':D < 0.9 fault dip decreases with depth; (ii) D':D = 0.9-1.1 the fault is 217 218 planar; and (iii) D': D > 0.9 fault dip increases with depth. Error envelopes are $\pm 15\%$. (D) Dip map of EF1 and EF2. (E) Fault dips calculated along each measured transect for EF1 and EF2 219 plotted against their corresponding seismic horizon (i.e. a proxy for depth). The dip profiles 220 are grouped for D':D < 0.9 and D':D > 0.9; inset schematics show how changes in fault dip 221 beneath horizon HF impact D':D. 222

224	Figure 4 : (A) Map of displacement and displacement maxima across EF1 and EF2.
225	Displacement maxima are plotted against distance, with error bars of $\pm 15\%$, and combined to
226	show cumulative maximum displacement. (B) Depth-displacement profiles for EF1 and EF2;
227	error bars are $\pm 15\%$. See (A) for locations. (C) Along-strike variations in total extension
228	across EF1 and EF2, compared to cumulative heave at horizon HK and Dike E's seismic
229	expression width measured from Figure 1A; error bars are $\pm 15\%$. Average dip of both faults
230	at each site are highlighted. (D) Schematic showing how localized zones of high
231	displacement may form in response to dike thickening. (E) Schematic showing how isolated
232	fault segments may nucleate in response to dike propagation, then grow and link when the
233	dike stalls and thickens (e.g., Woods et al., 2019). Lateral separation of fault segments may
234	reflect magma break-out from the dike nose (Healy et al., 2018).
235	
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