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Temperature Dependent Piezoelectric Properties of Lead-Free $(1-x)\text{K}_{0.6}\text{Na}_{0.4}\text{NbO}_3-x\text{BiFeO}_3$ Ceramics

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$(1-x)\text{K}_{0.4}\text{Na}_{0.6}\text{NbO}_3-x\text{BiFeO}_3$ lead-free piezoelectric ceramics were successfully prepared in a single perovskite phase using the conventional solid-state synthesis. Relative permittivity (ϵ_r) as a function of temperature indicated that small additions of BiFeO_3 not only broadened and lowered the cubic to tetragonal phase transition (T_C) but also shifted the tetragonal to orthorhombic phase transition (T_{O-T}) toward room temperature (RT). Ceramics with $x = 1$ mol.% showed optimum properties with small and large signal piezoelectric coefficient, $d_{33} = 182$ pC/N and $d_{33}^* = 250$ pm/V, respectively, electromechanical coupling coefficient, $k_p = 50\%$, and $T_C = 355^\circ\text{C}$. k_p varied by $\sim 5\%$ from RT to 90°C , while d_{33}^* showed a variation of $\sim 15\%$ from RT to 75°C , indicating that piezoelectric properties were stable with temperature in the orthorhombic phase field. However, above the onset of T_{O-T} , the properties monotonically degraded in the tetragonal phase field as T_C was approached.

Keywords: piezoelectrics, lead free, $\text{K}_{0.5}\text{Na}_{0.5}\text{NbO}_3$, temperature dependence, BiFeO_3

INTRODUCTION

Piezoelectric materials are essential in many applications and used in different electronic circuits as a sensor, actuator, or a transducer (Holterman and Groen, 2013). Commercial piezoelectric materials contain about 60% of PbO by weight. The toxicity of lead is well documented and legislation against its use are becoming more stricter with time, which has increased interest in lead-free alternatives for piezoelectric applications (Rödel et al., 2015). Amongst the potentially useful lead-free piezoelectrics, only Ca^{2+} and Zr^{4+} modified BaTiO_3 and $(\text{Na,K})\text{NbO}_3$ -based ceramics have low coercive fields similar to lead zirconate titanate (PZT). However, BaTiO_3 -based piezoelectric ceramics generally exhibit a low Curie temperature ($T_C < 100^\circ\text{C}$), making them unsuitable for high temperature piezoelectric applications (Liu and Ren, 2009). $(\text{K,Na})\text{NbO}_3$ has a high Curie temperature of $> 350^\circ\text{C}$ and capable of operating at low drive fields. Compositional engineering of $\text{K}_{1-x}\text{Na}_x\text{NbO}_3$ is usually carried out around $x = 0.5$, i.e., part of the phase diagram where several various polymorphs have similar free energies. On cooling ceramics with $x = 0.5$, the crystal structure successively changes from cubic to tetragonal, tetragonal to orthorhombic,

and orthorhombic to rhombohedral. Almost all compositions with large piezoelectric (d_{33}) and coupling coefficients (k_p) are optimized by substituents/dopants that shift the orthorhombic-tetragonal transition (T_{O-T}) toward room temperature (RT; Wu et al., 2015; Hussain et al., 2019). Recently new phase boundaries have been constructed in (K,Na)NbO₃ based ceramics by simultaneously moving the rhombohedral and tetragonal phases toward RT. Such a coexistence of rhombohedral-orthorhombic-tetragonal phase boundaries has been very successful in improving the d_{33} values and have significantly improved the temperature stability in these ceramics (Tao et al., 2019; Lv et al., 2020; Zheng et al., 2020). Although ceramics with $x = 0.5$ are most commonly investigated, piezoelectric properties are optimized in $K_{1-x}Na_xNbO_3$ for $0.4 \leq x \leq 0.6$. The piezoelectric properties are similar throughout this compositional range but for compositions with $x = 0.6$ (Na⁺ rich) have lower T_{O-T} in comparison to $x = 0.5$ (Wu et al., 2008; Tellier et al., 2009).

BiFeO₃ is one of the most extensively investigated perovskite compounds because of its RT multiferroic properties (Khesro et al., 2016a). It is rarely, however, (Sun et al., 2008; Zuo et al., 2008) investigated in solid solution with (K,Na)NbO₃. BiFeO₃ could be an interesting choice for solid solution with KNN because of its relatively low melting point. Its ability to form a liquid phase can help in densification of KNN based ceramics (Na et al., 2011) in addition to the possibility of forming a phase boundary at RT.

Since, BiFeO₃ was expected to have only limited solid solubility (Jiang et al., 2010), K_{0.4}Na_{0.6}NbO₃ was chosen to increase the prospect of bringing the T_{O-T} closer to RT. Moreover, K⁺ rich compositions are prone to volatilization and are thus more difficult to process with precise stoichiometry (Wang et al., 2016). Therefore, in the present study, the dielectric, ferroelectric and piezoelectric properties of the solid solution $(1-x)K_{0.4}Na_{0.6}NbO_3-xBiFeO_3$ are studied. *In situ* measurements of the piezoelectricity were performed to verify the temperature stability of these ceramics.

EXPERIMENTAL METHODS

$(1-x)K_{0.4}Na_{0.6}NbO_3-xBiFeO_3$ for $x = (0, 0.5, 0.75, 1, 1.25, 1.5, 2, \text{ and } 3)$ mol.% ceramics were prepared via a mixed oxide solid state route using K₂CO₃, Na₂CO₃, Bi₂O₃, Fe₂O₃, and Nb₂O₅ raw materials. K₂CO₃ and Na₂CO₃ were dried at 300°C, Bi₂O₃, and Fe₂O₃ were dried at 500°C and Nb₂O₅ was dried at 900°C. Raw materials were weighed according to the molar ratios of the compositions and mixed/milled for 1 h in an attrition mill using 3 mm diameter yttria-stabilized zirconia media in isopropanol. Powders were dried in an oven at 80°C, sieved, and calcined in a covered alumina crucible at 850°C for 6 h. The calcined powders were remilled, dried and sieved. Polyvinyl alcohol (PVA) binder solution was added and the powders were pressed into 10 mm diameter pellets using a uniaxial pellet press. After binder burnt out at 550°C, pellets were sintered in the temperature range 1100 to 1140°C for 6 h, at a heating/cooling rate of 5°/min. Densities of the sintered

pellets were measured using Mettler Toledo model MS104S digital densitometer.

Ceramics with $x = 0.5, 0.75,$ and 1 mol.% showed a relative density >94% while the remaining samples ranged between 88–90%. Phase analysis of the sintered specimens was carried out using a Bruker D2-Phaser X-ray powder diffractometer (XRD). The microstructure of the samples was examined using a FEI Inspect-F scanning electron microscope (SEM). For electrical measurements, sintered samples were electroded with silver. Samples were poled at RT in silicone oil with at an applied field of 30–40 kV/cm. The small signal piezoelectric coefficient (d_{33}) was measured using a Piezotest PM300 d_{33} meter. Polarization hysteresis and strain-electric field measurements were carried out using an aixACCT TF 2000 ferroelectric tester at a frequency of 1 Hz from RT to 150°C, where the displacement data was synchronously captured by a laser interferometer. Relative permittivity (ϵ_r) and $\tan \delta$ data was measured from RT to 500°C using an Agilent 4184A multifrequency precision LCR meter. The planar electromechanical coupling factor (k_p) was determined from the resonance and antiresonance frequencies peaks, which were measured using an Agilent 4294A impedance/gain-phase analyzer according to IEEE standards on piezoelectricity (American and Standard, 1988).

RESULTS AND DISCUSSION

Figure 1 shows RT XRD patterns of sintered $(1-x)K_{0.4}Na_{0.6}NbO_3-xBiFeO_3$ ($x = 0-3$ mol.%) ceramics. Traces were indexed according to a single perovskite phase with no secondary peaks. For K_{0.5}Na_{0.5}NbO₃-based ceramics, the (200) doublet peak is usually considered to define the structure. For orthorhombic structure, $I_{002}/I_{200} = 2:1$ ($I = \text{intensity}$; Feng et al., 2016) but for the tetragonal structure, an opposite trend is observed, having $I_{002}/I_{200} = 1:2$ (Zhou et al., 2015). In our samples at $x = 0$, obvious split of the 200 peak was detected at $2\theta \sim 46^\circ$ which is consistent with the orthorhombic phase frequently reported for K_{0.5}Na_{0.5}NbO₃ ceramics (Sun

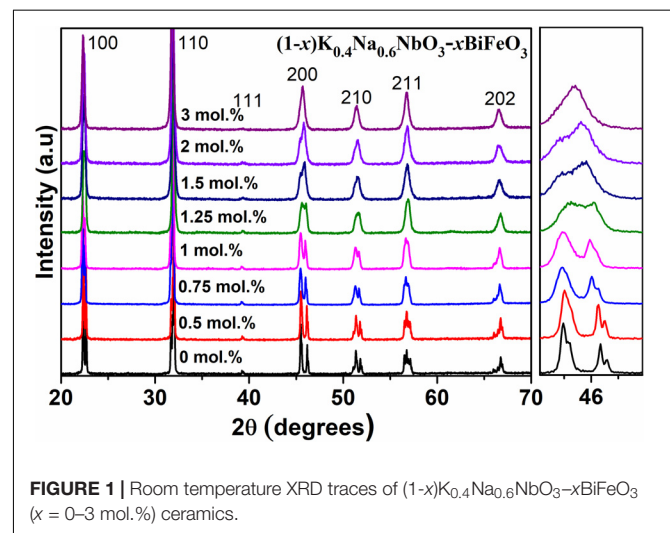


FIGURE 1 | Room temperature XRD traces of $(1-x)K_{0.4}Na_{0.6}NbO_3-xBiFeO_3$ ($x = 0-3$ mol.%) ceramics.

et al., 2008). With increase in concentration of BiFeO₃, the splitting became less apparent, coupled with a decrease in the intensity's ratios. At $x = 1.25$ mol.%, the peaks merged, indicating a co-existence of tetragonal, and orthorhombic phases. At $x = 1.5$ mol.%, a shoulder was observed on the left-hand side of the (200) peak but without the clear splitting expected from a tetragonal structure. At $x = 3$ mol.%, the structure appears to be pseudocubic, showing only one broad peak which may be ascribed to nanoscale competition between tetragonal and orthorhombic phases (Bomlai et al., 2007). To confirm the phase evolution of KNN-BF, full-pattern Rietveld refinement of XRD data was conducted using a two-phase mix of orthorhombic (Bmm2), and tetragonal KMO (P4mm) as given in **Figure 2**. With the increase of BF content, coexistence of two phases was found at $x = 1.25$ mol.%, and then the fraction of tetragonal phase gradually increased and dominated as shown in **Table 1**.

Figure 3 shows SEM micrographs of sintered $(1-x)\text{K}_{0.4}\text{Na}_{0.6}\text{NbO}_3-x\text{BiFeO}_3$ ($x = 1-3$ mol.%) ceramics which

revealed that the average grain size decreases with increase in x . For samples with $x = 0$ and 0.5 mol.%, few grains indicated abnormal growth of ($>5 \mu\text{m}$). Such abnormal grain growth is usually associated with liquid phase sintering (Jo et al., 2006; Song et al., 2007; Han et al., 2012). Each large grain observed is believed to be the combination of many small grains which self-assemble into a larger cluster. The sintering temperature of $\text{K}_{0.5}\text{Na}_{0.5}\text{NbO}_3$ is close to its melting-point and consequently it is not easy to achieve a dense ceramic without liquid phase sintering (Wang and Li, 2012). It has been reported (Zhen and Li, 2007; Kim et al., 2009) that grain size and core-shell structures in such grains influence piezoelectric properties. The BF content is affecting the sintering temperature, for larger contents of BF the conditions don't favor formation of large cluster and the constituent grains are disintegrated, thereby showing smaller grains. This is evident from a sharp decrease at $x = 0.75$ mol.%. With further increase of BiFeO₃ the grain size gradually decreased to $\sim 100-400$ nm for $x = 3$ mol.%.

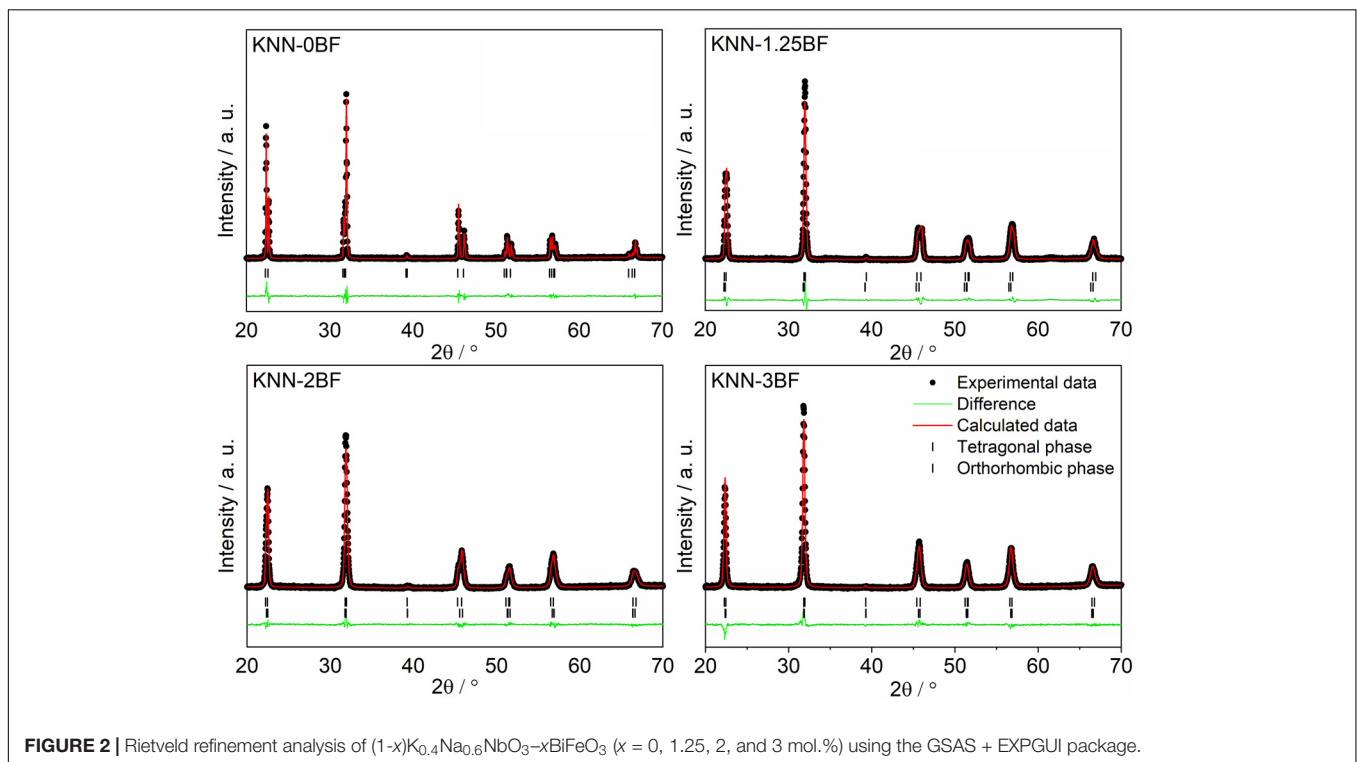


FIGURE 2 | Rietveld refinement analysis of $(1-x)\text{K}_{0.4}\text{Na}_{0.6}\text{NbO}_3-x\text{BiFeO}_3$ ($x = 0, 1.25, 2,$ and 3 mol.%) using the GSAS + EXPGUI package.

TABLE 1 | Refined structural parameters of $(1-x)\text{K}_{0.4}\text{Na}_{0.6}\text{NbO}_3-x\text{BiFeO}_3$.

	Space group	Cell volume/Å ³	Density/g/cm ³	Lattice parameter			Phase fraction		GOF	R _{exp}	R _{wp}
				a/Å	b/Å	c/Å	O/%	T/%			
KNN-0BF	Bmm2	125.513 (12)	4.549 (4)	5.6300 (3)	3.9368 (2)	5.6629 (3)	100	0	1.23	8.98	10.98
KNN-1.25BF	Bmm2	125.8 (2)	4.539 (7)	5.611 (6)	3.9958 (12)	5.611 (6)	74 (3)	26 (3)	1.41	6.73	9.49
	P4mm	62.26 (5)	4.586 (3)	3.9504 (12)		3.9897 (16)					
KNN-2BF	Bmm2	125.2 (3)	4.562 (10)	5.629 (9)	3.9514 (19)	5.628 (8)	51 (4)	49 (4)	1.14	8.02	9.13
	P4mm	62.73 (5)	4.552 (4)	3.9401 (15)		4.0001 (15)					
KNN-3BF	Bmm2	125.1 (2)	4.562 (8)	5.623 (7)	3.9603 (14)	5.621 (6)	34 (3)	66 (3)	1.26	7.67	9.66
	P4mm	62.6 (5)	4.562 (4)	3.9596 (15)		3.9925 (13)					

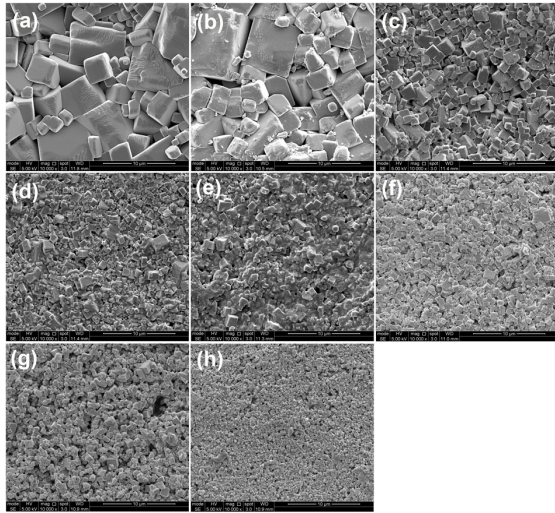


FIGURE 3 | SEM images of as sintered $(1-x)K_{0.4}Na_{0.6}NbO_3-xBiFeO_3$ ($x = 1-3$ mol.%) ceramics. Where (a) shows $x = 0$; (b) shows $x = 0.5$ mol.%; (c) shows $x = 0.75$ mol.%; (d) shows $x = 1$ mol.%; (e) shows $x = 1.25$ mol.%; (f) shows $x = 1.5$ mol.%; (g) shows $x = 2$ mol.%; and (h) shows $x = 3$ mol.%.

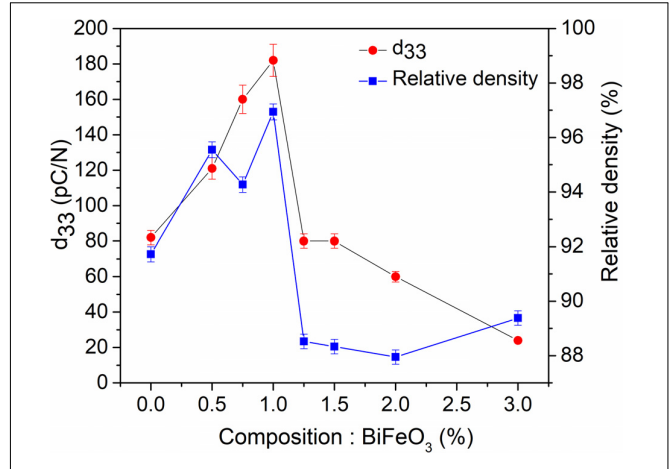


FIGURE 5 | d_{33} and relative density as a function of composition in the system $(1-x)K_{0.4}Na_{0.6}NbO_3-xBiFeO_3$ ($x = 0-3$ mol.%).

ϵ_r versus temperature for all $(1-x)K_{0.4}Na_{0.6}NbO_3-xBiFeO_3$ compositions are shown in **Figure 4**. At $x = 0$, T_{O-T} was observed at $\sim 175^\circ C$, which is lower than that for $Na_{0.5}K_{0.5}NbO_3$ ceramics

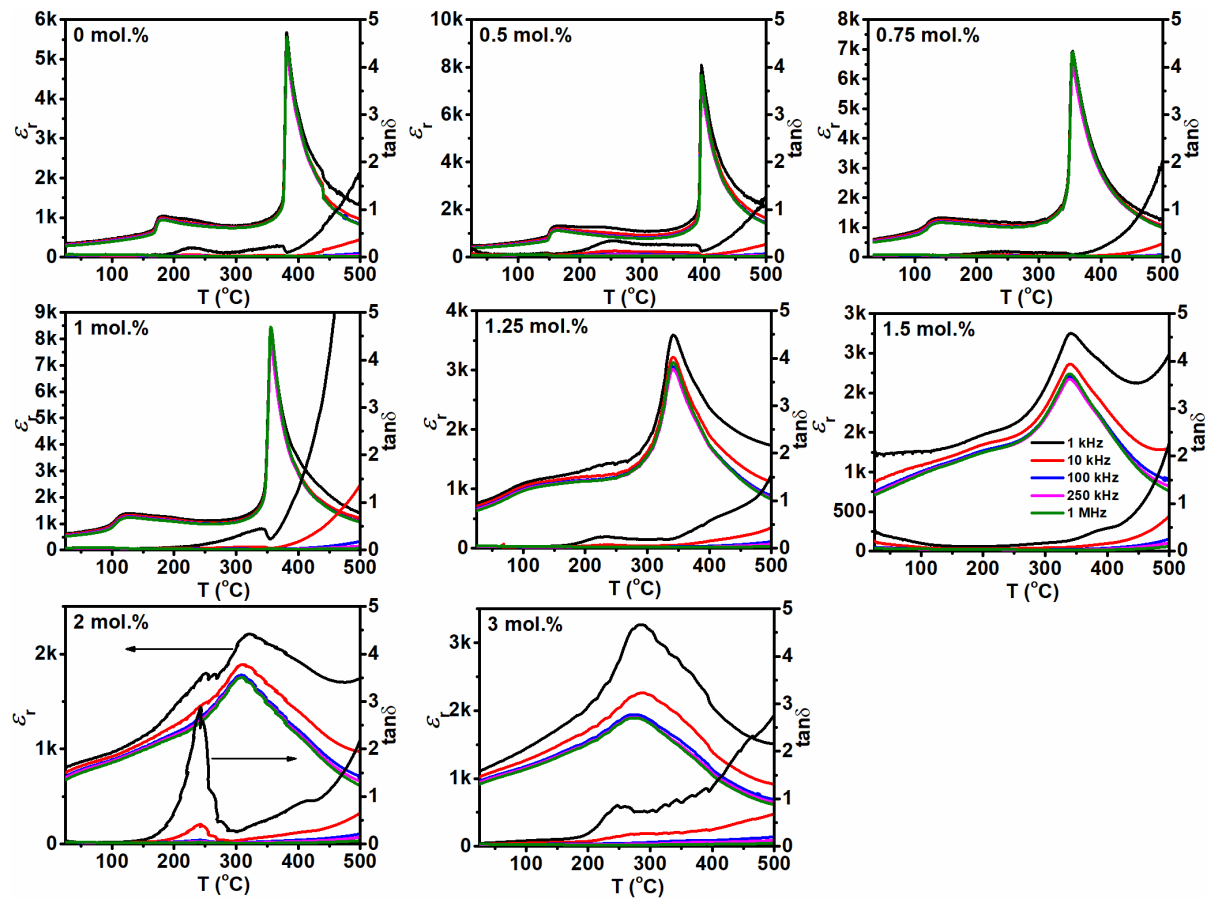


FIGURE 4 | Relative permittivity and $\tan \delta$ as a function of temperature at constant frequencies of 1, 10, 100, 250 kHz, and 1 MHz for $(1-x)K_{0.4}Na_{0.6}NbO_3-xBiFeO_3$ ($x = 1-3$ mol.%) ceramics.

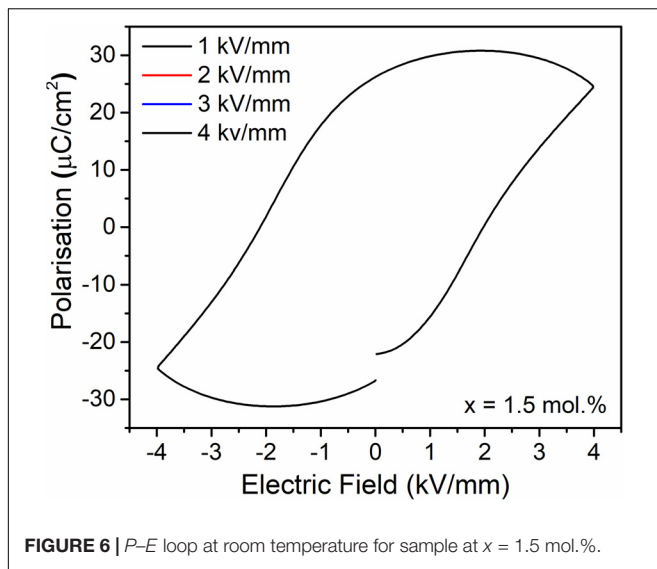


FIGURE 6 | P - E loop at room temperature for sample at $x = 1.5$ mol.%.

(i.e., $\sim 200^\circ\text{C}$). $T_{\text{O-T}}$ decreased with increasing BiFeO_3 amount from $\sim 176^\circ\text{C}$ ($x = 0$) to $\sim 107^\circ\text{C}$ ($x = 1$ mol.%). For sample with $x = 1.25$ mol.%, $T_{\text{O-T}}$ is not sharp but diffused consistent with the overlapped peaks observed in XRD plot (Figure 1). As BiFeO_3 concentration increases, no anomaly associated with the $T_{\text{O-T}}$ is observed. It is expected that $T_{\text{O-T}}$ may have been shifted below RT and/or may have smeared out because of chemical heterogeneity. It is noted that the sharp peak observed for the tetragonal to cubic transition (T_{C}) in samples with $x \leq 1$ mol.% has also broadened for $x > 1$ mol.%. In addition, samples with $x > 1$ mol.% showed smaller magnitude of ϵ_r at peak maxima

which is strongly frequency dependent. Low ϵ_r is attributed to low density, but its frequency dependence is most evident in the range 1 to 10 kHz. Above 100 kHz, ϵ_r is frequency independent. Such behavior indicates contributions from space charge polarization at lower frequencies due to ion migration which relax at > 1 kHz (Lingwal et al., 2006). The contribution from space charge and increased with increase in x , which may be due to vaporization of volatile species such as Bi, Na, and K ions. A similar trend was observed in the dielectric loss versus temperature where high $\tan\delta$ was noticed at low frequencies. We also note that $\tan\delta$ (100 kHz) is less than 5% at RT but the sample with $x > 1$ mol.% exhibit greater loss as a function of temperature in comparison to samples with $x \leq 1$ mol.%. Higher losses at $x > 1$ mol.% can be attributed to low densification and/or volatility of A-site cations. Moreover, BF itself is intrinsically very leaky and its larger contents may be resulting in higher conduction.

Figure 5 shows d_{33} for $(1-x)\text{K}_{0.4}\text{Na}_{0.6}\text{NbO}_3-x\text{BiFeO}_3$ ($x = 1-3$ mol.%) ceramics after DC poling at 40 kV/mm for 5 min. At $x = 0$, $d_{33} = 82$ pC/N was obtained which was similar to previously reported data (Egerton and Dillon, 1959; Jaeger and Egerton, 1962). d_{33} increased with BiFeO_3 concentration and reached a maximum of ~ 182 pC/N at $x = 1$ mol.%. The increase in d_{33} may be due to a decrease in $T_{\text{O-T}}$ as noticed in dielectric data (Figure 4) and/or an increase of the density, whereas the sharp decrease in d_{33} observed for $x > 1$ mol.% may be correlated to the significantly lower densities, as shown in Figure 5. In addition, high electrical conductivities in these samples are responsible for low d_{33} values, as they inhibit poling and often result in electrical breakdown. $T_{\text{O-T}}$ is supposed to be at RT for $x = 1.25-1.5$ mol.% which should lead to higher d_{33} values, provided that ceramics exhibiting higher resistivities, and densities can be successfully fabricated. The higher conductivity exhibited by ceramics with

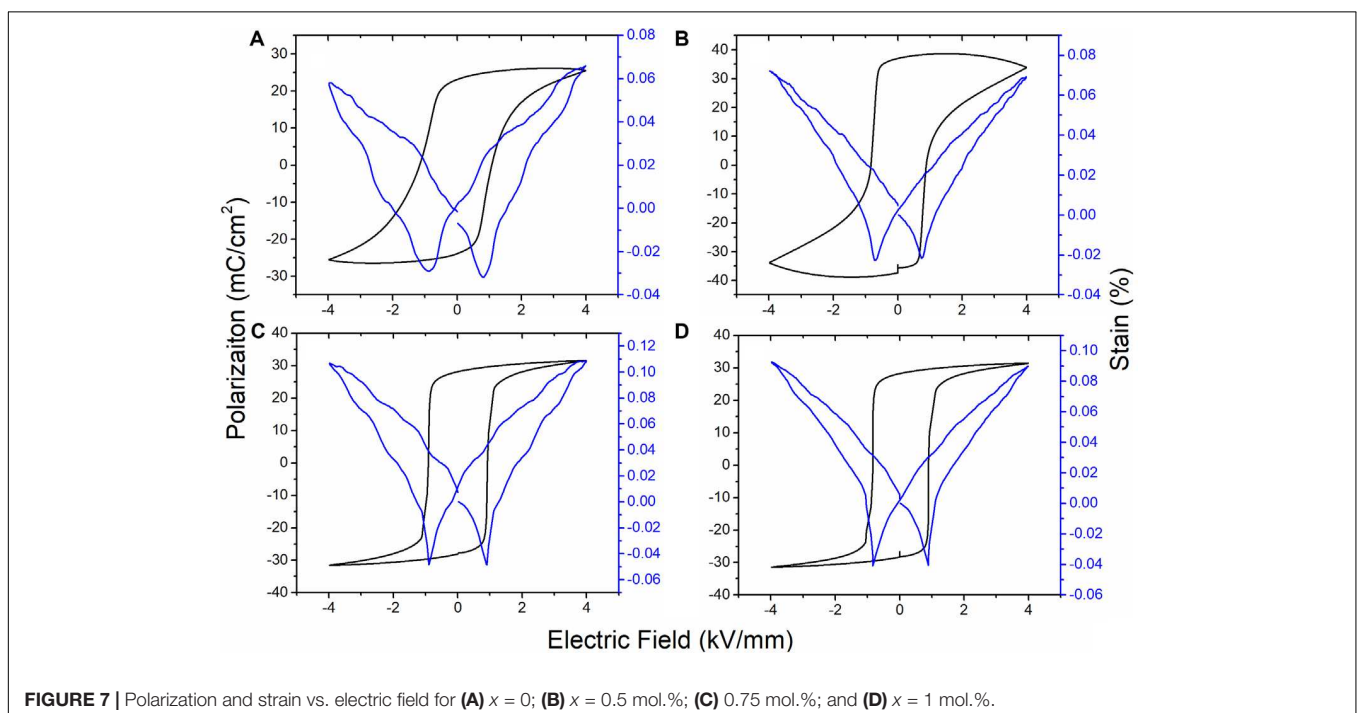


FIGURE 7 | Polarization and strain vs. electric field for (A) $x = 0$; (B) $x = 0.5$ mol.%; (C) 0.75 mol.%; and (D) $x = 1$ mol.%.

$x > 1$ mol.% leads to rounded polarization (P) vs. electric field (E) loops, with remanent polarization (P_r) higher than maximum polarization (P_{max}) which suggest high leakage current, **Figure 6**. Therefore, it is concluded that samples with $x > 1$ mol.% are unsuitable for large field measurements without further processing efforts to increase density and increase resistivity.

Figure 7 shows polarization and strain vs. electric field loops for samples $(1-x)K_{0.4}Na_{0.6}NbO_3-xBiFeO_3$ with 0–1 mol.%. Ceramics with $x = 0.5$ mol.% also exhibited high loss and hence the value of P_r is meaningless but samples with $x = 0.75$ and 1 mol.% exhibited well saturated loops with a high P_r of $\sim 28 \mu C/cm^2$ and low coercive field (E_c) of <1 kV/mm. It was also noted that the P - E loops for $x = 0.75$ and 1 mol.% are square. According to Haertling and Zimmer (1966), the degree of squareness (R_{sq}) of a P - E loop can be calculated from the empirical formula introduced in Eq. 1, which for an ideal square loop is equal to 2.

$$R_{sq} = \frac{P_r}{P_s} + \frac{P_{1.1}E_c}{P_r} \quad (1)$$

where “ P_s ” is saturation polarization and $P_{1.1} E_c$ is the polarization at 1.1 times of coercive field (E_c).

Samples with $x = 0.75$ and 1 mol.% exhibited $R_{sq} = 1.94$ and 1.95, respectively, which is closer to the ideal value of 2, indicating uniform grain size and better homogeneity (Haertling, 1999). The strain was observed to increase from 0.06 to 0.09% with increase in x from 0 to 1 mol.% at an applied $E = 4$ kV/mm.

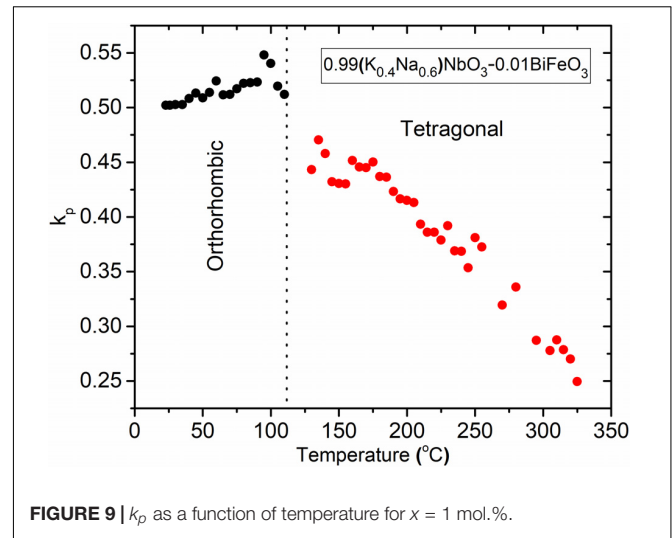


FIGURE 9 | k_p as a function of temperature for $x = 1$ mol. %.

Figure 8A shows that well saturated P-E loops are obtained at an electric field of 2 kV/mm for optimized compositions with $x = 1$ mol.%. The coercive field was estimated to be 0.8 kV/mm from current (I) vs. E curve (**Figure 8B**), where a sharp peak was observed at the point of switching. The sharp peaks are indicative of well-defined coercive fields because of instantaneous domain switching, which is consistent with the square loops observed for these samples. S-E loops with peak to peak strain of 0.08% at

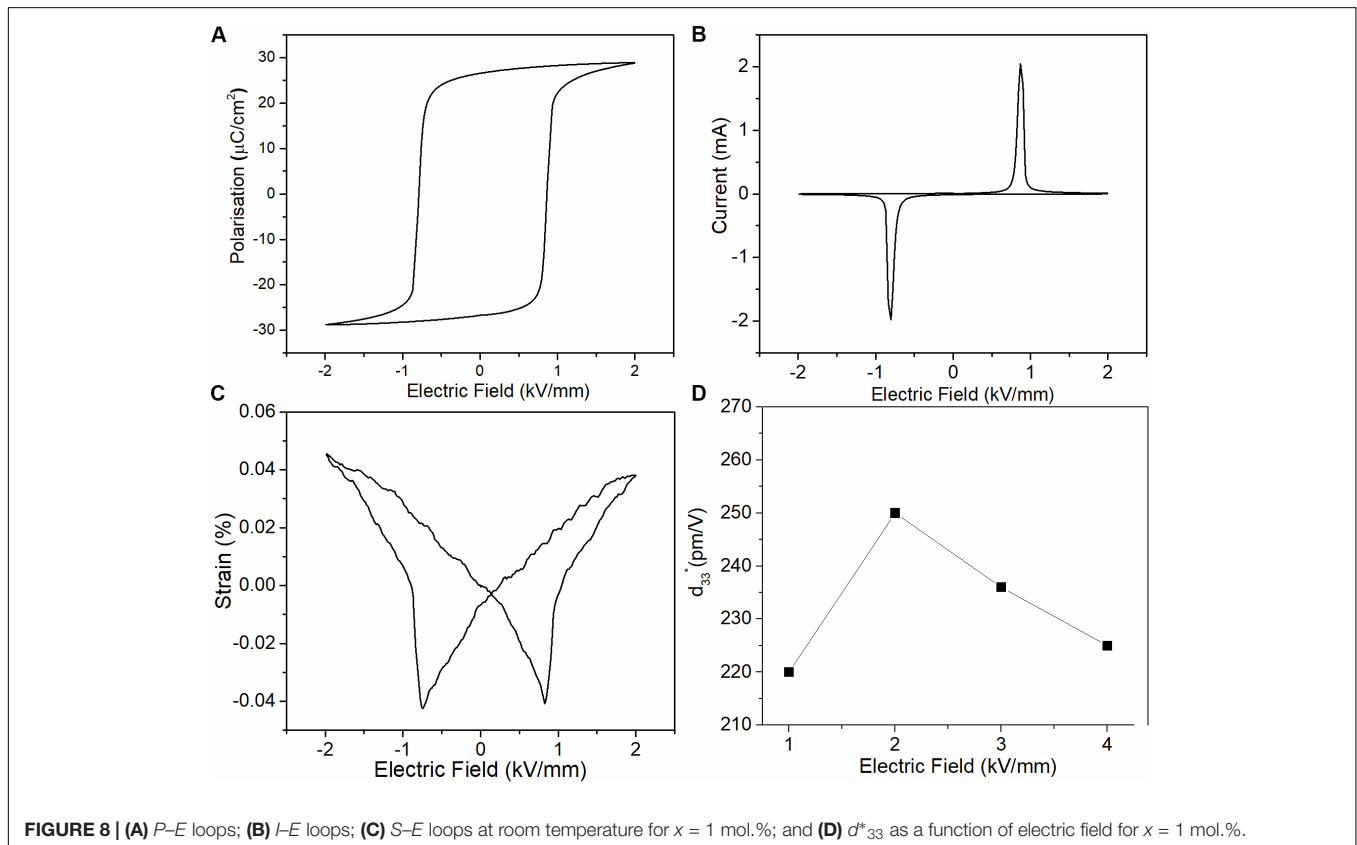


FIGURE 8 | (A) P - E loops; (B) I - E loops; (C) S - E loops at room temperature for $x = 1$ mol.%; and (D) d^*_{33} as a function of electric field for $x = 1$ mol. %.

$E = 2$ kV/mm are shown in **Figure 8C**. However, for practical applications, only a positive strain of 0.05% is useful. The negative strain in S-E loops is indicative of long-range ferroelectric order, consistent with the P-E loops. Strain values are influenced by both intrinsic and extrinsic factors (Donnelly et al., 2007). The extrinsic contributions are mainly dominated by domain wall motion, which due to low coercive field contributes at lower electric field. The optimum d^*_{33} value (250 pm/V) is therefore, observed at 2 kV/mm and further increase in electric field does not increase d^*_{33} , as shown in **Figure 8D**.

$(1-x)\text{K}_{0.4}\text{Na}_{0.6}\text{NbO}_3-x\text{BiFeO}_3$ ceramics have optimized piezoelectric properties at RT for ceramics with $x = 1$ mol.% ($d_{33} = 182$ pC/N, $d^*_{33} = 250$ pm/V, and $k_p = 50\%$). However, of equal importance for application are the temperature dependent of properties.

k_p as a function of temperature for the sample with $x = 1$ mol.% is shown in **Figure 9** which is stable up to 90°C with a variation of $\sim 5\%$ and then linearly decreased at temperatures $>100^\circ\text{C}$ to $\sim 50\%$ of its efficiency at 300°C . $T_{\text{O-T}} = 108^\circ\text{C}$, therefore, it can be concluded that k_p is stable in the orthorhombic state, but degradation occurs when the structure changes to tetragonal symmetry (Khesro et al., 2016b). Though the reason of this degradation is unclear at this point, however it may be possible that the samples starts depoling at the onset of the phase transition which results in lower values of k_p as the temperature is increased.

Figure 10A shows P-E loops at selected temperatures from 22 to 90°C . The coercive field decreased with increase in

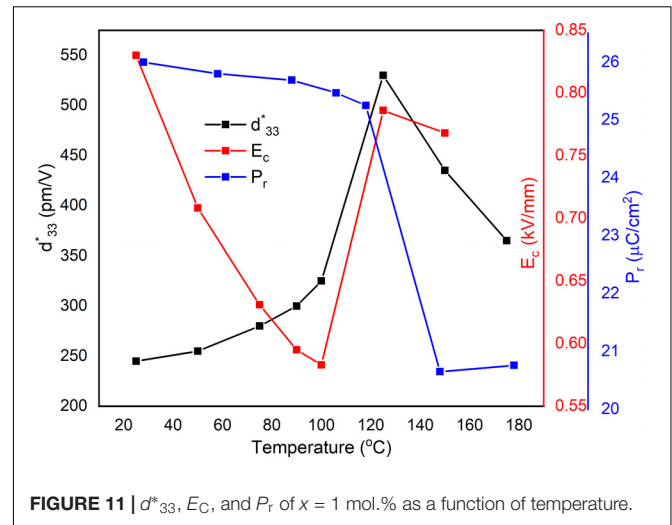


FIGURE 11 | d^*_{33} , E_e , and P_r of $x = 1$ mol.% as a function of temperature.

temperature, associated with easy domain switching at higher temperatures but the maximum polarization remains unchanged.

Figure 10B shows the corresponding bipolar S-E loops, which reveal a limited temperature dependence of the field-induced strain. The change in positive strain is about 15% from 22 to 75°C . With increasing temperature, as the phase transition is approached there are significant changes on both P-E and S-E responses, as illustrated in **Figures 10C–D**, respectively. In the

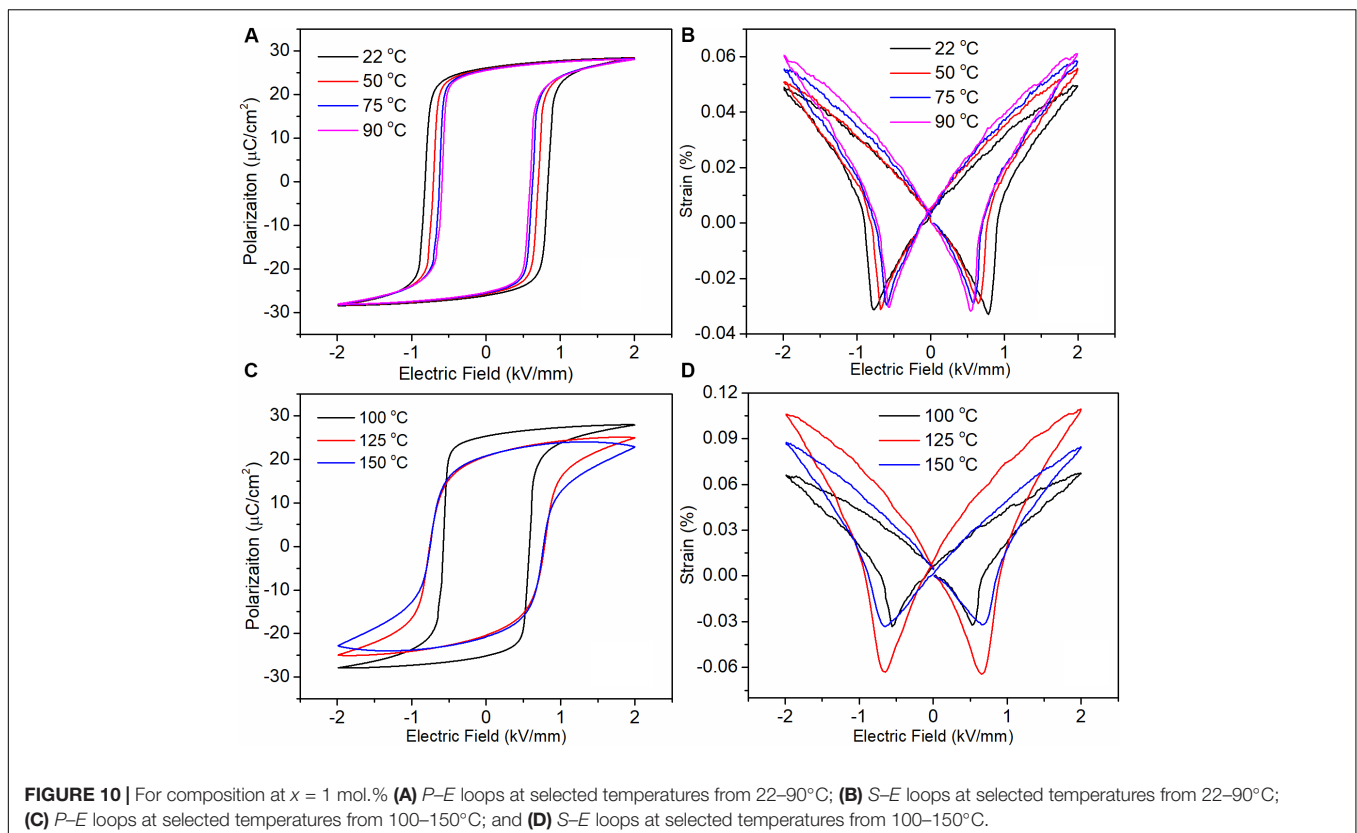


FIGURE 10 | For composition at $x = 1$ mol.% (A) P-E loops at selected temperatures from 22– 90°C ; (B) S-E loops at selected temperatures from 22– 90°C ; (C) P-E loops at selected temperatures from 100– 150°C ; and (D) S-E loops at selected temperatures from 100– 150°C .

tetragonal phase, the P–E loops become tilted with an increase in coercive field as shown in **Figure 10C**. This change occurs at 125°C, which corresponds to the temperature at which the largest field-induced strain is observed, as shown in **Figure 10D**. The peak to peak strain at this temperature is $\sim 0.16\%$ compared with ~ 0.08 at RT. In summary, bipolar strain is relatively stable up to 75°C, reaches a maximum at 125°C but decreases above the T_{O-T} transition. The maximum strain closer to the phase transition may be attributed to the increased domain wall motion due to increase in temperature and coexistence of crystal symmetries (Orthorhombic + Tetragonal) around 125°C, followed by a disappearance of the orthorhombic symmetry at higher temperatures, leading to lower achievable strains.

Figure 11 summarizes key parameters for $x = 1$ mol.% as a function of temperature but is evident that *in situ* measurements demonstrate that piezoelectric properties of $(1-x)K_{0.4}Na_{0.6}NbO_3-xBiFeO_3$ are severely temperature dependent.

This study was seeking to find a compromise between high piezoelectric coefficients and temperature stability by pushing the polymorphic phase out of the operating window and achieve a single tetragonal phase. In this respect $(1-x)K_{0.4}Na_{0.6}NbO_3-xBiFeO_3$ still shows some limitations because compositions with $x > 1$ mol. % could not be fabricated as dense ceramics. Furthermore, the piezoelectric properties continuously degrade even in the pure tetragonal phase and hence the absence of a structural phase transition may not be sufficient to achieve temperature stable properties in $K_{0.5}Na_{0.5}NbO_3$ -based ceramics. Despite these issues, incentives such as the potential for co-firing with low cost Ni (Hayashi et al., 2012) and Cu (Gao et al., 2016) internal electrodes make $K_{0.5}Na_{0.5}NbO_3$ a commercially attractive material for piezoelectric applications.

CONCLUSION

An investigation of the $(1-x)K_{0.4}Na_{0.6}NbO_3-xBiFeO_3$ system revealed that dense ceramics can be obtained for $x \leq 1$ mol.%. Piezoelectric properties were enhanced as $BiFeO_3$ content increased to 1%, beyond which the piezoelectric properties degraded. The degradation in properties was associated with

poor densification during sintering. Optimum properties were obtained for ceramics with $x = 1$ mol.% ($d_{33} = 182$ PC/N, $d^*_{33} = 250$ pm/V, and $k_p = 50\%$). Though the composition has a high $T_C = 355^\circ\text{C}$, stability is limited by T_{O-T} (108°C). The sample is stable in orthorhombic phase with k_p showing a variation of only $\sim 5\%$ from RT– 90°C . The strain-electric field curves (d^*_{33}) also showed stability RT– 75°C , provided a variation of 15% is considered acceptable. At the onset of T_{O-T} , large variations in piezoelectric coefficients are observed. The piezoelectric coefficients are not stable in tetragonal phase and a continuous degradation is observed as T_C is approached. This study concludes that temperature stability in a limited range can be achieved in $(1-x)K_{0.4}Na_{0.6}NbO_3-xBiFeO_3$ as long as T_{O-T} is ~ 100 – 120°C (Khesro, 2016).

DATA AVAILABILITY STATEMENT

The datasets generated for this study are available on request to the corresponding author.

AUTHOR CONTRIBUTIONS

AK performed all the experimental work and wrote the manuscript. IR and DW supervised the work. FH and RM helped with processing of ceramics. GW helped with the rietveld refinements. AF helped with strain measurements. All authors provided critical feedback and contributed to the final manuscript.

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Conflict of Interest: The authors declare that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

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