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The influence of excess K_2O on the electrical properties of $(K,Na)_{1/2}Bi_{1/2}TiO_3$ ceramics

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The influence of excess K_2O on the electrical properties of $(K,Na)_{1/2}Bi_{1/2}TiO_3$ ceramics

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The solid solution $(K_xNa_{0.50-x})Bi_{0.50}TiO_3$ (KNBT) between $Na_{1/2}Bi_{1/2}TiO_3$ and $K_{1/2}Bi_{1/2}TiO_3$ (KBT) has been extensively researched as a candidate lead-free piezoelectric material because of its relatively high Curie temperature and good piezoelectric properties, especially near the morphotropic phase boundary (MPB) at $x \sim 0.10$ (20 mol. % KBT). Here, we show that low levels of excess K_2O in the starting compositions, i.e., $(K_{y+0.03}Na_{0.50-y})Bi_{0.50}TiO_{3.015}$ (y-series), can significantly change the conduction mechanism and electrical properties compared to a nominally stoichiometric KNBT series $(K_xNa_{0.50-x})Bi_{0.50}TiO_3$ (x-series). Impedance spectroscopy measurements reveal significantly higher bulk conductivity (σ_b) values for $y \geq 0.10$ samples [activation energy (E_a) ≤ 0.95 eV] compared to the corresponding x-series samples which possess bandgap type electronic conduction ($E_a \sim 1.26$ – 1.85 eV). The largest difference in electrical properties occurs close to the MPB composition (20 mol. % KBT) where $y = 0.10$ ceramics possess σ_b (at 300 °C) that is 4 orders of magnitude higher than that of $x = 0.10$ and the oxide-ion transport number in the former is ~ 0.70 – 0.75 compared to < 0.05 in the latter (between 600 and 800 °C). The effect of excess K_2O can be rationalised on the basis of the (K + Na):Bi ratio in the starting composition prior to ceramic processing. This demonstrates the electrical properties of KNBT to be sensitive to low levels of A-site nonstoichiometry and indicates that excess K_2O in KNBT starting compositions to compensate for volatilisation can lead to undesirable high dielectric loss and leakage currents at elevated temperatures. © 2018 Author(s). All article content, except where otherwise noted, is licensed under a Creative Commons Attribution (CC BY) license (<http://creativecommons.org/licenses/by/4.0/>).

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Piezoelectric ceramics have been extensively used in applications such as actuators, sensors, and transducers since the 1950s due to their excellent electro-mechanical properties. Among all oxides, lead zirconate titanate [$Pb(Zr_{1-x}Ti_x)O_3$, PZT] has been the most widely investigated and used piezoelectric material; however, with growing concerns about the toxicity of lead, research on more environment-friendly, lead-free replacements for PZT has become imperative. Sodium bismuth titanate ($Na_{1/2}Bi_{1/2}TiO_3$, NBT), potassium bismuth titanate ($K_{1/2}Bi_{1/2}TiO_3$, KBT), and their solid solutions with each other and with other Pb-free ferroelectric perovskites such as $BaTiO_3$ are considered promising candidates due to their relatively high Curie temperatures and competitive piezoelectric properties.^{1–8} A common feature of PZT, KBT, and NBT is the volatility of the A-site cations during high temperature processing. In order to maintain charge balance, in some cases such volatility (e.g., Pb in PZT and Bi in NBT) can introduce oxygen vacancies which can lead to high levels of dielectric loss via oxide-ion or electronic conduction. Therefore, it is a common practice to add excess levels of A-site cation reagents in starting compositions in attempts to compensate for their volatility.

In recent years, we have demonstrated the electrical behaviour of NBT to be highly sensitive to low levels of A-site non-stoichiometry^{9–12} with three different types of conduction being identified depending on the A-site starting

composition. Type I NBT with a starting Na:Bi ratio of ≥ 1 possesses high oxide-ion conduction (oxide-ion transport number, $t_{ion} > 0.85$) which is comparable to/slightly lower than the best known oxide-ion conductors such as gadolinia-doped ceria (GDC) and yttria-stabilised zirconia (YSZ); type II NBTs with $Na:Bi \ll 1$ are mixed oxide-ion and n-type electronic conductors ($0.2 < t_{ion} < 0.6$); and type III NBTs with $Na:Bi < 1$ are excellent dielectric materials that exhibit near intrinsic electronic conduction ($t_{ion} < 0.1$) and low dielectric loss.¹¹ The difference in bulk conductivity between type I and III NBTs can be more than three orders of magnitude. In addition to A-site non-stoichiometry, the level of oxygen vacancies can also be suppressed by donor (e.g., Nb^{5+} for Ti^{4+}) dopants or further enhanced by acceptor (e.g., Mg^{2+} for Ti^{4+} or Sr^{2+} for Bi^{3+}) dopants, which can be employed to manipulate the level of oxide-ion conduction in NBT.^{13–16}

In contrast to NBT, the electrical properties of KBT do not exhibit such a strong dependence on the starting A-site non-stoichiometry. Although KBT can exhibit mixed oxide-ion/electronic conduction at high temperatures (> 600 °C),¹⁷ the level of oxide-ion conduction in KBT is rather low compared to NBT (~ 3 orders of magnitude lower). Although not fully understood, this has been attributed to the difference in polymorphism exhibited by these perovskites. Compared to NBT, KBT has the Na ion replaced by the larger K ion, which increases the tolerance factor and leads to a non-tilted

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perovskite-type structure. It is also noteworthy that below $\sim 300^\circ\text{C}$, KBT exhibits a significant level of volumetric proton conduction which is sensitive to the K content in the starting composition with higher K contents, leading to higher levels of proton conduction.¹⁷ Considering these differences, it is interesting to examine the binary solid solution between these two compounds.

The KBT-NBT solid solution (KNBT) is one of the candidates for lead-free piezoelectric ceramics. It has attracted interest because of its high permittivity and good electromechanical properties, especially at 16–20 mol. % KBT where there is a reported morphotropic phase boundary (MPB) between the room temperature rhombohedral (NBT) and tetragonal (KBT) structured end members.^{8,18–21} However, unlike NBT, most dielectric studies performed on KNBT show good dielectric properties with low dielectric loss ($\tan \delta$) despite the high oxide-ion conduction that can occur in NBT.^{18,22,23} Here, we investigate the electrical conduction mechanism(s) within the KNBT solid solution to improve our understanding of the structure–composition–property relationships not only for this solid solution but also for the two end members. In particular, we report on the influence of the K-content in the starting composition on the electrical properties of KNBT via two series of ceramics: nominally stoichiometric $(\text{K}_x\text{Na}_{0.50-x})\text{Bi}_{0.50}\text{TiO}_3$ ($0.00 \leq x \leq 0.50$, x-series) and K-excess $(\text{K}_{y+0.03}\text{Na}_{0.50-y})\text{Bi}_{0.50}\text{TiO}_{3.015}$ ($0.10 \leq y \leq 0.50$, y-series).

$(\text{K}_x\text{Na}_{0.50-x})\text{Bi}_{0.50}\text{TiO}_3$ ($0.00 \leq x \leq 0.50$, x-series) and $(\text{K}_{y+0.03}\text{Na}_{0.50-y})\text{Bi}_{0.50}\text{TiO}_{3.015}$ ($0.10 \leq y \leq 0.50$, y-series) ceramics were prepared by the conventional solid-state method. The mixtures of raw materials Na_2CO_3 (99.5%), K_2CO_3 (99.5%), Bi_2O_3 (99.9%), and TiO_2 (99.9%) were ball milled for 6 h, dried, sieved, and calcined at 800°C for 2 h. The resultant powders were ball milled for 4 h followed by another 2 h calcination at $850\text{--}900^\circ\text{C}$ and another 6 h ball milling. Pellets were sintered at $1050\text{--}1150^\circ\text{C}$ for 2 h. The phase purity, polymorphism, microstructure, and chemical composition of the sintered ceramics were determined by a combination of X-ray powder diffraction (XRD), scanning electron microscopy (SEM), and energy dispersive X-ray spectroscopy (EDX). The electrical properties were determined by Impedance Spectroscopy (IS). Oxide-ion transport number measurements (EMF) were performed on a ProboStat system. More details can be found in the [supplementary material](#).

XRD data (Fig. S1, [supplementary material](#)) showed a complete solid solution between NBT and KBT with no extra peaks observed from any secondary phase for both KNBT x and y series; however, SEM/EDX data (Fig. S2, [supplementary material](#)) revealed small amounts of $\text{K}_2\text{Ti}_6\text{O}_{13}$ (identification based on EDX data) as a secondary phase in x and y = 0.50. The calculated lattice parameters (Fig. S1, [supplementary material](#)) for the KNBT ceramics from XRD data showed a continuous increase with the increasing KBT content, therefore confirming the existence of a near complete solid solution between the end member phases. The grain size of the KNBT ceramics decreased significantly with the KBT content from about 5–10 μm for x = 0.00 to 0.5–1 μm for x and y = 0.10, (Fig. S3, [supplementary material](#)). The density of sintered ceramics (Fig. S4,

[supplementary material](#)) decreased with the increasing KBT content and most notably from $>90\%$ for x or y ≤ 0.20 to $\sim 70\%$ – 85% for x or y ≥ 0.30 . Low ceramic density does not significantly influence the magnitude of the bulk conductivity extracted from IS data and therefore allows comparison of conductivity trends across both series. In contrast, the dielectric properties are strongly influenced by porosity, and therefore, dielectric data are only shown for x and y = 0.10 where the ceramic density was $>95\%$ of the theoretical X-ray density.

Impedance complex plane (Z^*) plots for the x- and y-series ceramics at 600°C are shown in Fig. 1. A single arc was observed in the measured frequency range for all samples except x = 0.00 and 0.02 and y = 0.10. On the other hand, the x = 0.00 and 0.02 data consist of an incomplete higher frequency arc, a distorted lower frequency arc, and a low frequency (<1 Hz) electrode-type response [Fig. 1(b)], whereas data for y = 0.10 consisted of a single incomplete arc with a low frequency electrode-type response [Fig. 1(d)]. The associated capacitance for the high frequency arc (single arc in most cases) for all ceramics in both series was in the range of 52–147 pF/cm at 600°C which is consistent with the grain (bulk) response. In general, the bulk resistivity (R_b) increased with x and y for all KNBTs; however, the trend is clearly different between the two series. In the x-series, R_b can be separated into two different groups, i.e., x = 0.00 and 0.02 and the rest of the series. At 600°C , it increases initially from $\sim 600 \Omega \text{ cm}$ for x = 0.00 to $\sim 2.5 \text{ k}\Omega \text{ cm}$ for x = 0.02 [Fig. 1(b)]. When the KBT content is increased to 20 mol. % (x = 0.10), R_b dramatically increases to $\sim 150 \text{ k}\Omega \text{ cm}$ and remains in the range of $\sim 150\text{--}620 \text{ k}\Omega \text{ cm}$ with no clear trend for x ≥ 0.10 [Fig. 1(a)]. In contrast, there is a less dramatic increase in R_b for the y-series [Figs. 1(c) and 1(d)]. The R_b for y = 0.10 was only $\sim 4.8 \text{ k}\Omega \text{ cm}$ which further increased with the KBT content with a maximum value of $\sim 420 \text{ k}\Omega \text{ cm}$ obtained for y = 0.40 [Fig. 1(c)].

Comparing the x and y KNBT series, samples with 20 mol. % KBT (i.e., x and y = 0.10) display the largest difference in electrical properties. The R_b of x = 0.10 is about 2 orders of magnitude higher than y = 0.10 [e.g., $R_b \sim 150 \text{ k}\Omega \text{ cm}$ for x = 0.10 and $\sim 4.8 \text{ k}\Omega \text{ cm}$ for y = 0.10 at 600°C , Figs. 1(a) and 1(d), respectively]. In addition, a low frequency spike in the Z^* plot for y = 0.10 is consistent with Warburg diffusion and indicates a significant level of oxide-ion conduction in this sample [inset of Fig. 1(d), which is not present in x = 0.10, Fig. 1(a)].

The temperature dependence of the bulk conductivity, σ_b (where $\sigma_b = 1/R_b$), for all samples is summarised in an Arrhenius plot in Fig. 2. For the x-series, σ_b is sensitive to relatively low levels of KBT and decreases by more than three orders of magnitude for x ≥ 0.10 [Fig. 2(a)], whereas for the y-series, σ_b decreased gradually with the increasing KBT content [Fig. 2(b)]. It is noteworthy that the activation energy (E_a) for σ_b for these two series of samples is also significantly different. For the x-series, E_a changes from $\leq 0.85 \text{ eV}$ for x ≤ 0.02 to $\sim 1.26\text{--}1.85 \text{ eV}$ for x ≥ 0.10 , indicating a change in the conduction mechanism. In contrast, E_a remains relatively low and similar for all samples in the y-series ($<0.95 \text{ eV}$).

The 1.5 mol. % extra K_2O in the starting composition of y = 0.10 had a modest influence on the magnitude and

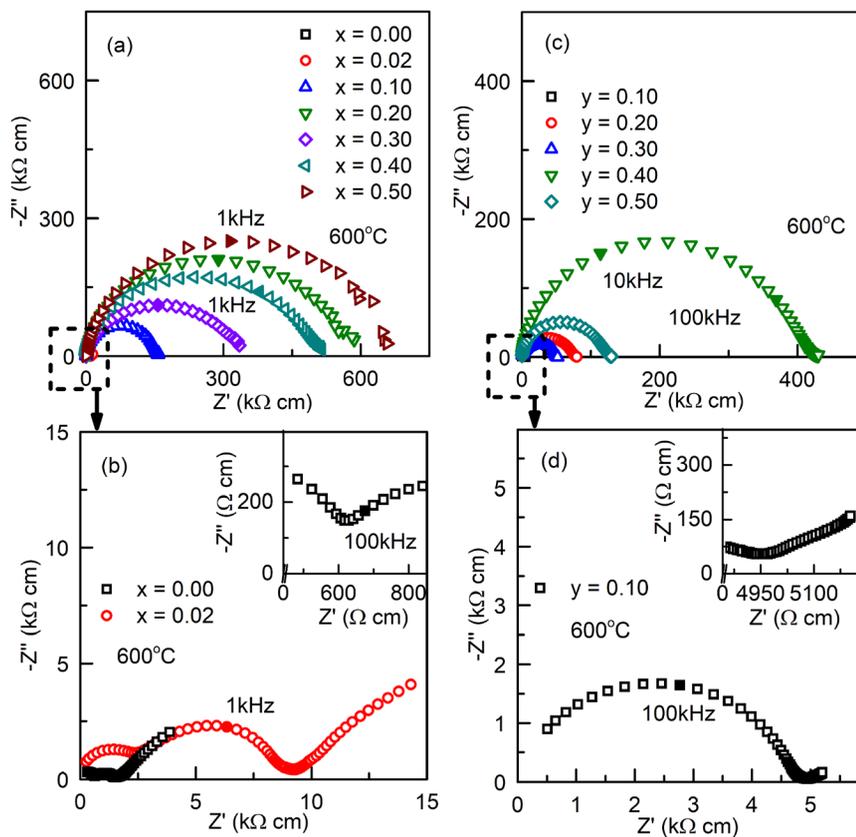


FIG. 1. Z^* plots of (a) $(K_xNa_{0.50-x})Bi_{0.50}TiO_3$ and (c) $(K_{y+0.03}Na_{0.50-y})Bi_{0.50}TiO_{3.015}$ series samples at 600°C. (b) and (d) High-frequency data of (a) and (c) on an expanded scale, respectively. The inset in (b) shows the bulk response for $x = 0.00$, and the inset in (d) shows the low-frequency data for $y = 0.10$.

temperature of the relative permittivity maximum ($\epsilon_{r,max}$) which was ~ 5820 at $\sim 300^\circ C$ for $x = 0.10$ and ~ 5480 at $290^\circ C$ for $y = 0.10$. In contrast, it had a dramatic effect on $\tan \delta$: $y = 0.10$ exhibited high levels of dielectric loss (> 0.15) above $\sim 400^\circ C$, whereas $x = 0.10$ displayed low loss (< 0.01) in the temperature range of $320\text{--}500^\circ C$ [Fig. 3]. The loss maximum observed at $< 300^\circ C$ shifts from $\sim 108^\circ C$ for $x = 0.10$ to $\sim 240^\circ C$ for $y = 0.10$.

The change in the conduction mechanism of the x -series but not in the y -series of samples was confirmed by EMF measurements using air/nitrogen gas [Fig. 4]. A significant level of oxide-ion conduction was observed for $y = 0.10$ with an ionic transport number (t_{ion}) $\sim 0.70\text{--}0.75$ from 600 to $800^\circ C$. In contrast, t_{ion} for $x = 0.10$ was less than 0.05 , indicating that the predominant conduction mechanism had switched from oxide-ion to electronic conduction. This is in agreement with the change in E_a in σ_b for the x -series [Fig. 2(a)].

The IS, LCR, and EMF data reveal the electrical behaviour of the two series of KNBT samples in this study to be different [Figs. 1–4]. The x -series with $x \geq 0.10$ exhibits excellent dielectric behaviour consistent with type III NBT with low σ_b and high associated E_a , low t_{ion} , and low dielectric loss above $300^\circ C$. In contrast, the y -series (1.5 mol. % excess K_2O in the starting composition) possesses mixed ionic-electronic type II NBT behaviour with relatively high σ_b with lower associated E_a , significant t_{ion} , and high dielectric loss above $300^\circ C$ which is consistent with significant levels of oxide-ion conduction. Clearly, the 1.5 mol. % extra K_2O in the starting compositions of the y -series leads to the difference in electrical behaviour.

The electrical properties of NBT are known to be highly sensitive to a low level of A-site non-stoichiometry in the

starting composition.¹² Nominally stoichiometric NBT, Bi-deficient, or Na-excess starting compositions (under our processing conditions) all produce type I oxide-ion conduction behaviour, whereas slightly Bi-excess (< 2 mol. %) or Na-deficient starting compositions can suppress the oxide-ion conduction and lead to type III insulating behaviour.^{9,10} It is worthy to note that the defect mechanisms for Na and Bi non-stoichiometry in NBT are different and can lead to opposite effects in their electrical properties. The most important parameter in controlling which defect mechanism will be adopted is the A-site Na:Bi ratio in the nominal starting composition. Starting compositions with Na:Bi ≥ 1 lead to the formation of oxygen vacancies in NBT and secondary phase(s), whereas starting compositions with Na:Bi < 1 lead only to the formation of secondary phase(s) without formation of significant levels of oxygen vacancies in NBT. In addition, it is now well known that the electrical properties of nominally stoichiometric NBT are strongly dependent on processing procedures such as the drying of raw materials prior to batching the powders for calcination and for covering pellets with sacrificial powder during sintering. Thus, the ratio of Na_2O - to Bi_2O_3 -loss during ceramic processing is critical to the electrical properties of nominally stoichiometric NBT as it can influence the Na:Bi ratio in sintered ceramics. Under our processing conditions, stoichiometric NBT is always a type I oxide ion conductor due to the loss of more Bi_2O_3 than Na_2O during processing. This results in an A-site Na:Bi > 1 and creates oxygen vacancies which produces the oxide-ion conduction in NBT.

In this study, the stoichiometric KNBTs (x -series samples) with $x \geq 0.10$ behave like type III insulating NBTs [Fig. 2(a)]. We attribute this rapid change in behaviour to a difference in the volatility of Na_2O and K_2O with K_2O being

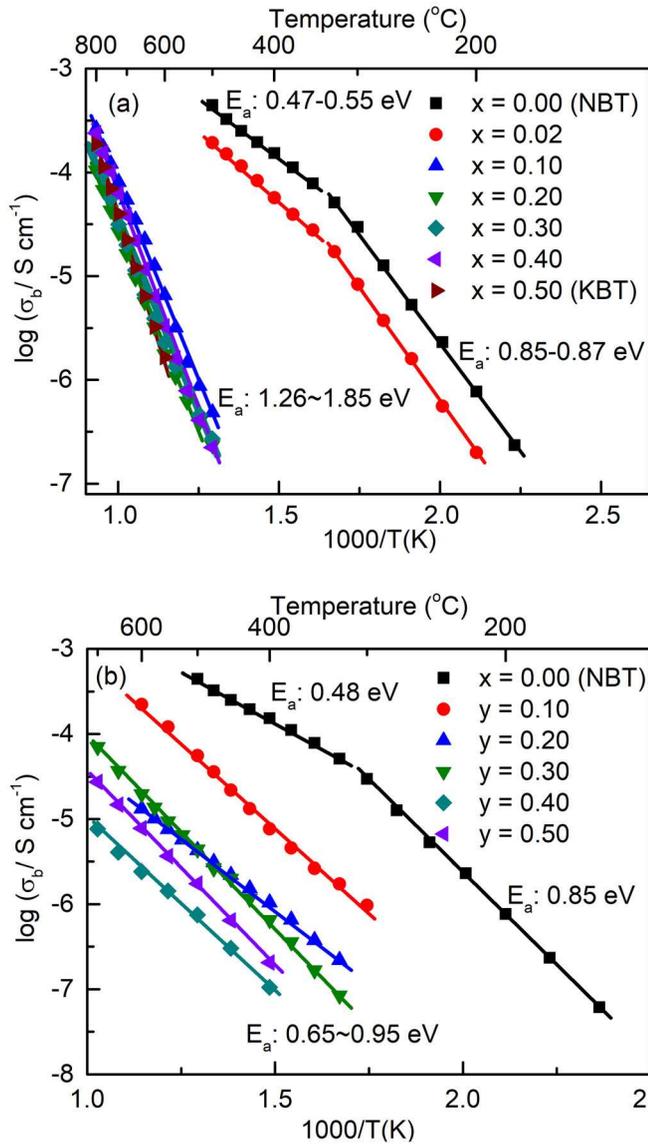


FIG. 2. Arrhenius-type plots of bulk conductivity for (a) $(\text{K}_x\text{Na}_{0.50-x})\text{Bi}_{0.50}\text{TiO}_3$ and (b) $(\text{K}_{y+0.03}\text{Na}_{0.50-y})\text{Bi}_{0.50}\text{TiO}_{3.015}$ series.

easier to volatilise during processing. If the loss of Bi_2O_3 in nominally stoichiometric NBT can be partially compensated by the loss of K_2O such that $(\text{K} + \text{Na}):\text{Bi}$ is closer to unity and then, σ_b will be reduced due to a decrease in the oxide vacancy concentration as in the case of $x = 0.02$ [Fig. 2(a)]. With the increasing K content in the starting compositions for both series, the loss of K_2O will be similar or surpass the loss of Bi_2O_3 during processing such that the composition of the perovskite phase in the KNBT ceramics will essentially be $(\text{K} + \text{Na}):\text{Bi} \leq 1$. Based on the previous results for NBT, it is known that starting compositions with $\text{Na}:\text{Bi} < 1$ have a low level of oxygen vacancies, and this leads to type III insulating behaviour as observed for $x \geq 0.10$ [Fig. 2(a)]. This suggestion is confirmed by the y-series results. In this case, the loss of K_2O during processing is partially compensated by the 1.5 mol. % excess K_2O in the starting compositions. The y-series are effectively nominally Bi-deficient due to the adjustment of $(\text{K} + \text{Na}):\text{Bi} > 1$, and although loss of K_2O , Na_2O , and Bi_2O_3 occurs during processing, this starting ratio is sufficient to ensure the formation of oxygen vacancies and

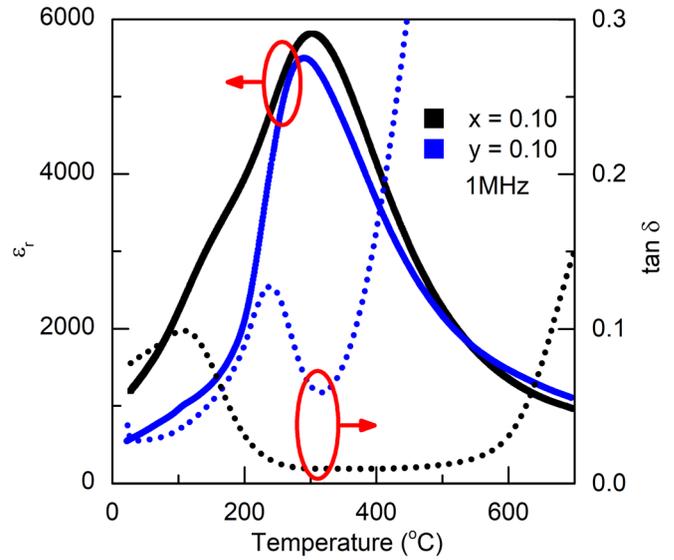


FIG. 3. Temperature dependence of ϵ_r (solid lines) and $\tan \delta$ (dashed lines) at 1 MHz for $(\text{K}_{0.10}\text{Na}_{0.40})\text{Bi}_{0.50}\text{TiO}_3$ ($x = 0.10$) and $(\text{K}_{0.13}\text{Na}_{0.40})\text{Bi}_{0.50}\text{TiO}_{3.015}$ ($y = 0.10$).

therefore oxide-ion conductivity, especially for $y = 0.10$ [Figs. 2(b) and 4].

Despite the excess K_2O in the nominal starting composition of the y-series to compensate for K-loss during processing, σ_b for the y-series still decreases with the increasing K-content; however, E_a remains unchanged. Combined with the modest decrease in t_{ion} when compared to NBT [Fig. 4], this suggests that the decrease in σ_b for the y-series is associated with a decrease in the charge carrier concentration rather than a change in the conduction mechanism. This decrease in the charge carrier concentration is related either to a small change in the $(\text{K} + \text{Na}):\text{Bi}$ ratio across the y-series or possibly to subtle, local structural changes associated with K doping in NBT. NBT exhibits a complex in-phase and out-of-phase TiO_6 tilted structure with off-centred and underbonded Bi ions.²⁴⁻²⁷ This leads to weak Bi-O bonding which plays a crucial role in the oxide-ion conduction in NBT. Such tilting of

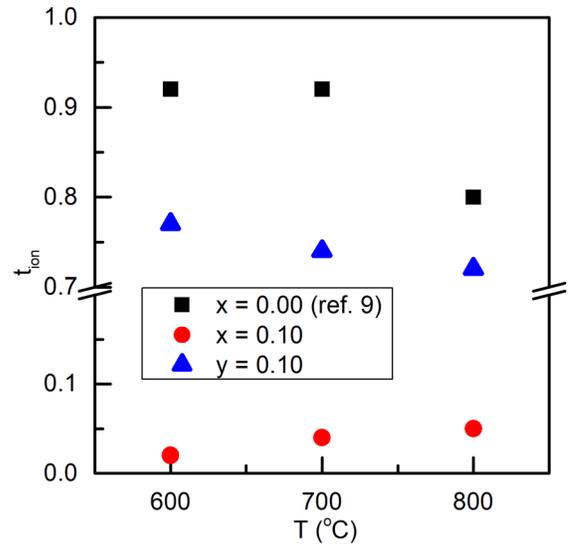


FIG. 4. Oxygen ionic transport number, t_{ion} , for $(\text{K}_{0.10}\text{Na}_{0.40})\text{Bi}_{0.50}\text{TiO}_3$ ($x = 0.10$) and $(\text{K}_{0.13}\text{Na}_{0.40})\text{Bi}_{0.50}\text{TiO}_{3.015}$ ($y = 0.10$) from EMF measurements using air/nitrogen gas.

octahedra are reduced when the smaller Na ion is replaced by the larger K ion and result in a non-tilted system for KBT contents ≥ 50 mol. %.¹⁹ The reduction of tilting will homogenise the Bi–O bond lengths which eventually strengthen the Bi–O bonding and reduce the concentration of mobile oxide ions (i.e., charge carrier concentration).

Unlike NBT, there are no reports of KNBT solid solutions being “leaky” which means that the insulating behaviour of the stoichiometric KNBTs (*x*-series) is reproducible and the loss of (K + Na) during processing surpasses the loss of Bi under different experimental conditions to ensure that (K + Na):Bi is < 1 in the perovskite lattice of sintered ceramics.^{28–34} KNBTs therefore always possess insulating behaviour unless extra K is intentionally added into the starting composition to compensate for the loss such that (K + Na):Bi ≥ 1 , as in the *y*-series. It is noteworthy that, as a candidate lead-free piezoelectric material, the best piezoelectric and dielectric properties in the NBT-KBT solid solution have been reported near the MPB which is located at 16–20 mol. % KBT. In this study, the largest difference in bulk conductivity and dielectric loss between the two series of samples occurred at ~ 20 mol. % KBT (i.e., x and $y = 0.10$). Diligence is therefore required when developing devices or conducting research based on the reported NBT-KBT MPB as small changes of the K content in the starting material may dramatically alter the dielectric loss properties of the final product [Fig. 3]. In the case of KNBT, adding an excess of K_2CO_3 to compensate for volatilisation is not recommended for high temperature dielectric/piezoelectric applications as this can adjust the (K + Na):Bi ratio to exceed unity and result in high levels of $\tan \delta$ above 300 °C due to significant levels of oxide-ion conductivity.

See [supplementary material](#) for a detailed experimental procedure, XRD, SEM, lattice parameters, and ceramic density results.

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