

Enhanced hyporheic exchange flow around woody debris does not increase nitrate reduction in a sandy streambed

Felicity Shelley 10 · Megan Klaar · Stefan Krause · Mark Trimmer

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Abstract Anthropogenic nitrogen pollution is a critical problem in freshwaters. Although riverbeds are known to attenuate nitrate, it is not known if large woody debris (LWD) can increase this ecosystem service through enhanced hyporheic exchange and streambed residence time. Over a year, we monitored the surface water and pore water chemistry at 200 points along a ~ 50 m reach of a lowland sandy stream with three natural LWD structures. We directly injected ¹⁵N-nitrate at 108 locations within the top 1.5 m of the streambed to quantify in situ denitrification, anammox and dissimilatory nitrate reduction to

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F. Shelley (⊠) · M. Trimmer (⊠) School of Biological and Chemical Sciences, Queen Mary University of London, Mile End Road, London E1 4NS, UK e-mail: f.c.shelley@qmul.ac.uk

M. Trimmer e-mail: m.trimmer@qmul.ac.uk

M. Klaar School of Geography, University of Leeds, Leeds, UK

S. Krause

School of Geography, University of Birmingham, Birmingham, UK

ammonia, which, on average, contributed 85, 10 and 5% of total nitrate reduction, respectively. Total nitrate reducing activity ranged from 0 to 16 μ M h⁻¹ and was highest in the top 30 cm of the stream bed. Depth, ambient nitrate and water residence time explained 44% of the observed variation in nitrate reduction; fastest rates were associated with slow flow and shallow depths. In autumn, when the river was in spate, nitrate reduction (in situ and laboratory measures) was enhanced around the LWD compared with non-woody areas, but this was not seen in the spring and summer. Overall, there was no significant effect of LWD on nitrate reduction rates in surrounding streambed sediments, but higher pore water nitrate concentrations and shorter residence times, close to LWD, indicated enhanced delivery of surface water into the streambed under high flow. When hyporheic exchange is too strong, overall nitrate reduction is inhibited due to short flow-paths and associated high oxygen concentrations.

Keywords Anammox · Denitrification · Large woody debris · Nitrate · Riverbed · Restoration

Introduction

Anthropogenic manipulation of the nitrogen cycle, primarily through mineral fertilizer production (Haber–Bosch process) and the burning of fossil fuels, has more than doubled the annual input of fixed nitrogen to the biosphere (Canfield et al. 2010; Gruber andGalloway 2008). Sustained population growth, and associated pressures on food and energy production, are likely to result in further unbalancing of this microbially-mediated macronutrient cycle (Godfray and Garnett 2014; Howden et al. 2013). Low nitrogen uptake efficiencies in agriculture [typically $\sim 50\%$ in the UK (Sylvester-Bradley and Kindred 2009)] mean that precipitation readily washes excess nitrogen from land into waterways. Although most fertilizer is applied as ammonium, the prevailing redox conditions in surface water allow the complete nitrification of ammonium to nitrate. This mass-delivery of nitrate to aquatic environments has already resulted in devastating ecological effects such as eutrophication (Camargo and Alonso 2006; Erisman et al. 2013; McIsaac et al. 2001), as well as risks to human health (Powlson et al. 2008), and increased costs in the treatment of drinking water (Shrimali and Singh 2001).

Rivers play an important role in both the downstream transport and the mitigation of nitrogen pollution (Alexander et al. 2007; Seitzinger et al. 2002). An estimated 23% of the 150 Tg of the nitrogen applied by humans each year to land is washed directly into rivers (Schlesinger 2009). Low-order (headwater) streams are important in the downstream transport of diffuse nitrate (Alexander et al. 2007). However, rivers are not inert pipelines, on the contrary, they are actually biogeochemical hot spots (Benstead and Leigh 2012; McClain et al. 2003; Pinay et al. 2015), which also play a major role in the transformation of reactive nitrogen to less ecologically active forms (Bernhardt et al. 2005; Bernot and Dodds 2005). Across large catchments, nitrate attenuation is inversely correlated with stream-order, due to the relatively large surface area to volume ratios in smaller streams which aids surface water contact with the hypoxic bed (Alexander et al. 2000; Peterson et al. 2001). Efforts to reduce the downstream transport of nitrogen pollution should therefore focus on enhancing the biological removal of nitrate in low-order streams (Craig et al. 2008; Dodds and Oakes 2008; Filoso and Palmer 2011).

Despite increasing efforts to reduce excess nitrate delivery to rivers, loadings remain critically high across many agricultural and urban catchments (Bouraoui and Grizzetti 2011; Burt et al. 2008; Howarth 2008). Therefore, there is now increasing pressure to develop in-stream methods for tackling nitrate pollution. The reintroduction of large woody debris (LWD) has become an integral part of many river restoration schemes world-wide and its impact on channel hydrological complexity, geomorphology and ecology have been evidenced in both field and experimental studies (Curran and Wohl 2003; Gippel 1995; Gurnell et al. 1995; Miller et al. 2010). LWD is known to enhance hyporheic exchange, through increased roughness (Kasahara et al. 2009), and there is increasing evidence of the importance of hyporheic flow-paths for nitrogen removal (Gomez-Velez et al. 2015; Krause et al. 2009, 2013). Further, LWD may also enhance nitrate removal as it encourages sediment accumulation and the decaying wood provides organic carbon (Krause et al. 2014). However, researchers are yet to examine the possible link between LWD in rivers and riverbed nitrogen removal in detail.

Previous attempts to determine the effect of LWD on nitrate attenuation (Aumen et al. 1990; Elosegi et al. 2016; Roberts et al. 2007; Warren et al. 2013; Webster et al. 2000) did not specifically measure nitrogen transformations within streambed sediments, but, instead, monitored downstream chloride and nitrate or ammonium concentrations following its release upstream of LWD structures. As such, these approaches provided first evidence of the potential net effect of LWD, without distinguishing between nitrate storage and transformation, and they were restricted in their spatial resolution. To properly determine whether LWD enhances the removal of nitrate from streams, high-resolution direct measurements of streambed nitrate processing are required to further elucidate previous reach-based assessments.

Here, we quantified nitrate reduction in a nitraterich sandy streambed rich in LWD. We combined in situ ¹⁵N-nitrate tracer process measurements (Lansdown et al. 2014) with the analysis of detailed physiochemical streambed properties, and pore water residence times, to unravel the key drivers of nitrate attenuation around the LWD. We hypothesised that LWD would enhance hydrodynamic forcing of nitraterich surface water into the streambed through, for example, increased topographic heterogeneity (Krause et al. 2014). We expected sustained delivery of nitrate into hypoxic pore waters to encourage the growth of nitrate reducing bacteria, which should result in enhanced rates of nitrate reduction in the vicinity of streambed LWD structures. However, should LWD only induce shallow hydrodynamic

forcing, we hypothesise that very short residence times will actually inhibit nitrate reduction.

In contrast to many previous stream nitrogen cycle studies, we aimed to simultaneously quantify all three of the known routes for microbial nitrate reduction [here, total oxidised inorganic nitrogen (NO₂⁻ + NO_3^{-})]: denitrification, anammox and dissimilatory nitrate reduction to ammonia. The push-pull technique for in situ measurement of nitrate reduction potential has been shown to give similar results to whole-reach ¹⁵N-tracer experiments, but with the additional benefit of being able to tease out the relative contribution of the three possible nitratereducing processes (Lansdown et al. 2014). Denitrification has received most attention and is usually considered the dominant mode of reduction (Seitzinger 1988) but that may in part be due to the techniques applied that couldn't distinguish between all three modes (Lansdown et al. 2014, 2016). Anaerobic ammonium oxidation (anammox) is less widely reported in freshwater environments but has recently been shown to play a significant role in N₂ production in permeable sediments (Lansdown et al. 2016; Zhou et al. 2014). Anammox is performed by obligate anaerobic bacteria which use nitrite to oxidise ammonia to produce di-nitrogen gas (Van de Graaf et al. 1996), the stoichiometry of which actually makes it a more efficient sink for reactive nitrogen over denitrification (Lansdown et al. 2016; Thamdrup et al. 2006). Finally, dissimilatory nitrate reduction to ammonia (DNRA) conserves nitrogen within the biosphere by reducing nitrate to ammonium. Therefore, from a reactive nitrogen removal perspective, denitrification and anammox are preferable to DNRA. To maximise the removal of nitrate as it flows through a river, diversion of the flow into the carbon-rich and oxygendepleted parts of the streambed is vital. Depending on the porosity, organic matter content and biogeochemical activity in the streambed, different flow-path lengths will be required in order for the nitrate to be fully reduced (Mulholland et al. 2008; Richardson et al. 2004; Trimmer et al. 2012; Zarnetske et al. 2011). In this sandy river we expected denitrification to be the dominant form of nitrate reduction, with lesser contributions for anammox and DNRA.

Methods

Field site

This study took place between September 2014 and October 2015 in a forested reach of the Hammer Stream, a sandy tributary of the River Rother in West Sussex, UK (Fig. 1). The catchment of the Hammer Stream covers 24.6 km² of agricultural (arable and pastoral) and forested land and the underlying geology is dominated by Greensands and Mudstones (British Geological Survey 2016) and it is a typical example of lowland rivers with elevated nitrate loading.

Ground penetrating radar (GPR) and sediment cores carried out for a parallel study (not presented here) showed that extensive clay lenses and peat layers at a depth of 1-2 m below the streambed effectively isolate the upper streambed in the reach used within this study from the underlying groundwater. Hyporheic flow is therefore dominated by down-welling surface water and bank flow contribution. The river banks are dominated by broadleaved deciduous trees which provide woody debris and leaf litter to the stream. Three prominent LWD structures were identified, each spanning > 50% of the channel width and causing visible depositional and erosional bed structures (Fig. 1). The several years old woody structures are natural and not part of any engineered restoration measures, and they were comprised of logs at least $1 \text{ m} \times 10 \text{ cm}$, as typically defines LWD (Keller and Swanson 1979).

Pore water and surface water sampling

Water level and temperature were measured using a pressure transducer (Levelogger 3001, Solinst, Ontario, Canada) and compensated for changes in atmospheric pressure changes using a barometer (Barologger Edge, Solinst, Ontario, Canada) installed in tandem at the site. Vertical head gradient measurements were obtained by standing the instream piezometers vertically for a minimum of 1 h prior to the use of a Solinst 102 M Mini Laser Marked Water Level Meter (Solinst, Georgetown, Ontario, Canada) to measure the height of the water level inside and on the outside of the piezometer tube relative to the top of the tube. Vertical hydraulic gradient (VHG) was calculated by subtracting the outside depth from the inside and dividing by the height from the top of the



Fig. 1 Location and experimental overview of the study site \mathbf{a} within the UK and \mathbf{b} within the hilly forested catchment, upstream of the lake (study reach coloured in red); \mathbf{c} a photograph of the most downstream LWD structure and newly installed flexible piezometer-sampling tube bundles, taken

piezometer to the streambed. Data were collected each season at the same time as the nutrient sampling. VHG data for each piezometer and season were then plotted in ArcGIS (10.3.1; ESRI, Redlands, CA, USA) and an Inverse Distance Weighting applied to interpolate between individual points.

Porewater was sampled via multi-level minipiezometers, comprising bundles of flexible Tygon tubing installed by hand at 40 locations along the reach (see Supplementary Fig. S1). Multi-level minipiezometers, largely following the designs of Krause et al. (2013) and Rivett et al. (2008), consisting of a central flexible tube (length 2.5 m, internal diameter (i.d.) 12 mm) with five smaller (i.d. 2 mm) water sampling tubes, terminated with nylon filter material at 10, 20, 30, 50 and 100 cm within the streambed, affixed around its edge, giving us 200 sampling points

facing upstream from a sandbar, under baseflow conditions (September 2014); **d** diagram of the 40 piezometer locations laid over the channel outline, with the LWD structures marked as brown lines. (Color figure online)

across a three-dimensional streambed array. During each campaign, the length of exposed tubing (above the sediment surface) was measured in order to adjust the "true depth" of the pore water sampling tubes which changed due to natural scour and deposition of sands.

Following installation in September 2014, weeklong sampling campaigns were conducted four times over a year from November 2014 (in November, February, May and July), during which all 200 streambed points and the surface water were sampled for background chemistries. Afterwards, a subset of locations (n = 76) were targeted for in situ measures of potential nitrate reduction (Lansdown et al. 2014). The subset consisted of the shallowest depth (10 cm), at all 40 locations (n = 40), and then an additional 9 locations at all depths (3 in the upstream section, 3 in the control reach, and 3 in the downstream section, n = 36). To maximise replication where tubes were either damaged or blocked, neighbouring depths were used instead.

To increase the spatial resolution around the two largest LWD structures in October 2015, a further 32 points in the streambed were investigated by installing stainless steel mini-probe samplers (Lansdown et al. 2014) to 15 cm into the bed (see Supplementary Fig. S1). The methods were carried out exactly as above to characterise the pore water chemistry and measure the potential for nitrate reduction in these additional locations.

The surface water was sampled mid-channel and mid-depth in the upstream (n = 3) and downstream (n = 3) sections, and pore water samples (10 mL) were withdrawn from the top of the sampling tubes using luer-lock sterile 12 mL syringes. To measure the ambient methane and nitrous oxide concentration, 3.5 mL of the sample was gently discharged into a 3 mL gas tight vial (Labco, Lampeter, UK) allowing to overflow slightly to minimise air contamination, before poisoning with ZnCl₂ (25 µL, 50% w/v) and capping. Next, oxygen, pH and temperature were measured using a calibrated fast-response glass oxygen electrode (OX50, Unisense, Aarhus, Denmark) and a field pH meter with a dual temperature and pH sensor (pH 100, VWR International, Radnor, USA). Finally, ~ 5 mL of the sample was filtered (0.45 μ m polypropylene, Gilson Scientific, Luton, UK) into plastic tubes (polypropylene, VWR International) and frozen in a portable freezer until analysis. In May, extra samples were taken for iron (II) whereby 1.5 mL of sample was dispensed directly into a solution of buffered phenanthroline (3.5:1, pH 4.5 acetate buffer/ 0.2% (w/v) 1-10-phenanthroline monohydrate) for preservation awaiting further colorimetric analysis in the laboratory (Eaton et al. 2005).

Analytical methods for determination of gas and nutrient concentrations

Gas chromatography (GC) was used to determine the concentration of methane in the pore water. A helium headspace (1 mL) was introduced into each gas-tight vial and, after equilibration (> 2 h shaking), 50 μ L of the headspace was withdrawn and injected into a GC fitted with a flame ionising detector (GC-FID) to measure CH₄ [Agilent Technology, UK, for full

specification see Sanders et al. (2007)]. The concentration in the original water sample was calculated using peak areas from a certified standard gas mixture (100 ppm CH_4 , Scientific and Technical Gases, UK) and appropriate solubility coefficients (Weiss and Price 1980; Yamamoto et al. 1976).

Using the filtered and frozen samples, the concentration of nitrite (limit of detection (LOD) 0.04 μ M), nitrate (LOD 0.1 μ M), ammonium (LOD 0.8 μ M) and soluble reactive phosphorus (SRP, LOD 0.1 μ M) was quantified using standard colorimetric methods (Kirkwood 1996), on an automatic segmented-flow analyser (Skalar, San++, De-Breda, Netherlands). Dissolved organic carbon (DOC) was measured in the filtered water samples using a total organic carbon analyser (TOC-VWP, Shimadzu, UK, LOD 50 μ M). Iron (II) concentration was determined by absorbance at 520 nm on an ultraviolet/visible spectrophotometer (LOD 1 μ M, precision 1%; Evolution 100, Thermo Fisher, USA).

Field methods for measuring in situ nitrate reduction

We used the isotope tracer "push-pull" technique previously described by Lansdown et al. (2014, 2016) to quantify the in situ potential for nitrate reduction to either to di-nitrogen gas (N_2) or ammonium (NH_4^+) . We took a 10 mL sample of the pore water to characterise ambient pore water chemistries prior (< 20 min) to injecting tracers and re-measured all parameters detailed above. The tracer solution consisted of deoxygenated (10 min bubbling with oxygen-free nitrogen, BOC, UK) artificial river water (as in Lansdown et al. 2014 modified from Smart and Barko 1985) with 300 µM¹⁵N-nitrate (98 at.%, Sigma Aldrich, UK) as a reactive tracer, and 10 mM potassium chloride as a conservative tracer. We injected 28 mL of tracer (8.2 µmol of ¹⁵N) at each location and then recovered 7 mL of the tracer/pore water mix after approximately 0, 10, 25 and 35 min. Following the recovery of each timed 7 mL sample, ~ 3.5 mL was discharged into a gas-tight vial and poisoned (as above) for ¹⁵N-N₂ and ¹⁵N-N₂O analysis, and the remaining sample was filtered (as above) and frozen for chloride and ¹⁵N-NH₄ analysis.

Advective-dispersive flow of streambed pore water was estimated by calculating the dilution of the conservative tracer (KCl) over the duration of the nitrate reduction measurements ($\sim 35-50$ min) and the linear portion of the decay in chloride concentration was used to calculate a rate. The concentration of chloride was measured in the laboratory, using an ionselective electrode (ISE Electrode, Cole Palmer, Stone, UK) which was calibrated against prepared standards (sodium chloride, 0–20 mM).

Laboratory determination of nitrate reducing potentials in sediment slurries

In addition to the in situ measurement of nitrate reduction described above, we also wanted to characterise the relative nitrate reducing potential of the sediments regardless of their in situ chemistry, under controlled laboratory conditions using sediment slurries. Surface sediments from the top 10 cm (< 15 cm horizontal distance from each piezometer bundle) were collected throughout the reach (n = 3) using a small plastic tub and then transferred into an anoxic glove-box (CV204, Belle Technology, Weymouth, UK). Following homogenisation, ~ 1 g wet sediment and 900 µL of nitrate-free artificial river water (Smart and Barko 1985) were added to gas-tight vials (3 mL). The sediment slurries were then left to "pre-incubate" for 24 h to reduce any traces of ambient ¹⁴N-nitrate and oxygen before starting the ¹⁵N experiments (Risgaard-Petersen et al. 2004). To start the experiment, 100 µL of 98 at.% ¹⁵N-sodium nitrate was injected through the butyl septum of each vial (n = 4)per original sediment sample), then they were then gently shaken (rpm 60, SSM1 Orbital Shaker, Stuart, Stone, UK) before bacterial activity was stopped via injection of 100 µL of zinc chloride after 0, 1.5, 4 and 6 h (see Lansdown et al. 2012 for more detail). One vial for each original sediment sample was left to incubate without ¹⁵N-sodium nitrate to serve as a reference measure of ¹⁵N-N₂ natural abundance.

Analytical methods for determination of nitrate reduction

Here we wanted to test the effect of large woody debris on any in situ sediment potential to reduce nitrate directly within the stream bed. To do that we injected ${}^{15}NO_3^-$ at the same, non-rate-limiting concentration at each point in the bed and used the ${}^{15}N$ -labelling of recovered N₂, N₂O and NH₄ pools, over time, relative to the reference samples, to calculate the in situ potential rate of ¹⁵N-nitrate reduction via denitrification, anammox and DNRA. The ¹⁵N-N₂ content was determined by mass spectrometry. Calibration was performed using internal reference gas (analytical grade nitrogen, BOC, Guildford, UK) and N₂ in a helium headspace added to air-equilibrated water at 22 °C, run at the same time as the samples (Lansdown et al. 2014). An auto-sampler was used to inject 50 μ L of the headspace into an elemental analyser interfaced with a continuous flow-isotope ratio mass spectrometer (Continuous Flow 20-22, Sercon Group, Crewe, UK), which measured the mass-charge ratios for m/z 28, 29 and 30 nitrogen ($^{28}N_2$, $^{29}N_2$ and $^{30}N_2$). To distinguish between ¹⁵N-N₂ production via denitrification and anammox in situ, we used the ¹⁵N labelling in any ¹⁵N-N₂O production as a proxy for the ratio of $^{15}NO_3^{-}$ to $^{14}NO_3^{-}$ being reduced (Lansdown et al. 2016; Trimmer et al. 2006). N₂O was pre-concentrated prior to analysis by continuous flow isotope-ratio mass spectrometry (Precon, ThermoFinnigan, Ringoes, USA) and mass-charge ratios for 44, 45 and 46 were measured. For the sediment slurries, the ratio of ¹⁵NO₃⁻ to ¹⁴NO₃⁻ being reduced was simply equivalent to the ¹⁵N at.% of the injected nitrate.

To quantify ¹⁵N-DNRA, we performed a hypobromite oxidation of NH₃ to N₂ (after Risgaard-Petersen et al. 1995) on 1 mL of the recovered porewaters to quantify their ¹⁵N-NH₄⁺ content. Standards were prepared from ¹⁵N-NH₄Cl (98 at.%, Sigma Aldrich) over a range of concentrations (5–600 μ M) and isotope labelling (1–20%) similar to that expected in the samples. The concentration of total NH₃ (i.e. ¹⁴NH₃ plus ¹⁵NH₃ measured by segmented-flow colorimetric analysis, as above) was multiplied by the excess-¹⁵N-N₂ (relative to natural abundance) in the sample to give total ¹⁵N-NH₄⁺ and linear regression of this production against time was used to calculate a potential in situ rate of ¹⁵N-DNRA.

We measured the production of ${}^{29}N_2$ as well as ${}^{30}N_2$ to calculate total ${}^{15}N_2$ production (denitrification + anammox), and the rate of either in situ or the sediment slurry activity was quantified using the following equation from Thamdrup and Dalsgaard (2000):

$$\Delta^{x} N_{2t=i} (nM N_{2}) = \left[\left(\frac{{}^{x} N_{2}}{\sum N_{2}} \right)_{t=i} - \left(\frac{{}^{x} N_{2}}{\sum N_{2}} \right)_{ambient} \right] \\ \times \sum N_{2} \times \alpha^{-1} \times V_{s}^{-1},$$
(1)

where $\Delta^x N_2$ is the excess ${}^{29}N_2$ or ${}^{30}N_2$ in the sample at time *i*, ${}^xN_2/\sum N_2$ is the proportion of ${}^{29}N_2$ or ${}^{30}N_2$ signal relative to the total signal ($\sum^{28}N_2$ + ${}^{29}N_2$ + ${}^{30}N_2$), α is the calibration factor (signal/ nmol N₂), and V_s is the volume of sample in the vial (L). The in situ rates were then adjusted for advective flow using the chloride measurements and following equation adapted from Lansdown et al. (2014):

$$\Delta^{adjx} N_{2t=i} (nM N_2) = \Delta^x N_{2t=i} + \left[\left(\frac{[Cl^-]_{t=i} - [Cl^-]_{tracer}}{[Cl^-]_{ambient} - [Cl^-]_{tracer}} \right) \right] \times \Delta^x N_{2(t=i)}.$$
(2)

 $\Delta^{\text{adjx}}N_2$ is the excess ²⁹N₂ or ³⁰N₂ in the sample at time *i*, corrected for any loss of ¹⁵N-N₂ or ¹⁵NO₃⁻ tracer via advective flow within the streambed; $\Delta^{\text{x}}N_{2\text{t=i}}$ is the excess ²⁹N₂ or ³⁰N₂ calculated from Eq. (1) and Cl⁻ is the concentration of chloride in either the tracer solution (tracer), ambient pore water (background), or sampling time after the injection of the tracer (t = *i*). Following this adjustment, the rate of each process was calculated using linear regression of ¹⁵N-produced against time.

To split total ¹⁵N-N₂ production into in situ potential rates of denitrification and anammox we used the ¹⁵N labelling of N₂O produced (after Trimmer et al. 2006):

$$r_{14}N_2O = \frac{\left(\frac{45}{N_2O}\right)_{sample} - \left(\frac{45}{N_2O}\right)_{ambient}}{2 \times \left[\left(\frac{46}{N_2O}\right)_{sample} - \left(\frac{46}{N_2O}\right)_{ambient}\right]},$$
(3)

where ${}^{45}N_20$ and ${}^{46}N_2O$ represent mass–charge ratios of 45 and 46, respectively, and $\sum N_2O$ is the sum of all three areas (${}^{44+45+46}N_2O$). We then compared the ${}^{15}N$ -labelling of the N₂O and N₂ produced in situ to calculate the contribution of anammox to total N₂ production as follows:

$$Q_{N_2O} = \frac{1}{1 + r_{14}N_2O},\tag{4}$$

contribution of anammox (%) = $\frac{2 - 2 \times \frac{Q_{N_2}}{Q_{N_2 o}}}{2 - \frac{Q_{N_2}}{Q_{N_2 o}}} \times 100,$ (5)

where Q_{N_2} was calculated in the same way as Q_{N_2O} but using the production of ²⁹N₂ and ³⁰N₂ for $r_{14}N_2$, rather than ⁴⁵N₂O and ⁴⁶N₂O, as was used for $r_{14}N_2O$. Subtracting the percentage contribution of anammox from total ¹⁵N₂ production gives the percentage contribution from denitrification.

The co-occurrence of DNRA and anammox could give rise to problems in calculating the relative contribution of each, due to the fact that DNRA will produce ¹⁵N-NH₄⁺ which could then be oxidised through anammox with ¹⁵NO₂⁻ (from the added ¹⁵NO₃⁻) to also produce ³⁰N₂ (A_{30}) in addition to that from denitrification (D_{30}). (see "Discussion" and Nicholls and Trimmer 2009).

Calculation residence times and Damköhler Numbers

We calculated water residence time from the conservative tracer data to asses if LWD-induced hydrological forcing affected the riverbed's ability to reduce nitrate. Further we calculated the nitrate reaction time which allowed calculation of the Damköhler number (DaN) for each individual push–pull measurement. This is a unit-less ratio between the water residence time, and nitrate reaction time. We calculated water residence time as follow:

water residence time
$$(h) = \left(\frac{1}{\Delta C l^{-} / C l_{MAX}^{-}}\right),$$
 (6)

whereby ΔCl^- is the rate of decay of chloride (calculated by linear regression), our conservative tracer, and Cl_{MAX} is the maximum chloride concentration, at the beginning of the experiment. We then calculated the reaction time of the ambient nitrate pool, given the measured rates of ¹⁵N-nitrate reduction as follows:

nitrate reaction time (h) =
$$\left(\frac{1}{\Delta NO_3^-/NO_{3ambient}^-}\right)$$
.
(7)

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Here, ΔNO_3^- is the rate of nitrate reduction (per litre of pore water) and NO_3^- ambient is the size of the nitrate pool in a litre of pore water. Thus, nitrate reaction time is the inverse of the nitrate turnover rate. Then, finally, we divided the water residence time by the nitrate reaction time as follows to give the unit-less Damköhler Number (DaN):

$$Damkohler Number = \frac{water \ residence \ time \ (h)}{nitrate \ reaction \ time \ (h)}.$$
(8)

When DaN < 1, the water is moving through the bed faster than the time taken for complete nitrate reduction (i.e. water residence time is shorter than the nitrate reaction time). Conversely, when DaN > 1, nitrate reduction exceeds water flux and so we would expect all of the nitrate present in the pore water to be completely reduced through denitrification, anammox and DNRA.

Statistical analyses

All statistical analyses were performed in the R software package (R Core Team 2015). Generalised mixed effects modelling was used to determine which physical and chemical drivers best explained the variation in measured nitrate reduction rate, which began by testing which of our random effects (month and piezometer) to include in the model. We first modelled the effect of each potential explanatory variable on nitrate reduction rate (log transformed) using a simple linear model. We then compared variations of each of these models in which we incorporated both month and piezometer location as a random effect on (i) the intercept only, (ii) the slope only and (iii) both the intercept and the slope (Bates et al. 2015). For each explanatory variable, we used a log-likelihood (ANOVA in R) approach to determine which model best explained variation in nitrate reduction rate (including or excluding random effects). Where there was no difference between the model with a random effect, and the simple linear model (ANOVA, p > 0.05) we concluded that the random effect did not significantly improve the fit of the model and it was therefore excluded from any further analysis. We then constructed a global linear mixed effects model which included temperature, ambient nitrate, ambient oxygen, depth and residence time as fixed effects. We also tested for covariance between our fixed effects and found no issues of multi-collinearity i.e. all five variables added power to the model [variable inflation factor < 4, "Car" package (Fox and Weisberg 2011)] and were therefore retained. Both month and piezometer were fitted as a random intercept. In addition, month was fitted as random effect on the slope of oxygen, whilst piezometer was fitted as random effect on the slope of ambient nitrate. All possible combinations of the global model terms were compared using the "dredge" function in the MuMIn package in R (Barton 2016) and we then used the small-sample corrected AIC (AICc) to determine the best fit model(s). Where the difference between a model's AICc and the lowest AICc (i.e. Δ AICc) was < 2, a set of best fit models was assumed and model averaging was used to identify the best predictor variables across the top candidate models and to determine their relative importance. Variable importance was calculated as the sum of the Akaike weights from all models in which they appear (Burnham and Anderson 2004).

Finally, to generate *F*-statistics and a significance level for each explanatory variable, we ran linear mixed effects models [R package nlme (Pinheiro et al. 2014)] for each variable, with the random effects included on the intercept, or slope and intercept (as above).

To test for differences in measured chemical variables and processes between locations in the LWD structures (< 1 m) and those away from the LWD (> 1 m), we performed a linear mixed effects model, with month and piezometer as random effects (intercept only), and we extracted the F and p values. The distance of 1 m from the LWD was chosen as a way of categorising the riverbed sampling positions as "in or very close to the LWD structures" or not. We acknowledge that the hydrological connectivity of the riverbed will vary across this reach, and while this may appear an arbitrary distance, our measures of vertical hydraulic gradient (see Fig. 2c) indicate that this is a reasonable distance to choose.



Fig. 2 Surface water **a** level above baseflow and **b** temperature, generated from 10 min interval data points, over the 12 month study period; **c** contour plots showing patterns in vertical hydraulic gradient across the network of 40 piezometers (depicted as black spots) spread along the study reach. The size and positioning of the three LWD structures are marked as brown lines and the colours represent strong positive head

Results

Seasonal site conditions

Surface water temperatures ranged from 2 to 20 °C and following a series of storm events, which increased water levels throughout the autumn and early winter (peak level 2.4 m above base flow), water levels dropped back towards base-flow, where they remained for spring and summer (Fig. 2). Water flowed over all three LWD structures when 1 m above base flow. Our sampling dates covered the entire range of water levels and temperatures measured in the stream (Fig. 2) which enabled us to test our hypotheses against a backdrop of natural variation.

Vertical hydraulic gradient (VHG) varied along the reach and the differences were most extreme in November and February (Fig. 2c) when the river level was high. Generally there was either no VHG or slightly gaining VHG around the top two LWD structures. But around the third and largest LWD structure (right of figures in 2c) the variation was extreme. In November when a flood forced flow over the downstream LWD and associated sandbar, there was intense (-25 cm), localised (< 1 m) negative head and this was seen again in July but on a smaller

(> 0.5 m, dark brown), through to neutral head (0 m, green) and negative head (0.5–0.8 m, lilac). Vertical grey bars on the first panels mark the five sampling periods with the first four when the vertical hydraulic gradient datasets were generated (i.e. main seasonal study), and the fifth grey bar marks when the additional work was carried out in October 2015 to increase resolution close to the LWD. (Color figure online)

scale. Conversely, in February and April we measured strongly gaining VHG around this same structure (Fig. 2c).

Pore water chemistry

Pore water depth profiles showed that the surface water chemical signature did not penetrate below 30 cm (and much shallower in some locations) and that there was no discernible groundwater influence (Fig. 3). The sharp decrease in oxygen and nitrate concentration over the top 10 cm of riverbed, and simultaneous increase in ammonium, showed that the conditions were ideal for nitrate reduction. The high concentrations of ammonium, iron (II), organic carbon and methane in the riverbed indicated a strongly reducing environment (Table 1). Statistical analyses found that pH (p < 0.0001), nitrate (p < 0.0001), (p < 0.012), temperature (p < 0.0001)oxygen decreased with depth, and ammonium (p < 0.003)and methane (p < 0.003) increased with depth, and this relationship interacted with sampling month for pH and temperature (see Supplementary Table 1 for detailed results of all tests). There was no linear change in the concentration of soluble reactive phosphorous, organic carbon or iron (II) with depth



Fig. 3 Depth distribution of dissolved **a** oxygen, **b** nitrate, **c** ammonium, **d** soluble reactive phosphorous and **e** pH in the surface water (shown at -20 cm as filled triangles) and pore water. Points from within 1 m of LWD are shown in filled circles and those more than 1 m from LWD are shown in

unfilled circles. Depth was calculated on each trip by measuring the distance from the sediment surface to the top of the piezometer bundle to account for any scour or deposition since installation

Variable	Surface water	Shallow sediment (0-30 cm)	Deep sediments (> 30 cm)
Dissolved oxygen (% sat.)	113.95	22.05	13.94
pH	6.97	6.68	6.46
Temperature (°C)	13.22	12.59	12.76
Methane (µM)	5.61	392.73	525.19
Iron II (µM)	3.16	177.68	178.80
Nitrite (µM)	1.34	0.76	0.63
Nitrate (µM)	189.39	35.25	10.39
Ammonium (µM)	7.23	122.71	157.95
Soluble reactive phosphorous (µM)	1.46	3.54	3.63
DOC (µM)	320.43	734.30	742.39

Data shown are mean averages including data over the whole year. Depths are true depths at each sampling time, i.e. seasonal change due to scour and deposition has been accounted for

into the bed; although, all were higher in the bed, relative to the overlying surface water throughout the year (Table 1).

Streambed nitrate reduction

Denitrification, anammox and DNRA were all detected at 108 discrete in situ locations in all seasons and denitrification was the most dominant form of nitrate reduction (Fig. 4). Total nitrate reduction ranged from 0 to $16 \ \mu M \ N \ h^{-1}$ and the average

contribution via denitrification, anammox and DNRA was 85, 10 and 5%, respectively. Below 60 cm into the bed, nitrate reducing activity was consistently low (< 1 µM N h⁻¹), but in shallower sediments there was substantial variation (Fig. 4). Total nitrate reduction decreased significantly with depth ($F_{1,128} = 104$, p < 0.0001), as did denitrification ($F_{1,128} = 4.2$, p = 0.04), but DNRA did not ($F_{1,128} = 2.7$, p = 0.104). There was no difference in the rate of denitrification ($F_{1,67} = 1.6$, p = 0.21) or of DNRA ($F_{1,36} = 1.3$,



Fig. 4 Total nitrate 1 (${}^{15}N_2$, ${}^{15}N_2O$ and ${}^{15}NH_4^+$) reduction rate measured in situ at 76 locations (repeated each season), plotted against depth; inset, ${}^{15}N$ reduction via the three different pathways plotted against depth

p = 0.27) between locations < 1 m from LWD and those > 1 m from LWD. However, despite high variation, anammox was on average 77% faster close to the wood (F_{1,67} = 4.2, p = 0.044). Similarly, as a percentage of total nitrate reduction, significantly more was transformed via anammox around the LWD (12% vs. 8%, F_{1,67} = 4.8, p = 0.03), whereas there was no difference in the percentage attributed to denitrification (F_{1,67} = 3.6, p = 0.06) or to DNRA (F_{1,36} = 0.32, p = 0.58) as a function off wood.

We also used sediment slurries to measure the potential for denitrification and anammox in 35 surface sediment samples under controlled laboratory conditions. Total N₂ production ranged from 0.9 nmol $g^{-1}h^{-1}$ to 11.0 nmol $g^{-1}h^{-1}$, and averaged 2.7 nmol $g^{-1}h^{-1}$. The percentage contribution from anammox ranged from 1 to 20% and averaged 9% with denitrification contributing 91% on average. DNRA was not quantified in these samples.

The effect of ambient temperature on nitrate reduction

Over the year, the pore water temperature ranged from 5 to 20 °C (average 12 °C) and, given the expected influence of temperature on metabolism, it was important to quantify its influence on our in situ estimates of nitrate reduction. Displaying the data on an Arrhenius plot (Fig. 5a) reveals a subtle temperature effect on total nitrate reduction (0.24 eV,

 $F_{1,285} = 4.1$, p = 0.045). When broken down into the individual routes of nitrate reduction we found that both anammox (0.48 eV, $F_{1,212} = 13.1$, p < 0.001) and DNRA (0.56 eV, $F_{1,235} = 12.0$, p < 0.001) activity depended on temperature while denitrification did not ($F_{1,284} = 2.3$, p = 0.13, Fig. 4b). The variation around the regression lines shows that other environmental variables are causing differences in the nitrate reduction rate and temperature alone cannot explain the intra- or inter-seasonal variation.

Exploring the controls on nitrate reduction rate and potential effect of LWD

Nitrate reduction in situ was limited by short water residence times, and the peak in activity coincided with mid-range water residence times (~ 1 h, Fig. 6a). Residence time was significantly shorter around the LWD, relative to locations > 1 m from the LWD (Fig. 6b, Table 2, $F_{1,67} = 5.1$, p = 0.027), as indicated by faster rates of chloride decay following the tracer injection ($F_{1,67} = 8.5$, p = 0.005) which we attribute to greater hyporheic exchange. Around the LWD, the (surface) water depth was almost 3 times shallower than the rest of the reach, and methane concentrations were 11% lower (Table 2), adding weight to the idea of greater surface water downwelling closer to the wood where sand accumulates (greater bed heterogeneity). The VHG plots show this



Fig. 5 The temperature dependency of nitrate reduction rates. a Arrhenius plot with centred temperature (where 0 is the mean average temperature) versus the natural logarithm of the three nitrate reduction processes. Unfilled circles are denitrification, red circles are anammox and blue triangles are DNRA. The slope of the regression line gives the activation energy. The black line is for total nitrate reduction, the red is for anammox,

hydraulic forcing is extremely localised around the LWD.

Nitrate reduction rate was highly variable when ambient nitrate was $< 40 \mu$ M, but above this threshold, nitrate reduction was suppressed (Fig. 6c). This high nitrate is indicative of strong connectivity with the surface water and suggests redox conditions do not permit nitrate reduction. Further, there was 60% more nitrate in the pore water around the wood (Fig. 6d, Table 2), which also suggested greater surface water inputs. The non-linear, inverse correlation between ambient nitrate and nitrate reduction was much stronger in the sediment slurries in the laboratory (see inset, Fig. 6b). However, there was no interaction with this relationship and proximity to LWD $(F_{1,31} = 1.2, p = 0.29)$, nor was there any difference in the nitrate reduction rates measured in the laboratory between sediments taken from around the LWD and those taken from further away ($F_{1,33} = 0.04$, p = 0.84).

Given the measured reduction rate and the ambient concentration, we calculated nitrate reaction time and found it was slower closer to the LWD (110 h vs. 29 h, $F_{1,67} = 4.1, p = 0.047$). Damköhler numbers collapse water residence time and nitrate reaction time into a

and the blue for DNRA. No line is shown for denitrification as this was not a significant regression. **b** Bar chart showing the activation energies of the total nitrate reduction and the individual processes, with error bars showing the error of the linear regression and *p*-values with asterisks to denote the level of significance (* < 0.05, ** < 0.005, *** < 0.0005). (Color figure online)

unit-less ratio, and Fig. 6e shows this data on a scatter plot. Although there was an inverse relationship between the two parameters (shorter water residence times associated with longer nitrate reaction times), there was no difference as a function of wood (Table 2). Similarly, there was no difference in the overall rate of nitrate reduction as a function of proximity to LWD (Table 2, Fig. 6f).

We constructed a global linear mixed-effects model to identify which variables best explained variation in the in situ rate of nitrate reduction and to determine their relative importance. The best fit model explained 44% of the variation (adjusted- R^2) in nitrate reduction rates (log transformed), and included depth, nitrate concentration and water residence time, as fixed variables, with month (repeat measures) and location within the reach (piezometer) included as random effects (see "Methods"). Three other candidate models, which displayed similar explanatory power included either temperature, oxygen or both, whilst retaining nitrate concentration, depth and water residence time, suggesting that these were the most important variables for explaining the observed variation in nitrate reduction rate (Supplementary Table 2). Individually ranked by explanatory power,



Fig. 6 a The rate of nitrate as a function of water residence time; **b** a boxplot showing the difference in water residence as a function of proximity to LWD; **c** nitrate reduction rate as a function of ambient nitrate concentration (main panel shows in situ push-pull measures (μ M h⁻¹) and inset panel shows potential measures in the laboratory (nmol g⁻¹ h⁻¹); **d** boxplot showing the difference in ambient nitrate with LWD proximity; **e** comparison of water residence time and nitrate reaction time

depth ($F_{1,128} = 104$, p < 0.0001) explained the most variation, followed by oxygen ($F_{1,128} = 5$, p = 0.029), temperature ($F_{1,128} = 5$, p = 0.035), water residence time ($F_{1,128} = 4$, p = 0.063) and finally ambient nitrate ($F_{1,128} = 2$, p = 0.14).

Mapping nitrate reduction over a woody streambed

Finally, we mapped our nitrate reducing activity data spatially in relation to the position of the LWD. The variation in water level (see Fig. 2), indicated that the hyporheic exchange flow likely varied across the year; we therefore mapped and analysed each season separately to tease out any effect of season on nitrate reduction in the shallow sediments (top 20 cm). We

which form the Damköhler number; **f** boxplot showing the comparative spread of in situ nitrate reduction rate. Filled circles or boxes are always points in the riverbed < 1 m from one of the LWD structures and those > 1 m from the LWD structures are unfilled (white). Where the data are significantly different (p < 0.05), considering random effects of date and repeat measures, an asterisk is placed above the boxes

overlaid the nitrate reduction data on a channel map, with the size and the orientation of all three LWD structures indicated, to examine the interaction between the three (see Fig. 7 and Supplementary Fig. S2).

In no individual seasons was nitrate reduction rate significantly faster around the LWD (Supplementary Fig. S2). However, in February, the concentration of pore water nitrate ($F_{1,28} = 6.1$, p = 0.02) was 188% higher around the LWD, and residence time was 39% shorter ($F_{1,28} = 5.7$, p = 0.02), indicating enhanced hyporheic exchange. However this difference was not significant in any other month. Although average nitrate concentration and nitrate reduction rate was generally higher around the LWD, due to small sample

Explanatory variable	Average < 1 m from LWD	Average > 1 m from LWD	Model output
Dissolved oxygen (µM)	36.6	31.3	$F_{(1,67)} = 2.8, p = 0.097$
pH	6.6	6.6	$F_{(1,67)} = 0.02, p = 0.89$
Temperature (°C)	12.2	12.0	$F_{(1,67)} = 0.0006, p = 0.97$
Nitrate (µM)	18.9	11.4	$F_{(1,67)} = 7.9, p = 0.007$
Ammonium (µM)	156.6	164.3	$F_{(1,67)} = 2.0, p = 0.16$
Phosphate (µM)	3.1	3.2	$F_{(1,67)} = 0.46, p = 0.50$
Methane (µM)	467.6	522.3	$F_{(1,67)} = 4.1, p = 0.048$
Organic carbon (µM)	817	1025	$F_{(1,67)} = 2.3, p = 0.14$
Water depth (cm)	14.6	40.6	$F_{(1,67)} = 76.4, p < 0.0001$
Residence time (h)	0.97	1.10	$F_{(1,67)} = 4.8, p = 0.032$
Total nitrate reduction $(\mu M h^{-1})$	2.24	1.84	$F_{(1,67)} = 0.01, p = 0.94$
Denitrification ($\mu M h^{-1}$)	2.08	1.75	$F_{(1,67)} = 1.6, p = 0.21$
Anammox $(\mu M h^{-1})$	0.13	0.08	$F_{(1,67)} = 4.2, p = 0.04$
DNRA (nM h ⁻¹)	34.7	20.6	$F_{(1,47)} = 3.7, p = 0.061$
Damköhler Number	0.48	0.50	$F_{(1,77)} = 2.7, p = 0.107$

Table 2 Mean averages concentrations for riverbed locations within 1 m of LWD and > 1 m from LWD

Statistical model output for testing whether measured chemistry and processes differ as a function of proximity to a LWD structure. We used linear mixed effects models and fitted month, piezometer location and depth as random effects and where necessary the data were log-transformed. Where the difference is significant (p < 0.05) *p*-values are in bold



Fig. 7 Bubble plot showing the magnitude of measured nitrate reduction in the top 15 cm across the study reach in autumn (November 2014 and October 2015). Bubble size is proportional to nitrate reduction (μ M h⁻¹), the relative size and orientation of large woody debris is depicted by brown cylinders and the direction of flow is indicated by the blue arrows. This plot is overlaid on top of a bathymetric contour plot. Inset (top) bar-

size particularly close to the LWD (n = 8-11), and the bi-modal spread of data (see Fig. 7) this difference was rarely statistically different.

charts to show the average nitrate reduction and ambient nitrate concentration in these shallow pore waters. Inset (right) scatterplots show the relationships between nitrate reduction rates, ambient nitrate concentration and residence time of the shallow pore water, both within 1 m of the wood (black symbols) and further away (white symbols)

The October dataset was acquired to increase our sample size close to the LWD and pooling these data with the November data from the previous autumn gave us more statistical power (Fig. 7). With these pooled data, pore water nitrate concentrations were higher (137%, $F_{1,71} = 5.6$, p = 0.021), residence times were shorter (32%, $F_{1,70} = 8.6$, p = 0.005), and nitrate reduction rates were faster (98%, $F_{1,69} = 6.3$, p = 0.014), around the LWD, than in non-woody streambed locations.

Discussion

To the best of our knowledge, this study is the first to simultaneously quantify in situ the effects of LWD on denitrification, anammox and DNRA activity in streambed sediments. By measuring a whole suite of physiochemical variables in the background pore water before each of our isotope-tracer experiments, we were able to align the measures of nitrate reduction with a detailed chemical picture of the in situ streambed pore water matrix to help address our hypotheses.

Quantifying nitrate reduction in a sandy streambed and net organic mineralisation

The pore water chemistry data confirmed that streambed pore water conditions at the field site were ideal for nitrate reduction. Low pore water oxygen and nitrate, coupled with high ammonium were found to correlate with high rates of nitrate reduction as found in other streambeds (Krause et al. 2013; Lansdown et al. 2014; Zarnetske et al. 2011) and where we know there is hyporheic exchange, low pore water nitrate (relative to surface water), indicates that the bed is a likely a nitrate sink. The total rate of nitrate reduction recorded in our study was up to ten times higher than that which Lansdown et al. (2014) measured in the River Leith, a sandstone river with larger grain size than at the Hammer Stream. This is largely because the surface water-pore water gradients in oxygen and nitrate are much stronger in the more reduced, lowpermeability fine-sand streambed sediments of the Hammer Stream (this study), compared to the far more permeable gravel/cobbled substrate at the Leith.

As hypothesised, denitrification was responsible for the bulk of in situ nitrate reduction in the Hammer Stream (average 85%), although anammox and DNRA were also quantified, and the calculated contribution of anammox was consistent between the in situ ($\sim 10\%$) 367

and laboratory, sediment slurry experiments (~ 9%). Anammox has only recently been reported in streambed sediments (Cheng et al. 2016; Han and Li 2016; Kim et al. 2016; Lansdown et al. 2016), largely due to the limited attempts to quantify it relative to the focus on denitrification. The similarity of results between in situ experiments and controlled laboratory experiments shows that the conditions in situ are close to optimal for anammox and that the push–pull method works well. This ~ 10% contribution of anammox to total nitrate reduction falls within the range measured across 9 other English lowland rivers (0–58%) and specifically, other work in permeable, sandy riverbeds also averaged 9% (Lansdown et al. 2016).

DNRA is similarly understudied in freshwater sediments principally because the techniques employed on many occasions in the past were either not capable of quantifying it directly (e.g. acetylene block) or were not sensitive enough (e.g. whole stream ¹⁵N additions) or perhaps because DNRA recycles reactive nitrogen (into ammonium) rather than removing it from the system it has not been focus of previous work (Burgin and Hamilton 2007). DNRA contributed $\sim 5\%$ of the in situ total nitrate reduction in our study site (locally 0-63%). Studies which only report the bulk reduction in nitrate concentration (i.e. do not specifically quantify DNRA) are likely to overestimate true inorganic-nitrogen removal from the system. The co-occurrence of anammox and DNRA can complicate the calculations as the latter could be providing ¹⁵N-labelled ammonium as a substrate for the former (Nicholls and Trimmer 2009). However, the ambient ammonium pool is so large (average 161 μ M) that even the highest rate of DNRA measured $(371 \text{ nM N h}^{-1})$ only contributed 0.2% to this pool per hour and it is therefore unlikely to have significantly altered our anammox calculations.

Each in situ injection contained the same amount of nitrate, so the observed patterns reveal true differences in the potential for each process should nitrate penetrate the streambed. As these measurements were performed in situ, it is important to remember that the results of this study are influenced by mixing with the ambient pore water and the hydrology (i.e. water residence time). Further, the injected ¹⁵N-nitrate was between 2 and 1300 times more concentrated than the ambient ¹⁴N-nitrate pool, depending on location. Therefore, we are reporting in situ potentials for nitrate reduction as a function of large woody debris,

which could be higher than the true rate under ambient nitrate concentration.

Our pore water data indicate intense mineralisation of organic matter within the streambed through oxygen and nitrate, in the upper layers, and then through iron and, eventually, methanogenesis deeper down (Fig. 3, Table 1). Indeed, if we assume steadystate pore water profiles and Redfield ratios (106C:16 N:1P), approximately 50% of organic matter mineralisation terminated in methane e.g. mean CH₄ (507 µM)/mean NH_4^+ $(161 \ \mu M) \times 6.6$ (C:N) = \sim 50%. In more permeable, sandy-gravels $[\sim 10^{-10} \text{ to } 10^{-9} \text{ m}^2 \text{ (Huettel and Rusch 2000)}]$ ammonium can accumulate at up to $\sim 3 \ \mu M$ to $9 \ \mu M$ (Lansdown et al. 2014; Zarnetske et al. 2011), whereas here we measured appreciably more at up to 161 μ M, which is more in line with similar, fine-sand sediments (Lansdown et al. 2016). With a median grain size of 258 µm, our fine-sand sediments have a lower permeability ($\sim 10^{-11} \text{ m}^2$, Huettel and Rusch 2000) than sandy-gravels and solute exchange would be tending towards diffusion and, as a result, we see appreciable net accumulation of ammonium, methane and SRP. Despite this intense mineralisation, SRP was approximately half that expected for the concentration of ammonium. Again, assuming Redfield ratios (16:1), at 161 μ M ammonium we would expect ~ 10 μ M SRP but we measured far less at $\sim 4 \,\mu$ M. Given that the sediments were rich in iron II (Table 1) some soluble phosphorus would have been precipitated with iron III complexes in the upper, oxidised layers (Froelich 1988; Sanders et al. 1997).

The influence of LWD on nitrate reduction

As highlighted by Krause et al. (2014), our mechanistic, system level understanding of the effectiveness of LWD in altering hydrological, geomorphological, thermal and biogeochemical processes in fine sediment dominated lowland streams is limited. This study has shown that the slower surface water velocities experienced in the observed lowland conditions reduce the impact of LWD on hydrodynamic forcing of surface water into the streambed in most instances, except where higher flow (e.g. February sampling period; Fig. 2c) results in increased hydraulic variation. This lack of LWD-induced forcing of surface water into the streambed and hyporheic zone, which facilitate longer residence times and exposure of nitrate-rich sources to denitrification hots pots, limits the influence of LWD in enhancing nitrate reduction.

We found that the presence of LWD only had a direct influence on the rate of nitrate reduction in autumn, when river discharge was high. Nitrate concentrations were highest at locations around LWD, particularly during the autumn high flow event, indicating increased down-welling of nitrate-rich surface water into the streambed at locations < 1 maway from LWD at high flow. This increased hyporheic exchange is likely due to enhanced surface water infiltration due to wood-induced bed-form complexity, as has been observed experimentally and in the field (Birgand et al. 2007; Elliott and Brooks 1997; Kail 2003; Klaar et al. 2011) and has been shown to be particularly effective at high discharge (Munz et al. 2011; Packman and Salehin 2003). Krause et al. (2014) predicted hyporheic residence times would be longer around LWD, due to fine sediment trapping around the wood structures. However, LWD didn't have such impact on the already fine sand dominated streambed characteristics at the field site, hence the opposite has been observed in our study; residence times were shorter in shallow sediments in close proximity to LWD, especially during high flow.

Previous research in nutrient poor upland streams revealed that hyporheic residence time (as a function of hyporheic exchange flow paths) was the dominant control of respiration and denitrification (Pinay et al. 1994; Zarnetske et al. 2011), where nitrate would be reduced when flow paths are long enough to ensure that high oxygen levels delivered by the surface water are depleted and sufficient organic carbon as an electron donor is still present to facilitate heterotrophic denitrification. For the lowland conditions observed in this study, the dominant fine grain size (average reach D50 = 0.28 mm), organic carbon rich streambed sediments and hypoxic pore-waters at the Hammer Stream caused immediate reduction of surface water born nitrate once it penetrated the streambed, meaning that surface water-born oxygen must have been respired in the top millimetres-centimetres of the streambed sediments.

Our results indicate that in lowland streams, simply allowing LWD to be recruited naturally may not provide significant increase in streambed roughness and hyporheic exchange flow to facilitate enhanced nitrate attenuation. Engineered log-jams and instream wood restoration projects which are able to manipulate the size and complexity of LWD structures may assist in enhancing nitrate attenuation by increasing hyporheic exchange flow and residence times by increasing the hydrogeomorphic impact of LWD on the stream channel (Dixon 2016; Gippel 1995; Gippel et al. 1996; Hughes et al. 2008). However, as highlighted by (Craig et al. 2008), restoration efforts to enhance the ability of large streams (> 3rd order) to attenuate reactive nitrogen is difficult, and restoration efforts should be focused on smaller streams.

LWD is expected to have more substantial impacts on streambed nutrient spiralling in streambed environments that are not as rich in organic carbon and as strongly anoxic as in the investigated conditions of this study. In streams with higher pore water oxygen, the addition of LWD and associated fine sediment trapping may have a more pronounced effect. Additionally, the installation of engineered log jams designed to withstand high flow events and movement (particularly in highly mobile sandy streambeds such as this) which are embedded into the streambed and banks are likely to enhance hyporheic exchange flows and residence time at a range of flows, resulting in enhanced seasonal nitrate reduction. We therefore recommend that future wood restoration in lowland streams considers the physical manipulation of wood structures exceeding the dimensions of natural accumulations in this study to ensure that structures are designed in a manner which ensures hyporheic exchange flow and advective pumping are maximised, and that LWD is installed at locations where organic carbon may be limited.

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