

This is a repository copy of *Evaluation of classical precipitation descriptions for y*" (Ni3Nb–D022) in Ni-base superalloys.

White Rose Research Online URL for this paper: http://eprints.whiterose.ac.uk/117009/

Version: Accepted Version

# Article:

Moore, I.J., Burke, M.G., Nuhfer, N.T. et al. (1 more author) (2017) Evaluation of classical precipitation descriptions for  $\gamma''$ (Ni3Nb–D022) in Ni-base superalloys. Journal of Materials Science , 52 (14). pp. 8665-8680. ISSN 0022-2461

https://doi.org/10.1007/s10853-017-1091-9

# Reuse

Items deposited in White Rose Research Online are protected by copyright, with all rights reserved unless indicated otherwise. They may be downloaded and/or printed for private study, or other acts as permitted by national copyright laws. The publisher or other rights holders may allow further reproduction and re-use of the full text version. This is indicated by the licence information on the White Rose Research Online record for the item.

# Takedown

If you consider content in White Rose Research Online to be in breach of UK law, please notify us by emailing eprints@whiterose.ac.uk including the URL of the record and the reason for the withdrawal request.



eprints@whiterose.ac.uk https://eprints.whiterose.ac.uk/

# Evaluation of classical precipitation descriptions for $\gamma''$ (Ni<sub>3</sub>Nb-D0<sub>22</sub>) in Ni-base Superalloys

I. J. Moore  $\cdot$  M. G. Burke  $\cdot$  N. T. Nuhfer  $\cdot$  E. J. Palmiere

Received: 1 February 2017 / Accepted: 13 April 2017

Abstract The growth/coarsening kinetics of  $\gamma''$  (Ni<sub>3</sub>Nb-D0<sub>22</sub>) precipitates have been found by numerous researchers to show an apparent correspondence with the classical (Ostwald-ripening) equation outlined by Lifshitz, Slyozov and (separately) Wagner for a diffusion controlled regime. Nevertheless, a significant disparity between the actual precipitate size distribution shape

and that predicted by LSW is frequently observed in the interpretation of these results, the origin of which is unclear. Analysis of the literature indicates one likely cause for this deviation from LSW for  $\gamma''$  precipitates is the

<sup>15</sup> "encounter" phenomenon described by Davies *et al.* [6] that is associated with secondary phases comprising a high volume fraction. Consequently, the distributions of both  $\gamma''$  precipitates described in the literature (Alloy 718) and measured in this research in Alloy 625 are analysed through employing the Lifshitz-Slyozov-Encounter-Modified (LSEM) formulation (created by Davies

*et al.*). The results of the LSEM analysis show good far better agreement than LSW with experimental distributions after the application of a necessary correction for what is termed in this research as "directional encounter".

I. J. Moore

5

10

Department of Materials Science and Engineering, The University of Sheffield, Sir Robert Hadfield Building, Mappin Street, Sheffield, S1 3JD, UK. Tel.: +44 114 222 5978 Fax: +44 114 222 5943

E-mail: imoore1@sheffield.ac.uk

M. G. Burke

Materials Performance Centre, The University of Manchester, The Mill, Sackville Street, Manchester, M13 9PL, UK.

N. T. Nuhfer

Department of Materials Science and Engineering, Carnegie-Mellon University, Pittsburgh, PA 15213, USA.

E. J. Palmiere

Department of Materials Science and Engineering, The University of Sheffield, Sir Robert Hadfield Building, Mappin Street, Sheffield, S1 3JD, UK.

Moreover, the activation energy for  $\gamma''$  coarsening in Alloy 625 shows conformity with literature data once the effect of heterogeneous (on dislocations) precipitate nucleation at higher temperatures is accounted for.

Keywords LSEM  $\cdot$  Precipitation Kinetics  $\cdot$  Coarsening  $\cdot$  Nickel base alloys  $\cdot$   $\gamma''$   $\cdot$  Activation energy

## **1** Introduction

Since its inception in 1961, the cube root law developed on either side of the iron curtain by Lifshitz, Slyozov [13] and Wagner [29] (LSW) to quantitatively describe the phenomenon of spherical particle coarsening (Ostwald ripening), has been successfully applied to several systems [9]. Furthermore, using an adaptation defined by Boyd *et al.* [2] a decade later, the LSW approach has been shown to yield an apparently good agreement with experimental measure-

<sup>35</sup> ments of the change in size of non-spherical particles such as  $\gamma''$  (Ni<sub>3</sub>Nb-D0<sub>22</sub>) in Ni-base alloys [7, 11, 28, 8, 23, 4, 30, 31]. Despite this apparent success, however, closer scrutiny of the results to which the latter formalism has been applied (such a coarsening of  $\theta''$  precipitates in Al-Cu alloys by Boyd *et al.* [2] in the derivation paper) reveals a marked discrepancy between the real and 40 calculated precipitate size distributions.

Considering the distribution of precipitates like  $\gamma''$  particles in Ni-base alloys and  $\theta''$  particles in Al-Cu, an immediate source for their distributions deviating from LSW can be identified as their high volume fraction *viz.* a small fraction (defined such that particle spacing >> particle dimensions) is

- <sup>45</sup> necessitated by the LSW mechanism. To this end, it is clear that a more accurate description of the coarsening behaviour of these spheroidal precipitates can only be achieved through the use of one of the many different adaptations to the LSW formalism to describe the evolution of precipitates comprising a high volume fraction [1].
- <sup>50</sup> Amongst the afore alluded to descriptions, almost all are based principally on approximate solutions/modifications to the solute diffusion description in LSW and, therefore, often require assumptions which are seemingly contradicted by experimental observations. In contrast, the Lifshitz-Slyozov-Encounter-Modified (LSEM) theory of Davies *et al.* [6] is physically sound
- <sup>55</sup> owing to its derivation being predicated on the mechanism of precipitate "encounter"; the broadening of the precipitate distribution from the classical LSW shape occurs by the coalescence of precipitates whose diffusion fields have overlapped *i.e.* they are said to have "encountered" one another. Such behaviour has been observed for  $\gamma''$  precipitates in a number of studies [11, 23, 26].
- The governing precipitate growth/coarsening equation originally composed by Davies *et al.* is strictly applicable only to spherical precipitates but, following the work of Boyd *et al.* [2] (in their original adaptation to the LSW model), an LSEM cube root law defining the growth of spheroidal particles can be composed according to Equation 1 where,  $\bar{L}_{\rm M}$  is the average major axis of ellipsoidal particles initially (0) and at time *t*,  $X^e$  is the equilibrium

solute concentration in the matrix,  $\zeta$  is the precipitate-matrix interfacial energy,  $V_{\rm m}$  is the molar volume of the precipitate,  $\alpha$  is the precipitate aspect ratio (minor axis length:major axis length), R is the ideal gas constant, D is the diffusion coefficient of the solute atoms in the matrix, T is the absolute temperature, and  $f_{\rm LSEM}$  and  $C_{\rm LSEM}$  are a function and system constant, re-

<sup>70</sup> temperature, and  $f_{\text{LSEM}}$  and  $C_{\text{LSEM}}$  are a function and system constant, respectively, defined by Davies *et al.* [6]. As a result, it is evident that a more appropriate LSW description of the evolution of the size distribution for high volume fraction ellipsoidal precipitates, accounting for "encounter", should be possible through LSEM.

$$\bar{L}_{\rm M}^3(t) - \bar{L}_{\rm M}^3(0) = \frac{32D\zeta V_{\rm m} X_{\gamma}^{\rm e} t}{\alpha \pi R T} \frac{f_{\rm LSEM}(\bar{L}_{\rm M}, L_{\rm M}^*)^3}{C_{\rm LSEM}}$$
(1)

- <sup>75</sup> Owing to the importance of the precipitate population in determining the mechanical properties of the superalloys containing  $\gamma''$  [16, 15], and in light of the aforementioned likely increase in the accuracy of the replicated size distribution that should result from adopting the LSEM theory *cf.* LSW, the principle aim of this work was to assess the evolution of  $\gamma''$  populations with respect to LSEM. In the absence of any adaptation being made to the LSEM
- theory, a verbatim repeat of its specific intricacies as discussed by Davies et al. [6] is avoided.

# 2 Literature Alloy 718 $\gamma^{\prime\prime}$ distributions

The study of  $\gamma''$  precipitate evolution with respect to LSW evolution kinetics has been most commonly investigated in Alloy 718, but only a handful of relevant studies report on the precipitate size distribution (PSD) [28, 11, 8]. As a result, given that analysis of the PSD shape constituted the raison d'être of this investigation it was purely the analysis of Han *et al.* [11], Sundararaman *et al.* [28] and Dong *et al.* [8] that formed the basis of the application of the LSEM theory to previously published  $\gamma''$  precipitation studies here.

2.1 Volume Fraction

As presented in Figure 1, both the LSEM probability density and  $C_{\text{LSEM}}$  depend crucially on the precipitate volume fraction Q. Unfortunately, however, neither Han *et al.* [11], Sundararaman *et al.* [28] nor Dong *et al.* [8] provide a direct quantification of Q in their studies. In general, this eventuality would present a significant problem as the separate calculation of Q would only be possible through extensive precipitation kinetics computations but in the case of high ( $\geq 10\%$ ) volume fraction precipitates such as  $\gamma''$ , the sensitivity of the LSEM probability density (Figure 1a) is such that an approximation is instead

<sup>100</sup> reasonable. Explicitly, the precipitate volume fraction can be set equivalent to one in which all of the niobium is contained within  $\gamma''$  precipitates. Consequently, assuming a stoichiometric Ni<sub>3</sub>Nb composition, the value of Q for  $\gamma''$  in each Alloy can be calculated from their respective compositions (at%) listed in Table 1 such that  $Q = 4 \times Nb(at\%)$ .



Fig. 1: a) LSEM distributions corresponding to different precipitate volume fractions Q where  $\bar{\rho}$  is average value of a precipitate size dimension. b)  $C_{\text{LSEM}}$  behaviour with Q calculated by Davies *et al.* [6].

Table 1: Compositions (at%) of the Alloy 718 samples reported in the cited studies. The indexes \* and + respectively signify the quantity is calculated from balance or was not indicated.

Study	Ni	Cr	Fe	Mo	Nb	C	Mn	Si	S	Al	Ti	В	Cu
Dong [8]	$50.65^{*}$	21.06	19.89	1.82	2.93	0.10	0+	0+	0+	2.15	1.39	0.02	$0^{+}$
Han [11]	$51.62^{*}$	20.26	19.90	1.85	3.07	0.14	0.20	0.62	0.01	1.11	1.17	$0^{+}$	0.04
Sundararaman [28]	$51.78^{*}$	20.39	18.66	1.75	3.73	0.19	0.22	0.60	0+	2.14	0.54	$0^{+}$	$0^{+}$

# 105 2.1.1 LSEM Results

The LSEM and LSW distribution profiles computed for the three Alloy 718 studies of Han *et al.* [11], Sundararaman *et al.* [28] and Dong *et al.* [8], as well

as the originally published PSDs, are presented in Figure  $2^1$  In each instance it is evident that the LSEM curves bare a much closer resemblance (*cf. LSW*) to the experimental data (particularly the measurements by Dong *et al.* [8] for precipitate populations existing after 100 hours at 1073K), however there

still remains a marked discrepancy. As a result of this outcome, whilst the LSEM description can be concluded as a far more appropriate description for  $\gamma''$  precipitation in Alloy 718, it is clear that additional modifications to the application of the theory are required.

 $<sup>^1~</sup>$  The data originally published by Dong et al. [8] were altered to account for a clear error in their values for  $\bar{L}_{\rm M}.$ 



Fig. 2: Original precipitate size distributions measured by a) Han *et al.* [11], b) Dong *et al.* [8] and c) Sundararaman *et al.* [28] in material (compositions in Table 1) aged at for the labelled conditions. LSW and LSEM distributions are also illustrated, with the corresponding Q values for the latter indicated. Owing to the specific focus on the shape of the precipitate size distributions, for ease of comparison each has been normalised to the same relative classified magnitude meaning their specific values are arbitrary.

# 2.2 Correction to LSEM for $\gamma^{\prime\prime}$ "Directional Encounter"

As depicted most strikingly in the literature by Suave *et al.* [24] (image reproduced for ease of reference in Figure 3), rather than the isotropic agglomeration behaviour mathematically described by Davies *et al.*,  $\gamma''$  precipitates are observed to coalesce though a directional mechanism (in that they seemingly almost always coalesce through conjunction along their major axis) referred to here on as "directional encounter".



Fig. 3: Secondary electron (SE) image obtained by Suave *et al.* [24] of extensive, large scale  $\gamma''$  in a sample of Alloy 625. A tendency for precipitates to agglomerate along their major axes and for the number of agglomerated precipitates to increase with resolvable precipitate size is clearly discernible. The results of Han *et al.* [11] indicates that this is not related to imaging or etching effects.

125

130

120

Considering the variables governing precipitate evolution it is clear that, given the continuity of the material condition, the principle cause of "directional encounter" can only be assigned to the varying misfit strains surrounding the precipitates:  $\gamma''$  has been shown to possesses a high coherency with the precipitate matrix, however its body-centre-tetragonal (BCT) structure leads to a significant variation in the misfit strain surrounding the precipitate [16]. Furthermore, as demonstrated from the results of Slama *et al.* presented in Table 2, the level of misfit strain (calculated according to the strain tensor defined by Cozar *et al.* [5]) along the two principle axes of a precipitate is

defined by Cozar *et al.* [5]) along the two principle axes of a precipitate is observed to follow opposite trends as the shape change discussed previously proceeds. Consequently, with smaller strain posing a lower energy barrier to precipitate "encounter", it is evident that coalescing precipitates will tend to not only join along their major axis but will do this with increasing propensity as they grow owing to the lower, and continually decreasing value, of the ratio  $\epsilon_{11}/\epsilon_{33}$ .

Table 2: Average values of the aspect ratio  $(\bar{\alpha})$  and the FCC-BCT strain tensor components  $\epsilon_{11}$  and  $\epsilon_{33}$  for  $\gamma''$  precipitates in Alloy 718 as measured by Slama *et al.* [23]. The directions of tensor components with respect to the precipitate are shown in Figure 4.

		Temperature (K)								
			953	_	1023					
		$\epsilon_{11}$	$\epsilon_{33}$	$\bar{\alpha}$	$\epsilon_{11}$	$\epsilon_{33}$	$\bar{\alpha}$			
	4	0.0080	0.0303	_	0.0089	0.0296	0.300			
Ageing Time (hours)	50	0.0042	0.0323	0.333	0.0036	0.0321	0.187			
	98	0.0033	0.0377	0.181	0.0030	0.0331	0.178			



Fig. 4: Directions of the strain tensor components  $\epsilon_{11}$  and  $\epsilon_{33}$  with respect to the oblate spheroidal shape of  $\gamma''$  precipitates.

In light of the aforementioned origin for "directional encounter", it is obvious that the phenomenon will principally act to inflate the values of  $L_{\rm M}$  and, thus, that application of LSEM to  $\gamma''$  precipitates would be more appropriately made to experimental curves where the effect of increased "encounter" probability with precipitate size has been removed. Accordingly, harnessing the fact that the enhancement probability correlates directly to both the relative and absolute values of  $\epsilon_{11}$  and  $\epsilon_{33}$ , an evaluation of its behaviour with  $\alpha$ 

145

can be determined through application of the results of Slama *et al.* at 1023K in Figure 5. Specifically, there are three important facts: 1)  $\epsilon_{11}$  evolves apparently linearly with respect to  $\alpha$ , 2) the evolution of the ratio  $\epsilon_{11}$  :  $\epsilon_{33}$  is also

150

155

well approximated by a linear relationship with respect to  $\alpha$  and 3) the probability of any two precipitates agglomerating and the  $\alpha$  of the particle they form are proportional to the average of their aspect ratios, the inflation of a specific precipitate size in the distribution can be quantified as proportional to  $\alpha^{-1}$  by the mechanism outlined previously. Consequently, in view of the exact relationship being unknown, the conversion of the original  $L_{\rm M}$  distribution to one compatible with LSEM can be performed to a reasonable first approximation through the multiplication of  $L_{\rm M}$  by the magnitude of  $\alpha(L_{\rm M})$ *i.e.*  $f(L_{\rm M}) \rightarrow f(L_{\rm M} \times \alpha(L_{\rm M}))$ .



Fig. 5: Evolution of the average value of the strain tensor components  $\epsilon_{11}$  and  $\epsilon_{33}$ , and separately their ratio, with the average aspect ratio of  $\gamma''$  precipitates measured by Slama *et al.* [23] in Alloy 718 aged at 1023K. Linear fits to  $\epsilon_{11}$  and the ratio are also indicated.

#### 2.3 Shape change

160

Fundamental to the previously described mechanism accounting for "directional encounter" is the evaluation of the function  $\alpha(L_{\rm M})$ . In this regard, the shape evolution behaviour of  $\gamma''$  analysed most comprehensively in the literature by Devaux *et al.* [7], through the comparison of their own results with others published in the literature (presented in 6), is utilised. Specifically, following the hyperbolic relationship demonstrated for this parameter in Alloy 625 by the present authors elsewhere [14], the behaviour of  $\alpha(L_{\rm M})$  is defined according to a hyperbolic decay curve fitted to values of  $\bar{\alpha}(L_{\rm M})$  measured by Devaux *et al.* and others. The use of separate fits for each dataset is precluded because the small number of data points and/or their relative narrow range with respect to  $L_{\rm M}(t)$ , despite the possible influences from temperature and composition differences. However, that being stated, it should be pointed out

that owing to the specific magnitude of the correction applied (explicitly that it essentially converts the major axis values in to minor axis values) the fact that Sundararaman *et al.* [28] also provided a quantification with respect to the minor axis distribution means that the application of the function is not needed to their data *viz.* this latter distribution set can be harnessed instead.



Fig. 6: Alloy 718  $\gamma''$  aspect ratio ( $\alpha$ ) vs major axis length plot constructed by Devaux *et al.* [7] based on measurements made on their own samples and literature data (Han [11], Slama [23], Sundararaman [28]). Hyperbolic fit made to the data for calculating aspect ratios in the present research for the precipitates contained within the PSDs of Han *et al.* [11] and Dong *et al.* [8] is indicated.

175 2.3.1 Results

195

Employing the predefined methodology, the LSEM distribution profiles and "directional encounter" corrected experimental PSDs computed for the three Alloy 718 studies of Han *et al.* [11] and Dong *et al.* [8] are presented in Figure 7a and b<sup>1</sup>. Additionally, the minor axis precipitate distribution measured by Sundararaman *et al.* [28], equivalent to  $f(L_{\rm M} \times \alpha(L_{\rm M}))$  is shown in Figure

- <sup>180</sup> Sundararaman *et al.* [28], equivalent to  $f(L_{\rm M} \times \alpha(L_{\rm M}))$  is shown in Figure 7c. Inspection of each distribution set reveals that the modification for "directional encounter" yields a much closer agreement with the both the LSEM and LSW curves, however the level and particular type of correspondence varies between studies and ageing conditions: All of the PSDs published by Han *et*
- <sup>185</sup> al. [11] (Figure 7a) display a consistent and strikingly good conformity with the constructed LSEM distribution except those measured from precipitates in samples aged at 998K for durations  $\geq 200$  hours as both retain a noticeable skew. Similarly, the PSDs measured by Sundararaman *et al.* [28] also show a generally good agreement with LSEM compared to LSW but the specific the shape and therefore level of agreement changes between curves.

In contrast to the other two studies, the curves of Dong *et al.* [8] highlight a transitional behaviour such that the curves for populations formed at times  $\leq 75$  hours agree strongly with LSW whereas populations measured after 100 hours of ageing conform with LSEM. Nevertheless, all of the curves can be seen to be far better parametrised by the respective mathematical distributions

after the implementation of the "directional encounter" correction.

Considering the results of Han *et al.* [11] first, the most obvious cause for the retention of the skew in the experimental data at 998K can be simply determined as the fit in Figure 6. Firstly, the necessary (due to the limited range and/or the sparsity of data points in any one study) use of results obtained from different alloys, with different compositions and aged at different temperatures, means the  $\alpha(L_M)$  trend is likely inaccurate for any one specific alloy and, therefore, leads to an error in the calculation pertaining to the removal of the "directional encounter" enhancement. Secondly, as "directional

<sup>205</sup> encounter" results in a consistent decrease in  $\alpha$  at large precipitate radii, the assumption of a hyperbolic relationship is likely not valid at larger  $L_{\rm M}$ values *viz*. the value of  $\alpha$  used in the "directional encounter" correction is overestimated in some instances, particularly the highlighted conditions used by Han *et al.* [11] which apparently yielded the largest precipitates. This latter result is supported by the  $\alpha(L_{\rm M})$  trends presented recently by Zhang *et al.* [31] which show a continued, significant reduction in  $\alpha$  when  $L_{\rm M} > 200$ nm.

Turning to the measurements of Dong *et al.*, the stronger agreement with the LSEM distribution at long ageing times and with the LSW distribution at short durations can be attributed to the specific nature of the  $\gamma''$  precipitation observed in the alloy: As described by Dong *et al.*, their modified Alloy 718 composition produced a compact  $\gamma' - \gamma''$  precipitate morphology. Consequently, it is straightforward to conclude that at the start of ageing the inhibiting influence of  $\gamma'$  reduced general precipitate "encounter" such that (aside from the "directional encounter" mechanism) an almost purely diffusion based evolution <sup>220</sup> took place. Similarly, whilst "encounter" still occurred, the higher probability for large  $\gamma''$  precipitates to be restricted by  $\gamma'$  suppressed their agglomeration to a value lower than it otherwise would have been. This second phenomena is actually evidenced in Figure 7 by the "over correction" of larger precipitate sizes in the more extensively aged material to values below that of the LSEM distribution but above LSW.





Fig. 7: Precipitate size distributions (corrected for "directional encounter") measured by a) Han et al. [11] and b) Dong et al. [8]. c)  $f(L_{\rm M} \times \alpha(L_{\rm M}))$ distribution measured by Sundararaman et al. [28]. Material (composition in Table 1) aged according to the correspondingly labelled conditions. LSW and LSEM distributions are also illustrated, with the corresponding Q values for the latter indicated.

# 3 Alloy 625 $\gamma''$ distributions

In light of the above results for Alloy 718, the correction devised and implemented for "directional encounter" can be seen to result in a far better adherence of measured  $\gamma''$  precipitate statistics to classical nucleation, growth and coarsening descriptions. Moreover, the LSEM theory can be concluded as 230 a more accurate representation of  $\gamma''$  than LSW. In this regard, therefore, an analysis of  $\gamma''$  precipitation in Alloy 625 was undertaken, utilising the correction for "directional encounter" in all instances.

3.1 Experimental Details

- Subsequent to a solution anneal at 1423K for 30 minutes to remove any previ-235 ously existing precipitates (following the successful demonstration by Shankar et al. [21] of such a treatment), Alloy 625 specimens (cut from a bar with the composition detailed in Table 3) were aged, based on the TTT curve published by Floreen et al. [10], at temperatures between 873-1023K for du-
- rations of up to 3000 hours. Quantification of the precipitate population was 240 made through analysis of < 100 > centred dark-field transmission electron microscopy (TEM) images obtained from electron-transparent specimens prepared through twin jet electropolishing (using a 20% HClO<sub>4</sub> 80% CH<sub>3</sub>OH electrolyte) 3mm discs of material mechanically thinned to a thickness of < 100

 $\mu m.$ 245

> Table 3: Composition (at%) of the Alloy 625 samples in analysed in this work. The index \* signifies the quantity is calculated from balance.

Ni	Cr	Fe	Mo	Nb	С	Mn	Si	Р	S	Al	Ti
$63.05^{*}$	24.85	3.05	5.32	2.43	0.10	0.22	0.49	0.02	0.01	0.26	0.20

#### 3.2 Results

#### 3.2.1 Evidence for "Directional Encounter"

An [001] oriented dark-field TEM image and a HRTEM image showing the crystal structures of two  $\gamma''$  precipitates that appear to have "coalesced" along their major axes in Alloy 625 aged at 923K is presented in Figure 8. A high degree of coherency/lattice matching at the interface between the  $\gamma''$  and FCC  $(\gamma)$  matrix is clearly evident, as these precipitates exhibit a well-defined orientation relationship with the matrix. In addition this particular  $\gamma''$  exhibits an apparent "defect" region at the location of the "coalescence" of two discrete precipitates, strongly suggesting an agglomeration process rather than simple 255

impingement has occurred; the presence of dislocations indicates that there is some degree of coherency and that the coalescence of the two precipitates is not complete. This result constitutes a significant progression on the tilting analysis of Han et al. [11] in Alloy 718 by providing direct evidence of the agglomeration process.

3.2.2  $\gamma'' \alpha(L_M)$ 

260

265

270

275

In contrast to the approach taken with respect to Alloy 718 previously, the acquisition of data from a large number (100s-1000s) of precipitates in each aged Alloy 625 sample facilitated the calculation of separate (isothermal) mathematical fits to define  $\alpha(L_{\rm M})$  as shown in Figure 9. Leaving aside the two population behaviour indicated at 1023K, as this will be discussed later, and accepting these fits as sufficient for the calculation of the distributions with respect to  $(L_{\rm M})$ , the lack of comparable data sets both with respect to precipitate number and temperature variation in the literature means it is worth remarking upon the specific behaviour exhibited.

Significantly, the separate isothermal plots for  $\alpha(L_{\rm M})$  in Figure 9 display not only a noticeable difference in the shape changing behaviour of  $\gamma''$  precipitates, but also the existence of a gradual continual evolution in each instance rather than the step change (attributable to a change in coherency) theorised (from experimental observations) by both Cozar et al. [5] and Devaux et al. [7] and the recent modelling work of Ji *et al.* [12].

The explanation for these observations is the change in physical characteristics of both the precipitate and matrix. As the shape behaviour of  $\gamma''$  precipitates is ultimately a consequence of precipitate-matrix strain anisotropy, which changes gradually with temperature [14, 23] different isothermal ageings

- 280 can exhibit different  $\gamma''$  evolution behaviours. Furthermore, the mathematical descriptions developed by Cozar et al. [5] and Ji et al. [12] assume constant values for parameters such as the misfit strain for coherent precipitates in contrast to the measurements of Slama et al. [23] in Table 2, which means that the step change can be more appropriately interpreted as the region where
- 285 these assumptions completely break down. This fact was accounted for by Ji et al. [12] through their alternate use of two sets of strain values in their calculations: one exclusively for fully coherent precipitates and one exclusively for semi-coherent precipitates. However, the step behaviour they computed (and
- set out to replicate based on the previous conclusions by Devaux et al. [7]) is 290 clearly still not in agreement with continuous behaviour presented in Figure 9, signifying that their two-stage behaviour treatment is also too simplistic.

## 3.2.3 $\gamma''$ Distributions

The "directional encounter" corrected distributions of the Alloy 625  $\gamma''$  precipitates measured in this research are presented, along with the corresponding LSW and LSEM plots, in Figure 10. Due to the availability of data, the cor-





Fig. 8: a) [001] oriented dark-field TEM image showing "coalescing"  $\gamma''$  precipitates (black arrows) and b) [100] oriented high-resolution-TEM (HRTEM) image of two coalescing  $\gamma''$  precipitates, both in Alloy 625 aged at 923K. The crystal structures of both the matrix (FCC) and precipitate (BCT) phases are clearly visible in image b indicating the presence of a "defect-like" region (arrowed) between the two BCT precipitate lattices at the join along their major axes.

rection was implemented individually to the raw values of  $L_{\rm M}$  using their corresponding  $\alpha$  values.

- Considering the data pertaining to ageing treatments at 873K and 923K, it is observed in Figure 10 that, compared to the previous analysis of Alloy 718 (Figure 7), the LSEM distributions for  $\gamma''$  precipitate more accurately represent those constructed from experimental measurements of populations in Alloy 625. That being said, the curves still display a minor discrepancy because of a remnant skew in the experimental data. Two principle reasons for
- this discrepancy are identified; 1) the sectioning of particles at the TEM sample surfaces acts to skew the data by concomitantly reducing the number of large particles and inflating the number of smaller ones, and 2) the similar effect of the image analysis technique through sectioning perpendicular particles (as  $\gamma''$  precipitates align exclusively along the [001] FCC matrix lattice planes
- <sup>310</sup> [22]) which have impinged one another owing to their edges being irresolvable. Nonetheless, notwithstanding these aforementioned sources of error (let alone any random sources), the close matching with the LSEM distribution can be interpreted as a success of the correction for "directional encounter".
- In contrast to the data obtained for lower ageing temperatures, a comparison of the shape LSEM distribution and the precipitate populations formed at 973K and 1023K reveals a marked disparity; only the populations formed at 973K after 3000 hours and after 200 hours at 1023K show a good correspondence with LSEM. The origin of this discrepancy can be attributed to the fact that at both of these temperatures, rather than a single precipitate population
- what is actually observed (as shown in Figure 11) is two separate populations, with one nucleated on dislocations and the other in the matrix. As directly evidenced by the two plots in Figure 9d, the first population to form preferentially on pre-existing dislocations evolves in a very different manner to those which nucleate homogeneously later in the matrix. Specifically, the different
- strain environment means the heterogeneously-nucleated precipitates do not experience the same forces for shape changing or "directional encounter" and ultimately grow much faster. It is the resultant effect of the statistics of the two precipitate populations being combined on the relative calculated magnitudes of  $L_{\rm M}$  which lies at the heart of the enhanced skew of the shorter aged
- <sup>330</sup> populations in Figures 10c and d and its reduction in the longer aged samples thanks to dominance of homogeneously-nucleated  $\gamma''$  (analogous to those observed at 873K and 923K).



Fig. 9:  $\gamma''$  aspect ratio vs major axis length plot created from populations formed when ageing at a) 873K, b) 923K, c) 973K and d) 1023K.



Fig. 10:  $\gamma''$  precipitate size distributions (corrected for "directional encounter") measured in Alloy 625 (composition defined in Table 3) aged for the indicated durations at a) 873K, b) 923K, c) 973K and d) 1023K. LSW and LSEM distributions corresponding to a Q value of 0.0972 in all cases are also illustrated.



(c)

(d)

Fig. 11: [001]-oriented dark-field TEM image of  $\gamma''$  precipitates in samples of Alloy 625 aged at 973K for a) 100 hours, b) 1000 hours and c) 3000 hours. d) A [001] selected area electron diffraction pattern showing reflections from the three variants of  $\gamma''$ , with the streaked precipitate reflections corresponding to the two edge-on variants [16]. A transition from an exclusively heterogeneously nucleated  $\gamma''$  population to one comprising both heterogeneously and homogeneously nucleated  $\gamma''$  precipitates is clearly visible. Also, needle-like  $\delta$  precipitates can be observed in (c).

Taking into account the present results alone, because of the faster removal/annealing rate of remnant dislocations that should accompany higher temperature ageing, the heterogeneous (on dislocations) to homogeneous nucleation transition behaviour observed could reasonably be considered as related to the Alloy 625 sample thermal history. However, in view of the published literature on similarly aged material it more likely to be attributable to the effect of undercooling as argued by Sundararaman *et al.* [26, 25] and

Pai et al. [17] (and based on the TTT diagrams of Schnabel et al. [19] and Floreen et al. respectively); by increasing the barrier to homogeneous nucleation in a system containing sufficient heterogeneous sites, a reduction in the differential to the solvus temperature will (according to classical theories [18]) ultimately lead to a change in the dominant nucleation site for  $\gamma''$  precipita-

tion. Furthermore, if the number of heterogeneous nucleation sites is reduced (through precipitation) by a sufficient amount, the transition between the two mechanisms at the same ageing temperature is reversed [26, 25, 17]. It should be pointed out that both Shaikh *et al.* [20] and Suave *et al.* [24] also report on the phenomenon but provide no discussion of the mechanism behind it.

# 350 3.3 Activation Energy for $\gamma''$ Coarsening

To complete the modified LSW assessment carried out in this research, the  $\bar{L}_{\rm M}^3$  growth behaviour and activation energy  $(E_{\rm A})$  for  $\gamma''$  coarsening is calculated using the methodology of previous authors [7]: Through inserting an Arrhenius equation for the diffusion coefficient D into Equation 1 the relationships

defined in Equation 2 are created. Consequently, the quantity U''(T) can be evaluated from a linear regression to a plot of  $\bar{L}_{\rm M}(t)^3$  for each ageing temperature as shown in Figure 12a. Finally, harnessing the values of U''(T) and  $\bar{\alpha}$  of each population,  $E_{\rm A}$  can be calculated from the gradient of a further linear regression as shown in Figure 12b. The values of  $\bar{L}_{\rm M}(t)^3$  in this research corresponded to the average of between 200-1000 precipitates (dependent on the precipitate frequency and image magnification) measured from a number of images of material aged at each condition.

$$\bar{L}_{\rm M}^3(t) - \bar{L}_{\rm M}^3(0) = U''t$$

$$U'' = \frac{32D_0\zeta V_{\rm m}X_{\gamma}^{\rm e}}{\alpha\pi RT} \frac{f_{\rm LSEM}(\bar{L}_{\rm M}, L_{\rm M}^*)^3}{C_{\rm LSEM}} \exp\left(\frac{-E_{\rm A}}{RT}\right)$$
(2)

\_ \_ \_

335

The value produced from the 823K-1023K fit in Figure 12b of  $E_{\rm A} = 1.8783 {\rm MJmol}^{-1}$  is far in excess of that reported by either Devaux *et al.* [7] (298 kJmol<sup>-1</sup>), Han *et al.* [11] (272 kJ mol<sup>-1</sup>), Wang *et al.* [30] (286 kJmol<sup>-1</sup>) or Zhang *et al.* [31] (292kJmol<sup>-1</sup>) due to the significant enhancement associated with the delayed homogeneous precipitation (discussed previously) at temperatures  $\geq 973 {\rm K}$ . In contrast, the value of  $E_{\rm A} = 211.7 {\rm kJmol}^{-1}$  calculated from the data points corresponding to samples unaffected by the transition in



Fig. 12: a)  $L^3$  growth behaviour of  $\gamma''$  precipitates in Alloy 625. b) Plot to facilitate the calculation of  $E_A$  in accordance with Equation 2. It should be noted that whilst the spread of the data points in the 973K series is clear evidence of a two stage (100-200 hours and 1000-3000 hours) precipitation behaviour, owing to the uncertainly in the start time of the homogeneous precipitation the whole series is subjected to the fit. In contrast, the wide disparity of the statistics pertaining to the heterogeneous population which exists after 50 hours of ageing at 1023K compared to the latter formed homogeneous one, and the relatively short time periods involved, means the 50 hour data point is excluded from the fit in this instance.

- <sup>370</sup> nucleation behaviours (873K-923K fit) is in much closer agreement with those previously found in Alloy 718. This fact is especially true when considering the decrease in  $E_{\rm A}$  that should accompany the lower temperature of the nose of the TTT curve for  $\gamma''$  in Alloy 625 [10] compared to Alloy 718 [3].
- In light of the aforementioned eventualities, comparison of the results produced in this research with those of Suave *et al.* [24] indicates that their enhanced value of 358kJmol<sup>-1</sup> in Alloy 625 is attributable primarily to delayed homogeneous nucleation at 973K and 1023K *viz.* the two stage behaviour in Figure 12 (remarked upon previously) is clearly also present in their plots of  $\bar{L}_{\rm M}^3(t)$ . Furthermore, the cause of the effect being diminished in their work can
- be identified as their use of shorter ageing times and therefore the more consistent capture of a predominantly heterogeneously nucleated  $\gamma''$  precipitate population.

### **4 Summary and Conclusions**

The separate, sequential key findings of this research can be summarised as follows: 385

1. The "directional encounter" process whereby agglomerating  $\gamma''$  coalesce along their major axis has been imaged directly through HRTEM.

23

- 2. Using the assumption of complete niobium depletion from the matrix, the LSEM description of classical precipitate growth/coarsening including the
- effect of "encounters" has been shown to be far more successful for  $\gamma''$  than 390 the original LSW theory once the directional coalescence mechanism of the ellipsoidal precipitates is accounted for.
- 3. The shape-changing evolution of  $\gamma''$  has been demonstrated to be temperature dependent and likely consequence from the change (measured by Slama et al. [23]) induced by temperature on the misfit strain. Con-395 comitantly, the results here find the coherence to incoherence step-change suggested by Cozar *et al.* [5] (and latterly Devaux *et al.* [7]) to be a manifestation of their assumptions rather than a physical phenomenon.
- 4. The activation energy for  $\gamma''$  coarsening in Alloy 625 reported herein and that reported by Suave et al. [24] are in agreement when the relative pre-400 cipitation mechanisms and kinetics are considered for the two studies.
  - 5. Based on the overall results, it clear that an LSEM-type formalism will only be successful with respect to  $\gamma''$  with detailed knowledge of the behaviour of  $\alpha(L_{\rm M})$  over all relevant times and temperatures and of the relationship between "directional encounter" and  $\alpha$ . However, this is a significant undertaking given the effect of phases such as  $\gamma'$  (Dong *et al.* [8]) and  $\delta$  phase (Sundararaman et al. [27]).

Acknowledgements The authors thank Dr O. Ciuca at the University of Manchester for his technical assistance. Funding of this work was provided by the Engineering and Physical Sciences Research Council under the auspices of the Nuclear FiRST Doctoral Training Centre based at The University of Sheffield and The University of Manchester.

#### References

- 1. A. Baldan, Review: Progress in Ostwald ripening theories and their applications to nickel-base superalloys. Part I: Ostwald ripening theories. Journal of Materials Science **37**(11), 2171–2202 (2002)
- 2. J.D. Boyd, R.B. Nicholson, The coarsening behaviour of  $\theta''$  and  $\theta'$  precipitates in two Al-Cu alloys. Acta Metallurgica 19(12), 1379–1391 (1971)
- 3. J.W. Brooks, P.J. Bridges, Metallurgical stability of Inconel alloy 718, in Superalloys 1988 (Proceedings of the Sixth International Symposium on
- Superalloys), ed. by S. Reichman, D.N. Duhl, G. Maurer, S. Antolovich, C. 420 Lund (The Minerals, Metals & Materials Society, Warrendale, PA, 1988), pp. 33–42

415

- 4. M.C. Chaturvedi, D.W. Chung, Effect of iron addition on the precipitation behavior of Co-Ni-Cr alloys containing Nb. Metallurgical Transactions A 10(11), 1579 - 1585 (1979)
- 5. R. Cozar, A. Pineau, Influence of coherency strains on precipitate shape in a Fe-Ni-Ta alloy. Scripta Metallurgica 7(8), 851–854 (1973)
- 6. C.K.L. Davies, P. Nash, R.N. Stevens, The effect of volume fraction of precipitate on ostwald ripening. Acta Metallurgica 28(2), 179–189 (1980)
- 7. A. Devaux, L. Nazé, R. Molins, A. Pineau, A. Organista, J.Y. Guédou, J.F. 430 Uginet, P. Héritier, Gamma double prime precipitation kinetic in Alloy 718. Materials Science and Engineering A **486**(1-2), 117–122 (2008)
  - 8. J. Dong, X. Xie, S. Zhang, Coarsening behavior of  $\gamma''$  precipitates in modified Inconel 718 superalloy. Scripta Metallurgica et Materiala **33**(12), 1933 - 1940 (1995)
  - 9. H. Fischmeister, G. Grimvall, Ostwald Ripening A Survey, ed. by G.C. Kuczynski, vol. 6 (Springer, Boston, MA, 1973), pp. 119–149
  - 10. S. Floreen, G.E. Fuchs, W.J. Yang, The Metallurgy of Alloy 625, in Proceedings of the International Symposium on Superalloys 718, 625, 706 and Various Derivatives, ed. by E.A. Loria (The Minerals, Metals & Materials Society, Warrendale, PA, 1994), pp. 13-37
  - 11. Y.F. Han, P. Deb, M.C. Chaturvedi, Coarsening behaviour of  $\gamma''$  and  $\gamma'$ particles in Inconel alloy 718. Metal Science 16(12), 555–562 (1982)
  - 12. Y. Ji, Y. Lou, M. Qu, J.D. Rowatt, F. Zhang, T.W. Simpson, L.Q. Chen,
- Predicting coherency loss of  $\gamma''$  precipitates in IN718 superalloy. Metal-445 lurgical and Materials Transactions A: Physical Metallurgy and Materials Science 47(6), 3235–3247 (2016)
  - 13. I.M. Lifshitz, V.V. Slyozov, The kinetics of precipitation from supersaturated solid solutions. Journal of Physics and Chemistry of Solids 19(1-2), 35-50(1961)
  - 14. I.J. Moore, M.G. Burke, E.J. Palmiere, Modelling the nucleation, growth and coarsening kinetics of  $\gamma''$  (D0<sub>22</sub>) precipitates in the Ni-base Alloy 625. Acta Materialia 119, 157-166 (2016)
- 15. J.M. Oblak, D.S. Duvall, D.F. Paulonis, An estimate of the strengthening arising from coherent, tetragonally-distorted particles. Materials Science 455 and Engineering 13(1), 51–56 (1974a)
  - 16. J.M. Oblak, D.F. Paulonis, D.S. Duvall, Coherency strengthening in Ni base alloys hardened by D0<sub>22</sub>  $\gamma''$  precipitates. Metallurgical Transactions **5**, 143–153 (1974b)
- 17. H.C. Pai, M. Sundararaman, A comparison of the precipitation kinetics 460 of  $\gamma''$  particles in virgin and re-solutioned Alloy 625, in *Proceedings of* the International Symposium on Superalloys 718, 625, 706 and Various Derivatives, ed. by E.A. Loria (The Minerals, Metals & Materials Society, Warrendale, PA, 2005), pp. 487-495
- 18. D.A. Porter, K.E. Easterling, Phase Transformations in Metals and Alloys, 465 2nd edn. (CRC Press, Boca Raton, FL, 1992)
  - 19. E. Schnabel, H.J. Schueller, P. Schwaab, Precipitation and recrystallization behavior of the nickel-base alloy Inconel 625 [Das ausscheidungs und

425

435

440

rekristallisationsverhalten der nickelbasislegierung Inconel 625]. Praktische Metallographie/Practical Metallography **8**(9), 521–527 (1971)

- M.A. Shaikh, M. Ahmad, K.A. Shoaib, J.I. Akhter, M. Iqbal, Precipitation hardening in Inconel \* 625. Materials Science and Technology 16(2), 129– 132 (2000)
- V. Shankar, K. Bhanu Sankara Rao, S.L. Mannan, Microstructure and me chanical properties of Inconel 625 superalloy. Journal of Nuclear Materials
   288(2-3), 222-232 (2001)
  - C.T. Sims, N.S. Stoloff, W.C. Hagel, *Superalloys II*, 1st edn. (John Wiley & Sons, New York, NY, 1987)
  - C. Slama, C. Servant, G. Cizeron, Aging of the Inconel 718 alloy between 500 and 750°C. Journal of Materials Research 12(9), 2298–2316 (1997)
- 24. L.M. Suave, J. Cormier, P. Villechaise, A. Soula, Z. Hervier, D. Bertheau, J. Laigo, Microstructural evolutions during thermal aging of Alloy 625: Impact of temperature and forming process. Metallurgical and Materials Transactions A: Physical Metallurgy and Materials Science 45(7), 2963–2982 (2014)
  - 25. M. Sundararaman, P. Mukhopadhyay, Heterogeneous precipitation of the  $\gamma''$  phase in Inconel 625. Materials Science Forum **3**, 273–280 (1985)
  - 26. M. Sundararaman, R. Kishore, P. Mukhopadhyay, Some aspects of the heterogeneous precipitation of the metastable  $\gamma''$  phase in Alloy 625, in
- <sup>490</sup> Proceedings of the International Symposium on Superalloys 718, 625, 706 and Various Derivatives, ed. by E.A. Loria (The Minerals, Metals & Materials Society, Warrendale, PA, 1994), pp. 405–418
  - 27. M. Sundararaman, P. Mukhopadhyay, S. Banerjee, Precipitation of the  $\delta$ Ni<sub>3</sub>Nb phase in two nickel base superalloys. Metallurgical Transactions A **19**(3), 453–465 (1988)
  - M. Sundararaman, P. Mukhopadhyay, S. Banerjee, Some aspects of the precipitation of metastable intermetallic phases in Inconel 718. Metallurgical Transactions A 23(7), 2015–2028 (1992)
- 29. C. Wagner, Theory of precipitate change by redissolution. Z. Electrochem
   65(7-8), 581-591 (1961)
  - L. Wang, Y. Wang, Y. Liu, X. Song, X.D. Lü, B.J. Zhang, Coarsening behavior of γ' and γ" phases in GH4169 superalloy by electric field treatment. International Journal of Minerals, Metallurgy and Materials 20(9), 861–866 (2013)
- 505 31. J.L. Zhang, Q.Y. Guo, Y.C. Liu, C. Li, L.M. Yu, H.J. Li, Effect of cold rolling and first precipitates on the coarsening behavior of γ"-phases in Inconel 718 alloy. International Journal of Minerals, Metallurgy and Materials 23(9), 1087–1096 (2016)

25

470

480