

Waste-derived activated carbons for control of nitrogen oxides

Amal S.S. Al-Rahbi MSc

Research student, School of Chemical and Process Engineering, University of Leeds, Leeds, UK

Mohamad A. Nahil PhD

Research Fellow, School of Chemical and Process Engineering, University of Leeds, Leeds, UK

Chunfei Wu PhD

Research Fellow, School of Chemical and Process Engineering, University of Leeds, Leeds, UK

Paul T. Williams MSc, PhD, CEng, FEI, MCIWM

Professor, School of Chemical and Process Engineering, University of Leeds, Leeds, UK

Activated carbons were produced from waste and investigated for their efficiency for the removal of mono-nitrogen oxides (NO_x) in simulated flue gases at a low temperature. The wastes used were waste biomass (date seeds), processed municipal solid waste in the form of refuse-derived fuel and waste tyres. The morphology, porous texture and surface chemistry of the prepared activated carbons were evaluated by scanning electron microscopy, energy-dispersive X-ray spectrometry, nitrogen adsorption and Boehm titration, and were compared with several commercial activated carbons. The carbons were then investigated in terms of their use in adsorbing NO_x at a low temperature. The waste-derived activated carbons had NO_x adsorption efficiencies at 50°C which were between 50 and 70% of those achieved for the commercial activated carbons. Increasing the adsorption temperature from 25 to 100°C significantly reduced nitrogen oxide (NO) adsorption. It was also shown that the NO adsorption efficiency depends on the porous structure, particularly the presence of micropores in the activated carbon, but to a lesser extent on the surface area of the carbons and acid–base surface groups on the carbon surface.

1. Introduction

The combustion of solid fuels such as coal, biomass and wastes generates nitrogen oxides (NO_x) which cause environmental problems such as acid rain and smog. NO_x emissions in the flue gases are most commonly present as nitrogen oxide (NO; typically about 90%) and nitrogen dioxide (NO₂; typically about 10%). NO_x arise mainly from the nitrogen (N₂) in the fuel ('fuel NO_x') and by direct combination of nitrogen and oxygen (O₂) present in the combustion air, which occurs more rapidly at high temperatures ('thermal NO_x'). In practice, thermal NO_x is formed almost exclusively at high flame temperatures.

Several technologies have been developed to control NO_x emissions (Belhachemi *et al.*, 2014; Gómez García *et al.*, 2005; Sousa *et al.*, 2013). The addition of ammonia (NH₃, or urea) to the flue gases (selective non-catalytic reduction) can reduce NO_x by reaction to produce nitrogen and water, but is effective only over a narrow temperature range (~850–950°C). Selective catalytic reduction (SCR) uses a catalyst in the presence of added ammonia, which reproduces the ammonia reduction reaction but at a lower temperature (~250–400°C). The effectiveness of SCR for NO_x reduction can reach 85% and is a widely

used technology (Belhachemi *et al.*, 2014). However, the use of SCR has some drawbacks such as the difficulty of chemical handling and storage, and potential 'slippage' of ammonia, due to <100% reaction (Gómez García *et al.*, 2005; Sousa *et al.*, 2013). Additionally, SCR is a costly method and the catalyst is prone to deactivation when sulfur dioxide (SO₂) is present in the flue gases. Therefore, there is interest in the development of low-cost and efficient techniques to control NO_x to meet the current stringent environmental regulations on emission limits. Of particular interest for NO_x control are low-temperature processes where the NO_x can be adsorbed after the gas scrubbing unit and where consequently low temperatures are encountered.

Removal of pollutants by adsorption is an effective method for the control of a range of pollutants. Although different adsorbents have been investigated including metal oxides, alumina, FeOOH, silica and activated carbon (Azambre *et al.*, 2009; Lévassieur *et al.*, 2012; Lopez *et al.*, 2007), activated carbon has been used as an adsorbent for many pollutants such as heavy metals (particularly mercury), sulfur dioxide and NO_x. The efficiency of activated carbon for the adsorption of pollutants is controlled by the degree of pore structure development

and the chemical arrangement and the type and number of heteroatoms on the carbon surface (Kante *et al.*, 2009; Lee *et al.*, 2004).

Development of low-cost activated carbon adsorbents using waste materials has attracted the attention of many researchers as a route to producing valuable materials from wastes which also acts as an alternative to waste disposal. A variety of solid waste and biomass waste feedstocks have been used to produce activated carbon (Amalraj and Piu, 2013; Buah and Williams, 2010; El-Kady *et al.*, 2013; Gil *et al.*, 2014; Gundogdu *et al.*, 2013; Gupta *et al.*, 2014; Hajizadeh *et al.*, 2011; Illingworth *et al.*, 2012; Liu *et al.*, 2014; Nahil and Williams, 2010). For example, activated carbons have been produced from municipal solid waste and used in the metal extraction industry (Buah and Williams, 2010); from waste tyres and used for dioxin adsorption from flue gases (Hajizadeh *et al.*, 2011); also from waste tyres for use in the adsorption of phenolic compounds (Gupta *et al.*, 2014); from waste fibreboard for use for copper (II) adsorption (Liu *et al.*, 2014); from tannery wastes for use in the removal of dyes (Amalraj and Piu, 2013); from agricultural wastes from the removal of pesticides from water (El-Kady *et al.*, 2013) and so on.

There have been several reports on the use of activated carbons to control NO_x. The kinetics of NO_x removal by carbon of commercial origin has been studied by many researchers (Claudino *et al.*, 2004; Klose and Rincón, 2007; Mochida *et al.*, 1994; Shirahama *et al.*, 2002; Teng and Suuberg, 1993; Zhang *et al.*, 2008) and it has been concluded that the origin, the natural impurities in the feedstock, surface chemistry and the conditions used to prepare activated carbon are the main factors that can control its efficiency for NO_x reduction (Xu *et al.*, 2003). Although there has been much research into NO_x control using activated carbons, the factors controlling the NO_x adsorption process are still not clear. The porous texture including the surface area and pore volume, the acidic and basic groups, the nitrogen content or nitrogen groups and the oxygen surface groups all can affect the NO removal by carbon. For example, Illan-Gomez *et al.* (1993) reported that no correlation was found between the NO reduction activity and carbon structure, and that activated carbons with different surface areas were all effective for NO reduction. The same conclusion was reported by other researchers, such as Guo *et al.* (2001), Neathery *et al.* (1997) and Ruiz Machado and Hall (1998). Neathery *et al.* (1997) found that the activated carbon with the lowest total pore volume and an intermediate surface area had the highest NO uptake capacity. In contrast, Rubio and Izquerido (2013) reported that the surface area and the carbon content were the main factors that influenced the removal efficiency of the activated carbon obtained from carbon-enriched coal fly ashes. Kaneko *et al.* (1988) claimed that the absorbability of activated carbon fibres

in relation to NO, ammonia and sulfur dioxide at low temperature increased with specific surface area. Mochida *et al.* (1994) reported that the main factor determining NO reduction activity was the nitrogen content of the samples. However, Illan-Gomez *et al.* (1993) found no correlation between the nitrogen content of activated carbons and the NO reduction activity. There is clearly uncertainty in the literature in relation to the influence of activated carbon characteristics on NO_x removal.

In this paper, the authors have produced activated carbons from low-cost waste materials in the form of biomass waste (date seeds) refuse-derived fuel (RDF) produced from the processing of municipal solid waste and waste tyres. The aim of this study was to examine the efficiency of these activated carbons for NO removal and to compare them with commercial carbons with varied porous texture and surface chemistry to determine the main carbon properties that influence NO adsorption. The NO adsorption was investigated at low temperatures, between 25 and 100°C to determine the effectiveness of NO control at low temperature.

2. Experimental

2.1 Materials

The activated carbon samples were designated as AC-D for the date seed biomass waste, AC-R for the activated carbon produced from RDF and AC-T for the carbons produced from waste tyres. Since municipal solid waste is a heterogeneous waste which has not been sorted and shredded, RDF was selected to represent the municipal solid waste with the elimination of recyclable materials such as metals and glass. The RDF sample was carefully prepared from 2 kg of RDF and was mixed, coned and quartered and further shredded to enhance homogeneity. The waste tyre sample was a shredded mixture of waste truck tyres. The sample was prepared by removing the steel followed by shredding and sieving. The date seeds were obtained from Oman and were crushed and sieved. All the samples were ground and sieved to a particle size of 1.7–3 mm. For comparison, four different commercial carbons (labelled C-AC1, C-AC2, C-AC3 and C-AC4) with different characteristics and porosity were used in this study and were obtained from Norit Ltd, the Netherlands. The carbons were of particle size 0.15–3 mm. The elemental analysis of the commercial and waste-derived activated carbons was carried out using a Carlo Erba Flash EA 1112 elemental analyser. A Shimadzu TGA-50H analyser was used to perform the proximate analysis of activated carbons. The metal content of the samples was determined using an Olympus Innovex X-5000 X-ray fluorescence (XRF) spectrometer. The device was equipped with an Rh source. The three waste materials were ashed in a furnace at 550°C for several hours. A lithium borate flux

was added to the ash and heated to 900°C to form a melt. The melt was cooled down quickly to form a disc which was presented to the XRF spectrometer for analysis.

Table 1 shows the properties of the raw waste RDF, tyre and date seeds. The RDF had a significant ash content at 11.0 wt% consisting of mainly alumina-silicates and also a significant metal content, including heavy metals. The tyre also had a high ash content at 7.1 wt%, with zinc, as a prominent additive to the tyre manufacturing process, and also with the presence of other heavy metals and filler materials. The date seeds had

Proximate analysis: wt%	RDF	Tyre	Date seeds
Volatiles	72.0	62.2	18.2
Moisture	5.0	1.3	7.5
Ash	11.0	7.1	4.0
Fixed carbon	13.0	29.4	69.9
Minerals analysis: wt%			
Zinc oxide	0.06	2.95	0.01
Silicon dioxide	4.64	1.74	0.14
Iron oxide	0.36	0.40	0.03
Calcium oxide	1.86	0.24	0.21
Potassium oxide	0.28	0.07	1.98
Aluminium oxide	2.31	0.17	0.04
Phosphorus pentoxide	0.05	0.03	0.90
Copper oxide	0.01	0.06	<0.01
Magnesium oxide	0.50	0.05	0.61

Table 1. Composition of raw waste materials

the lowest ash content at 4.0 wt% consisting of mainly nutrients such as calcium, potassium, magnesium and phosphorus.

2.2 Preparation of activated carbons

The activated carbons produced from the waste materials were prepared by pyrolysis followed by activation of the product char using steam. Pyrolysis of the date seeds, RDF and tyres was carried out in a fixed bed batch reactor, 250 mm in length by 30 mm internal diameter and was externally heated by an electric furnace (Figure 1(a)). The reactor was fully instrumented in terms of gas flow control, furnace temperature control and temperature monitoring throughout. The waste (10 g) was held in a sample crucible in the reactor and heated to a final temperature of 600°C at a heating rate of 10°C/min and held at this final temperature for 1 h. The recovery of char from the original raw material was 23.6, 31 and 37.5 wt% for the date seeds, RDF and waste tyres, respectively. Nitrogen was used as the carrier gas. A condenser system consisting of a water-cooled condenser and two solid carbon dioxide-cooled condensers was used to trap the condensable liquids. Non-condensable gases were collected in a Tedlar gas sample bag.

The chars recovered from the pyrolysis reactor were ground and sieved to 1.5–2 mm and dried at a temperature of 105°C overnight and then activated in the pyrolysis reactor, which was adapted to incorporate steam injection by the addition of a steam generator at the inlet to activate the chars produced from the pyrolysis experiments (Figure 1(b)). During the activation process, the samples were heated at a heating rate of 20°C/min to an activation temperature of 900°C. Once the activation temperature was attained, the steam was introduced

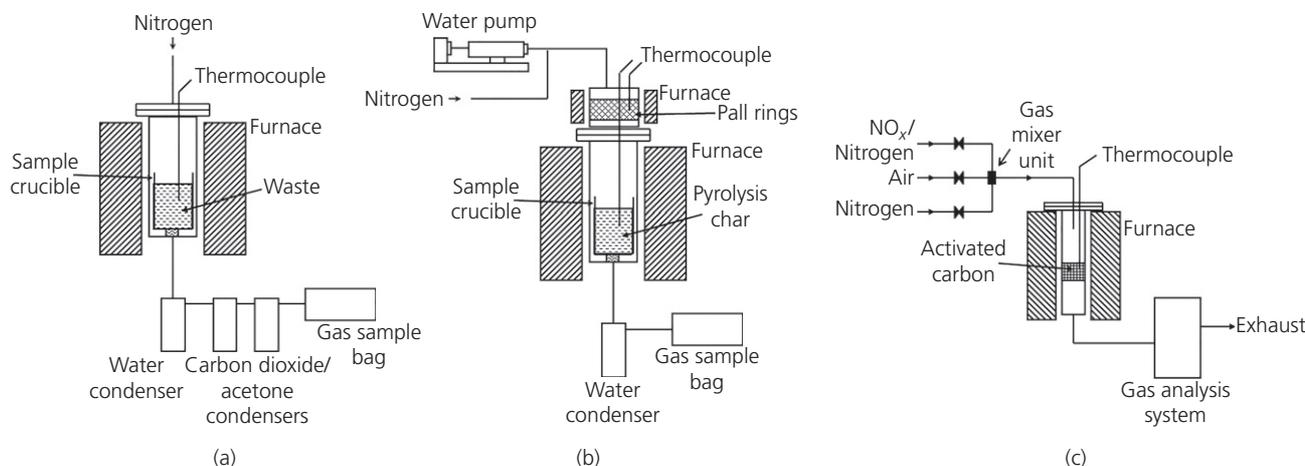


Figure 1. (a) Schematic diagram of the waste pyrolysis reactor; (b) the char activation reactor; and (c) the gas adsorption reactor

for a period of 3 h. A Sage instrument model 255-2-syringe pump was used to inject deionised water into the steam generator which was maintained at 300°C.

2.3 NO_x adsorption reactor system

The NO adsorption tests on the commercial and waste-derived activated carbons were conducted using a stainless steel fixed-bed reactor externally heated by an electric furnace (Figure 1(c)). The reactor system consisted of a gas mixing unit, the activated carbon-NO_x adsorption reactor and an online gas analysis system. Air, nitrogen and NO/nitrogen with an NO concentration of 1000 ppm was supplied by B.O.C. Special Gases Ltd, UK. The gases were mixed together before entering the reactor in a gas mixing unit. The NO_x adsorption reactor was of 20 cm height and 2.2 internal diameter, with a 10 cm sample holder used to hold the activated carbon bed inside the reactor. The temperature of carbon was monitored with a thermocouple. The adsorption tests were conducted with a fixed activated carbon mass of 2.8 g, which was previously treated under nitrogen at 500°C for 30 min in order to clean the surface oxides and desorb the adsorbed gases on the carbon surface (Claudino *et al.*, 2004; Lopez *et al.*, 2007). The bed depth was about 3 cm which gave ~1.7 s gas residence time through the carbon bed. The adsorption was carried out for 2 h at different temperatures of 25, 50 and 100°C and in the presence of a gas mixture of 5% oxygen and 800 ppm NO, with a balance of nitrogen. The presence of oxygen in the gas mixture is essential, since it increases the adsorption of nitric oxide through the catalytic oxidation of NO to NO₂, which results in an increase of NO adsorption due to the higher adsorption potential of NO₂ (Klose and Rincón, 2007; Yang *et al.*, 2000). In this work, experiments in the absence of oxygen showed that NO removal efficiency was only about 5%; similar findings have been reported in the literature (DeGroot *et al.*, 1991; Teng and Suuberg, 1993). The outlet gas was directed to a gas analyser system. The gas composition was recorded every minute using a gas analyser unit supplied by Horiba Instruments UK Ltd, and consisted of a Horiba VA-3000 chemiluminescence analyser for nitrogen oxide/NO_x and a separate Horiba VA-3000 paramagnetic analyser for oxygen.

The NO removal efficiency of the used adsorbents was calculated according to Equation 1

$$1. \quad \text{NO removal efficiency (\%)} = \frac{(C_{\text{NO}}^0 - C_{\text{NO}})}{C_{\text{NO}}^0} \times 100$$

where C_{NO}^0 and C_{NO} are the NO concentration before adsorption (at the outlet of the bypass) and after adsorption, respectively.

2.4 Activated carbon characterisation

The physical properties of activated carbons including BET (Brunauer, Emmett & Teller) surface area and porosity of activated carbons were determined by the adsorption of nitrogen at 77 K using a Micromeritics TriStar 3000 apparatus, which measures the quantity of nitrogen adsorbed onto or desorbed from a solid sample at different equilibrium vapour pressures. Prior to the analysis, the samples (0.1 g) were degassed under vacuum for 3 h at 300°C. The micropore and mesopore volumes were determined by Dubinin–Radushkevich and Barret–Joyner–Halenda methods, respectively. Pore size distribution was obtained by the density functional theory (DFT) method.

The Boehm titration method was used to determine the acidic and basic oxygen groups of the commercial and waste-derived activated carbons. The basic sites were determined by mixing 1 g of activated carbon with 50 ml of 0.05 M hydrochloric acid (HCl) in a closed flask and shaken for 24 h. The solution was then filtered. An aliquot of 5 ml was taken and titrated with 0.05 M sodium hydroxide (NaOH). The acidic groups were determined by a similar procedure, where activated carbon was mixed with 0.05 M sodium hydroxide and the titrant solution was 0.05 hydrochloric acid.

A SEM LEO 1530 high-resolution scanning electron microscope (SEM) coupled to an energy-dispersive X-ray spectroscope (EDXS) was used to characterise and examine the surface morphology of the prepared carbons with EDXS providing an indication of the metal content of the carbons.

3. Results and discussion

3.1 Properties of the commercial and waste-derived activated carbons

The proximate and ultimate analyses of the commercial activated carbons and the activated carbons produced from the waste materials are shown in Table 2. There are large differences in the ash content of the commercial carbons compared with the activated carbons produced from the waste materials, particularly the carbons produced from RDF and tyres. The mineral matter found in the original feedstock, becomes progressively concentrated through the process of pyrolysis, will reduce the mass of solid product through loss of volatiles as condensable liquids and non-condensable gases to produce the char. Additionally, during the activation process, the mineral matter is further concentrated as the carbon reacts with steam to produce gases, such as carbon dioxide, carbon monoxide, hydrogen, methane and so on as the char is activated (gasified). As can be observed from Table 2, the commercial carbons have high carbon contents (88–93%). Among the used waste materials, date seeds showed the highest elemental carbon content (74 wt%), fixed carbon (83.9 wt%) and had a significant amount of nitrogen

Sample	Proximate analysis: wt%			Elemental analysis: wt%			
	Volatiles	Ash	Fixed carbon	Carbon	Hydrogen	Nitrogen	Oxygen ^a
C-AC1	2.5	2.4	85.6	89.9	0.3	0.8	6.0
C-AC2	5.1	5.0	90.9	90.8	0.3	0.8	0.3
C-AC3	5.5	1.3	89.3	93.5	0.6	0.4	4.1
C-AC4	1.7	8.2	85.6	88.0	0.3	0.6	2.0
AC-R (RDF)	6.1	60.9	28.9	36.4	0.4	1.5	0.4
AC-T (tyre)	2.8	23.9	73.3	61.1	0.2	1.4	9.3
AC-D (biomass)	4.1	10.0	83.9	74.5	0.6	2.1	12.8

^aBy difference

Table 2. Proximate and ultimate analysis of activated carbons

(2.10 wt%). These properties have been reported to accelerate NO adsorption by activated carbons (Zhang *et al.*, 2008). The abundance of nitrogen content in AC-D could have a role in enhancing NO adsorption as reported by Rathore *et al.* (2010) in which the highest NO adsorption at room temperature was found with the sample containing the highest amount of nitrogen-containing groups. Bashkova and Bandosz (2009) concluded that a high NO₂ adsorption was found with carbon containing quaternary nitrogen groups, which was ascribed to the presence of positive charge centres for the adsorption of NO₂ and NO, which can be further reduced to nitrogen or oxidised to nitrate. In addition, nitrogen-containing groups provide the basic properties to the carbon which was reported to enhance the interaction with acid molecules (Sousa *et al.*, 2013).

Table 3 shows the analysis of activated carbons for their metal contents using XRF. There were clear differences between the carbons in terms of their ash composition. These differences may be attributed to the composition of the original precursor

Minerals analysis: wt%	C-AC1	C-AC2	C-AC3	C-AC4
Silicon dioxide	0.15	0.07	0.04	1.07
Iron oxide	0.39	0.22	0.06	3.44
Calcium oxide	0.74	1.78	0.14	1.97
Potassium oxide	0.47	0.92	0.81	0.08
Aluminium oxide	0.02	0.01	<0.01	0.52
Phosphorus pentoxide	0.47	0.10	0.05	0.08
Magnesium oxide	0.03	0.04	0.01	0.07
Manganese oxide	0.03	0.13	0.01	0.04

Table 3. Mineral composition of commercial activated carbons

raw material (which was not known) or related to additives to the carbons during the preparation process.

The metal contents and surface morphology of the activated carbons produced from the waste materials were estimated from the SEM-EDXS analysis and are presented in Figure 2. The SEM images show that the type of activated carbon precursor has a strong influence on the development of porous texture of the resulting activated carbon. As shown in Figure 2, both the activated carbons derived from waste tyres and date seeds (AC-T and AC-D) present a smooth and a regular surface, while the RDF activated carbon (AC-R) shows a heterogeneous structure. The EDX spectra indicate the existence of a high percentage of calcium, sodium and other minerals with AC-R, while AC-T showed the presence of a high amount of zinc. The presence of abundant amounts of alkaline minerals in a sample cannot be assumed to give high reactivity for NO_x, for example, Ahmed *et al.* (1993) reported a high nitrogen oxide adsorption activity with a sample that contained the lowest mineral content of alkaline metal oxides (calcium oxide, magnesium oxide and sodium oxide).

3.2 Nitrogen oxide removal using commercial and waste-derived activated carbons

The produced waste-derived activated carbons and the commercially obtained activated carbons were investigated for their NO adsorption characteristics with the NO_x adsorption reactor using a gas mixture of nitrogen oxide (800 ppm) and air (5 vol% oxygen) at an adsorption temperature of 50°C. The NO removal efficiency curves for the commercial activated carbons and the waste-derived activated carbon are shown in Figures 3(a) and 3(b), respectively. There is an initial high adsorption of nitrogen oxide by the activated carbons, but the level of adsorption decreases before reaching a steady level of adsorption. The highest removal efficiency of

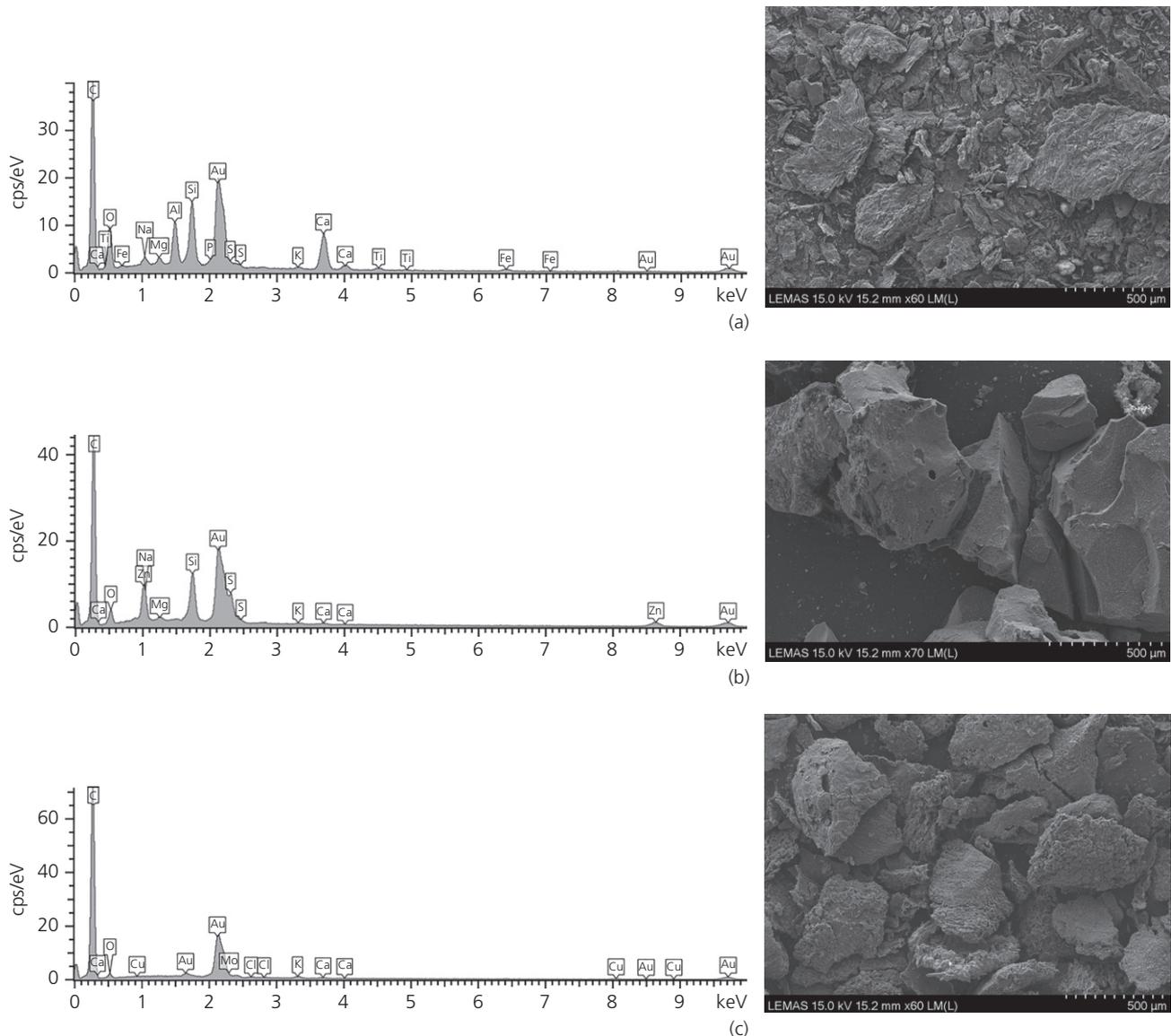


Figure 2. SEM-EDXS results of waste-derived activated carbons: (a) activated carbon from RDF (AC-R); (b) activated carbon from waste tyre (AC-T); and (c) activated carbon from date seeds (AC-D)

60% was found for the commercial C-AC1 activated carbon, achieved after the 120 min test time period. The other commercial activated carbons achieved about 40% NO removal after 120 min. For the waste-derived activated carbons, the nitrogen oxide concentration after 2 h adsorption was reduced to 630 ppm with the tyre-derived activated carbon, to 585 ppm for the RDF carbon and to 480 ppm for the biomass (date seeds) activated carbon. The waste-derived activated carbons showed a lower, but still an effective level of NO adsorption, with removal efficiencies of 40, 26 and 21% for the AC-D,

AC-R and AC-T, respectively, at 120 min. It should also be noted that the lower performance of the tyre and RDF activated carbons is linked to the high ash contents of these carbons. Consequently, from Table 2, the actual mass of carbon present in the NO adsorption reactor for the RDF activated carbon (60.9 wt% ash) was only 40% of that used for the commercial activated carbon experiments. Similarly, for the waste tyre activated carbon (23.9 wt% ash), there was only 76% of carbon present compared with the tests using the commercial activated carbons. Therefore, to achieve NO

adsorption efficiencies comparable to those obtained from commercially available activated carbons, a higher mass of waste-derived activated carbon would be needed.

3.2.1 Surface area and pore characteristics of activated carbons

To understand the differing levels of nitrogen oxide removal efficiency found by the different adsorbents, the properties of surface area and porosity of activated carbons were investigated. Pore size for activated carbons are classified into average pore size classes: micropores are of pore width <2 nm, mesopores of pore width 2–50 nm and macropores are of pore width >50 nm. The pore width refers to the distance between the walls of slit-shaped pores or the radius of cylindrical-shaped pores.

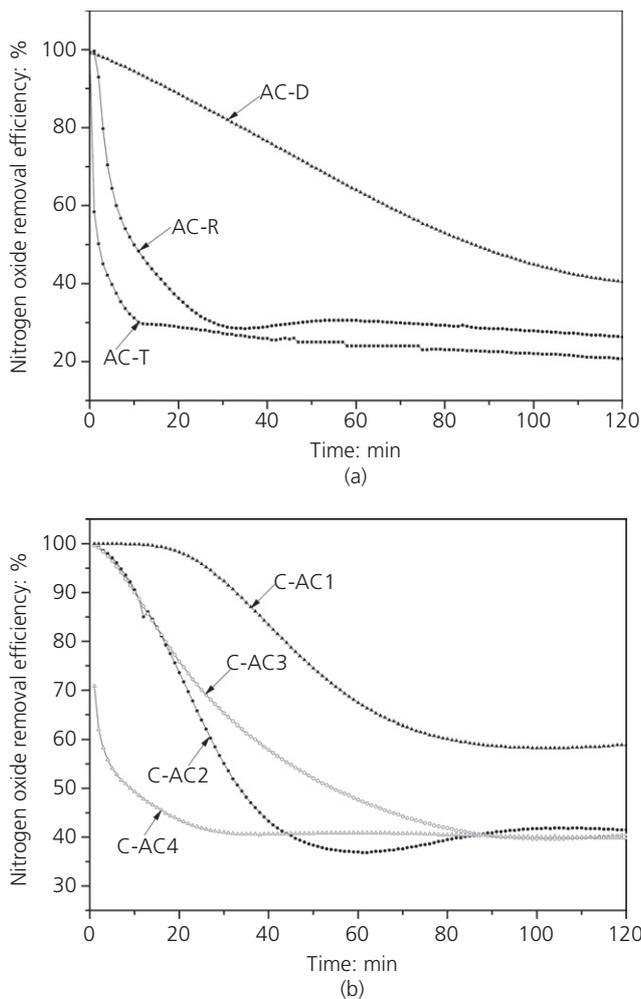


Figure 3. Nitrogen oxide removal efficiency curves for: (a) commercial activated carbons and (b) waste-derived activated carbons at 50°C adsorption temperature

The nitrogen adsorption–desorption isotherms of the commercial and waste-derived activated carbons are shown in Figures 4(a) and 4(b), respectively. The data suggest that the activated carbons for C-AC1, C-AC2, C-AC3, C-AC4 produced adsorption–desorption isotherms characteristic of type I and type IV isotherms according to the International Union of Pure & Applied Chemistry (IUPAC) classification (Sing *et al.*, 1985). Therefore, these activated carbons contained both micropores and mesopores. Type I isotherm is characterised by the initial steep portion of the adsorption isotherm at low relative pressures, which represents the filling of the micropores by the adsorbate. The isotherm then reaches a plateau indicating

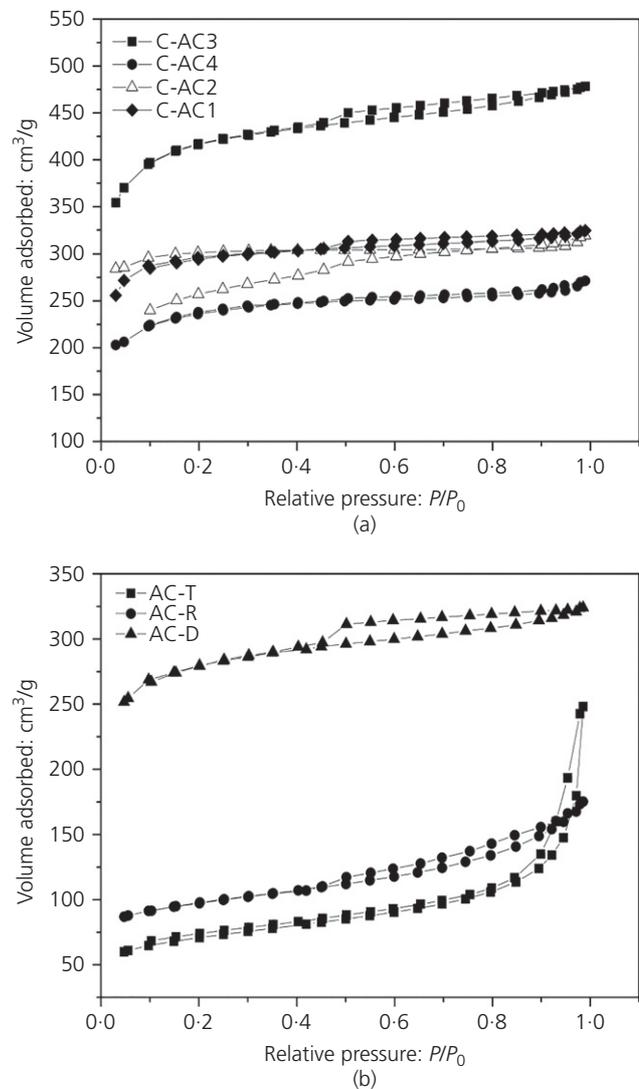


Figure 4. Nitrogen adsorption desorption isotherms for: (a) the commercial activated carbons and (b) the waste-derived activated carbons

that the amount adsorbed by a unit mass of activated carbon reaches a limiting value. Type IV isotherm exhibits a significant adsorption–desorption hysteresis loop indicating the filling and emptying of mesopores by capillary condensation. The isotherms obtained for AC-T and AC-R were more similar to type 5 isotherms (Sing *et al.*, 1985), which indicate a more mesoporous type of activated carbon. The amount of nitrogen adsorbed by activated carbons derived from waste is smaller than that of the commercial activated carbons and the knees of their isotherms are more open indicating that they contain more mesopores.

Table 4 shows the surface area, mesopore and micropore volumes of activated carbons. The development of the surface area and porosity characteristics of an activated carbon produced by pyrolysis of the waste raw material followed by steam activation of char is determined by the characteristics of the original raw materials and the process conditions of pyrolysis and activation. The commercial activated carbons had high surface areas, ranging from 558 to 988 m²/g. In the case of activated carbons produced from waste, surface areas were somewhat lower than the commercial activated carbons at 270 m²/g for the AC-T, 340 m²/g for the AC-R, but the activated carbon produced from date seeds had a high BET surface area of 867 m²/g.

In relation to the influence of the surface area and pore size characteristics of the activated carbons on NO adsorption, the BET surface area showed no clear correlation with NO removal efficiency. For example, the highest nitrogen oxide adsorption (60%) was achieved with the C-AC1 carbon which had the second highest surface area of 944 m²/g, but C-AC2 and C-AC3 had high surface areas of 912 and 988 m²/g but had very different NO adsorption efficiencies. Additionally, date seeds with a surface area of 867 m²/g showed a NO removal efficiency similar to C-AC2 and C-AC4 commercial carbons with a surface area of up to 900 m²/g. There is also

Sample	Surface area S_{BET} : m ² /g	Micropore volume V_{mic} : cm ³ /g	Mesopore volume V_{mes} : cm ³ /g
C-AC1	944	0.479	0.304
C-AC2	912	0.466	0.109
C-AC3	988	0.510	0.324
C-AC4	750	0.350	0.145
AC-T (tyre)	270	0.214	0.784
AC-R (RDF)	340	0.223	0.620
AC-D (biomass)	867	0.478	0.203

Table 4. Surface area and pore size characteristics of commercial and waste-derived activated carbons

disagreement in the literature regarding the influence of surface area and porosity on the rate of nitrogen oxide reduction on a carbon surface. Several authors (Guo *et al.*, 2001; Ruiz Machado and Hall, 1998) have considered that the rate of NO adsorption is proportional to the internal surface area of the char. However, Neathery *et al.* (1997) observed that the NO adsorption capacity of the studied activated carbons was not directly related to their surface areas and micropore volumes. The same conclusion was derived by Guo *et al.* (2001) and Ruiz Machado and Hall (1998). Other overriding factors that may influence NO adsorption over the carbon surface area are the size of the molecule being adsorbed such that the pollutant cannot enter the micropores of the carbon and the surface chemistry of the carbon which may not be conducive to nitrogen oxide adsorption (Mohan and Pittman, 2006).

The pore size characteristics (Table 4) of the commercial carbons showed that C-AC1, C-AC2, C-AC3 AC-D contained a mixture of micropores and mesopores and C-AC4 was mainly microporous and the tyre (AC-T) and RDF activated carbons (AC-R) were mainly mesoporous.

Figures 5(a) and 5(b) shows the pore size distribution of the commercial adsorbents and activated carbon produced from the wastes, respectively, as calculated by the DFT method. For the adsorbents produced in this study, analysis of pore size data presented in Table 4 and Figure 5, indicate that NO adsorption could potentially depend, on the one hand, on the origin of the carbon and, on the other hand, on the pore volume and pore size distribution. The lower removal efficiency of activated carbons produced from waste tyre and RDF compared with those of commercial carbons or date seeds is largely due to the differences in porous structure. The pores of the commercial activated carbons and biomass date seeds are mostly located in the micropore range of 1–2 nm, while the activated carbons produced from RDF and tyre have a much greater number of pores with diameters in the range of 2–10 nm, particularly many pores >4 nm. Pores of these sizes are probably unsuitable for effective NO adsorption, since the kinetic diameter of NO is 0.317 nm, suggesting microporous activated carbons would be more suitable for NO adsorption. The prevalence of mesopores in the tyre- and the RDF-derived carbons seems to reduce the efficiency of the product activated carbon to capture NO. Carbons with pore diameters of 1.1 nm have been found to have a much higher capacity than those with pore diameters larger than 1.1 nm (Neathery *et al.*, 1997).

To further study the influence of surface area and porosity on NO adsorption, one of the waste materials (waste tyre) was activated to different degrees of carbon burn off, to prepare activated carbons with different surface area and pore size

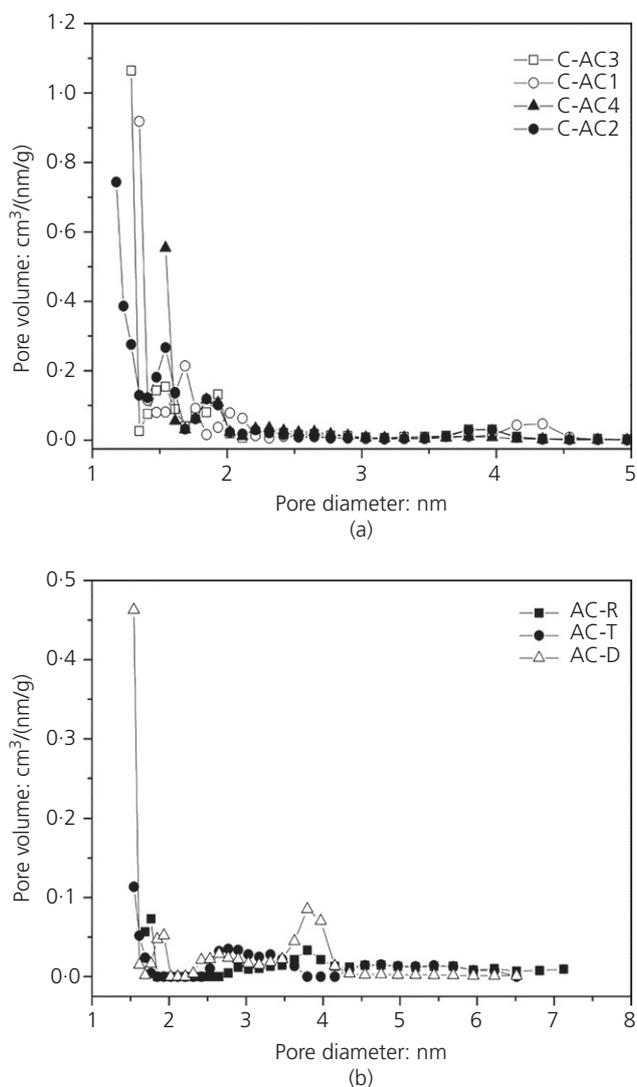


Figure 5. Pore size distribution for: (a) commercial activated carbons and (b) waste-derived activated carbons

characteristics together with the NO adsorption efficiency after 120 min of operation (Table 5). The data presented in Table 5 show that increasing the activation time led to an increase in the BET surface area (S_{BET}) and micropore volume (V_{mic}), which is accompanied by a proportional increase in NO removal. This suggests that the porous texture has a role in determining NO capture by the studied carbons. However, there appeared to be no correlation with the mesoporosity of the tyre-derived activated carbons and NO removal efficiency.

3.2.2 Acid–base properties

The surface chemistry of the product activated carbons may also influence the uptake of NO. The chemical structure of activated carbons is associated with heteroatoms (hydrogen, oxygen, nitrogen and sulfur) which are bonded at the edges of aromatic carbon sheets or to carbon atoms within the carbon matrix forming various surface functional groups which can be acidic, basic or neutral (Guo and Lua, 1999). These functional groups are responsible for the uptake of pollutants. The commercial and the waste-derived activated carbons were therefore analysed by Boehm titration to determine the concentration of basic and acidic chemical groups on the carbon surface. The results are shown in Table 6. For the commercial

Sample	pH	Basic groups: mmol/g	Acidic groups: mmol/g	Total content of surface oxides
C-AC1	9.52	1.22	0.05	1.27
C-AC2	9.20	1.17	0.13	1.29
C-AC3	9.24	0.66	0.02	0.67
C-AC4	7.58	0.69	0.00	0.68
AC-R (RDF)	10.67	2.65	0.00	2.65
AC-T (tyre)	8.11	0.51	0.30	0.82
AC-D (biomass)	7.53	0.71	0.00	0.71

Table 6. Acid and base properties of activated carbons

Sample	Activation time: min	Surface area S_{BET} : m ² /g	Mesopore volume V_{mes} : cm ³ /g	Micropore volume V_{mic} : cm ³ /g	Nitrogen oxide: %
AC-T (tyre)	45	88	0.61	0.09	9
AC-T (tyre)	90	70	0.54	0.08	7
AC-T (tyre)	180	270	0.70	0.20	23

Table 5. Influence of surface area (S_{BET}), mesopore volume (V_{mes}) and micropore volume (V_{mic}) of the tyre-derived activated carbons on nitrogen oxide removal efficiency at 120 min

carbons, the content of the basic surface groups varied in the range of 0.66–1.22 mmol/g, while for the RDF waste-derived activated carbon, the content of basic surface groups was almost double (2.65 mmol/g). The very high content of basic groups with RDF could be due to presence of the high mineral components and metal compounds found in the raw precursor material (Table 1) and also as shown by the SEM-EDXS analysis of waste-derived activated carbons (Figure 2).

Hu *et al.* (2011) and Nowicki and Pietrzak (2011) found that activated carbons with the highest content of basic groups and the lowest content of acidic groups had the highest NO_x sorption capacity. A comparison of the acidic and basic groups on the activated carbons (Table 6) with the NO removal data shown in Figure 3 showed that the commercial activated carbon with the highest basic groups C-AC-1 had the highest NO removal efficiency. C-AC1 and C-AC2 have a similar amount of basic groups but C-AC2 has a higher amount of acidic groups which could be the reason for the lower NO removal efficiency of C-AC2. The inhibitory effect of acidic groups to the nitrogen oxide adsorption capacity of carbons has been reported in the literature (Nowicki and Pietrzak, 2011). For the activated carbon produced from waste, the AC-R had the highest concentration of basic groups but showed no significant influence on NO removal compared with the other activated carbons, suggesting that other inhibitory factors related to metal content or pore structure influence nitrogen oxide adsorption for the RDF activated carbon.

3.3 Influence of temperature and nitrogen oxide concentration on nitrogen oxide adsorption

The influence of the process parameters of adsorption temperature and NO gas concentration on the adsorption of nitrogen oxide was examined for tyre- and biomass-derived activated carbons. The RDF activated carbon was not further investigated due to the high ash content of the product carbon. Table 7 shows the influence of activated carbon temperature using the NO adsorption reactor (Figure 1(c)). Adsorption experiments were carried out at temperatures of 25, 50 and 100°C and fixed NO concentration of 800 ppm and oxygen concentration of 5%. Both the tyre-derived carbon and the biomass-derived carbon showed a decrease in NO removal efficiency as the adsorption temperature was increased. At low temperature, physisorption of NO takes place on the carbon surface which means that activated carbon acts as a medium for adsorbing the reactants and not as a catalyst (chemisorption), this will lead to a decrease in NO conversion with increasing temperature. Guo *et al.* (2001) also reported a decrease in the adsorption of NO with an increase in temperature from 30 to 100°C for NO adsorption onto activated carbon fibres.

Parameter	Nitrogen oxide adsorption: %	
	AC-T (tyre)	AC-D (biomass)
Adsorption temperature: °C		
25	37	65
50	23	41
100	6	12
Nitrogen oxide concentration (ppm) (for an adsorption temperature of 25°C)		
200	27	80
400	31	77
800	35	65

Table 7. Influence of process parameters on nitrogen oxide removal efficiency at 120 min for tyre-derived (AC-T) and biomass (AC-D)-derived activated carbons

The NO removal efficiency of carbon will also depend on the nitrogen oxide concentration in the flue gas. The effect of varying the inlet flue gas nitrogen oxide concentration on the adsorption capacity of activated carbons produced from waste tyre and biomass date seeds was assessed. Experiments were carried out with NO inlet concentration of 200, 400, 800 ppm in the flue gas and with a fixed oxygen concentration of 5% at 25°C. The effect of increasing the NO concentration did not reveal the same trend for both carbons; this could be due to the difference in the surface chemistry of the adsorbents. For the date seeds, there was a substantial increase in adsorption as the NO was increased from 200 to 400 ppm and then declined at 800 ppm. In the case of waste tyre, NO removal efficiency increased with increasing NO concentration (Table 7). A similar behaviour was observed by others (Guo *et al.*, 2001; Klose and Rincón, 2007; Mochida *et al.*, 2000). For example, Guo *et al.* (2001) investigated the influence of NO concentration on NO adsorption with activated carbon and reported a 69% NO adsorption capacity at 600 ppm NO concentration, reducing to 65% at 200 ppm but reducing markedly to 40% at 50 ppm.

4. Conclusions

Adsorption of NO at low temperatures was studied using activated carbon produced from waste materials. Different commercial carbons with different porous texture and surface chemistry were used for comparison. The porous structure and surface chemistry of the studied adsorbents were analysed and compared with the nitrogen oxide removal efficiency of carbons. From the presented results and analysis, it can be concluded that the micropore size and the pore width play an important role in determining the efficiency of activated carbons for NO capture, but less so for surface

area. The differences in performance of the activated carbons could also be attributed to the influence of porous texture and surface chemistry. The waste-derived activated carbons had NO removal efficiencies of 40, 26 and 21% for the carbons derived from date seeds, RDF and waste tyres, respectively, at 50°C adsorption temperature. Commercially produced activated carbons had NO removal efficiencies of between 40 and 60%. Therefore, although the waste-derived activated carbons were somewhat less effective than commercially produced carbons they still showed a high and effective level of NO removal. In addition, the use of waste materials for the minimisation of a problematic pollutant is a novel reuse of resources.

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