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9 **TRANSFERABILITY OF CAR-FOLLOWING MODELS BETWEEN DRIVING**
10 **SIMULATOR AND FIELD TRAFFIC**
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1

1 **ABSTRACT**
2
3 Over the last few decades, there have been two parallel streams of driving behaviour research:
4 models using trajectory data collected from the field (using video recordings, GPS, etc.) and
5 models using data from the driving simulators (where the behaviours of the drivers are recorded in
6 controlled laboratory conditions). While the former source of data is more realistic, it lacks
7 information about the driver and is typically not suitable for testing effects of future vehicle
8 technologies and traffic scenarios. On the other hand, driving behaviour models developed using
9 driving simulator data may lack behavioral realism. However, there has not been any previous
10 study which compares these two different streams of mathematical models and investigates the
11 transferability of the models developed using driving simulator data to real field conditions in a
12 rigorous manner. The present paper aims to fill in this research gap by investigating the
13 transferability of the car-following models between a driving simulator and two comparable
14 real-life traffic motorway scenarios, one from the UK and the other one from the US. In this
15 regard, stimulus-response based car-following models have been developed using three different
16 microscopic data sources: (i) experimental data collected from the University of Leeds Driving
17 Simulator (UoLDS), (ii) detailed trajectory data collected from Motorway 1 (M1), UK and (iii)
18 detailed trajectory data collected from Interstate 80 (I-80), CA, USA. The parameters of these
19 car-following models are estimated using the Maximum Likelihood Estimation technique and
20 transferability of the models are investigated using statistical tests of parameter equivalence and
21 Transferability Test Statistics. Estimation results indicate transferability in the model level but not
22 fully in the parameter level for both pairs of scenarios.
23
24 *Keywords: Car-following, NGSIM, Driving Simulator, Validation, Transferability*

1   **1. BACKGROUND**

2   Road safety continues to be an important issue with road crashes among the leading causes of
3   death - accounting for more than 1.2 million fatalities and 50 million injuries globally each year
4   *(1)*. Driver behaviour is a factor in over 90 percent of crashes, with speeding as one of the major
5   contributors *(1)*. Driving behaviour models, which provide mathematical representations of how
6   the drivers make decisions involving acceleration-deceleration, lane-changing, overtaking, etc.,
7   are increasingly being used for evaluation and prediction of road safety parameters and
8   formulating remedial measures. Reliable driving behaviour models are also critical for accurate
9   prediction of congestion levels in microscopic traffic simulation tools *(2)* and analyses of
10   emissions *(3)*. Moreover, driving behavior models have significantly contributed to the
11   development and deployment of different Intelligent Transportation Systems (ITS) measures *(4),*
12   *(5)*.
13   Microscopic driving behaviour models are typically developed using two types of data, (a) driving
14   simulator data (where participant drivers drive an instrumented vehicle in a simulated roadway)
15   and (b) real traffic data. Data from the driving simulators are collected following standardized
16   procedures and are more controllable and reproducible. Further, driving simulators allow
17   researchers to manipulate the surrounding conditions (e.g. geometric layout of the road, number
18   and type of vehicles, weather and pavement conditions and so on) as well as driver specific
19   conditions (e.g. level of distraction and fatigue) and run various hypothetical scenarios. However,
20   there is scepticism regarding the simulator fidelity (physical and behavioural) of how well the
21   driver's behaviour in simulator match with his/her behaviour in real roads *(6)*. On the other hand,
22   the real traffic data best represent the true driving behaviour, but have several limitations:
23   measurement errors, complex confounding of influencing factors, less control on the external
24   factors, and absence of driver characteristics to name a few. Given the difference in the nature of
25   the two data sources, it is of paramount importance to investigate the transferability of the model
26   parameters between the driving simulator and the real traffic. It may be noted that in addition to
27   these two sources, naturalistic driving data collected using instrumented vehicles (e.g UDRIVE
28   *(7)*, SHRP2 *(8)* etc.) have also been used in research, but given the high costs involved, the
29   availability of these data are still very limited. Moreover, similar to the driving simulator data, the
30   naturalistic data are likely to be prone to behavioural incongruence; and similar to the field data,
31   the external variables are often not fully controllable and it is not possible to test the effects of
32   hypothetical scenarios.
33   There have been several previous researches on validation of driving behaviour observed in the
34   driving simulator using isolated measures (e.g. speed, acceleration, reaction time, etc.). For
35   instance, Törnros *(9)* attempted to validate driver's behaviour in terms of speed and lateral position
36   in a simulated road tunnel. The results have shown that (i) behavioural validity in absolute terms is
37   not satisfactory, especially referring to speed choice, while (ii) relative validity is achieved in both
38   parameters. Godley et al. *(10)* conducted two different experiments in an instrumented car and a
39   driving simulator comparing speed measurements. In both cases, the test roadway contained
40   transverse rumble stripes at three locations and three additional control points (without rumble
41   strips). The results again have demonstrated relative validity indicating that drivers decelerate in a
42   similar pattern in the rumble strips, but have shown that drivers tend to drive faster in the real-life
43   case than in the simulator and have hence failed to demonstrate absolute validity. Bella et al. *(11)*
44   conducted a simulator validation study comparing drivers' speeds, in a deceleration lane and also
45   found though relative validity was satisfactory in all scenarios, the differences in the mean speeds
46   were significantly high in the simulator in non-demanding configurations (e.g. in presence of
47   curves with large radius). This was assumed to stem from the different risk perception on the

1   simulated road as opposed to the real road. A similar study conducted from Yan et al. *(12)*,
2   simulated a real signalized intersection, comparing drivers' speed behaviours in both cases.
3   Comparisons of the surrogate safety measures from the simulator with the crash analyses for the
4   field data have demonstrated relative validity. Further, the results illustrated that both the observed
5   and simulated speed data followed normal distributions with equal means for each intersection
6   approach - which validated the driving simulator in absolute terms as well. In addition, McGehee
7   et al. *(13)* investigated the validity of the simulator using drivers' reactions and performances in an
8   intersection scenario by conducting a series of experiments in Iowa Driving Simulator and a
9   similar field scenario and showed the statistical equivalence of the driver's reaction times between
10   the real-life and simulation cases. A validation study by Engen *(14)* used three different datasets
11   from (a) driving simulator, (b) an instrumented vehicle and (c) and road side monitoring and
12   compared data in terms of reaction times, speeds and lateral positions and time gaps. The findings
13   have shown that the outputs from the simulator have less variance compared to field traffic. A
14   recent study of Risto and Martens *(15)* compared drivers' choices in terms of headway while
15   driving a driving simulator and an instrumented vehicle. Both experiments were conducted on
16   same participants and the results have demonstrated significant similarity in speeds and headways
17   in two cases. Another validation study conducted by Lee *(6)* analysed the behaviour of older
18   drivers in driving simulator and on-road experiments and found significant positive association
19   between the two driving performance indices (developed using principal component analyses) and
20   after adjustment for age and gender of the drivers, was able to explain over two-thirds of the
21   variability of the on-road driving performance indices.
22   Majority of the validation studies thus confirm relative validity, though the findings regarding the
23   absolute validity are mixed. This raises the question whether or not the mathematical models of
24   driving behaviour are transferable between the two settings. To the best of our knowledge, there
25   has not been any previous research that examines the transferability of the parameters of a
26   mathematical model of driving behaviour between a driving simulator and a similar filed traffic
27   condition. This paper aims to fill in this critical research gap.
28   The objective of this paper is to investigate the transferability of the car-following models between
29   a driving simulator and real traffic scenarios. In this regard, a state-of-the-art car-following model
30   is re-estimated using two sets of microscopic traffic data extracted from video recordings of real
31   traffic: one from the UK and the other one from the US (referred as Field Model UK and Field
32   Model US respectively) and trajectory data from a comparable scenario in the driving simulator
33   (referred as Sim Model). The performances of the models have been examined independently by
34   using informal tests (i.e. signs and values of the parameter estimates) and formal tests of statistical
35   differences (e.g. t-tests of parameter equality *(16)* and Transferability Test Statistic *(17)*).
36   The remainder of this paper is organized as follows: Section 2 focuses on the datasets, Section 3
37   outlines the details of the model structure, Section 4 presents the estimation results of the proposed
38   models and Section 5 focuses on the transferability analyses. Finally, Section 6 summarizes the
39   conclusions and suggests future research actions.
40
41   **2. DATA**

42   The following three secondary datasets have been used in this research:
43   • Driving simulator data of a UK Motorway scenario
44   • Video data from a segment of Motorway 1 (M1), UK
45   • Video data are from a segment of US101, USA

1   The descriptions of the study areas and the datasets are presented below followed by a critical comparison
2   which highlights their similarities and differences.
3
4   **2.1 Study Area**
5
6   2.1.1   Driving Simulator Data

7   The simulator data has been derived from an experimental study in the University of Leeds
8   Driving Simulator (UoLDS), one of the most advanced driving simulators in Europe. UoLDS has a
9   Jaguar S-type vehicle cab (see Figure 1a) with all driver controls fully operational. The vehicle's
10   internal Control Area Network (CAN) is used to transmit driver control information between the
11   Jaguar and a network of nine high performance computers that manages the complete simulation.
12   Control feedback is generated so that the driver seated in the cab feels (steering and pedal loading),
13   sees (dashboard instrumentation) and hears (engine, transmission and environmental noise) an
14   appropriate simulation of the driving environment (Figure 1b). The simulator incorporates an eight
15   degree-of-freedom motion system. A hexapod motion platform, carrying the 2.5t payload of the
16   dome and vehicle cab combination allows limited motion in all six orthogonal degrees-of-freedom
17   of the Cartesian inertial frame. Additionally, the platform is mounted on a railed sled that allows a
18   further 5m of effective travel in sway and surge. These aim to reduce, while not fully eliminate,
19   differences between real world and simulator driving behaviour *(18)*.
20

21
22   a. Simulator Experience   b. Motorway
23
24   **FIGURE 1:** Sample of driving Scenarios in UoLDS *(18)*
25
26   The experiment included forty participants (20 females, 20 males) aged between 19 to 83 years.
27   Each participant had to drive approximately 30-40 minutes on a road section of 2,000 meters (see
28   following Fig. 2). The participants were instructed to drive the simulator vehicle cab as if it were in
29   a real-life vehicle, obeying the specific speed limits and all legal regulations. The full simulator
30   study, performed as part of the Smart Motorway Project of the UK Highways Agency *(19)*,
31   included driving decisions in presence of lane closures and roadwork, but in order to preserve
32   similarity with the field scenario (described in 2.1.2), only part of the data that had no disruption,
33   similar network topography and traffic flow levels as the field data has been used in this study.
34   Since, the focus of the study is on car-following behavior, the lanes affected by road closure
35   (which are likely to have more lane changes) are excluded and only data from the two rightmost
36   lanes have been retained for the model development. The full road network of the driving
37   simulator study and the selected segment are presented in Figure 2.
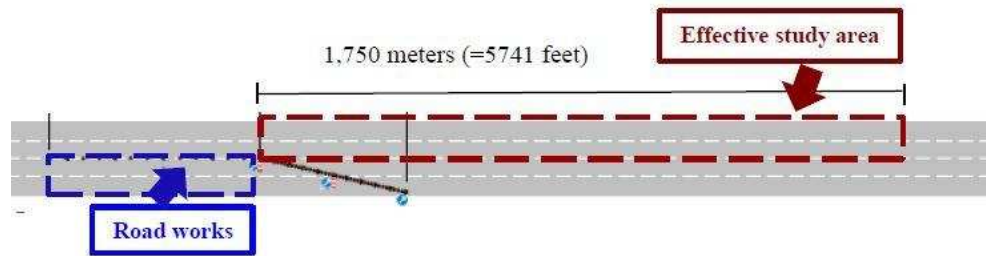
1
2 **FIGURE 2:** Schematic of road section, which was used in UoLDS experimental study
3 (Source: figure adopted from Highways Agency, UK *(19)*)
4
5 2.1.2 Field Data UK

6 The disgggregate vehicle trajectory data collected between J42-J43 of the M1 motorway network in
7 the UK has been used as the first source of field data. The data was collected in May 2013 from an
8 over-bridge located 620m downstream from J42 and the trajectory data was extracted using a
9 semi-automated vehicle trajectory extractor application by Lee et al. *(20)*. Due to the camera angle
10 and features of the trajectory extraction software, only data from the first 320m was found to be
11 usable. The details of the data collection and processing have been reported by Kusuma et al. *(21)*.
12 The road section constitutes of five traffic lanes (Figure 3). Since, the focus of this research is on
13 car-following behaviour, the lanes that have the lowest number of lane changes (lanes 4 and 5)
14 have been used in this research.
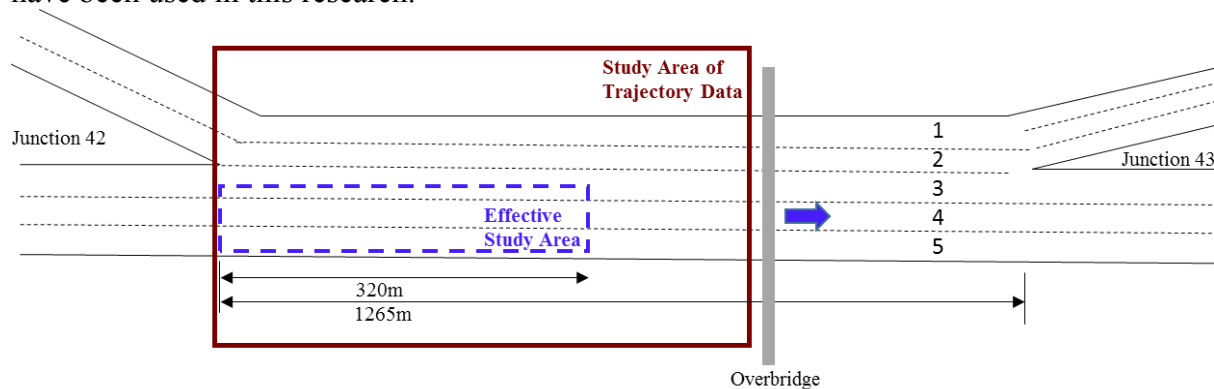
15
16 **FIGURE 3:** Estimation data collection site at the M1 motorway
17 (Source: figure adopted from Kusuma et al. *(21)*)
18
19 2.1.3 Field Data US

20 The diaggregate vehicle trajectory data collected from the eastbound direction of Interstate 80
21 (I-80) in Emeryville, California, USA as part of the Next Generation Simulation (NGSIM)
22 program has been used as the field data. The data was collected in April 2005 using seven
23 synchronized digital video cameras set on top of tall buildings and covering a road length of
24 approximately 500 meters (1640 feet). Detailed coordinates of individual vehicles have been
25 extracted using the customized software NG-VIDEO at a 0.1 second time resolution *(20)*.
26 The original road section constitutes of six traffic lanes including a high-occupancy vehicle (HOV)
27 lane (Figure 4). Since, the focus of this research is on car-following behaviour, the lanes that have
28 the lowest number of lane changes (lanes 3 and 4) have been used in this research. Further, since

1   maximum similarity with the driving simulator scenario is a critical element of this research, data
2   between 5:15-5:30 pm, when the average flow rates were similar, have been used in the study. The
3   explanatory variables used in the model estimation are created by VISUAL BASIC scripts (full
4   details available in Papadimitriou2015) *(23).*
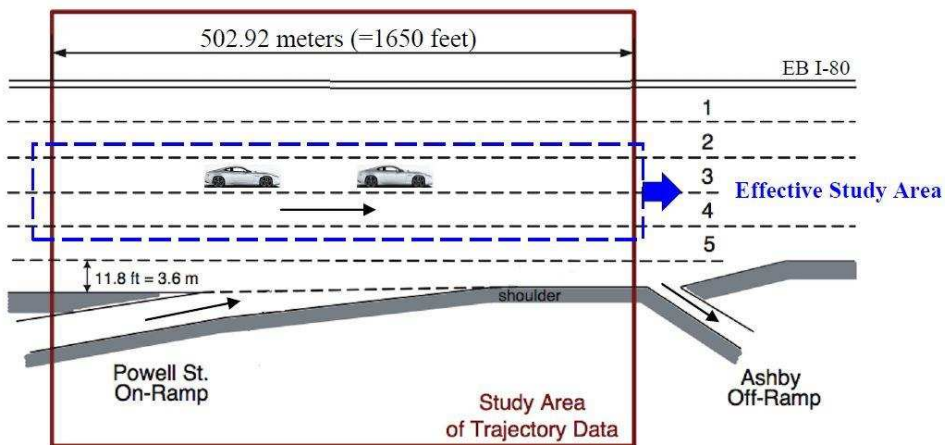
5

6   **FIGURE 4:** Estimation data collection site at the I-80 motorway
7   (Source: figure adopted from Choudhury et al. *(24)*)

8
9   **2.2 Comparison**

10   Though a conscious effort has been made to maximize the similarity between the simulator and the
11   field datasets, since they are all secondary datasets, there are some differences. It may be noted that
12   even in a primary data collection using the driving simulator, even though the traffic flow rates and
13   the behavior of the ambient traffic are controllable, since the speeds and accelerations are driven
14   by the decisions taken by the participant, the observed speed and acceleration distributions are not
15   fully controllable.
16   The key aggregate characteristics of the three datasets are presented in Table 1. Figure 5 presents
17   the comparison between the distributions of the key variables in the three datasets.
18   As seen in Table 1 and Figure 5, the average speeds of the drivers are higher in the UoLDS data
19   compared to the Field Data US. This is not unusual since in the simulator environment, though the
20   participants have been instructed to drive as they would do in real roads, there is no actual risk of
21   potential injury. This may encourage the driver to drive aggressively. It may be noted though that
22   the difference was found to be much smaller between the UoLDS data and the Field Data UK.
23   Moreover, though the mean acceleration/deceleration levels in all three datasets had similarity, the
24   driving simulator data revealed a larger clustering around the mean value. This is not unexpected
25   given the much smaller number of drivers in the Sim Data. In all three datasets, accelerations close
26   to 0 was found to have higher proportions (see Table 1 and Figure 5).
27   Concerning the distribution of the time headway, the UoLDS and the Field Data UK had flatter
28   distributions compared to the Field Data US, but values from 2 sec to 4 sec appeared to be the most
29   frequent in all three data sets (see Figure 5). It may be noted that in all three datasets, time headway
30   values have been restricted to the upper bound (=5 sec) due to adopted definition of the
31   car-following regime. Overall, though the three datasets had significant similarities in terms of
32   geometry and flow levels, the speeds, accelerations and headways had significant variations.

1 **TABLE 1:** Summary of aggregate characteristics

	Sim Data	Field Data UK	Field Data US
Survey year	2014	2013	2005
Source	University of Leeds	University of Leeds	NGSIM, FHWA
Road category	Motorway	Motorway	Motorway
Survey duration (min)	≈ 30-35 minutes of driving for each participant	15 minutes (17:15-17:30)	15 minutes (17:00-17:15)
Luminance conditions	Daytime	Daytime	Daytime
Pavement conditions	Dry	Dry	Dry
Number of vehicles	40	527	598
Number of observations	116,644	6,836	379,397
Time resolution (sec)	0.17	1.00	0.10
Length of road section (m)	1,750	320	502.92
Traffic flow (veh/h/lane)	1,700	1,500	1,600
Comments	2 out of 4 traffic lanes seperated roadwork parts seperated and removed (see Fig. 2)	2 out of 5 traffic lanes seperated (see Fig. 3)	2 out of 6 traffic lanes seperated (see Fig. 4)

Variables

|	Maximum	Minimum	Mean	Median	Std. Dev.	Maximum	Minimum	Mean	Median	Std. Dev.	Maximum	Minimum	Mean	Median	Std. Dev.
Acceleration (m/s/s)	2.04	-5.52	0.00	-0.01	0.29	6.96	-6.97	-0.70	-0.55	1.40	3.41	-3.41	-0.03	0.00	1.34
Subject speed (m/s)	39.18	18.99	29.72	30.36	3.08	50.36	11.35	26.93	26.08	5.65	29.05	0.13	5.00	4.58	2.08
Front vehicle speed (m/s)	40.57	18.71	29.67	30.10	3.95	50.36	11.35	25.87	68.48	4.36	29.05	0.02	4.84	4.57	2.21
Time headway (sec)	5.00	0.00	2.69	2.64	1.14	5.00	0.02	2.30	2.22	0.03	5.00	0.00	3.07	3.02	0.96
Space headway (m)	190.97	0.00	80.18	77.71	35.18	129.91	3.24	51.25	43.43	29.04	60.00	0.00	14.22	13.10	5.61

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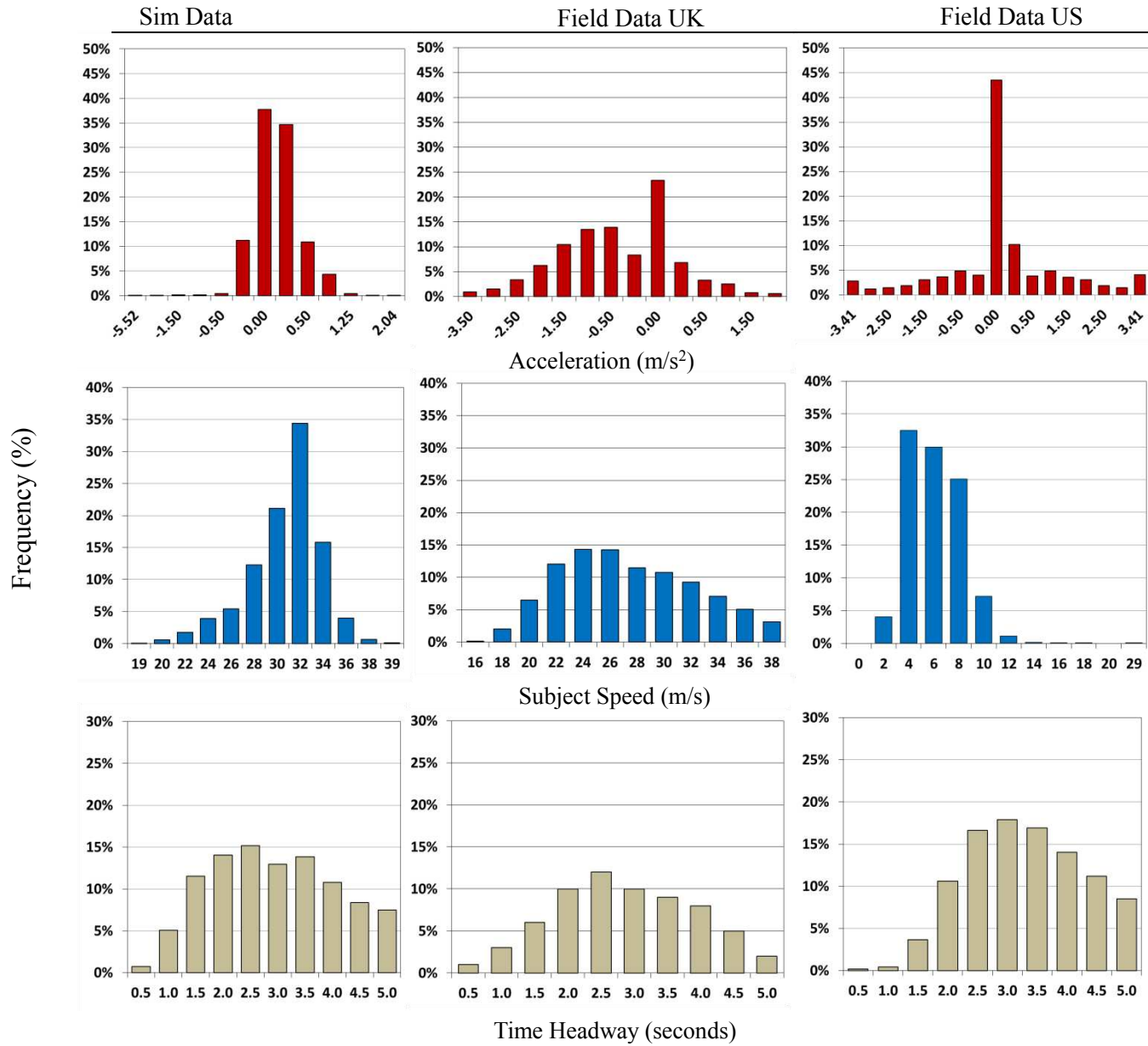
FIGURE 5: Distribution of key variables in three datasets

1 **3. METHODOLOGY**

2 This section covers the details of the model structure, the likelihood function used for estimation
3 and the transferability tests used in this study.
4
5 **3.1 Model Structure**
6
7 The longitudinal movement decisions of the driver tend to vary significantly depending on the
8 headway with the front vehicle. The acceleration models therefore typically have 2 states:
9
10   (a) car-following regime (constrained driving conditions)
11   (b) free-flow regime (unconstrained driving conditions)
12 The model structure used in this study is derived from Ahmed's study *(25)*, which was practically
13 an extension of the earlier stimulus-response studies such as Subramanian's *(26)* and Gazis et al.
14 *(27)*. In the stimulus-reponse framework, the subject driver accelerates/decelerates in response to
15 the stimulus (generally the speed difference) of the vehicle in the front (leader). The sensitivity
16 towards this stimulus can vary among the drivers and for the same driver on different situations.
17 Due to reaction time (typically between 0.5 to 3 seconds), there is a time lag between the stimulus
18 and the observed actions (accelerations/ decelerations). Ahmed's *(25)* model extended this basic
19 model by making it more flexible by assuming non-linear functions for the sensitivity function.
20 The stimulus part is typically a function related to the leader's relative speed (see Equation 1):
21

22     $\Delta V_n (t) = V_n^{Leader}(t) - V_n (t)$ (1)

23   Where,

24     $\Delta V_n (t)$ = Relative speed of driver n with respect to the leader at time t;

25     $V_n^{Leader}(t)$ = Speed of the lead vehicle of driver n at the time t;

26     $V_n (t)$ = Speed of driver n at the time t.

27 Further, the stimulus component can have two variations (i) when the speed difference between the
28 leader and the subject driver is positive, which essentially means that the leader drives faster than
29 the follower and (ii) when the difference is negative, which means that the follower drives faster
30 than the leader. The first case refers to acceleration conditions, whereas the second to deceleration.
31
32   The overall car-following acceleration is given by:

33     $a_n(t) = \begin{cases} a_n^{cf,acc}(t), \text{if } V_n (t - \tau_n) \geq 0 \\ a_n^{cf,dec}(t), \text{otherwise} \end{cases}$ (2)

34
35 However, it should be clarified that the correspondence to positive and negative stimuli may be
36 different for the simple reason that these two situations are fundamentally different and expected to
37 trigger different behavioural responses. The acceleration decisions, which are triggered by a
38 positive leader relative speed, is likely to be caused by speed advantage reasons and by
39 'herd-effect' (i.e. when people tend to adopt their behaviors or actions according to the others).
40 Deceleration decisions on the other hand are likely to be prompted by safety considerations. In
41 order to capture the aforementioned situations, the coefficients of explanatory variables of the
42 model can be positive or negative according to each stimuli.

1 The sensitivity part is a function related to the explanatory variables such as subject vehicle speed,
2 space and time headway, relative speed, etc.
3 The general formulation can be expressed as follows:

4 $$a_n^j(t) = s^j \left[X_n^j(t) \right] k^j \left[\Delta V_n(t - \tau_n) \right] + \varepsilon_n^j(t) \quad j \in \{acc, dec\}$$ (3)

5 Where,

6 $s^j[.] =$ sensitivity function;

7 $X_n^j(t) =$ explanatory variables affecting the sensitivity of the driver n at observed time t;

8 $k^j[.] =$ stimulus function;

9 $\varepsilon_n^j(t) =$ random error term of driver n at time t;

10 $\varepsilon_n^j(t) \sim N(0, \sigma_j^2)$, that is, the random error is assumed to be distributed normally.
11
12 The model assumes that the correlations between acceleration decisions from the same driver over
13 time are captured only by the reaction time. The observations of the same driver are therefore
14 independent conditional on the reaction time. Under this assumption, the probability density
15 function of the car-following acceleration and car-following deceleration are given by:

16 $$f\left(a_n^j(t) \mid \tau_n\right) = \frac{1}{\sigma_j} \phi\left(\frac{a_n^j(t) - s^j\left[X_n^j(t) \right] k^j\left[\Delta V_n(t - \tau_n) \right]}{\sigma_j} \right)$$ (4)

17 The distribution of the combined car-following model is given by:

18 $$f\left(a_n(t) \mid \tau_n\right) = f\left(a_n^{acc}(t) \mid \tau_n\right)^{V_n(t-\tau_n) \geq 0} f\left(a_n^{dec}(t) \mid \tau_n\right)^{V_n(t-\tau_n) < 0}$$ (5)

19 The trajectory data constitutes as series of acceleration decisions of the same driver. The
20 acceleration profile of the driver can be expressed as follows:

21 $$f(a_n(1), a_n(2), a_n(3)...., a_n(\tau_n) \mid \tau_n) = \prod_1^{T_n} f(a_n(t) \mid \tau_n)$$ (6)

22 Where, T_n is the number of observations of driver n. Assuming the observations of different drivers
23 are independent, the log-likelihood function (conditional on reaction time) is presented by
24 Equation (5).
25

26 $$LL = \int_{\tau_n} \sum_{n=1}^{N} \ln\left[f(a_n(1), a_n(2), a_n(3)...., a_n(\tau_n)) \right]$$ (7)

27   The unconditional likelihoods can be derived by integrating the function over the reaction
28 time distribution and the model parameters can be derived by maximizing this likelihood function.
29
30 **3.2 Evaluating Models Performance and Transferability**

31 Review of literature revealed several formal statistical tests of transferability *(28)* among which
32 the *t-tests of individual parameter equality* and *Transferability Test Statistic* (TTS) have been
33 found to be most widely used and selected for this study.

1 The t-tests of individual parameter equality compares the individual pairs of coefficients by testing
2 the t-stat for absolute difference between the parameter estimates of equivalent variables between
3 the two models (e.g. of Galbraith and Hensher's study, *(16)*). The t-stat differences can be
4 expressed as follows:

5
$$t_{\text{diff},k} = \frac{\hat{\beta}_{\text{trans},k} - \hat{\beta}_{\text{appl},k}}{\sqrt{(\frac{\hat{\beta}_{\text{trans},k}}{t_{\text{trans},k}})^2 + (\frac{\hat{\beta}_{\text{appl},k}}{t_{\text{appl},k}})^2}}$$
(8)

6 Where,

7 $\hat{\beta}_{\text{trans},k}$ and $\hat{\beta}_{\text{appl},k}$ = estimates for the k-th parameter in the transferred and application models;

8 $t_{\text{trans},k}$ and $t_{\text{appl},k}$ = the respective t-stat. ratios of the parameter estimates;

9 $t_{\text{diff},k}$ = t-stat. ratio for the difference between parameters. At 95% level of confidence, the model
10 parameters are classified to be statistically different (i.e. non-equal) if t $_{diff,\,k}$ > 1.96.
11
12 The Transferability Test Statistic (TTS) (Atherton and Ben-Akiva's study, *(17)*) refers when the
13 transferred model is statistically equivalent to the applicable (estimated) model in the application
14 context, is rejected or not. The respective formula is presented below:
15

16
$$\text{TTS}_{\text{appl}}(\hat{\beta}_{\text{trans}}) = -2(\text{LL}_{\text{appl}}(\hat{\beta}_{\text{trans}}) - \text{LL}_{\text{appl}}(\hat{\beta}_{\text{appl}}))$$
(9)

17 Where,

18 $\text{LL}_{\text{appl}}(\hat{\beta}_{\text{trans}})$ = log-likelihood on the application context data using transferred context
19 parameters;

20 $\text{LL}_{\text{appl}}(\hat{\beta}_{\text{appl}})$ = log-likelihood on the application context data using application context
21 parameters;

22 $\text{TTS}_{\text{appl}}(\hat{\beta}_{\text{trans}})$ = transferability test statistic of the transferred model in application context.
23
24 The TTS value follows a chi-squared (χ^2) distribution with degrees of freedom (dof) equal to the
25 number of parameters. At 95% level of confidence, the models are classified to be statistically
26 different (i.e. non-transferable) if $\chi^2 > \chi^2_{\text{critical}}$ *(17)*.
27
28 **4. RESULTS**

29 The development of the models aimed to achieve three key objectives,
30   (i)   A logical structure
31   (ii)   Rational signs of model parameters according to the stimulus-response concept and
32   (iii)   Best goodness-of-fit and statistically significant model parameters.

1   The OX Metrics econometric package *(29)* was used for the estimation of the acceleration model
2   parameters. The explanatory variables were statistically checked, both individually (e.g. standard
3   errors and t-stat values) and according to its correlation with the other explanatory variables (e.g.
4   covariance matrices). The critical time headway (differentiating between car-following and
5   free-flow) has been selected to be 5 seconds in line with previous studies on motorway scenarios
6   *(25)*.
7   According to the literature, reaction time ranges from a minimum value of 0.5 seconds to a
8   maximum value of 2.5 seconds *(25-40)*. Models have been estimated using different reaction times
9   within this range and reaction time equal to 0.5 seconds has been selected for both cases based on
10   goodness of fit values.
11   Adjusted Rho Square ($\overline{\rho^2}$) measures the fraction of an initial log-likelihood value explained by the
12   final model taking into account the model complexity (i.e. discounting for the additional
13   parameters). The formula is defined as follows:
14

15   $$\overline{\rho^2} = 1 - \frac{LL(\beta^*) - k}{LL(0)}$$ (10)

16   Where, $LL(\beta^*)$ is the maximum log-likelihood value $LL(0)$ is the maximum log-likelihood value
17   and *k* is the number of estimated parameters.
18
19   The final estimation results are presented in Table 2.
20
21   **TABLE 2**: Estimation Results

Car-following acceleration

Variable	Sim Model		Field Model UK		Field Model US		t-stat. diff* (absolute values)	
	Parameter	t-stat.	Parameter	t-stat.	Parameter	t-stat.	Sim Model & Field Model UK	Sim Model & Field Model US
Constant	0.247	10.46	0.039	10.77	0.154	5.80	8.70	2.62
Relative speed (m/s)	0.226	3.86	3.266	20.35	3.989	28.54	17.79	24.83
Time headway (sec)	0.012	0.29	0.028	1.17	1.348	6.18	0.36	6.03
Sigma	0.152	38.56	0.024	24.79	0.233	24.60	31.62	7.84

Car-following deceleration

Variable	Sim Model		Field Model UK		Field Model US		t-stat. diff* (absolute values)	
	Parameter	t-stat.	Parameter	t-stat.	Parameter	t-stat.	Sim Model & Field Model UK	Sim Model & Field Model US
Constant	-0.218	-12.39	-0.145	-11.85	-3.722	-1.65	3.41	1.55
Relative speed (m/s)	0.327	4.50	1.984	48.42	11.098	28.54	19.86	27.23
Time headway (sec)	0.054	2.04	0.089	13.82	1.463	6.41	1.28	6.13
Sigma	0.127	44.36	0.024	25.38	0.227	54.60	34.07	19.95

22   *t-tests of individual parameter equivalence (Galbraith and Hensher, 1982)
23   It may be noted that a couple of additional variables have also been tested but not included in the
24   final models. These include the current and lagged speed and acceleration of the driver, the type of
25   the front vehicle, the type of the subject vehicle type and traffic density. The coefficients of these
26   variables were found to be non-intuitive and insignificant.

4.1 Estimation Results of the Sim Model (Driving simulator data)

The car-following acceleration model estimated using the driving simulator data is defined as follows:

$$a_n^{cf,acc}(t) = 0.247 \frac{1}{\Delta T_n(t)^{0.012}} \left| \Delta V(t-\tau_n) \right|^{0.226} + \varepsilon_n^{cf,acc}(t) \tag{11}$$

$$\varepsilon_n^{cf,acc}(t) \approx N(0,(0.152)^2)$$

Where,

t = current time period;

τ_n = reaction time for driver n;

$a_n(t)$ = acceleration for driver n at time t;

$\Delta T_n(t)$ = time headway at time t (sec);

$|\Delta V(t-\tau_n)|$ = absolute value of relative speed between subject and leader vehicle at time t

Whereas, the estimated car-following deceleration model is:

$$a_n^{cf,dec}(t) = -0.218 \frac{1}{\Delta T_n(t)^{0.054}} \left| \Delta V(t-\tau_n) \right|^{0.327} + \varepsilon_n^{cf,dec}(t) \tag{12}$$

$$\varepsilon_n^{cf,dec}(t) \approx N(0,(0.127)^2)$$

As can be seen in Table 2 and equations (11) and (12), all estimated coefficients of the Sim model have the expected signs and magnitudes. Concerning the stimulus term of the car-following regime, it increases with relative speed hence as expected and the sign is positive in both cases of acceleration and deceleration models (referring to a positive correlation between the relative speed and the magnitude of acceleration that the driver applies).
In the sensitivity component, the signs of the constant parameters are positive for acceleration and negative for deceleration as expected. Apart from this, both constant parameters have similar magnitudes showing similarity in acceleration and deceleration ranges if all else are equal.
Regarding, the time headway, as expected, the drivers tend to be less sensitive to the same stimulus as the time headway gets larger. On the other hand, in deceleration model, it can be concluded that drivers tend to decelerate more to the same stimulus when the time headway reduces. That could be logically justified for the reason that drivers' safety concerns grow when the time headway decreases, by making them to decelerate so as to obtain again a safe headway from leader vehicle.
Most of the parameters are significant at 95% level of confidence, except for time headway. This t-stat. value of this variable is equal to 0.26 and this may be related to low time headway variability in driving simulator data (see Figure 5). This has however been retained for comparison purposes since the time headway was found to be a statistically significant variable in the Field Model US.
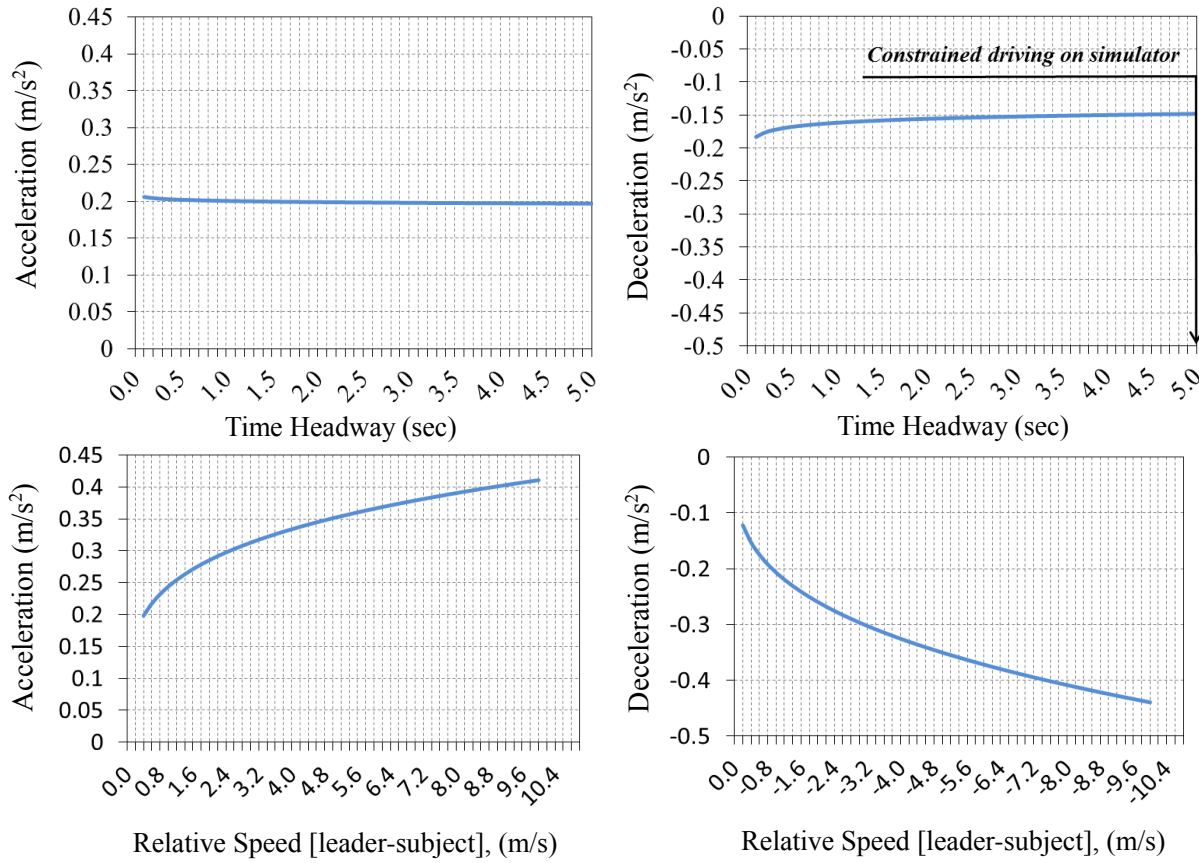
FIGURE 6: Sensitivity of different variables in car-following acceleration and deceleration models according to the Sim Model

Figure 6 presents the sensitivity analysis showing the performance of variables in both acceleration and deceleration models. The default values set assumed to be: the relative speed equal to 0.5 or (-0.5) m/s and time headway equal to 2.7 sec. These numbers have been derived from mean values of driving simulator sample.

According to the sensitivity analysis it is apparent that the mean acceleration (deceleration) is not substantially affected in magnitude by time headway. On the contrary, relative speeds have larger impacts on acceleration-deceleration magnitudes.

4.2 Estimation Results of the Field Model UK (Real Traffic Data from M1, UK)

The car-following acceleration model estimated using field data from the UK is as follows:

$$a_n^{cf,acc}(t) = 0.039 \frac{1}{\Delta T_n(t)^{0.028}} \left| \Delta V(t - \tau_n) \right|^{3.266} + \varepsilon_n^{cf,acc}(t) \tag{13}$$

$$\varepsilon_n^{cf,acc}(t) \approx N(0, (0.024)^2)$$

Where,

t = current time period;

1   τ_n = reaction time for driver n;

2    $a_n(t)$ = acceleration for driver n at time t;

3    $\Delta T_n(t)$ = time headway at time t (sec);

4    $|\Delta V(t - \tau_n)|$ = absolute value of relative speed between subject and leader vehicle at time t

5

6   Whereas, the estimated car-following deceleration model is as follows:

7

8    $$a_n^{cf,dec}(t) = -0.145 \frac{1}{\Delta T_n(t)^{0.089}} |\Delta V(t - \tau_n)|^{1.984} + \varepsilon_n^{cf,dec}(t) \qquad (14)$$

9

10   $$\varepsilon_n^{cf,dec}(t) \approx N(0,(0.024)^2)$$

11

12   Similar to the Sim Model, signs of all parameters of the Field Model UK have the expected logical
13   signs. Further, all model parameters are statistically significant at 95% level of confidence apart
14   from the coefficient of time headway which was insignificant also in the Sim Model. However, the
15   parameter has been retained as the sign is intuitive and the corresponding parameter has been
16   found to be statisitically significant in the Field Model US.
17   Regarding the stimulus part of the model, both car-following acceleration and decelerations
18   increase with relative speeds. It may be noted that these parameters are much larger in magnitude
19   compared to the Sim Model parameters. The behavioural incongruence while driving the driving
20   simulator can be a potential reason for this.
21   In the sensitivity component, the time headway parameters have expected positive signs. This
22   referes that the drivers tend to accelerate less as the time headway with the leader increases. On the
23   other hand, in the deceleration model, it can be concluded that as the time headway decreases, the
24   drivers tend to decelerate more to the same stimulus, due to safety concerns in order to avoid a
25   potential collision and finally obtain again a safe headway from the leader vehicle. The time
26   headway parameter is slightly larger for deceleration compared to acceleration as expected since
27   acceleration only leads to speed advantage whereas, deceleration is prompted by collision
28   avoidance (safety). It may be noted that the similar trend has been observed for Sim Model as well.
29   The following Figure 6 shows the sensitivity analysis, presenting the performance of the models.
30   The default values set assumed to be: relative speed = 0.7 or (-0.7) m/s and time headway equal to
31   2.3 sec. These numbers derived from the corresponding mean values in the sample dataset. An
32   attempt has been made to keep the sensitivity analysis in low values of acceleration-deceleration,
33   so as to highlight the drivers' behaviours under these crucial and sensitive constrained traffic
34   conditions.
35   According to Figure 7. the drivers are extremely sensitive to the changes in the relative speed, both
36   for the acceleration and for deceleration compared to the Sim Model. The effect of the time
37   headway variable however is more similar to that of the driving simulator.
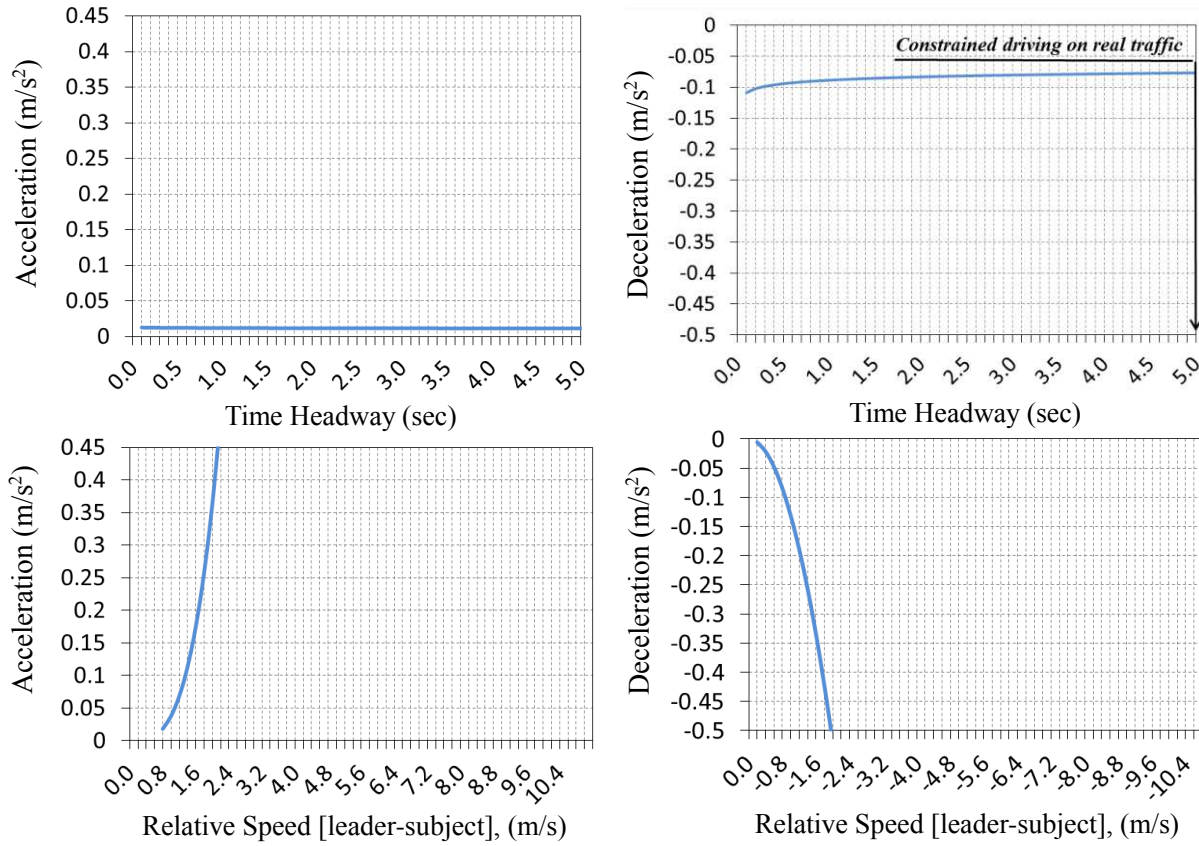38
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6 **FIGURE 7:** Sensitivity of different variables in car-following acceleration and deceleration
7 models according to the Field Model UK

8

9 **4.2 Estimation Results of the Field Model US (Real Traffic Data from US101, USA)**

10 The estimated car-following acceleration usung field data is as follows:
11

12 $$a_n^{cf,acc}(t) = 0.154 \frac{1}{\Delta T_n(t)^{1.348}} |\Delta V(t - \tau_n)|^{3.989} + \varepsilon_n^{cf,acc}(t) \tag{15}$$

13   (15)

14

15 $$\varepsilon_n^{cf,acc}(t) \approx N(0, (0.233)^2)$$

16

17 Where,
18 t = current time period;
19 τ_n = reaction time for driver n;
20 $a_n(t)$ = acceleration for driver n at time t;
21 $\Delta T_n(t)$ = time headway at time t (sec);
22 $|\Delta V(t - \tau_n)|$ = absolute value of relative speed between subject and leader vehicle at time t

1
2   Whereas, the estimated car-following deceleration model is as follows:
3

$$a_n^{cf,dec}(t) = -3.722 \frac{1}{\Delta T_n(t)^{1.463}} \left| \Delta V(t-\tau_n) \right|^{1\,1.098} + \varepsilon_n^{cf,dec}(t) \tag{16}$$

5

$$\varepsilon_n^{cf,dec}(t) \approx N(0,(0.227)^2)$$

7
8   Similar to the Sim model, signs of all parameters of the Field model have the expected logical
9   signs. Further, all model parameters are statistically significant at 95% level of confidence apart
10   from the constant for acceleration (which is statistically significant at 90% level of confidence).
11   Regarding the stimulus part of the model, both car-following acceleration and decelerations
12   increase with relative speeds. It may be noted that these parameters are much larger in magnitude
13   compared to the Sim model parameters (particularly for the decleration model). The behavioural
14   incongruence while driving the driving simulator can be a potential reason for this.
15   In the sensitivity component, the time headway parameters have expected positive signs. This
16   referes that the drivers tend to accelerate less as the time headway with the leader increases. On the
17   other hand, in the deceleration model, it can be concluded that as the time headway decreases, the
18   drivers tend to decelerate more to the same stimulus, due to safety concerns in order to avoid a
19   potential collision and finally obtain again a safe headway from the leader vehicle. The time
20   headway parameter is slightly larger for deceleration compared to acceleration as expected since
21   acceleration only leads to speed advantage whereas, deceleration is prompted by collision
22   avoidance (safety).
23   The following Figure 8 shows the sensitivity analysis, presenting the performance of the models.
24   The default values set assumed to be: relative speed = 0.7 or (-0.7) m/s and time headway equal to
25   3 sec. These numbers derived from the mean values of the sample. An attempt has been made to
26   keep the sensitivity analysis in low values of acceleration-deceleration, so as to highlight the
27   drivers' behaviours under these crucial and sensitive constrained traffic conditions.
28   According to Figure 7 the mean acceleration values are exteemely sensitive in low time headway
29   values showing a noticeable aggressive way of driving compared to the Sim Data and the Field
30   Data UK. As the time headway increases, drivers tend not to accelerate at all and maintain stable
31   speed. On the other hand, deceleration values show that the drivers decelerate at a slower rate as
32   the time headway grows. For the relative speed, for acceleration, the drivers are extremely
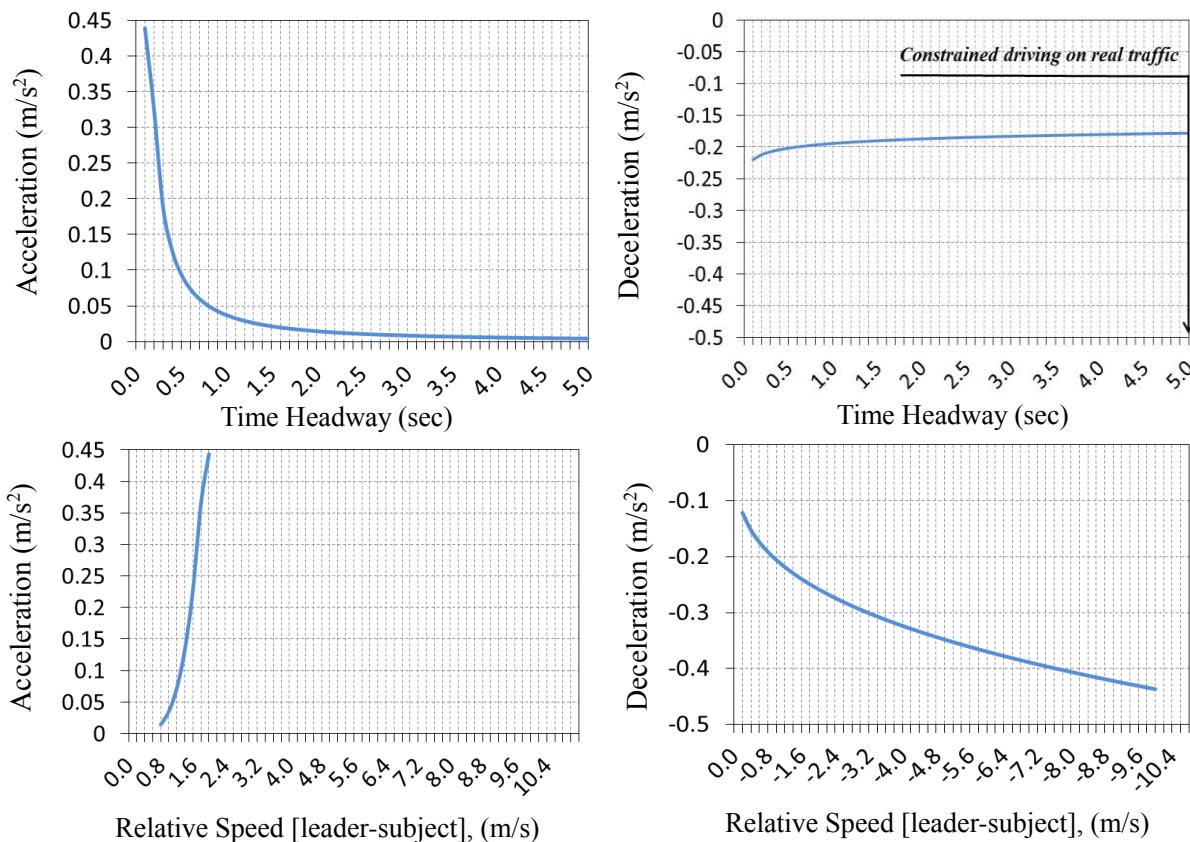33   sensitive to the changes in the relative speed as in the Field Model UK (but not in the Sim Model).
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4   **FIGURE 8:** Sensitivity of different variables in car-following acceleration and deceleration
5   models according to the Field Model US

6

7   **5. MODEL COMPARISON AND TRANSFERABILITY**

8   As mentioned, two forms of formal transferability tests have been conducted: the t-tests of
9   individual parameter equality (parameter level transferability) and TTS (model level
10   transferability).

11

12   Comparison of the model parameters and t-stat differences (as presented in the last two columns of
13   Table 2) reveal the following:
14   • There are statistically significant differences in magnitudes of the relative speed (stimulus)
15   parameters between the Sim Model and both Field Models. This reflects the behavioural
16   incongruence of drivers in the driving simulator which is in line with the findings of the
17   driving simulator validation studies (detailed in Section 2).
18   • The differences in the magnitudes of the time headway (sensitivity) parameters are
19   however not statistically different only between the Sim Model and Field Model US. It
20   may be noted though for acceleration componenets, the time headway parameter was not
21   found to be statistically significant in the Sim Model and Field Model UK in the first place.
22   However, the results provide some indication that some parameters may be more
23   transferable between the driving simulator and the field if the driver population is similar
24   (i.e. both from the same location).

- Most parameters (apart from the deceleration constant) are not directly transferable between the driving simulator and the Field Data US.

The Transferability Test Statistic (TTS) results are summarized in Table 3.

TABLE 3: Transferability Test Statistic (TTS) Results

	Case 1		**Case 2**	
Summary statistics	Sim to Field 1	Sim to Field 2	Field 1 to Sim	Field 2 to Sim
Degrees of freedom (df)	2	2	2	2
LLapplic(βtransf)	4578.24	59.6819	12.1245	10.2592
LLapplic(βapplic)	4579.63	60.7376	13.2316	13.2316
-2[LLapplic(βtransf) -LLapplic(βapplic)]	**2.78**	**2.11**	**2.21**	**5.94**

As presented in Table 3, two different scenarios have been tested so as to validate if driving simulator behaviour can be transferred to real-life world and vice versa. Comparison with the critical $\chi^2_{critical}$ value at 95% level of significance (which is 5.99) indicates that the models are transferable for both directions (i.e. driving simulator to field and vice versa). The former is of more practical importance.

6. CONCLUSIONS

In this paper, we have investigated the transferability of the parameters of a car-following model between a driving simulator and two real world scenario using secondary datasets from the UK and USA. According to the results of the t-tests of individual parameter equality between the Sim Model and the Field Model USA, most of the model parameters have been found to be significantly different in parameter level at 95% level of confidence (except the constant parameter of the car-following deceleration model). The parameter level transferability has been found to be slightly better between the Sim Model and the Field Model UK where the sensitivity parameter (coefficient of the time headway variable) has also been found to be transferable. The transferability statistical test (TTS) results however indicate bi-directional transferability on the model level in both cases. This means that as a package, the models are transferable from the driving simulator to the field. This holds even if there are differences in geographical locaitons. For instance, for the second case study, the Sim Data was collected in the UK while the Field Data was collected from the USA, but the model level transferability still holds. On a practical term, this indicates that the predictions of acceleration/deceleration values generated from models (as in microsimulation packages) using Simulator or Field data will result insignificant differences. This is an important endorsement for use of driving simulator data for development of driving behaviour models for application in microsimulation tools. However, if an analyst is interested about effects of a specific variable in isolation (e.g. effect of headway on acceleration or effect of relative speed on acceleration, etc.), the results may not be directly transferable. This finding is expected to have immense practical importance while applying the driving behaviour models estimated using driving simulator data for quantifying the relative benefits of alternative safety improvement measures in the field. In this particular research, the discrepancy appears to be less if the field location is geographically/spatially closer.

1   However, it may be noted that the results need to be used with caution since the two field datasets
2   have been collected and processed by different teams using different hardware and software.
3   Though, the state-of-the-art technologies have been used in both cases, given the state of image
4   processing technology, both datasets are likely to have some measurement errors and in the
5   absence of ground truth data, it is not possible to precisely determine the extent of such errors. This
6   initial finding therefore needs to be investigated further with additional field datasets from
7   geographically closer and further locations preferably cross-verified with more accurate
8   datasources (e.g. high precision GPS data).
9   The results also have some other limitations - mainly due to the nature of the secondary data used
10   in the two different environments (real roads and simulation). For instance, though care has been
11   taken to maximize the similarity between the Sim and the Field datasets, differences in speeds,
12   accelerations and headways (partially arising from differences in congestion levels) have been
13   observed. This is in line with previous studies on driving simulator validation though, where the
14   drivers have been observed to drive at higher speeds in the driving simulator in similar speed limits
15   and congestion levels. Primary data collection in the driving simulator, can however help to
16   minimize these differences.
17   Further, the models developed as part of the study ignores the heterogeneity among the drivers in
18   reaction times, desired headways and headway thresholds demarakating car-following and other
19   acceleration regimes *(41)*. In this regard, an interesting direction can be to incorporate the effect of
20   driver charcteristics (e.g. age, gender, experience) in the combined models which are also expected
21   to improve the predictive capabilities of the models (for instance better capture the heterogeneity
22   in the reaction times and headways) .
23   Moreover, the scope of this study is limited to car-following models based on stimulus-response
24   framework. Further research is required to test if the similar findings hold for other acceleration
25   regimes (e.g. free-flow, emergency, etc.), different model frameworks (e.g. the Intelligent-Driver
26   Model, Psycho-physical Models, etc.) as well as other choice dimensions (e.g. lane changing).   It
27   will be also interesting to validate the findings of this study by examining differences in traffic
28   predictions of Sim Models and Field Models in microscopic traffic simulation tools.
29   Based on the findings of this study, we are currently investigating methods to make the models
30   more transferable using updating mechanisms (e.g. Bayesian Updating *(42)*), Combined Transfer
31   Estimation Techniques *(43)* as well as estimating the models jointly with both data sources using
32   data combination techniques (e.g. *(44)*). On a parrallel study we are investigating the spatial and
33   temporal transferability of driving behavior models (which also includes investigating the effects
34   of different congestion levels) in further detail which may provide further insights to the results of
35   this research.
36
37   **ACKNOWLEDGEMENTS**
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REFERENCES

1. World Health Organization. Violence, Injury Prevention and World Health Organization, Global Status Report on Road Safety, 2015.
2. Barceló, J. Fundamentals of traffic simulation. International Series in Operations Research and Management. New York: Springer, Vol. 145, 2010.
3. Ahn, K., Rakha, H., Trani, A., and Van Aerde, M. Estimating Vehicle Fuel Consumption and Emissions based on Instantaneous Speed and Acceleration Levels. Journal of Transportation Engineering, Vol. 128, No. 2, 2022, pp. 182-190.
4. Vaa, T. Modelling Driver Behaviour on Basis of Emotions and Feelings: Intelligent Transport Systems and Behavioural Adaptations. In Modelling driver behaviour in automotive environments. Springer London, 2007, pp. 208-232.
5. Koutsopoulos, N.H., and Farah, H. Latent Class Model for Car Following Behavior In Transportation Research Record: Journal of the Transportation Research Board, Methodological, Vol. 46, Transportation Research Board of the National Academies, Washington, D.C., 2012, pp. 563-578.
6. Lee, H.C. The validity of driving simulator to measure on-road driving performance of older drivers. Transport Engineering in Australia, Vol. 8, No. 2, 2003, pp. 89.
7. UDRIVE. European Naturalistic Driving Study. Available on-line at: http://www.udrive.eu, Assessed Feb. 28, 2016.
8. SHRP2. Strategic Highway Research Program. Available on-line at: http://www.shrp2nds.us, Assessed Mar. 13, 2016.
9. Törnros. J. Driving behaviour in a real and a simulated road tunnel—a validation study. Journal of Accident Analysis & Prevention, Vol. 30, No.4, 1998, pp. 497-503.
10. Godley, S. T., Triggs, T. J., and Fildes, B. N. Driving Simulator Validation for Speed Research. Journal of Accident Analysis & Prevention, Vol. 34, No. 5, 2002, pp. 589-600.
11. Bella, F., Garcia, A., Solves, F., and Romero, M.A. Driving simulator validation for deceleration lane design. Proceedings of the 86th Transportation Research Board Annual Meeting, No. 07-0894, Washington, D.C., 2007.
12. Yan, X., Abdel-Aty, M., Radwan, E., Wang, X., and Chilakapati, P. Validating a driving simulator using surrogate safety measures. Journal of Accident Analysis & Prevention, Vol. 40, No. 1, 2008, pp. 274-288.
13. McGehee, D.V.,Mazzae, E. N., and Baldwin, G. S. Driver Reaction Time in Crash Avoidance Research: Validation of a Driving Simulator Study on a Test Track. Proceedings of the Human Factors and Ergonomics Society Annual Meeting. SAGE Publications, Vol. 44, No. 20, 2000, pp. 3-320.
14. Engen, T. Use and Validation of Driving Simulators. Fakultet for Ingeniørvitenskap og teknologi, 2008.
15. Risto, M., and Martens, M.H. Driver Headway Choice: A Comparison between Driving Simulator and Real-Road Driving. In Transportation Research Record: Journal of the Transportation Research Board, Part F: Traffic Psychology and Behavior, Vol. 25, Transportation Research Board of the National Academies, Washington, D.C., 2014, pp. 1-9.
16. Galbraith, R.A., and Hensher, D.A. Intra-Metropolitan Transferability of Mode Choice Models. Journal of Transport Economics and Policy, 1982, pp.7-29.
17. Atherton, T.J., and Ben-Akiva, M.E. Transferability and Updating of Disaggregate Travel Demand Models. No. 610. 1976, 1976.
18. University of Leeds Driving Simulator. UoLDS. Smart Motorways: All Lanes Running.

Faculty of Environment. Institute for Transport Studies. Official Data. Leeds, United Kingdom. 2014.

19. Highways Agency. Smart Motorways. UK Government. Available on-line at: https://www.gov.uk/government/collections/smart-motorways#history, Accessed Aug. 9, 2015.

20. Lee, T., Polak, J.W. and Bell, M.G.H. Trajectory Extractor Version 1.0. Centre for Transport Studies. Imperial College, London, UK. 2008.

21. Kusuma, A., Liu, R., Choudhury, C. and Montgomery, F. Analysis of the Driving Behaviour at Weaving Section using Multiple Traffic Surveillance Data. Transportation Research Procedia, Vol. 3, 2008, pp.51-59.

22. Halkias, J., and Colyar, J. NGSIM Program. Interstate 80 Freeway Dataset. Fact Sheet. U.S. Department of Transportation, Federal Highway Administration, 2006, Available on-line at: http://www.fhwa.dot.gov/publications/research/operations/06137/06137.pdf, Assessed Jul. 8, 2015.

23. Papadimitriou, S. Investigating the Transferability of Car-Following Models between Driving Simulator and Real- Life Traffic. MSc thesis, University of Leeds, Institute for Transport Studies, Leeds, UK, 2015.

24. Choudhury, C., Ramanujam, V., and Ben-Akiva, M.E. Modeling Acceleration Decisions for Freeway Merges. In Transportation Research Record: Journal of the Transportation Research Board, No. 2124, Transportation Research Board of the National Academies, Washington, D.C., 2009, pp.45-57.

25. Ahmed, K.I. Modeling Drivers' Acceleration and Lane Changing Behavior. Ph.D. thesis, Massachusetts Institute of Technology, Boston, USA, 1999.

26. Subramanian, H. Estimation of Car-following Models. Ph.D. thesis, Massachusetts Institute of Technology, Boston, USA, 1996.

27. Gazis, D.C., Herman, R., and Rothery, R.W. Nonlinear Follow-The-Leader Models of Traffic Flow. Operations Research, Vol. 9, No. 4, 1961 pp. 545-567.

28. Sikder, S., Pinjari, A. R., Srinivasan, S., and Nowrouzian, R. Spatial Transferability of Travel Forecasting Models: A Review and Synthesis. International Journal of Advances in Engineering Sciences and Applied Mathematics, Vol. 5, No. 2-3, 2013, pp. 104-128.

29. OX Metrics Software. Timberlake Consultants Ltd. Version: 6.2. 2012. Available on-line at: http://www.oxmetrics.net/pages/software.html, Assessed April 9, 2015.

30. Johansson, G., and Rumar, K. Drivers' Brake Reaction Times. Human Factors: The Journal of the Human Factors and Ergonomics Society, Vol. 13, No. 1, 1971, pp. 23-27.

31. Gipps, P. G. A Behavioural Car-Following Model for Computer Simulation. In Transportation Research Record: Journal of the Transportation Research Board, Part B: Methodological, Vol. 15, No. 2, Transportation Research Board of the National Academies, Washington, D.C., 1981, pp. 105-111.

32. Fambro, D.B., Koppa, R.J., Picha, D.L., and Fitzpatrick, K., 1988. Driver Perception-Brake Response in Stopping Sight Distance Situations. In Transportation Research Record: Journal of the Transportation Research Board, No. 1628, Transportation Research Board of the National Academies, Washington, D.C., 1988, pp. 1-7.

33. Green, M. How long does it take to stop? Methodological Analysis of Driver Perception-Brake Times. Journal of Transportation Human Factors 2, Vol. 3, 2000, pp. 195–216.

1 34. Summala, H. Brake Reaction Times and Driver Behavior Analysis. Journal of
2   Transportation Human Factors 2, Vol. 3, 2000, pp. 217-226.
3 35. Taieb-Maimon, M., and Shinar, D. Minimum and Comfortable Driving Headways: Reality
4   Versus Perception. Journal of Transportation Human Factors 2, Vol. 43, No. 1, 2001, pp.
5   159-172.
6 36. Brunson, S.J., Kyle, E.M., Phamdo, N.C., and Preziotti, G.R. Alert Algorithm Development
7   Program: NHTSA Rear-end Collision Alert Algorithm. DOT HS 809- 526, Final Report,
8   The John Hopkins University in Cooperation with the NHTSA and General Motors
9   Corporation, 2002.
10 37. Yang, X., Liu, J., Vaidya, N.F., and Zhao, F. A Vehicle-to-Vehicle Communication
11   Protocol for Cooperative Collision Warning. Proceeding of the First Annual International
12   Conference on Mobile and Ubiquitous Systems: Networking and Services, 2004.
13   MOBIQUITOUS 2004. IEEE, 2004, pp. 114–123.
14 38. Ranjitkar, P., Suzuki, H., and Nakatsuji, T. Microscopic Traffic Data with Real-Time
15   Kinematic Global Positioning System. Proceeding of Annual Meeting of Infrastructure
16   Planning and Management, Japan Society of Civil Engineer, Miyazaki, Preprint CD-ROM,
17   Dec., 2005.
18 39. Magister, T., Krulec, R., Batista, M., and Bogdanović, L. The Driver Reaction Time
19   Measurement Experiences. Proceedings of Innovative Automotive Technology (IAT'05)
20   Conference, Bled. 2005.
21 40. Bilban, M., Vojvoda, A., and Jerman, J. Age Affects Drivers' Response Times. Collegium
22   Antropologicum, Vol. 33, No. 2, 2009, pp. 467-471.
23 41. Toledo, T., Koutsopoulos, H. N., and Ben-Akiva, M. Integrated Driving Behavior
24   Modeling. In Transportation Research Record: Journal of the Transportation Research
25   Board, Part C: Emerging Technologies, Vol. 15, No. 2, 2007, pp. 96-112.
26 42. Dey, S.S., and Fricker, J.D. Bayesian Updating of Trip Generation Data: Combining
27   National Trip Generation Rates with Local Data. Transportation, Vol. 21, No. 4, 1994, pp.
28   393.
29 43. Ben-Akiva, M., Bradley, M., Morikawa, T., Benjamin, J., Novak, T., Oppewal, H., and
30   Rao, V. Combining Revealed and Stated Preferences Data. Marketing Letters, Vol. 5, No.
31   4, 1994, pp. 335-349.
32 44. Ben-Akiva, M., and Morikawa, T. Estimation of Travel Demand Models from Multiple
33   Data Sources. Proceedings of the International Symposium on Transportation and Traffic
34   Theory, 11th, 1990, Yokohama, Japan.