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## The effect of grading the atomic number at resistive guide element interface on magnetic collimation

R. A. B. Alraddadi, A. P. L. Robinson, N. C. Woolsey, and J. Pasley

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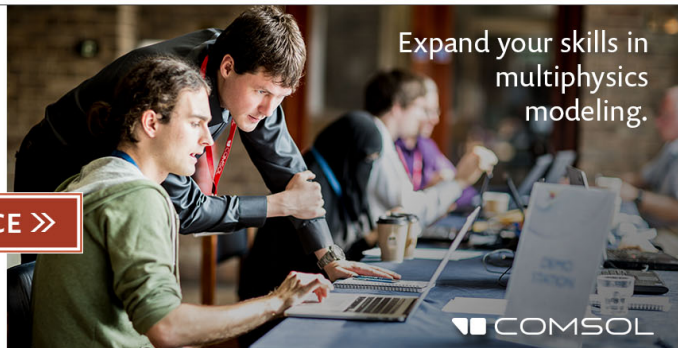
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# The effect of grading the atomic number at resistive guide element interface on magnetic collimation

R. A. B. Alraddadi,<sup>1</sup> A. P. L. Robinson,<sup>2</sup> N. C. Woolsey,<sup>1</sup> and J. Pasley<sup>1,2</sup>

<sup>1</sup>York Plasma Institute, University of York, York YO10 5DD, United Kingdom

<sup>2</sup>Central Laser Facility, STFC Rutherford-Appleton Laboratory, Didcot OX11 0QX, United Kingdom

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Using 3 dimensional numerical simulations, this paper shows that grading the atomic number and thus the resistivity at the interface between an embedded high atomic number guide element and a lower atomic number substrate enhances the growth of a resistive magnetic field. This can lead to a large integrated magnetic flux density, which is fundamental to confining higher energy fast electrons. This results in significant improvements in both magnetic collimation and fast-electron-temperature uniformity across the guiding. The graded interface target provides a method for resistive guiding that is tolerant to laser pointing. *Published by AIP Publishing.*

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## I. INTRODUCTION

Plasma resistivity induces a significant magnetic field inside an overdense plasma when a shear in the fast electron current density or resistivity gradient exists. This is described by the induction equation in the hybrid approximation<sup>1</sup>

$$\frac{\partial \vec{B}}{\partial t} = \eta (\nabla \times \vec{j}_f) + (\nabla \eta) \times \vec{j}_f, \quad (1)$$

where  $\vec{B}$  is the flux density of the magnetic field,  $\eta$  is the resistivity, and  $\vec{j}_f$  is the fast electron current density. The first term on the right-hand side generates a magnetic field that directs electrons towards regions of higher current density, and thus, acts to collimate the fast electron beam. The second term, which forms the basis of the resistive guiding concept,<sup>2,3</sup> generates a magnetic field at resistivity gradients which acts to keep the fast electrons within regions of higher resistivity. The resistivity gradient is created by a transition between two materials with different atomic number  $Z$ . This can be in the form of high- $Z$  solid wire (the guide) embedded in a lower- $Z$  substrate.<sup>4</sup> The resistivity gradient is in the transverse direction to that of the fast electron beam propagation. The fast electrons are generated within the guide, and the magnetic field at the interface between this guide and the substrate (of lower  $Z$  material) will deflect the electrons and keep them inside the high- $Z$  material.

The ability of a resistive guide to confine fast electrons depends on the ratio of the fast electron Larmor radius to the generated azimuthal magnetic field width  $L_\phi$ . The confinement condition of the fast electrons along the guide is expressed as<sup>2,5</sup>

$$B_\phi L_\phi \geq \frac{P_f}{e} (1 - \cos \theta_d), \quad (2)$$

where  $B_\phi$  is the azimuthal magnetic flux density,  $P_f = \gamma_f v_f m_e$  is the fast electron momentum,  $\gamma_f$  is the Lorentz factor,  $v_f$  is the fast electron velocity, and  $\theta_d$  is the fast electron divergence angle. This implies that the product of  $B_\phi L_\phi$  needs to be larger than the fast electron momentum to reflect

the fast electrons back towards the guide axis.<sup>2,4</sup> For fast electrons entering the guide at an angle of  $\theta_d = 30^\circ$  with an energy of 1.8 MeV, a  $B_\phi L_\phi$  of  $10^{-3}$  Tm is needed for confinement. The product of  $B_\phi L_\phi$  needs to be larger than this when either the entrance angle or the fast electron energy increases. For example,  $B_\phi L_\phi$  has to be about  $\approx 7 \times 10^{-3}$  Tm for 4.5 MeV fast electrons with an angle of  $\theta_d = 50^\circ$ .

The resistive guide has been suggested for applications such as the Fast Ignition approach to the inertial confinement fusion scheme<sup>6,7</sup> where the energetic fast electrons need to be guided through an overdense stand-off distance of 100  $\mu$ m or more<sup>8</sup> and deposited into the compressed core of deuterium-tritium (DT) plasma. It has been suggested that a resistive guide element can also be used as a driver in hydrodynamic experiments<sup>4,9</sup> since strong heating occurs where the fast electron beam is collimated. Robinson *et al.*<sup>4</sup> have investigated analytically and numerically the most significant parameters that affect the heating of the resistive guide element. They find that, for example, the ratio of the guide radius to the laser spot radius needs to be comparable in order to obtain good heating. In a real laser system, this condition is difficult to achieve due to the limitation of the laser pointing stability. If the laser hits the edge of the resistive guide element rather than its centre, the guide will not achieve its aim as a collimator and the fast electrons will couple into the substrate. Therefore, a larger radius guide is needed. However, numerical work<sup>4,9</sup> shows that by using a larger radius guide, magnetic fields develop within the guide close to its axis degrading heating uniformity. These ‘‘interior’’ magnetic fields are due to inhomogeneous propagation of the fast electrons.<sup>10</sup> They produce an annular transport pattern which leads to preferential heating of the outer regions of the guide.

Hitherto, the resistive guide in all previous experimental<sup>11,12</sup> and numerical<sup>4,9</sup> studies, has an engineered step-like atomic number interface between the guide and the substrate regardless of the guide geometry. We will refer to this configuration as ‘‘step-like’’ resistive guide configuration. Since the resistive magnetic field is produced at the guide-substrate interface, changing the interface resistivity away from a

TABLE I. Table of guide geometric parameters.

Simulation	$r_{guide}$ ( $\mu\text{m}$ )	$r_{core}$ ( $\mu\text{m}$ )	$r_{spot}$ ( $\mu\text{m}$ )	$\chi$	Guide-substrate interface shape (shown in Figure 2)
A	5	5	3.5	1.4	(a)
B	2.5	2.5	3.5	0.7	(b)
C	5	2.5	3.5	0.7	(c)
D	5	2.5	3.5	0.7	(d)

step-like interface offers a means to improve electron guiding and enable heating of a larger radius guide. We find that grading the atomic number across a layer at the guide-substrate interface (so that the atomic number, and thus the resistivity, decreases with increasing radius) enhances the growth of resistive magnetic field. This cladding layer can lead to a larger integrated magnetic flux density, which improves the magnetic collimation of the fast electrons. Furthermore, as a result of this, simulations show an improvement in radial heating uniformity in the larger radius guide.

This paper is structured as follows; Sec. II contains a description of the different resistive guide designs. Sec. III outlines the simulation set up and the simulation results and discussion are contained in Secs. IV and V, respectively.

## II. GRADING THE ATOMIC NUMBER AT THE INTERFACE OF THE GUIDE ELEMENT

To highlight the impact of a graded-interface, four simulations are reported. Two use a step-like interface (simulations A and B in Table I) and two use a shaped or graded interface (C and D in Table I). The aim of these simulations is to compare the resulting magnetic collimation and radial temperature profiles in the guides. The guide is a cylindrical wire in all simulations as summarised in Table I.  $r_{guide}$  is the total radius of the embedded guide whereas  $r_{core}$  is the radius of the core of the guide. The core has not been graded.  $\chi$  is the ratio of the radius of the core  $r_{core}$  to the laser radius spot  $r_{spot}$ . It was found that for graded-interface targets, this ratio needs to be less than 1. When  $\chi > 1$ , the fast electron beam breaks into filaments inside the guide resulting in non-uniform radial heating of the guide.

Figures 1(a)–1(d) show 2-dimension z-x plane slices of the target Z profile for targets A to D. These figures are taken in the mid y-direction at  $-15 < z < 15$  along the x-direction. The materials used in simulations A and B are solid density ( $2.7 \text{ g cm}^{-3}$ ) aluminium guide ( $Z = 13$ ) embedded into a solid ( $1.0 \text{ g cm}^{-3}$ ) CH plastic ( $Z = 3.5$ ) substrate. The difference between simulations A and B is the guide radius, which is  $5 \mu\text{m}$  and  $2.5 \mu\text{m}$ , respectively. The resistive guide design in simulation C (Figure 1(c)) is an Al guide clad in a carbon (density  $2.2 \text{ g cm}^{-3}$ ) layer. This resembles a co-axial cable design. We refer to this design as “co-axial” resistive guide, and the overall radius of this co-axial guide is  $5 \mu\text{m}$ . Simulation D, Figure 1(d), uses an Al guide of radius  $2.5 \mu\text{m}$  clad in a graded layer of material of linearly decreasing Z from  $Z = 6$  to  $Z = 3.5$  between radial positions of  $2.5 \mu\text{m}$  and  $5 \mu\text{m}$ . The overall radius of the guide (with cladding) is  $5 \mu\text{m}$ . This is embedded in a CH plastic substrate. The radial atomic number profiles are shown in Figures 2(a)–2(d). The

fast electrons are injected into the guide from the left hand side at  $x = 0$  and the centre of y and z.

## III. SIMULATION SET UP

The simulations were performed using the 3 dimensional particle hybrid code ZEPHYORS,<sup>4,13</sup> which is based on the hybrid method developed by Davies in a series of publications.<sup>13,14</sup> ZEPHYORS is used to simulate the 3D relativistic motion of electrons under the influence of self-generated resistive electric and magnetic fields, as well as collisions. The fast electron current  $\vec{j}_f$  propagates into the plasma when it is spatially coincident and nearly balanced with cold return electron current  $\vec{j}_r$  that is drawn from the background,<sup>15</sup> i.e.,  $\vec{j}_f \approx -\vec{j}_r$ . The resistive electric field is estimated from Ohm’s law,  $E = -\eta \vec{j}_f$ , with displacement current dropped from the Ampere law. Ignoring displacement current relies on the assumption that the change in the electric field with time is slow. This is valid since the width of the beam, i.e., the fast electron bunch radius, is much smaller than the length of the fast electron bunch. In addition, the electron pressure term ( $-\nabla P_e/n_e$ ) is also neglected in Ohm’s law. The reason for this is that the contribution of the electric field from this term is small by about two orders of magnitude compared to the electric field obtained from the resistive term. Thus, from Faraday’s law, the resulting resistive magnetic field arising due to the fast electrons can be written as Eq. (1). The return electron current heats the background plasma, via Ohmic heating, with power density  $\vec{j}_r \cdot E \approx \eta j_f^2$ . The background electrons are treated as a static fluid that experience heating, ionization, and change in resistivity. The static treatment of the background is reasonable as the hydrodynamic displacement is about  $0.1 \mu\text{m}$  in 1 ps for targets heated to 100 eV, assuming that the sound speed is  $10^5 \text{ m/s}$ . The Thomas-Fermi model is used to obtain the ionisation and specific heat capacity of the background. The resistivity is temperature dependent and based on that of Lee and More resistivity model.<sup>16</sup> The temperature is calculated by the energy deposition due to the slowing down of the fast electrons and the Ohmic heating induced by the return electron current. The fast electron population is described kinetically using the Vlasov equation, which is solved via the particle-in-cell (PIC) method. Collisions are included using the Fokker-Planck collisional operators, which account for angular fast electron scattering from background ions and electrons, together with drag generated by the background electrons. The mathematical expressions of the collisional operators are obtained from Davies<sup>13</sup> equations (1) and (2). More details about the physics of hybrid code can be found in the study by Robinson *et al.*<sup>8</sup>

A  $200 \times 100 \times 100$  grid was used with a  $0.5 \mu\text{m}$  cell size in each direction. The number of macroparticles injected into each of the cells was 126. This helped to reduce statistical noise. The target, as described above, consisted of a CH plastic substrate within which a guide of radius  $r_{guide}$  was embedded. This guide is co-linear along the x-axis and centred on y and z as shown in Figure 1. The laser irradiation intensity was  $1.27 \times 10^{20} \text{ W cm}^{-2}$  with a pulse duration of 2 ps and the laser wavelength of  $1 \mu\text{m}$ . It is assumed that 30% of the laser energy was coupled to the fast electrons. The temporal profile of the fast electron beam is top-hat shaped and the transverse profile

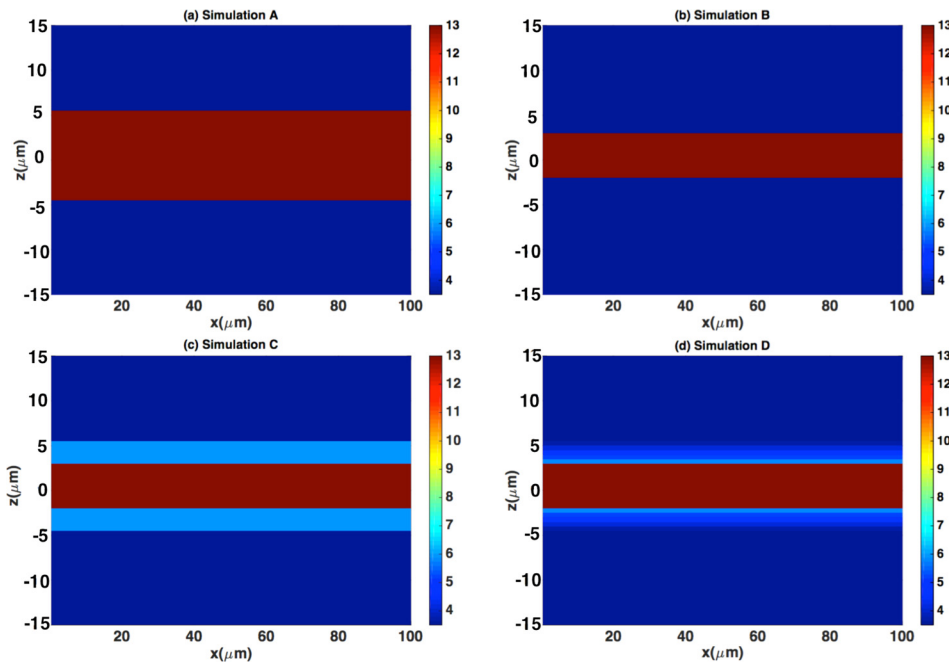


FIG. 1. (a)–(d) show the target Z profile for simulations A to D, respectively. Simulations A and B use a step-like interface and the difference between the two is only in the guide radius. Simulation C uses a shaped interface resembling a co-axial cable design. Simulation D uses the graded interface resistivity cladding guide.

is  $\propto \exp[-\frac{r^2}{2r_{spot}^2}]$ , where  $r_{spot} = 3.5 \mu\text{m}$ . The choice of  $r_{spot} = 3.5 \mu\text{m}$  was to ensure that the electron beam source is within the resistive guide of  $5 \mu\text{m}$ . It is worth mentioning that these choices of small sizes of both  $r_{spot}$  and  $r_{guide}$  were to minimise the simulation time. The fast electron angular distribution is uniform over a solid angle and defined by the half-angle of divergence  $50^\circ$ . The energy distribution of the fast electrons is from the reduced Wilks' ponderomotive scaling,<sup>17</sup> giving  $T_f = 2.7 \text{ MeV}$ .<sup>18</sup> The resistivity uses the Lee and More model and a minimum mean free path as  $5r_s$ , where  $r_s$  is the inter-atomic spacing. From Table I, it can be seen that simulations

A, C, and D have total  $r_{guide} > r_{spot}$  ensuring that the electron beam source is within the guide. This is not the case in simulation B where  $r_{guide} < r_{spot}$ . However,  $r_{core}$  in simulation B is identical to that in simulations C and D.

## IV. RESULTS

### A. The effect of design on the azimuthal magnetic field rate

Figures 3(a)–3(d) show an  $x$ - $z$  slice taken at the mid-plane of  $y$  of the generated magnetic field at 2.2 ps for

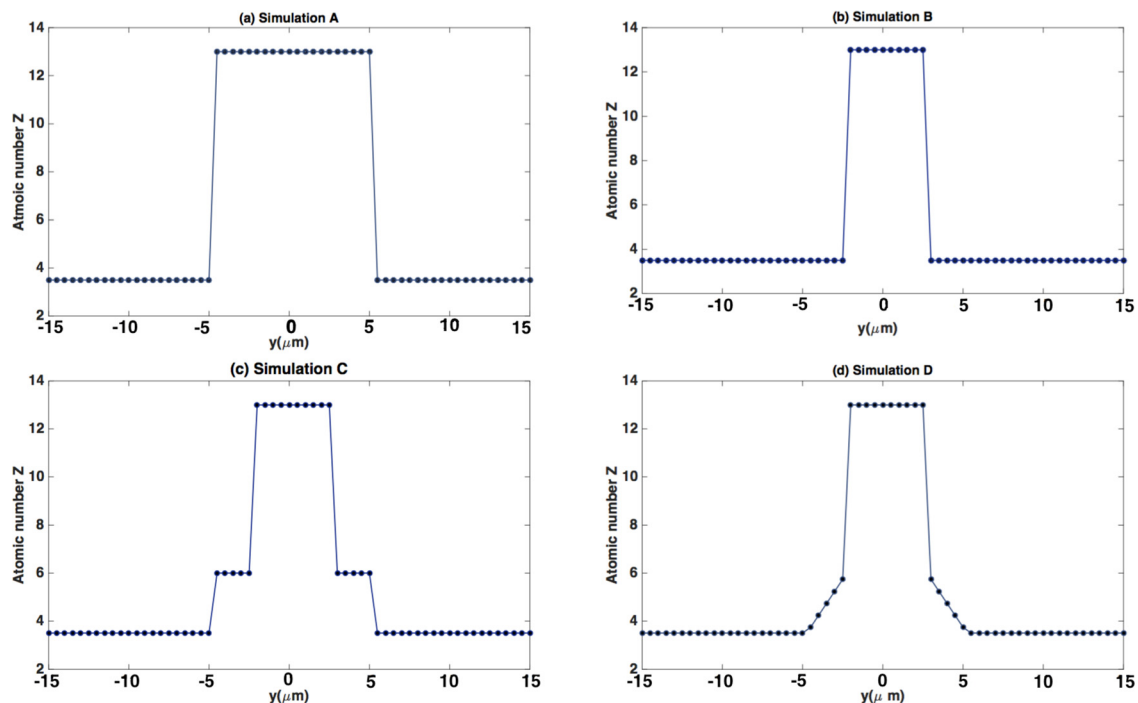


FIG. 2. (a)–(d) show the radial atomic number profile for simulations A to D, respectively. Simulations A and B use Aluminium guide. Simulation C uses an Al guide clad in a carbon layer. Simulation D uses an Al guide clad in a graded layer of the material of linearly decreasing Z. All the guides are embedded into the CH plastic substrate.

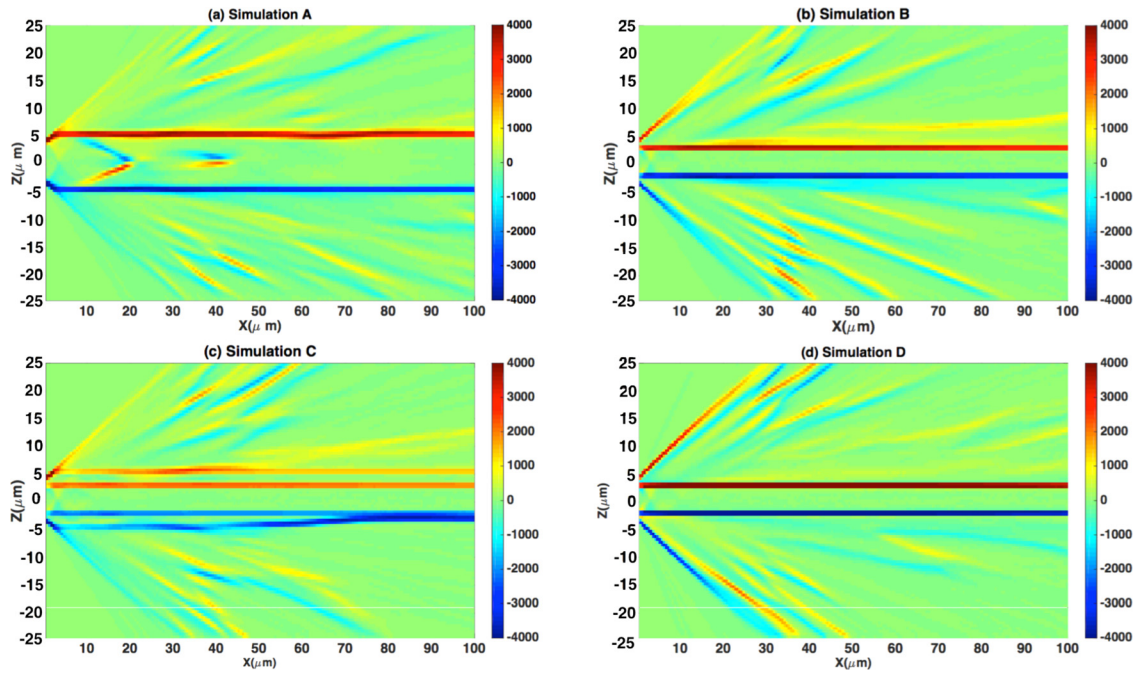


FIG. 3. x-z slice of the magnetic field (T) in the y midplane at 2.2 ps for simulations A to D.

simulations A to D. Generally, an azimuthal magnetic field has been generated at the interface between the guide and the CH plastic substrate. This field provides collimation for the fast electrons. Radial expansion of the fast electron beam is evident from the formation of the magnetic field in the CH plastic substrate outside the guide. In simulation A (Figure 3(a)), magnetic field features are evident within the guide, and these are close to the axis and are most noticeable occurring between  $x = 20 \mu\text{m}$  and  $x = 40 \mu\text{m}$ . Here, the  $r_{\text{guide}} > r_{\text{spot}}$  and  $\chi$  is larger than 1. This “interior” magnetic field is due to the inhomogeneous propagation of the fast electrons.<sup>10</sup> The generation of these fields within the guide is undesirable and inhibits radially uniform fast electron heating.

Magnetic fields interior to the guide are not observed in simulations B, C, and D where  $\chi < 1$  although  $r_{\text{guide}} > r_{\text{spot}}$  in simulations C and D. This implies that more uniformity of the fast electron propagation is obtained in these guides. In simulation C, the co-axial resistive guide, two azimuthal magnetic fields are observed, the first is between the guide and the CH plastic substrate at radial positions of  $5 \mu\text{m}$  and the second is between the carbon cladding and the aluminium core, i.e., at radial position of  $2.5 \mu\text{m}$ . Because of this, the fast electrons are confined at three individual positions, between  $-5 \mu\text{m}$  and  $-2.5 \mu\text{m}$ ,  $-2.5 \mu\text{m}$  and  $+2.5 \mu\text{m}$ , and  $+2.5 \mu\text{m}$  and  $+5 \mu\text{m}$  as shown in Figure 3(c). The azimuthal magnetic fields in simulations B and D shown in Figures 3(b) and 3(d), respectively, are similar although the total guide radius in simulation D is twice that in simulation B. In simulation D, the azimuthal magnetic field is generated along the graded region of the guide and located along the interface with the core of the guide. The observation that the magnetic flux density in simulation D is higher than that in simulation B, which has a step-like interface, by  $10^3 \text{T}$  is notable and important. Simulation D also indicates that changing the interface shape does not significantly affect the width of the magnetic field.

Figure 4 shows the resulting product  $B_{\phi}L_{\phi}$  as a function of time which is extracted at  $x = 10 \mu\text{m}$ , and in the y mid-plane for all the simulations. The product  $B_{\phi}L_{\phi}$  is calculated from the peak of the magnetic field and the FWHM. Simulation D has the largest product  $B_{\phi}L_{\phi}$  of all simulations and indicates that this guide can confine higher energy electrons. A high value of  $B_{\phi}L_{\phi}$  ( $10^{-3} \text{Tm}$  at 200 fs in simulation D) is important to collimation of the fast electron beam and subsequent heating of the guide. Simulation B achieves a similar  $B_{\phi}L_{\phi}$  by 300 fs; however, since  $r_{\text{guide}} < r_{\text{spot}}$ , more fast electrons escape the guide and move into the CH plastic substrate. This reduces the  $B_{\phi}L_{\phi}$  product further limiting the fast electron confinement. The  $B_{\phi}L_{\phi}$  product in simulation C is inferior to that in simulation A as the fast electrons are confined in multiple regions of the guide as shown in Figure 3(c). Nevertheless, we find (see in Sec. IV B) that the radial heating within the guide in simulation C is more uniform

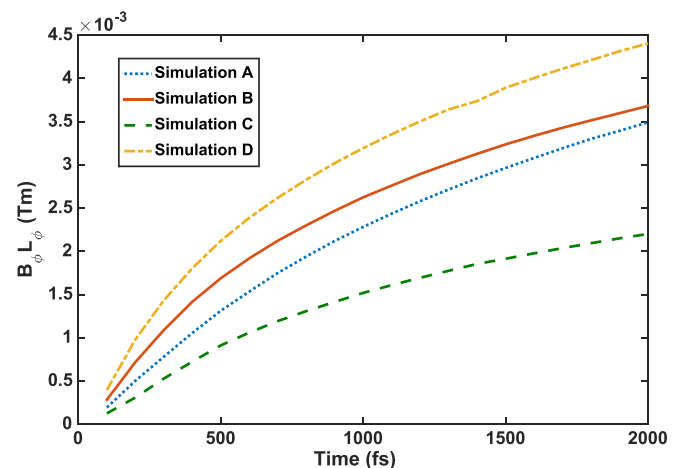


FIG. 4. The product of  $B_{\phi}L_{\phi}$  near the head of the beam  $x = 10 \mu\text{m}$  at different times in fs.

than in simulation A. This is because electron beam filamentation is suppressed even in situation where a coaxial guide has higher current densities. In summary, a resistive guide using a graded interface increases the magnetic flux density and produces a significantly larger  $B_\phi L_\phi$  product. This enhances electron confinement.

## B. The effect of design on the guide heating

Figure 5 shows an  $x$ - $z$  slice of the background temperature in eV taken in the mid  $y$ -plane at 2.2 ps for simulations A to D. Strong resistive return current heating occurs in the guides where the fast electrons are collimated. There is a gradient in temperature with depth along the guide ( $x$ -direction) which is observed in all simulations. However, this gradient differs in each simulation due to electron confinement which results from the differences in the generated azimuthal magnetic field. Non-uniform radial heating is observed in simulation A with striking annular temperature profiles at  $x = 20 \mu\text{m}$  and  $x = 40 \mu\text{m}$ . This corresponds to the location of the interior magnetic field previously noted (see Figure 3(a)). More uniform heating is obtained in simulation B; this is due to the small radius of the guide, and similar results are noted by Robinson *et al.*<sup>4</sup> The heating in simulation B is comparable to simulation D which has twice the guide radius. This result is important and identifies a possible method for designing targets that are tolerant of laser pointing stability. The key is to increase the guide radius using a graded resistivity cladding. The laser pointing stability in this design will be subject of future work as we will closely examine this in

more detail. The resulting guide has good radial temperature uniformity and relatively unstructured decrease in temperature along the depth. The resistivity grading between the guide core and plastic substrate with  $\chi < 1$  ensures that the fast electrons with diverging trajectories are redirected towards the higher resistivity regions. Temperatures in simulation C are lower and more structured than in simulations B and D. This is expected based on the simulated  $B_\phi L_\phi$ . The temperature in simulation C is higher than in simulation A although the  $B_\phi L_\phi$  product is lower. This results from the lack of internal magnetic field in co-axial target design.

The cross-section from Figure 5 is shown in Figure 6. These are taken at 2.2 ps along the guide depth at the centre of  $y$  and  $z$  axes. The effect of the internal magnetic field excluding fast electrons and leading to poor heating at  $x = 20 \mu\text{m}$  and  $x = 40 \mu\text{m}$  in the centre of the guide in simulation A is evident. An important comparison is between simulations B, C, and D where  $\chi < 1$ . There is oscillation in their temperature profiles within  $15 \mu\text{m}$  of the surface. This is due to inhomogeneity in the fast electron propagation near the injection region. After this, a gradual reduction in the temperature occurs. The differences in temperature between simulations B and D is due to the fact that that  $r_{\text{guide}} > r_{\text{spot}}$  in simulation D while  $r_{\text{guide}} < r_{\text{spot}}$  in simulation B.

It is worth mentioning that the fast electrons heat the resistive guide structure to high temperatures in few picoseconds. As discussed in Sec. III, the hydrodynamic motion becomes important on a timescale of 10–30 ps and it should be negligible at time up to 1–3 ps. It is expected that a strong hydrodynamic expansion of the guide and the thermal

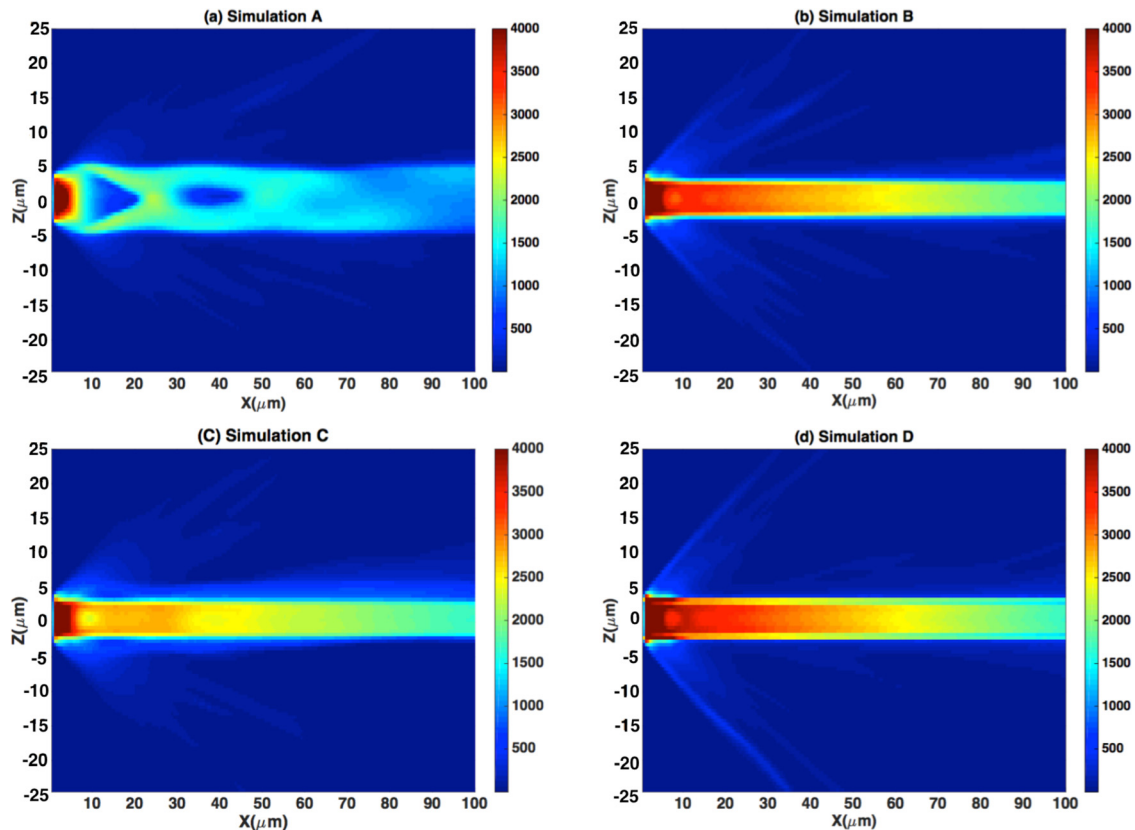


FIG. 5.  $x$ - $z$  slice of the background temperature (eV) in the  $y$  midplane at 2.2 ps for simulations A to D.

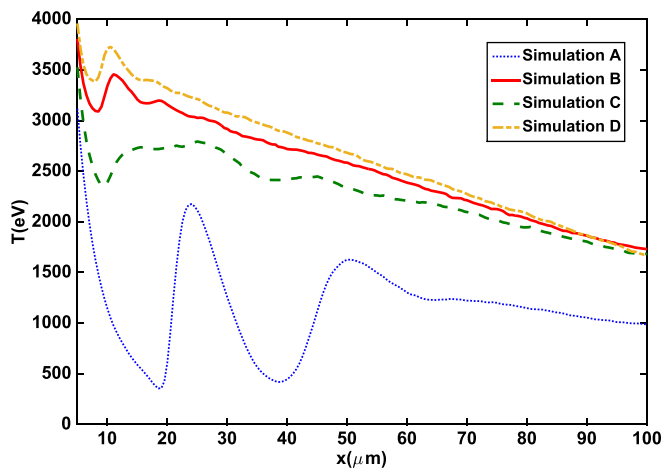


FIG. 6. Line-out of the background temperature in eV at 2.2 ps in simulations A to D along  $x$ -direction at the centre of  $y$  and  $z$ .

electron transport into the surrounding material will have significant role in the multi-picosecond timescale. In addition, depending on the choice of different parameters, the strong heating of the resistive guide may potentially lead to the generation of strong shocks into the surrounding material.<sup>4</sup> Our simulations only capture the dominant physics in the regime of interest of 1 to few ps timescales where the fast electron can heat the guide before any significant hydrodynamic motion occurs or thermal transport.

## V. DISCUSSION AND CONCLUSION

In this paper, we have investigated the effect of changing resistivity (by changing  $Z$ ) on the cladding layer around the core of a fast electron guide. We find that a cladding layer leads to superior guiding of electrons than in structures with a step-like change in resistivity. We find that a linear gradation in  $Z$  enhances the growth of resistive magnetic field, leading to an improvement in the magnetic collimation. The product  $B_\phi L_\phi$  becomes significantly larger with a graded-interface compared to step-like and co-axial resistive guides. The graded-interface configuration is beneficial for four reasons; it helps in collimating the fast electrons uniformly in the core of the guide. Second, a larger guide radius is possible using the graded interface. This is more tolerant to the laser pointing stability. Third, an increase in the  $B_\phi L_\phi$  product early in the electron injection into the guide promotes fast electron confinement. And last, it helps reduce interior magnetic fields. The condition for best performance of the graded interface resistivity cladding is when the ratio

between the core of the guide and the laser spot radius is less than 1.

The fabrication of the graded interface resistivity cladding guides is possible using the alloys. Our simulations suggest that improved heating uniformity afforded by a fast electron guide with a graded resistivity cladding is of considerable benefit. Although the fabrication processes are not easy task compared to the step-like resistive guide, the gains obtained from this type of design mean that the fabrication development effort will be worthwhile. The development in micro-scale target fabrication indicates that target fabricators will soon be able to manufacture such targets.

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