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Measurement of OH reactivity by laser flash photolysis coupled with laser-induced fluorescence spectroscopy

Daniel Stone¹, Lisa K. Whalley^{1,2}, Trevor Ingham^{1,2}, Peter M. Edwards^{1,a}, Danny R. Cryer¹, Charlotte A. Brumby¹, Paul W. Seakins^{1,2}, and Dwayne E. Heard^{1,2}

¹School of Chemistry, University of Leeds, Leeds, LS2 9JT, UK

²National Centre for Atmospheric Science (NCAS), University of Leeds, Leeds, LS2 9JT, UK

^anow at: Wolfson Atmospheric Chemistry Laboratories, Department of Chemistry, University of York, Heslington, York, YO10 5DD, UK

Correspondence to: Dwayne E. Heard (d.e.heard@leeds.ac.uk)

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Abstract. OH reactivity (k'_{OH}) is the total pseudo-first-order loss rate coefficient describing the removal of OH radicals to all sinks in the atmosphere, and is the inverse of the chemical lifetime of OH. Measurements of ambient OH reactivity can be used to discover the extent to which measured OH sinks contribute to the total OH loss rate. Thus, OH reactivity measurements enable determination of the comprehensiveness of measurements used in models to predict air quality and ozone production, and, in conjunction with measurements of OH radical concentrations, to assess our understanding of OH production rates. In this work, we describe the design and characterisation of an instrument to measure OH reactivity using laser flash photolysis coupled to laser-induced fluorescence (LFP-LIF) spectroscopy. The LFP-LIF technique produces OH radicals in isolation, and thus minimises potential interferences in OH reactivity measurements owing to the reaction of HO₂ with NO which can occur if HO₂ is co-produced with OH in the instrument. Capabilities of the instrument for ambient OH reactivity measurements are illustrated by data collected during field campaigns in London, UK, and York, UK. The instrumental limit of detection for k'_{OH} was determined to be 1.0 s^{-1} for the campaign in London and 0.4 s^{-1} for the campaign in York. The precision, determined by laboratory experiment, is typically $< 1 \text{ s}^{-1}$ for most ambient measurements of OH reactivity. Total uncertainty in ambient measurements of OH reactivity is $\sim 6 \%$. We also present the coupling and characterisation of the LFP-LIF instrument to an atmospheric chamber for measurements of OH reactivity during simulated experiments, and provide

suggestions for future improvements to OH reactivity LFP-LIF instruments.

1 Introduction

OH radicals dominate atmospheric oxidation chemistry, controlling the lifetimes of most primary pollutants and greenhouse gases emitted into the atmosphere, including methane, CO, volatile organic compounds (VOCs), NO₂ and SO₂, whilst also contributing to the production of secondary pollutants such as ozone, sulphuric acid and secondary organic aerosol (SOA) (Stone et al., 2012). Appreciation of the factors controlling atmospheric OH radical concentrations is thus essential to understanding the processing and fate of trace species in the atmosphere, and to our ability to understand and predict air quality and climate change. Moreover, the short chemical lifetimes of the OH radical and the closely related HO₂ radical make OH and HO₂ ideal species for testing the chemical mechanisms used in atmospheric models since their concentrations are controlled by in situ chemistry alone and are not influenced by transport processes. However, model simulations of OH concentrations require calculation of both OH production and loss rates, and there is potential for agreement between modelled and observed OH concentrations based on opposing errors in the production and loss terms. Similarly, when model calculations show poor agreement with observations, it can be problematic to determine whether the model discrepancies result from in-

complete knowledge of the total production rate or of the total loss rate.

Observations of OH radical concentrations made in conjunction with measurements of OH reactivity (k'_{OH}), the total loss rate of OH and the inverse of the OH chemical lifetime (τ_{OH}) thus provide a means to separate the production and loss terms for OH, enabling a more robust test of our understanding of OH radical concentrations and of atmospheric oxidation chemistry. In addition, comparison of measured OH reactivity with calculated OH reactivity, based on observed concentrations of OH sinks and known rate coefficients for their reactions with OH (Eq. 3), also provides an indication of the presence and importance of unmeasured OH sinks:

$$-d[\text{OH}]/dt = \Sigma k_x [\text{X}][\text{OH}] \quad (1)$$

$$= k'_{\text{OH}}[\text{OH}] \quad (2)$$

$$k'_{\text{OH}} = \Sigma k_x [\text{X}], \quad (3)$$

where k_x is the rate coefficient for reaction of OH with species X and k'_{OH} is the OH reactivity (the pseudo-first-order rate coefficient for reaction of OH with all reaction partners present). Finally, using both $[\text{OH}]$ and k'_{OH} to determine $-d[\text{OH}]/dt$ experimentally, it is possible to evaluate the completeness of our knowledge of OH sources, which when added together should equal $+d[\text{OH}]/dt$ if the steady-state budget is closed (Martinez et al., 2003; Whalley et al., 2011; Fuchs et al., 2013; Lu et al., 2013).

Measurements of OH reactivity in the atmosphere have been made by three different techniques – the flow tube technique, the laser flash photolysis technique and the comparative reactivity method, with all three methods relying on production of above ambient concentrations of OH radicals and monitoring of the OH decay rate, either directly or indirectly. The flow tube method (Kovacs and Brune, 2001) typically generates OH radicals at the tip of a sliding injector by photolysis of water vapour (Reaction R1) using a mercury vapour lamp, also resulting in production of HO_2 radicals (Reaction R2).



The OH radical signal is monitored downstream of the injector after mixing with a flow of ambient air in the main tube. By changing the position of the sliding injector relative to the point at which OH is detected it is possible to vary the contact time of OH with the ambient air, and thus to determine the total loss rate for OH in the flow tube. However, the technique has a number of disadvantages. The time resolution of measurements made by the flow tube method is relatively poor, owing to the need to measure OH signals at a number of different injector positions to obtain a kinetic profile, during which time the ambient OH reactivity could show significant variability, although Mao et al. (2009) overcome this issue

for airborne measurements of OH reactivity by reducing the number of time points used to determine the OH decay rate. The flow rates of sampled air in the flow tube method are relatively high ($\sim 300\text{--}900$ standard L min^{-1}), with turbulent flow conditions leading to high wall loss rates of OH in the flow tube and relatively high uncertainties in determinations of OH reactivity owing to uncertainties in the wall loss rates. Knowledge of the flow velocity in the flow tube, requiring direct measurement or knowledge of the flow regime, total flow rate and cross-section of the flow tube, is also needed to convert the distance over which OH and ambient air are mixed to reaction time, and can lead to uncertainties in the contact time between OH and reactants in ambient air. A significant disadvantage of the flow tube method is the generation of equal concentrations of OH and HO_2 following photolysis of water vapour at the tip of the sliding injector (Reactions R1–R2), leading to the potential for production of OH in the flow tube on the timescale of the experiment owing to the reaction of HO_2 with ambient NO (Reactions R3).

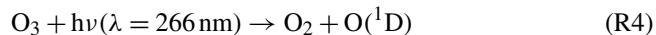


The production of OH from Reaction (R3) reduces the observed decay rate of OH in the flow tube, and measurements of OH reactivity using the flow tube method thus also require simultaneous measurements of ambient NO concentrations in order to correct for interferences from $\text{HO}_2 + \text{NO}$, which can be quite significant. For example, for 75 ppb NO, a typical rush hour mixing ratio in Mexico City, a correction factor of ~ 1.7 was required to account for the production of OH from $\text{HO}_2 + \text{NO}$ within the flow tube (Shirley et al., 2006).

In the comparative reactivity technique, a reactive molecule not usually present in air, typically pyrrole, is entrained in a gas flow and the rate of its decay owing to reaction with artificially high concentrations of OH is measured in “zero” air and ambient air by proton transfer quadrupole mass spectrometry (PTR-QMS) (Sinha et al., 2008), proton transfer time of flight mass spectrometry (PTR-ToFMS) (Michoud et al., 2015) or photoionisation detection (GC-PID) (Nölscher et al., 2012). Comparison of the rates of decay of the molecule in “zero” air and ambient air enables determination of the competition between the reaction of OH with the known concentration of the reactive molecule and the reaction of OH with sinks in ambient air, thus enabling measurement of the ambient OH reactivity. Absolute measurement of the physical loss rate of OH is not required for the technique, and the limit of detection of comparative reactivity instruments is determined by the sensitivity to changes in the signal corresponding to the concentration of the reactive species. However, OH radicals are typically produced in comparative reactivity instruments through Reactions (R1–R2), in a similar manner to that used in flow tube instruments and thus also producing high concentrations of HO_2 . Interferences resulting from OH production from $\text{HO}_2 + \text{NO}$ are thus also potentially problematic for comparative reactivity instruments and knowledge of NO concentrations are required to correct for

any interferences. In addition, the amount of OH produced is dependent on humidity, and it is essential to ensure constant humidity between measurements made in “zero” air and those made in ambient air, with significant corrections often necessary to account for any differences (Michoud et al., 2015).

The laser flash photolysis technique (Sadanaga et al., 2004a) produces OH in isolation (i.e. with no simultaneous production of HO₂) via laser photolysis of O₃, typically at a wavelength of 266 nm, followed by reaction of O(¹D) with ambient H₂O (Reactions R4–R5):



The production of OH without initial co-production of HO₂ minimises potential interferences from HO₂ + NO and renders the flash photolysis technique more suitable to high NO_x (NO_x = NO + NO₂) environments. The laser flash photolysis method also has the advantage that the production of OH radicals is uniform throughout the reaction cell, minimising the risk of poor mixing which is potentially problematic for the flow tube and comparative reactivity techniques. Flow rates of sampled air are typically lower for the laser flash photolysis instruments (~ 12 – 20 standard L min^{−1}) (Sadanaga et al., 2004a) than for those using flow tubes (~ 300 – 900 standard L min^{−1}) (Kovacs and Brune, 2001; Kovacs et al., 2003; Ingham et al., 2009; Hansen et al., 2014), and the resulting laminar flow of gas reduces contact of the gas with the walls of the instrument, thus reducing the physical loss rate of OH and associated uncertainties. Although averaging of data is often required to improve signal-to-noise, a significant advantage of the laser flash photolysis technique is the ability to measure ambient OH reactivity in “real-time” through time-resolved measurements of the OH decay following photolysis. The technique has the potential for significantly enhanced time resolution, both in terms of the number of time points obtained during the decay of OH, and the averaging time over which the data are reported, compared to the flow tube or comparative reactivity methods.

The first atmospheric measurements of total OH reactivity were made at an urban background site in Nashville, TN, USA, in summer 1999 using the flow tube technique (Kovacs and Brune, 2001; Kovacs et al., 2003). Calculations of OH reactivity, using VOC measurements co-located with the reactivity measurements, underestimated the total observed reactivity by ~ 30 % on average owing to unmeasured or unknown VOCs and VOC oxidation products (Kovacs et al., 2003). Subsequent measurements at an urban background site in New York, NY, USA, were, on average, within 10 % of the calculated reactivity in summer 2001 (Ren et al., 2003), but were underestimated by 30–40 % during morning and evening rush hours in winter (Ren et al., 2006a). Significant underestimation of the measured OH reactivity in the morning rush hour was also reported for observations

in the Mexico City Metropolitan Area (MCMA), with the observed reactivity reaching 120 s^{-1} (Shirley et al., 2006). High OH reactivity has also been observed in Paris during the MEGAPOLI campaign in 2010, with k_{OH} reaching 130 s^{-1} for continental air masses and calculations based on measured VOC concentrations underestimating the reactivity by up to 75 % (Dolgorouky et al., 2012). Reactivity measurements in Tokyo were underestimated in summer, spring and autumn, but reproduced to within 5 % in winter, with the reactivity correlating well with NO_x throughout the year (Sadanaga et al., 2004b; Yoshino et al., 2006; Chatani et al., 2009; Yoshino et al., 2012). Aircraft measurements of OH reactivity have also shown that reactivity tends to decrease with altitude, with discrepancies between observed and calculated reactivity most pronounced at altitudes up to 2 km and tending towards agreement at altitudes above 4 km (Mao et al., 2009).

Flow tube measurements at an urban site in Houston, US, during the TEXAQ2000 and TRAMP2006 campaigns (Mao et al., 2010) and at a forested site at Whiteface Mountain, NY, USA (Ren et al., 2006b), were well reproduced by model calculations. However, measurements made at a coastal site in Norfolk, UK, typically characterised by relatively “clean” air were significantly underestimated and attributed to the presence of numerous high molecular mass VOCs at low concentrations which were not included in the VOC measurement suite (Lee et al., 2009; Ingham et al., 2009). The presence of unmeasured VOCs was also indicated for the PROPHET 2000 campaign at a forested site in Michigan, USA, during which the measured OH reactivity was underestimated by ~ 50 % on average, with the “missing” OH reactivity exhibiting a strong temperature dependence potentially resulting from temperature-dependent emissions of unmeasured biogenic VOCs (Di Carlo et al., 2004). Uncertainties in emissions and chemistry of biogenic VOCs, particularly in the oxidation chemistry of isoprene and its oxidation products, have also been responsible for underpredictions of observed OH reactivity in forested regions in Suriname (Sinha et al., 2008) and Borneo (Whalley et al., 2011; Edwards et al., 2013). Model calculations of OH reactivity in Borneo underestimated the observed diurnal mean reactivity by 30 %, and indicated that uncertainties in the chemistry and deposition rates of secondary oxidation products could potentially explain the observed reactivity without the need for additional primary VOC emissions, and that at least 50 % of the carbon-containing compounds which react with OH were not measured (Edwards et al., 2013). Biogenic VOCs also dominated the daytime OH reactivity in the Pearl River Delta region, China, with isoprene and its oxidation products comprising ~ 40 % of the total OH reactivity in the afternoon and observed reactivity underestimated by ~ 50 % when calculated from measured OH sinks but reproduced by model calculations considering the contributions from secondary oxidation products (Lou et al., 2010). However, observations of OH reactivity in a forested region in Colorado,

USA, during the BEACHON-SRM08 campaign were underestimated by model calculations ($\sim 30\%$), with the dominant VOCs found to be 2-methyl-3-buten-2-ol (MBO) and monoterpenes (Nakashima et al., 2014).

Using a branch enclosure technique, Kim et al. (2011) demonstrated that underestimations of observed OH reactivity at the PROPHET field site, Michigan, USA, during the 2009 CABINEX campaign were related to oxidation products of known and measured biogenic VOCs, rather than to unknown or unmeasured primary VOC emissions. Model calculations were able to reproduce the CABINEX OH reactivity observations below the forest canopy, but discrepancies were apparent above the canopy, indicating the presence of unmeasured trace gases above the forest canopy (Hansen et al., 2014). Model calculations and experiments using the comparative reactivity method at a forested site in Finland also observed differences between OH reactivity measured in the forest canopy and above the canopy (Mogensen et al., 2011; Nölscher et al., 2012). While the in-canopy reactivity was typically higher than the above-canopy reactivity, transport of wildfire plumes to the site significantly increased the above-canopy reactivity, increasing it above the in-canopy level and increasing the “missing” reactivity above the canopy from 58 % for “normal” conditions to 73 % for periods impacted by transported pollution (Nölscher et al., 2012).

OH reactivity measurements have also been used to determine ozone production rates in southwestern Spain during the DOMINO campaign (Sinha et al., 2012) and in London during the ClearfLo campaign (Whalley et al., 2016), and have been used in laboratory studies to assess our understanding of combustion systems (Nakashima et al., 2010) and atmospheric isoprene oxidation mechanisms (Nakashima et al., 2012; Nölscher et al., 2014).

Measurements of OH reactivity thus have a number of applications, and can be used to improve our understanding of atmospheric composition and chemistry. In this work we present the design and characterisation of an instrument using laser flash photolysis coupled with laser-induced fluorescence (LFP-LIF) to measure OH reactivity in the field and in chamber experiments.

2 Experimental

A schematic of the OH reactivity instrument is given in Fig. 1. The instrument comprises a reaction cell (described in Sect. 2.1) and a detection cell (described in Sect. 2.2), with the two cells typically situated approximately 5 m above ground level on the roof of a shipping container housing the FAGE (fluorescence assay by gas expansion) mobile laboratory during ambient measurements. During laboratory and chamber measurements, the instrument is configured within the laboratory. Thus, for ambient measurements, and laboratory and chamber measurements made at room temperature,

the temperature in the OH reactivity instrument is the same as the source of the air being sampled.

2.1 Reaction cell

The reaction cell consists of a cylindrical stainless steel tube of 50 mm internal diameter and 85 cm in length. Ambient air is drawn through a stainless steel sampling line (50 mm internal diameter and 20 cm in length), enters the reaction cell at 90° to the air flow in the tube, and is drawn along the tube by an extractor fan (612F, DC Axial Fan, EBM-Papst) mounted on the exit arm situated immediately prior to the OH detection cell (Sect. 2.2), as shown in Fig. 1. More recently, the connection between the reaction cell and the exhaust has been replaced with an exhaust that draws air out of the cell over the full circumference of the cell. Although the data recorded with the new exhaust are not reported in this paper, we do not see any significant change in results between the different exhaust designs, but this will be discussed in future publications.

The fan speed determines the flow rate of gas in the reaction cell, and is set to ensure a laminar flow of air through the cell with a Reynold's number less than 2300. The flow rate of gas, determined by measurement of the flow velocity using a hot-wire anemometer (TSI Air velocity transducer 8455-150) or set by calibrated mass flow controllers during laboratory experiments (Sects. 4, 6, and 7) and measurements of instrument zeroes (Sect. 3.1), is in the range 12 to 14 standard L min^{-1} , giving a residence time of 7 to 8 s in the reaction cell and a Reynold's number of ~ 360 , which is below that required for laminar flow.

Production of OH radicals within the reaction cell is achieved by the 266 nm laser photolysis of O_3 in the presence of water vapour (Reactions R4–R5). A flashlamp pumped Nd:YAG laser (Big Sky Laser CFR 200, Quantel USA) is used to generate laser light at 1064 nm, which is frequency doubled to 532 nm (lithium triborate, LiB_3O_5 , doubling crystal) and then frequency doubled to generate the fourth harmonic 266 nm radiation (caesium lithium triborate, $\text{CsLiB}_6\text{O}_{10}$, doubling crystal) with pulse energies of ~ 50 mJ, pulse length 8 ns, and beam diameter of 6.35 mm. The pulse repetition frequency is typically 1 Hz, and has been varied in experiments between 0.1 and 1 Hz with no significant impact observed. The laser is operated with a Q -switch to modulate the intracavity losses and maximise the pulse energy.

The 266 nm laser head is situated adjacent to the reaction cell in order to minimise the footprint of the instrument when used in the field. The laser head is powered, controlled and water cooled by an Integrated Cooler and Electronics unit (Big Sky Laser ICE450, Quantel USA) which is housed within the FAGE shipping container and powered via an uninterruptible power supply (APC 1000VA, American Power Conversion by Schneider Electric).

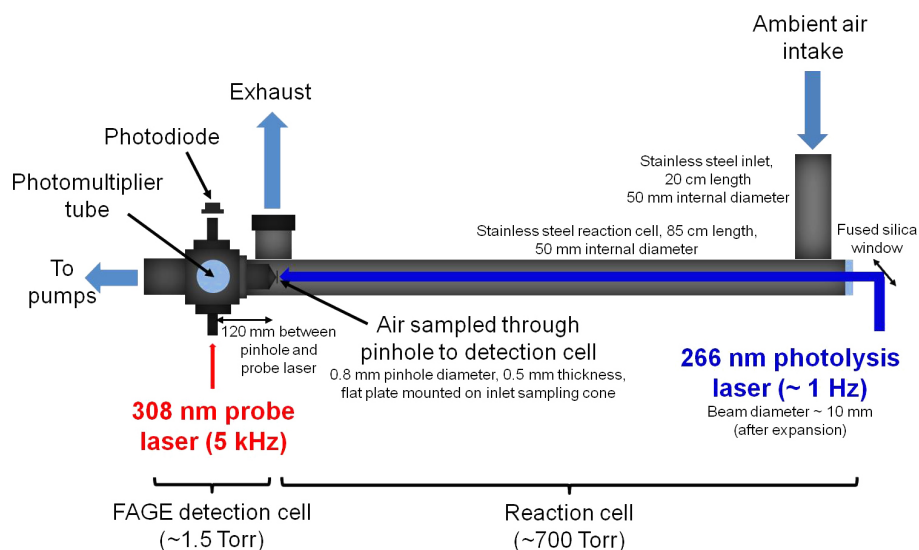


Figure 1. Schematic of the laser flash photolysis laser-induced fluorescence OH reactivity instrument for experiments and field measurements in which the FAGE detection cell was situated at the end of the reaction cell and sampled from the centre of the photolysed volume, leading to OH decays described by a single exponential. All laboratory and field measurements shown in this work were obtained with the instrument configuration as shown here. See text for further details.

Laser light exiting the laser head is directed into the reaction cell using two dielectrically coated 266 nm turning mirrors of 1" diameter (Thorlabs, NB1-K04). Immediately prior to the reaction cell, the 266 nm beam is expanded to a diameter of ~ 10 mm by a telescope incorporating a plano-concave lens (Thorlabs LC4252, focal length = -30 mm) and a plano-convex lens (Thorlabs LA4148, focal length = 50 mm) housed in a lens tube (SM1M20, Thorlabs) to increase the photolysis volume within the reaction cell. The photolysis laser enters the reaction cell through a fused silica window, initiating OH radical production.

Typically, there is sufficient production of OH in the instrument from Reactions (R4–R5) at ambient concentrations of O_3 and water vapour in order to measure a temporal decay of OH. At low ambient concentrations of O_3 (< 10 ppb) or during laboratory tests (Sects. 4, 6 and 7) and measurement of instrument zeroes (Sect. 3), the OH radical concentration in the reaction cell is increased by passing a small flow (0.5 standard L min^{-1}) of humidified ultra-high purity air (BTCA 178, BOC Special Gases) across a low pressure Hg vapour lamp and mixed with the main sampled air flow (12 – 14 standard L min^{-1}) in the inlet to the reaction cell. The mixing ratio of ozone in the reaction cell is increased by ~ 50 ppb by this method (measured by an ozone analyser (Thermo Environmental Instruments Inc., 49C O_3 Analyser) situated at the end of the reaction cell during laboratory tests). Given knowledge of the rate coefficient for reaction of OH with O_3 ($k_{\text{OH}+\text{O}_3} = 7.3 \times 10^{-14} \text{ cm}^3 \text{ s}^{-1}$, Atkinson et al., 2004), the chemical loss of OH resulting from the addition of 50 ppb O_3 is $< 0.1 \text{ s}^{-1}$ at 298 K, and any loss of VOCs

in the reaction cell through reaction with ozone is extremely small given the reaction times involved.

2.2 OH detection cell

OH radicals in the reaction cell are monitored by laser-induced fluorescence (LIF) using the FAGE technique. The LIF-FAGE detection cell has been described previously in detail (Ingham et al., 2009), thus only a brief description will be given here.

Initial experiments were conducted with the detection cell situated midway along the reaction cell, and sampling at 90° to the direction of air flow along the reaction cell, in a similar design to that described by Sadanaga et al. (2004a) and Lou et al. (2010). However, the observed OH decays in such a configuration displayed biexponential behaviour, comprising a fast initial decay followed by a slower decay representative of the expected OH reactivity, as observed in previously described instruments (Sadanaga et al., 2004a; Lou et al., 2010). In this configuration, the photolysis laser is aligned such that the beam passes across the inlet to the detection cell without hitting the inlet. The air sampled in to the detection cell thus likely contains air that has experienced the photolysis laser (containing elevated OH concentrations) and air that has not experienced the photolysis laser (which will have significantly lower or zero OH concentrations), with this mixing of air potentially leading to an apparent increase in the initial OH decay rate owing to dilution of the air containing elevated OH concentrations with air containing lower (or zero) concentrations. Once mixing of the air having experienced the photolysis laser with that outside the beam diameter has

occurred sufficiently to give uniform OH concentrations in the reaction cell the observed OH decay will result from the chemical losses in the instrument, leading to biexponential decays. Such biexponential behaviour has been attributed to similar effects of non-homogeneous spatial distributions of OH near the inlet to the detection cell (Lou et al., 2010) and to local heating and turbulence of the gas flow caused by the photolysis laser (Sadanaga et al., 2004a). A comparison between sampling at 90° to the direction of air flow along the reaction cell and sampling along the axis of the direction of air flow from the centre of the reaction cell has been reported previously (Amedro et al., 2012), with different fitting procedures required to extract the OH reactivity for the different instrument configurations attributed to differences in physical effects such as diffusion which were more significant when sampling at 90° (Amedro et al., 2012).

Subsequent experiments in this work (including all those described below) were performed with the detection cell situated at the end of the reaction cell along the same axis as the direction of air flow to sample air directly from the centre of the reaction cell. This configuration reduces the chance of sampling air into the detection cell that has not experienced the photolysis laser beam, and thus reduces the impact of physical effects such as diffusion. The observed OH signals in this instrument configuration are described by a single exponential decay, although biexponential decays can still be obtained if the photolysis laser is not correctly aligned along the axis of the reaction cell.

Air is sampled from the centre of the reaction cell through a pinhole of 0.8 mm diameter and 0.5 mm thickness into the aluminium detection cell, which consists of three orthogonal axes and is black anodised to minimise light scattering within the cell. The pressure in the cell is measured by a capacitance manometer (Sensotec Z/606-01ZA) and is maintained at ~ 1.5 Torr by a roots blower backed by a rotary pump (Leybold Vacuum SV200/WAU1001), resulting in an air flow of approximately $4 \text{ standard L min}^{-1}$ and a supersonic expansion of the air as it is drawn through the pinhole.

The probe laser consists of a Nd:YAG pumped Ti:sapphire laser (Photonics Industries) which generates broadband radiation in the range 690–1000 nm. A diffraction grating is used to select radiation with $\lambda = 924 \text{ nm}$, which is frequency tripled through generation of the second harmonic at 462 nm followed by sum-frequency mixing of the 462 nm radiation with that at 924 nm to produce the 308 nm light with a pulse repetition frequency (PRF) of 5 kHz, pulse length (full width half maximum (FWHM)) of 35 ns, laser line width (FWHM) of 0.065 cm^{-1} and beam diameter of $\sim 3 \text{ mm}$ (Bloss et al., 2003).

A reference fluorescence cell, containing a heated nichrome wire filament and humidified air at ~ 2 Torr to produce a constant stable source of OH radicals from dissociation of water vapour, is used to facilitate tuning the probe laser to the precise wavelength required for the desired OH transition. Approximately 1 mW of the 308 nm laser light is

used for this purpose, with $\sim 9 \text{ mW}$ used to make measurements of OH reactivity and a further $\sim 13 \text{ mW}$ remaining to make measurements of ambient OH, HO_2 and RO_2 concentrations in a separate instrument (see, for example, Whalley et al., 2016).

The probe laser, reference cell and pumps are all situated inside the shipping container. The $\sim 9 \text{ mW}$ of the 308 nm laser light used to measure OH reactivity is passed to the detection cell on the roof of the shipping container via an anti-reflective coated optical fibre with an angled and polished end (Oz Optics, QMMJ-55-UVVIS-200/240-3-30-AR2-SP, length = 30 m) through a baffled side-arm at 90° to the air flow. The probe laser light exits the detection cell through a baffled side-arm and is directed onto a photodiode (New Focus Large Area Photoreceiver 2032) to measure the laser power to enable normalisation of fluorescence signals for fluctuations in laser power. For a recent intercomparison at the SAPHIR chamber, the OH reactivity instrument, comprising the reactor flowtube and OH fluorescence and associated equipment was placed in the shipping container itself.

Fluorescence from electronically excited OH radicals resulting from excitation of the $Q_1(1) A^2\Sigma^+ (v' = 0) - X^2\Pi_{3/2} (v'' = 0)$ transition at 308 nm is collimated by a symmetrical biconvex collimating lens (Melles-Griot, focal length = 50 mm at $\lambda = 546.1 \text{ nm}$, diameter = 50 mm) and focused onto the photocathode of a channeltron photomultiplier tube (PMT) (Perkin Elmer C 943P) by two plano-convex focusing lenses (UQG Optics Ltd., focal length = 75 mm at $\lambda = 250 \text{ nm}$, diameter = 50 mm). A narrow band UV interference filter (Barr Associates Inc., FWHM bandwidth of $8 \pm 1.6 \text{ nm}$ centred at $309 \pm 1 \text{ nm}$ with a peak transmission of $> 50\%$ at 308 nm and a blocking factor of 10^6 at other wavelengths) is situated between the excitation region in the detection cell and the PMT to minimise detection of scattered solar photons. The solid angle from which fluorescence is collected is effectively doubled through the use of a spherical concave mirror coated for high UV reflectance which is mounted in the detection cell opposite the side-arm bearing the PMT. Discrete photon signals on the PMT are processed using a multi-channel scaler photon counting card (Becker and Hickl, PMS 400, minimum bin width of 250 ns) in the computer used to control the instrument.

2.3 Instrument control

A digital delay pulse generator (Stanford Research Systems DG535) produces a 5 kHz TTL (transistor-transistor logic) pulse to trigger the Ti:sapphire laser and a second delay generator (Stanford Research Systems DG535) which subsequently triggers the gating of the PMT detector for the reactivity instrument and a third digital delay pulse generator (Berkeley Nucleonics Corporation 555) to trigger the 266 nm photolysis laser and the photon counting card at the specified pulse repetition frequency in synchronisation with the

308 nm probe laser. A personal computer is used to automate data collection, with analogue signals from measurements of the pressure in the detection cell and the power of the 308 nm probe laser at the photodiode attached to the detection cell digitised by an A/D card (Measurement Computing, PCI-DAS 1200). Electrical power to all parts of the instrument is supplied via an uninterruptible power supply (APC 1000VA).

2.4 Data acquisition

Data acquisition is initiated by triggering of the photon counting card, with a background signal measured for 100 ms before triggering of the 266 nm photolysis laser and production of OH in the reaction cell. To avoid saturation of the PMT resulting from detection of the 308 nm laser pulse itself, the PMT is gated off at the onset of the 308 nm laser pulse (35 ns FWHM) until ~ 100 ns after the laser pulse, thereby preventing detection of any reflected or scattered laser light. The fluorescence signal is typically collected for 1 μ s following each 308 nm probe laser pulse. Repeated measurements of the OH fluorescence signal are taken for 900 ms following each 266 nm photolysis laser pulse, during which time the OH concentration and hence the fluorescence signal will decay to the background level. Under normal conditions this occurs within ~ 300 ms of the photolysis laser pulse, although this is of course dependent upon the magnitude of the OH reactivity, and may be longer. The pulse repetition frequency of the 308 nm probe laser (5 kHz) results in measurement of the OH fluorescence signal every 200 μ s throughout the measurement period. The data collection cycle, as illustrated in Fig. 2 is typically repeated every 1 s (i.e. with the photolysis laser having a pulse repetition frequency of 1 Hz). Experiments, both in the laboratory and in the field, in which the PRF of the photolysis laser was varied between 0.1 and 1 Hz showed no effect on the observed OH reactivity (Sect. 8).

When measurements of OH reactivity are made alongside those of ambient OH concentrations, the acquisition of OH reactivity data is linked to measurements of ambient OH concentrations owing to the dual use of the 308 nm excitation laser. Under such circumstances, measurements are taken on an approximate 7 min cycle, with a 5 min “online” period during which the 308 nm laser is at the precise wavelength to excite the OH transition, followed by a 1 min “offline” period during which the wavelength of the laser is moved to a nearby wavelength at which the OH transition is not excited in order to enable measurement of a background signal for determination of ambient OH concentrations (see, for example, Whalley et al. 2010). Approximately 1 min is then required to scan the laser wavelength over the OH transition to find the maximum OH fluorescence signal in the reference cell (Sect. 2.2). OH reactivity measurements are thus taken during the 5 min online period, and data from successive measurement cycles during each online period are co-added to improve the signal-to-noise ratio. Figure 3 shows typical OH decays de-

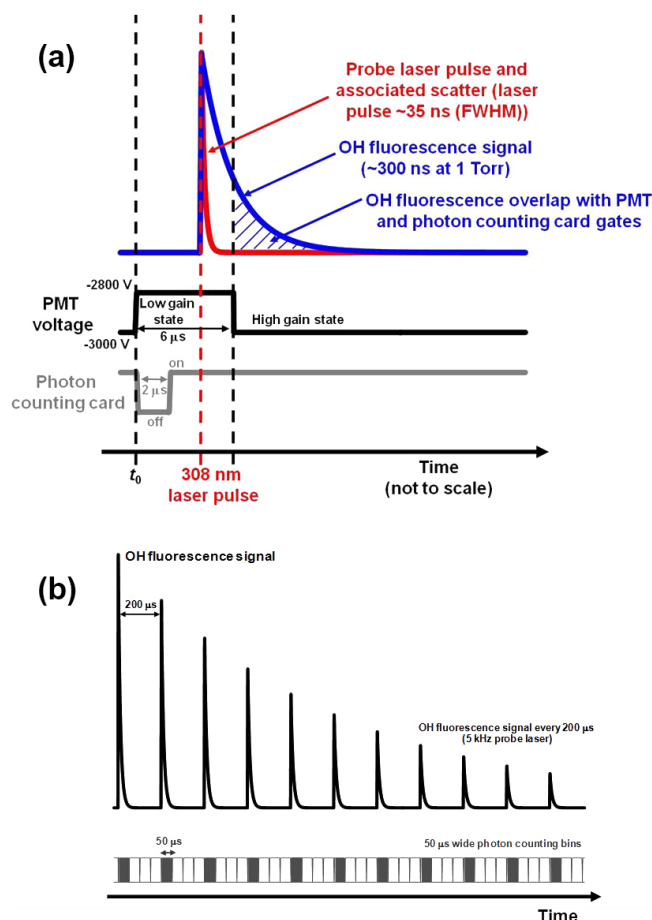


Figure 2. (a) Schematic to illustrate the Stanford Research Systems delay generator controlled gate timing of the PMT detector and photon counting card in the OH reactivity instrument. The blue hatched region indicates the overlap between the OH fluorescence signal and the photon counting gates; (b) Schematic to illustrate the photon counting bin structure used to collect OH fluorescence photons after each 308 nm probe laser pulse (5 kHz pulse repetition frequency). Four 50 μ s wide photon counting bins cover the time period between each 308 nm laser pulse, but only the bins immediately after the laser pulse collect any fluorescence photons (shaded bins), and only the photon counts from these bins are used to construct the OH decay.

rived from the co-addition of data recorded throughout 5 min online periods during the Clean Air for London (ClearfLo) campaign in summer 2012.

Measurements of OH reactivity may also be made independently of any other use of the 308 nm probe laser, in which case the timescale over which successive measurement cycles are co-added may be selected as desired, with the laser periodically scanned over the OH transition to ensure that the maximum OH signal is obtained.

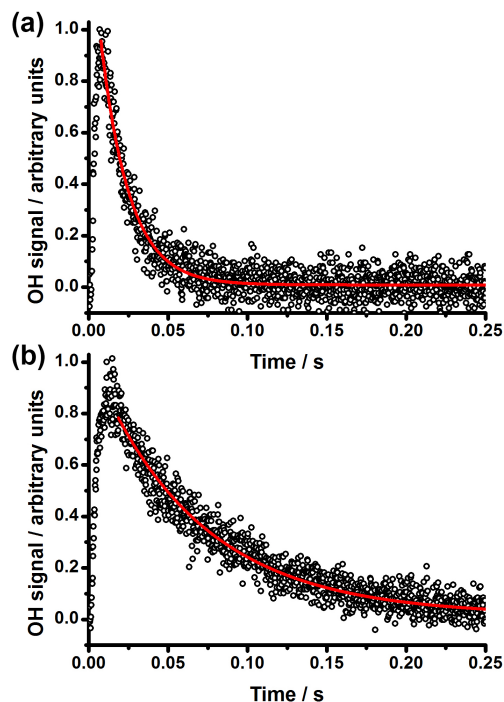
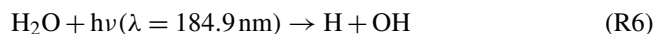


Figure 3. Typical OH time profiles following photolysis of ambient air (mixed with a small flow of $\text{N}_2/\text{O}_2/\text{O}_3/\text{H}_2\text{O}$) observed during the Clean Air for London (ClearFLo) campaign (black points) with fits of Eq. (5) (red lines) to the LIF data to determine k'_{OH} for data recorded (a) during a polluted period on 25 July 2012 ($k'_{\text{OH}} = (46.6 \pm 3.2) \text{ s}^{-1}$) and (b) during a cleaner period on 7 August 2012 ($k'_{\text{OH}} = (13.9 \pm 0.9) \text{ s}^{-1}$). Time zero is defined as the time at which photolysis occurs. Decays represent data co-added throughout 5 min periods.

2.5 Calibration of the FAGE detection cell

Calibration of the detection cell, although not strictly necessary for measurements of OH reactivity, is required to ensure that pseudo-first-order conditions are met in the reaction cell (i.e. combined concentrations of OH sinks are in excess over the OH concentration) and provides a means to determine any potential interferences from production of OH via ambient $\text{HO}_2 + \text{NO}$ in the reaction cell (from ambient HO_2 which may survive the sampling inlet, and any HO_2 generated following oxidation of OH sinks in the instrument) and to monitor potential changes in instrument sensitivity with time.

The calibration procedure has been described in detail by Commane et al. (2010). Production of OH (and HO_2) is achieved through Reaction (R1) (and HO_2 through Reaction R2) by passing a turbulent flow of humidified ultra-high purity air (BTCA 178, BOC Special Gases) across a low pressure mercury vapour lamp to photolyse water vapour at $\lambda = 184.9 \text{ nm}$.



The concentration of OH is given by Eq. (4):

$$[\text{OH}] = [\text{H}_2\text{O}] \sigma_{\text{H}_2\text{O}} \varphi_{\text{OH}} F \delta t, \quad (4)$$

where $\sigma_{\text{H}_2\text{O}}$ is the absorption cross-section of H_2O at 184.9 nm ($7.1 \pm 0.2 \times 10^{-20} \text{ cm}^2$ (Cantrell et al., 1997; Creasey et al., 2000)), φ_{OH} is the quantum yield for OH production ($\varphi_{\text{OH}} = 1$), F is the photon flux of the mercury lamp at 184.9 nm and δt is the residence time in the photolysis region. The product $F \delta t$ is determined by N_2O actinometry (Commane et al., 2010), with F varied by changing the current supplied to the lamp, and δt controlled by the flow rate of the gas used in the calibration. The concentration of water vapour in the flow is determined by diverting a small known flow of the air to a dew point hygrometer (CR4, Buck Research Instruments), and was varied between 300 and 10 000 ppm during calibration experiments.

The calibration for OH was conducted over a range of mercury lamp fluxes and water vapour mixing ratios (between 300 and 10 000 ppm), giving a calibration factor (C_{OH}) of $(2.13 \pm 0.27) \times 10^{-8} \text{ counts s}^{-1} \text{ molecule}^{-1} \text{ cm}^3 \text{ mW}^{-1}$. The 1σ instrumental limit of detection for OH radicals was determined to be $\sim 10^7 \text{ cm}^{-3}$ for a 5 min integration period, enabling observation of sufficient changes in OH radical concentrations in the reaction cell to allow measurements of ambient OH reactivity.

For a minimum ambient O_3 mixing ratio of 10 ppb (below which $\sim 50 \text{ ppb}$ is added to the instrument (Sect. 2.1), an absorption cross-section for O_3 of $9.65 \times 10^{-18} \text{ cm}^2$ at 266 nm (Atkinson et al., 2004), typical laser fluence of $\sim 50 \text{ mJ cm}^{-2}$ and a quantum yield of 0.9 for production of $\text{O}(^1\text{D})$ (Matsumi et al., 2002), the initial $\text{O}(^1\text{D})$ number density following photolysis is $\sim 1.6 \times 10^{11} \text{ cm}^{-3}$. For a water vapour concentration of $5 \times 10^{17} \text{ cm}^{-3}$ ($\sim 2\%$), competition between reaction of $\text{O}(^1\text{D})$ with water ($k_{\text{O}^1\text{D}+\text{H}_2\text{O}} = 2.1 \times 10^{-10} \text{ cm}^3 \text{ s}^{-1}$, Atkinson et al., 2004), leading to 2 OH, and quenching of $\text{O}(^1\text{D})$ by N_2 ($k_{\text{O}^1\text{D}+\text{N}_2} = 3.1 \times 10^{-11} \text{ cm}^3 \text{ s}^{-1}$, Atkinson et al., 2004) or O_2 ($k_{\text{O}^1\text{D}+\text{O}_2} = 4.0 \times 10^{-11} \text{ cm}^3 \text{ s}^{-1}$, Atkinson et al., 2004), to produce $\text{O}(^3\text{P})$, typically leads to an initial OH concentration in the reactivity instrument of $> 3 \times 10^{10} \text{ cm}^{-3}$, in agreement with the calibration results. At higher ambient mixing ratios of O_3 , the initial OH concentration in the reactivity is increased, whilst maintaining pseudo-first-order conditions for OH. For example, an ambient O_3 mixing ratio of 100 ppb, as observed in some polluted environments, would be expected to generate $> 3 \times 10^{11} \text{ cm}^{-3}$ OH (at 2% humidity), leading to improvements in the signal-to-noise ratio and minimisation of any potential interferences in measurements of OH reactivity (Sect. 6).

3 Determination of OH reactivity

The observed pseudo-first-order rate coefficient for OH loss (k_{loss}) is determined by least-squares fitting Eq. (5) to the time-resolved OH decay:

$$S_{\text{OH},t} = S_{\text{OH},0} \exp(-k_{\text{loss}}t) + b, \quad (5)$$

where $S_{\text{OH},t}$ is the fluorescence signal at time t after firing of the 266 nm photolysis laser, $S_{\text{OH},0}$ is the fluorescence signal at time zero (i.e. immediately following firing of the 266 nm laser and production of OH in the reaction cell), k_{loss} is the observed rate coefficient for loss of the fluorescence signal, t is the time since firing of the 266 nm photolysis laser and b is the background fluorescence signal measured by the PMT averaged for the 100 ms prior to firing of the photolysis laser (typically zero). Fits are typically started within 5 ms of the peak in the OH signal, and data are fitted until the OH signal is essentially back to the background level by the end of the fit. Values for $S_{\text{OH},0}$ and k_{loss} are permitted to vary in the fitting process. Since the OH decays are well described by first-order kinetics, the fitted values for $S_{\text{OH},0}$ and k_{loss} do not depend in any way on the time period over which the decays are fitted. Figure 3 shows typical fits of Eq. (5) to measurements of OH reactivity made in ambient air.

The value for k_{loss} determined from the fit contains a contribution from $k'_{\text{OH,obs}}$, the rate coefficient for OH loss owing to chemical losses of OH in the reaction cell (the OH reactivity), and k_{phys} , the instrument “zero” corresponding to the rate coefficient for physical losses of OH owing to diffusion out of the sampling volume and heterogeneous losses on the walls on the reaction cell. The chemical loss of OH in the reaction cell is thus given by Eq. (6), and in order to determine the OH reactivity from measurements of k_{loss} it is therefore essential to characterise k_{phys} (Sect. 3.1).

$$k'_{\text{OH,obs}} = k_{\text{loss}} - k_{\text{phys}} \quad (6)$$

At low ambient concentrations of ozone (< 10 ppb) and in laboratory experiments (Sects. 4, 6 and 7) and measurements of k_{phys} , it was necessary to add a small flow of humidified air containing a constant mixing ratio of ozone (~ 50 ppb) to the main air flow sampled in order to produce sufficient OH radicals in the reaction cell. This “non-ambient” ozone added to the reaction cell results in a small loss of OH owing to the reaction of O_3 with OH, but is expected to be < 0.1 s⁻¹ at 298 K (Sect. 2.1). However, addition of the small ozone-containing air flow (0.5 standard L min⁻¹) to the sampled flow of ambient air (12 standard L min⁻¹) does require a correction for the dilution of the ambient air flow, such that the OH reactivity (k'_{OH}) is given by Eq. (7):

$$k'_{\text{OH}} = k'_{\text{OH,obs}}(1 + f), \quad (7)$$

where f is the dilution factor of the ambient air flow, given by the ratio of the small ozone-containing flow rate to the

total flow rate of the air in the reaction cell (~ 0.04 for the conditions used in this work). Potential errors arising from errors in measurements of k_{phys} and f have been included in overall reported errors for k'_{OH} , and contribute, on average, 70 and 25 %, respectively, to the total uncertainty in k'_{OH} .

3.1 Determination of k_{phys}

Determination of k_{phys} is critical to the evaluation of the true OH reactivity from observations of the total OH loss rate in the instrument (Eqs. 7 and 8), and requires the measurement of the OH loss rate in the absence of any chemical removal processes such that k_{loss} is equal to k_{phys} . A single value for k_{phys} is determined (from several experiments) independently of any measurements of k_{obs} , and is fitted over as much of the observed OH decay as possible using the procedure described above in order to obtain the best possible determination of k_{phys} since fitting k_{phys} over as much of the decay as possible reduces the uncertainty in the fit. As described above, determinations of k_{phys} (and k_{obs}) are independent of the time period over which the data are fitted since the observed OH decays follow first-order kinetics and can be described with a single exponential function.

To minimise the chemical losses of OH in the reaction cell (and thus to minimise $k'_{\text{OH,obs}}$) the loss of OH in the instrument is measured in ultra-high purity air (BTCA 178, BOC Special Gases) passed through scrubbers (Gatekeeper Gas Purifiers) to remove H_2 , CO and CO_2 to sub-ppb levels. Despite the use of scrubbed ultra-high purity air, low levels of residual VOCs can remain in the air, leading to chemical losses. Such residual VOCs in the scrubbed ultra-high purity air have been quantified by gas-chromatography and their contributions (< 1 s⁻¹) to the observed OH loss subtracted.

Furthermore, humidification and addition of a small amount of O_3 to the ultra-high purity air are necessary for the production of OH in the instrument during experiments to determine k_{phys} . Approximately 50 ppb of O_3 is added to ensure production of sufficient OH, leading to a chemical loss of < 0.1 s⁻¹ at 298 K through the reaction of OH with O_3 . Moreover, despite the use of purified water for humidification, obtained using a water purification system (PURELAB flex PRIPLB0163, Elga LabWater, Veolia Water Solutions & Technologies), impurities in the water can lead to significant chemical losses for OH and the components in the purification system must remain uncontaminated in order to ensure accurate determinations of k_{phys} .

Determination of k_{phys} in the laboratory and in the field for the ClearfLo campaign in London in 2012 gave an average value $(1.1 \pm 1.0) \text{ s}^{-1}$ (precision of 0.4 s^{-1}) and $(1.25 \pm 0.42) \text{ s}^{-1}$ (precision of 0.2 s^{-1}) for the campaign in York in 2014 (Sect. 7).

4 Instrumental validation via measurements of $k_{\text{OH}+\text{CO}}$ and $k_{\text{OH}+\text{CH}_4}$

As a real-time technique, the accuracy of the time axis during which the OH decay is obtained is determined by the accuracy of the delay generators used to trigger the lasers and other delays (as described in Sect. 2.4 and shown in Fig. 2), which should be absolute within 1 ps. Hence the method should be absolute in terms of the time separation between points in the decay. However, owing to various reasons, for example the appropriateness of the function used to fit the decay, or any recycling of OH from oxidation products (for example the reaction of HO₂ with NO), it is prudent to characterise the instrument through the use of known concentrations of reactants for which the rate coefficient with OH is also well known. In order to validate measurements of ambient OH reactivity, the well-known rate coefficients for reactions of OH with CO and CH₄ were both measured under pseudo-first-order conditions using the instrumental setup described above. Ultra-high purity air (BTCA 178, BOC Special Gases) was mixed with an excess of either CO (5 % in N₂, BOC Special Gases) or CH₄ (BOC, CP grade, 99.5 %), producing a main flow of 11.5 standard L min⁻¹ with known concentrations of CO or CH₄, prior to mixing with a small flow of humidified air (0.5 standard L min⁻¹) containing ~50 ppb O₃ generated by passing the air flow across a mercury vapour lamp.

Figure 4 shows the OH reactivity, determined by fitting Eq. (5) to the OH decay and subtracting k_{phys} (Sect. 3), for a series of CO and CH₄ concentrations. The bimolecular rate coefficients for OH + CO ($k_{\text{OH}+\text{CO}}$) and OH + CH₄ ($k_{\text{OH}+\text{CH}_4}$), determined at 298 K from the relationships $k'_{\text{OH}} = k_{\text{OH}+\text{CO}}[\text{CO}]$ and $k'_{\text{OH}} = k_{\text{OH}+\text{CH}_4}[\text{CH}_4]$, were found to be $(2.4 \pm 0.2) \times 10^{-13}$ and $(6.4 \pm 0.6) \times 10^{-15} \text{ cm}^3 \text{ s}^{-1}$, respectively (errors are 1 σ). The values for $k_{\text{OH}+\text{CO}}$ and $k_{\text{OH}+\text{CH}_4}$ determined here are in agreement with the literature values of $(2.3^{+0.6}_{-0.5}) \times 10^{-13}$ and $(6.4^{+1.3}_{-1.1}) \times 10^{-15} \text{ cm}^3 \text{ s}^{-1}$ at 298 K (Atkinson et al., 2004), respectively, providing confidence in measurements of ambient OH reactivity.

5 Limit of detection, precision and total uncertainty

The instrumental limit of detection for measurements of k'_{OH} is determined by the fit error in k_{loss} (Eq. 5), the determination of k_{phys} , and its associated uncertainty, and the number of measurements used to determine k_{phys} . For the ClearfLo campaign, k_{phys} was determined to be $(1.1 \pm 1.0) \text{ s}^{-1}$, with a precision of 0.4 s^{-1} and a 1 σ limit of detection for k'_{OH} of 1.0 s^{-1} . During the York campaign (Sect. 7), k_{phys} was determined to be $(1.25 \pm 0.42) \text{ s}^{-1}$, with a precision of 0.2 s^{-1} and a 1 σ limit of detection for k'_{OH} of 0.4 s^{-1} .

Experiments described in Sect. 4 indicate that OH reactivities of up to $\sim 150 \text{ s}^{-1}$ can be measured reliably with

the instrument described in this work, with the possibility for measurements of higher reactivities described in Sect. 9. Replicates of k'_{OH} measurements at fixed concentrations of CO and CH₄ (Sect. 4 and Fig. 4) also enable determination of the instrument precision. The majority of ambient k'_{OH} measurements are $< 35 \text{ s}^{-1}$, for which the measurements under controlled conditions using known concentrations of CO and CH₄ indicate a precision of $\sim 1 \text{ s}^{-1}$. For reactivities of $\sim 110 \text{ s}^{-1}$, which were observed in London during the ClearfLo campaign (Sect. 7, Whalley et al., 2016), measurements using known concentrations of CO and CH₄ indicated a precision of $\sim 5 \text{ s}^{-1}$. In the field, reactivities of up to $\sim 140 \text{ s}^{-1}$ have also been measured, with fit errors of $\sim 6 \text{ s}^{-1}$, although the precision at higher reactivities is worse compared to lower reactivities.

On average, the total uncertainty in measurements of k'_{OH} is 6 %, with the uncertainty in k_{phys} comprising ~ 70 % of the total uncertainty. When addition of O₃ to the instrument is necessary to improve the OH signal (at ambient mixing ratios of O₃ of less than 10 ppb and during laboratory experiments and measurements of k_{phys}), the uncertainty associated with the dilution of the main flow contributes ~ 25 % to the total uncertainty in k'_{OH} .

6 Potential interferences

Potential interferences in measurements of k'_{OH} were investigated through model simulations of OH decay traces under various scenarios to investigate the possible effects of OH recycling, and subsequent impacts on measurements of k'_{OH} , through the reaction of ambient NO with any HO₂ or RO₂ radicals that may be generated within the instrument.

The initial OH concentration in the instrument, following photolysis of O₃ by the 266 nm laser, is estimated at $> 3 \times 10^{10} \text{ cm}^{-3}$ (Sect. 2.5), with no co-production of HO₂ following photolysis of O₃. However, there is production of HO₂ from the reaction of OH with CO in the instrument, and of RO₂ radicals from the reactions of OH with VOCs. The HO₂ radicals produced have the potential to recycle OH through reactions with NO, which would lead to an apparent reduction in the observed OH reactivity. In addition, there is potential for production of HO₂ from the photolysis of oxygenated volatile organic compounds (oVOCs) in the instrument, with previous studies indicating significant radical production following photolysis of oVOCs in urban environments (Volkamer et al., 2010; Sheehy et al., 2010). During the ClearfLo campaign in London (Sect. 7), the mean observed HCHO mixing ratio was 9.3 ppb, potentially leading to production of $\sim 1 \times 10^8 \text{ cm}^{-3}$ HO₂ following the photolysis of HCHO at 266 nm within the reactivity instrument. Other oVOCs, notably CH₃CHO, C₃H₇CHO, IPRCHO ((CH₃)₂CHO), C₄H₉CHO, methacrolein (MACR) and methyl vinyl ketone (MVK) during the ClearfLo campaign, are also potentially photolysed by the 266 nm laser

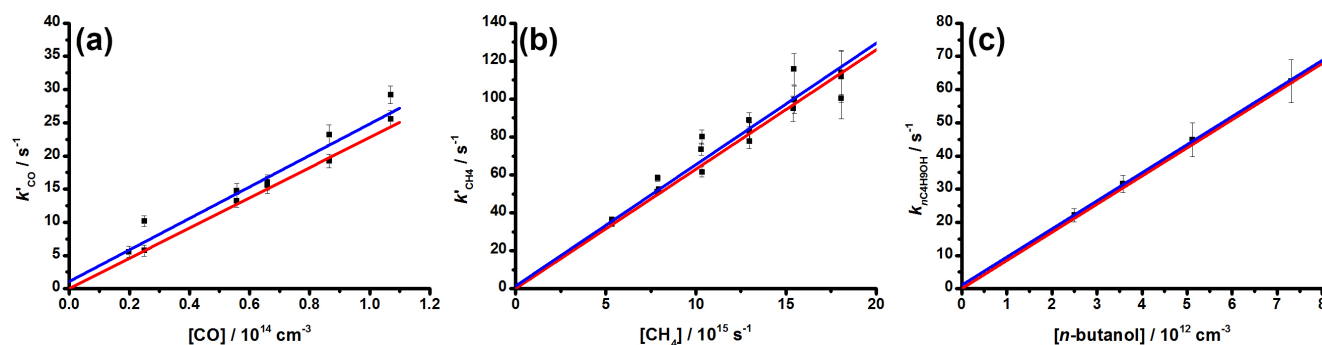


Figure 4. Bimolecular plots of pseudo-first-order rate coefficients describing OH loss (k'_{OH}) against known concentrations of reactive gases during laboratory tests (black points) with best fit lines (blue) and literature values (red) for (a) CO at 298 K (intercept = 1.1 s^{-1}); (b) CH₄ at 298 K (intercept = 1.3 s^{-1}); (c) *n*-butanol (*n*-C₄H₉OH, sampling from the chamber) at 298 K (intercept = 1.1 s^{-1}). Literature values are taken from Atkinson et al. (2004). Corrections for dilution have been applied (Eq. 7). Errors are 1σ from the fits to the observed OH decays. Note the change in vertical scale between the three panels.

in the OH reactivity instrument, leading to production of HO₂. For the mean oVOC mixing ratios observed during ClearfLo, and literature absorption cross-sections at 266 nm (Atkinson et al., 2004), there is potential for production of $\sim 2.5 \times 10^8 \text{ cm}^{-3}$ HO₂ in the reactivity instrument, including that produced by photolysis of HCHO, with CH₃CHO representing the dominant oVOC photolysed. The effects of HO₂ and RO₂ radicals produced by OH reactions within the instrument, and of HO₂ production following oVOC photolysis, were therefore investigated over a range of NO mixing ratios.

Model simulations, using the numerical integration package Kintecus (Ianni, 2002), were initiated with a conservative estimate of the initial OH radical concentration of $1 \times 10^{10} \text{ cm}^{-3}$ and a total OH reactivity of 25 s^{-1} comprised of losses to CO (producing HO₂), VOCs (producing RO₂) and NO₂ (leading to loss of radicals from the system). The relative contributions of CO and VOCs to the total OH reactivity (7 and 68 %, respectively) were set to the average values determined by Whalley et al. (2016) for field measurements in London (Sect. 7). The contribution from NO₂ was set to increase with increasing NO in the model with the NO₂ : NO ratio set to the average ratio observed during measurements in London (Bohnenstengel et al., 2015; Whalley et al., 2016), and the model includes the reaction between HO₂ and NO₂ to form HO₂NO₂, and the reverse reaction (which is slow and negligible on the timescale of the reactivity measurement). Initial concentrations of HO₂ were, in separate model simulations, set to 0, 1×10^8 and $2.5 \times 10^8 \text{ cm}^{-3}$ to investigate the potential effects of oVOC photolysis. Initial mixing ratios of NO were varied from zero to 75 ppb, the maximum observed during field measurements of k'_{OH} in London in 2012 (Whalley et al., 2016). The model was run forwards in time and output for OH was analysed in an identical manner to that applied to the OH decays measured by the reactivity instrument to determine k'_{OH} . Comparison of

the values for k'_{OH} determined by fitting to the simulated OH decays to the total reactivity input to the model thus enables assessment of any potential interferences.

Figure 5 shows the impact of NO on the OH reactivity determined by fitting to the model output for OH. For model simulations with the initial concentration of HO₂ set to zero (i.e. no photolytic sources of HO₂), but with subsequent generation of HO₂ following reaction of OH with CO, it can be seen that the OH reactivity determined by fitting to the model output for OH shows only a small deviation of from the true OH reactivity in the model, through the recycling of OH through HO₂ + NO. At 75 ppb of NO, the deviation from the true OH reactivity is $\sim 4 \%$, which is less than the overall uncertainty in measurements of k'_{OH} . For model runs which simulate photolytic production of HO₂ from oVOCs, with initial HO₂ concentrations of 1.0×10^8 or $2.5 \times 10^8 \text{ cm}^{-3}$, it can be seen that the impact of OH recycling through HO₂ + NO is dependent on the initial OH concentration. For initial OH concentrations of 10^9 cm^{-3} , the impact of photolytic HO₂ production is potentially large, with a deviation of 18 % from the true reactivity for an initial HO₂ concentration of $1.0 \times 10^8 \text{ cm}^{-3}$ and a deviation of 10 % for an initial HO₂ concentration of $2.5 \times 10^8 \text{ cm}^{-3}$ at 75 ppb of NO. However, as discussed in Sect. 2.5, the initial OH concentration produced in the instrument is expected to be significantly higher than 10^9 cm^{-3} . For an initial OH concentration of 10^{10} cm^{-3} , which is still a conservative estimate of the initial OH concentration, the impact of any photolytically generated HO₂ is minimal, with the deviation from the expected OH reactivity at 75 ppb of NO similar to that determined in the absence of any photolytically produced HO₂ at $\sim 5 \%$. However, we note that it is not possible to fully assess the impact of unmeasured or unknown oVOCs, and recommend maintaining high initial OH concentrations in the reactivity instrument in order to maximise the OH : HO₂ ra-

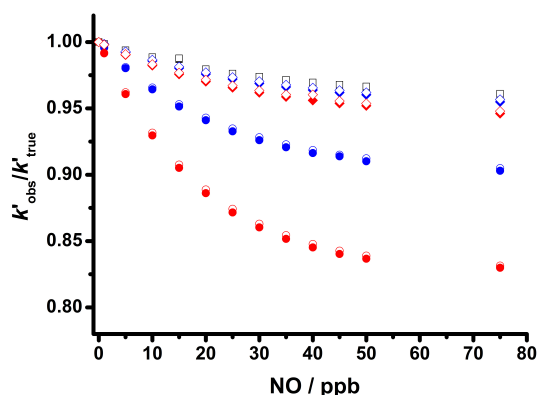


Figure 5. Impact of NO on the ratio of the k'_{OH} fitted to model simulations for OH to the k'_{OH} used as input for the model (i.e. the equivalent of $k'_{\text{observed}}/k'_{\text{true}}$). Black points show results for model simulations with the initial HO_2 concentration set to zero; blue data points show results for model simulations with the initial HO_2 concentration set to $1 \times 10^8 \text{ cm}^{-3}$; red data points show results for model simulations with the initial HO_2 concentration set to $2.5 \times 10^8 \text{ cm}^{-3}$; circles represent data points with an initial OH concentration of 10^9 cm^{-3} ; diamonds represent data points with an initial OH concentration of 10^{10} cm^{-3} ; filled data points represent simulations with the initial RO_2 concentration set to zero; open data points represent simulations with an initial RO_2 concentration of $1 \times 10^{10} \text{ cm}^{-3}$.

tio and thereby minimise any potential interferences arising from production of HO_2 in the instrument.

Model simulations were also performed with an initial RO_2 concentration of $1 \times 10^{10} \text{ cm}^{-3}$ to investigate the possible effects of incompletely refreshing the gas sample in the reactivity instrument between photolysis pulses, which could potentially lead to increased RO_2 concentrations in the reaction cell through $\text{OH} + \text{VOC}$ reactions. A reaction between RO_2 and OH was also added to the model, with a rate coefficient of $1 \times 10^{-10} \text{ cm}^3 \text{ s}^{-1}$, as observed for $\text{CH}_3\text{O}_2 + \text{OH}$ (Bossolasco et al., 2014) and $\text{C}_2\text{H}_5\text{O}_2 + \text{OH}$ (Farago et al., 2015). Figure 5 shows that the impact of RO_2 chemistry within the instrument is not expected to have a significant impact on the observed OH reactivity, with the potential increase in observed OH reactivity of 1 s^{-1} from an initial RO_2 concentration of $1 \times 10^{10} \text{ cm}^{-3}$ and $k_{\text{RO}_2 + \text{OH}} = 1 \times 10^{-10} \text{ cm}^3 \text{ s}^{-1}$, being less than the total uncertainty in ambient measurements of k'_{OH} . In addition, experiments in which the pulse repetition frequency of the photolysis laser was varied between 0.1 and 1 Hz, thus varying the extent to which the gas sample was replaced between laser pulses, did not show any significant change in the observed OH reactivity. Despite the expectation that the impact of $\text{OH} + \text{RO}_2$ chemistry on observations of k'_{OH} will be minimal, we include an additional 1 s^{-1} uncertainty in ambient measurements of k'_{OH} to reflect the potential for interferences owing to RO_2 production in the reactivity instrument. We note that the contribution to the uncertainty in the total

OH reactivity from $\text{RO}_2 + \text{OH}$ chemistry is itself subject to significant uncertainty and the additional 1 s^{-1} uncertainty applied to the total OH reactivity represents an upper limit which is included in order to be thorough and complete.

We thus conclude that the reactivity instrument described in this work does not suffer from significant interferences associated with potential production of HO_2 or RO_2 within the instrument. We do note, however, that measurements of OH reactivity using this instrument in environments which may contain significant concentrations of oVOCs would benefit from high initial concentrations of OH. We also note that any OH decays observed during field or laboratory experiments that cannot be reliably fitted by a single exponential function describing a first-order loss for OH (Eq. 5) would be treated with caution and, where appropriate, other fitting functions would be applied.

7 Field measurements

The laser flash photolysis OH reactivity instrument was deployed at the North Kensington measurement site ($51^\circ 31' \text{ N}$, $0^\circ 12' \text{ W}$) during the Clean Air for London (ClearfLo) summer campaign in July and August 2012 (Bohnenstengel et al., 2014), with near-continuous measurements made from the 21 July to 18 August 2012, alongside FAGE measurements of OH, HO_2 and RO_2 radical concentrations. Measurements of O_3 , CO, NO, NO_2 , HONO, VOCs and aerosol mass and composition were also made at the site during the campaign.

Figure 6 shows the full time series of measured OH reactivity for the campaign. The observed reactivity was highest for air masses that had previously passed over central London (24–27 July (Julian days 206–209) and 8–10 August (Julian days 221–223)), with a maximum reactivity of 116 s^{-1} recorded during rush hour on 24 July 2012. Measurements taken on the 25 July 2012 (Julian day 207) are shown in Fig. 7 to highlight the capability of the instrument, and the average diurnal profile for the campaign is shown in Fig. 8. A peak reactivity, on average, of $\sim 27 \text{ s}^{-1}$ was observed during morning rush hour, with a minimum of $\sim 15 \text{ s}^{-1}$ during the afternoon and a second peak during evening rush hour. Detailed analysis of these data, including model calculations using the Master Chemical Mechanism constrained to observed concentrations of long-lived species, is described by Whalley et al. (2016). The modelling study shows that the observed OH reactivity can be reproduced by the model (to within 6 %) when larger VOCs than those typically measured are included in the model, and demonstrates the importance of oxidation intermediates and the role of heavy VOCs, particularly biogenics, in controlling the total OH reactivity and the oxidation budget in a megacity such as London.

Field measurements of OH reactivity have also been made at a site at the University of York ($53^\circ 56' \text{ N}$, $1^\circ 02' \text{ W}$) from the 19 May to 16 June 2014, approximately 3 km south-east of the centre of York and 2 km west of a major road,

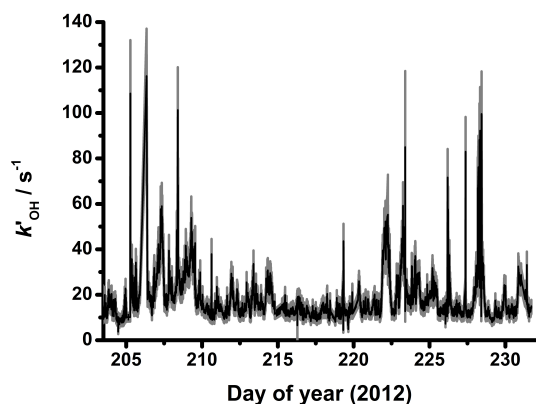


Figure 6. Time series of OH reactivity observed during the Clean Air for London (ClearfLo) campaign (21 July to 18 August 2012). Uncertainties (represented by the shaded area) represent 1σ combined uncertainties from the fits to observed OH decays (Eq. 5), determinations of k_{phys} (Eq. 6) and uncertainties in the dilution factor, f (Eq. 7).

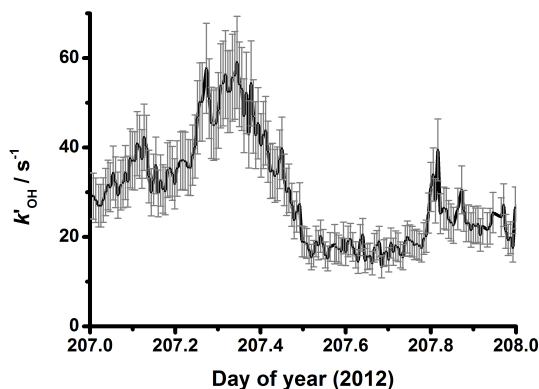


Figure 7. Time series of OH reactivity observed during the Clean Air for London (ClearfLo) campaign on the 25 July 2012 (Julian day 207). Error bars represent 1σ combined uncertainties from the fits to observed OH decays (Eq. 5), determinations of k_{phys} (Eq. 6) and uncertainties in the dilution factor, f (Eq. 7).

with a small wooded area immediately to the east, and thus subject to anthropogenic emissions and local biogenic emissions. Figure 9 shows the average diurnal during this period. The observed OH reactivity was typically lower than that observed during the ClearfLo campaign, with a maximum in the diurnal average of $\sim 6\text{ s}^{-1}$. Measurements of O_3 , CO, NO, NO_2 , VOCs and were also made at the site during this period, alongside measurements by a new instrument coupling an OH reactor to measurements of VOCs by gas chromatography with time of flight mass spectrometry (GC-ToFMS) to aid identification of any “missing” OH reactivity. Detailed analysis of the results will be given in future publications.

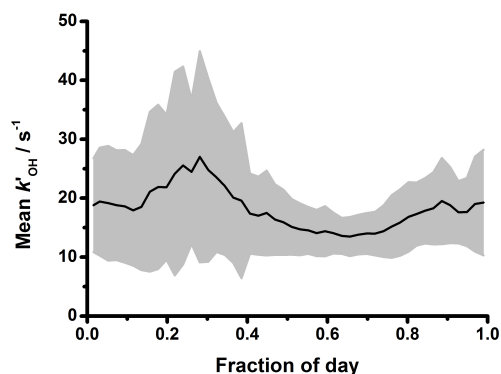


Figure 8. Diurnal average for observed OH reactivity (15 min averages) during the Clean Air for London (ClearfLo) campaign (21 July to 18 August). Shaded areas represent the measurement variability from day to day during the campaign.

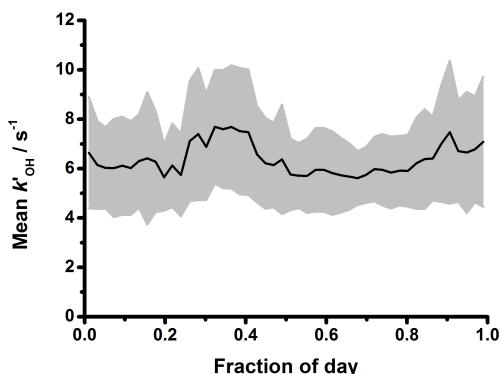


Figure 9. Diurnal average for observed OH reactivity (15 min averages) during in York (19 May to 16 June 2014). Shaded areas represent the measurement variability from day to day.

8 Chamber measurements

The field instrument described above has also been modified in order to interface to the Highly Instrumented Reactor for Atmospheric Chemistry (HIRAC) to enable measurements of OH reactivity during VOC oxidation under controlled conditions. For complex reaction mechanisms, the oxidation pathway followed will have a characteristic time-evolution of the reactivity as secondary products are generated, and measurement of OH reactivity and comparison with a model prediction provides greater constraint for experimental determination of the mechanism.

HIRAC is a 2.25 m^3 stainless steel chamber equipped with UV photolysis lamps to initiate photochemistry and a comprehensive suite of analytical instrumentation, including gas chromatography (GC), Fourier transform infrared (FT-IR) spectroscopy, cavity ringdown spectroscopy (CRDS) and LIF-FAGE for radical measurements. Photolysis lamps within the chamber enable initiation of photochemistry, and experiments can be conducted at temperatures between 203

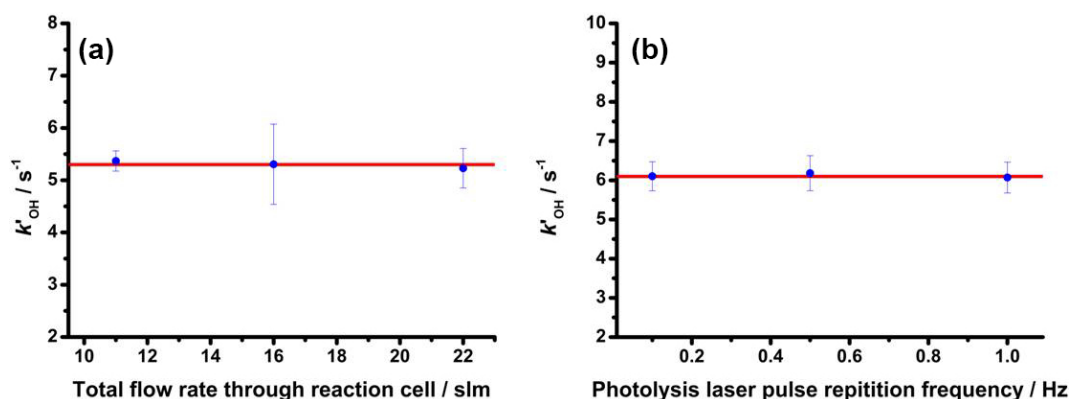


Figure 10. Observed OH reactivities for a fixed gas composition (for which the expected OH reactivity is shown in red) (a) as a function of the total flow rate through the reaction cell (slm = standard L min^{-1}) and (b) as a function of the pulse repetition frequency of the photolysis laser.

and 343 K and pressures up to 760 Torr (Glowacki et al., 2007; Malkin et al., 2010; Winiberg et al., 2015).

Gas is sampled from HIRAC through 1/2" PTFE tubing at a flow rate of 1 standard L min^{-1} and diluted with 5 standard L min^{-1} of ultra-high purity air immediately on exiting the chamber, then diluted further with 9 standard L min^{-1} of humidified ultra-high purity air and 1 standard L min^{-1} of ultra-high purity air passed over a low pressure Hg lamp in order to generate O_3 , giving a total flow of 16 standard L min^{-1} and hence a dilution factor of 1 : 16. The diluted gas flow, containing ~ 45 ppb O_3 , is then directed into the reaction cell of the OH reactivity instrument, with instrument operation and analysis as described in Sects. 2 and 3 (including the correction of observed reactivity for dilution of sampled gas from the chamber using Eq. (7), which is significant for these experiments in order to avoid measurement of high reactivities (Sect. 9) and to reduce the volume of gas removed from the chamber for the reactivity measurements). The uncertainty associated with the dilution contributes $\sim 25\%$ to the total uncertainty in k'_{OH} , which is approximately 6–8 %.

Experiments were conducted to verify the sampling procedure by filling HIRAC with air containing known concentrations of a reactive gas, with a well-characterised rate coefficient for reaction with OH, followed by measurement of the OH reactivity in the chamber. Determination of the pseudo-first-order rate coefficients describing the OH loss for each of the given reactive gas concentrations in the chamber enabled determination of the bimolecular rate coefficient for reaction of the reactive gas with OH for comparison with literature values, as for experiments described in Sect. 4. Figure 4c shows the bimolecular plots for experiments in which the chamber was filled with *n*-butanol (*n*- $\text{C}_4\text{H}_9\text{OH}$) in air at total pressures of 760 Torr and temperatures of 298 K. A bimolecular rate coefficient of $(8.5 \pm 0.1) \times 10^{-12} \text{ cm}^3 \text{ s}^{-1}$ was obtained, in comparison to the literature value of $(8.5^{+3.5}_{-2.5}) \times 10^{-12} \text{ cm}^3 \text{ s}^{-1}$ (Atkinson et

al., 2004), thus indicating the validity of the sampling procedure. No dependence of the observed reactivity was observed on the total flow rate through the instrument, which was varied between 10 and 22 standard L min^{-1} , or on the pulse repetition frequency of the photolysis laser, which was varied between 0.1 and 1 Hz, as shown in Fig. 10.

The coupling of OH reactivity measurements to chamber studies will enable detailed assessment of our understanding of the chemistry of secondary products in complex oxidation mechanisms by providing increased constraint on oxidation budgets during chamber experiments, and will be explored further in future work.

9 Effects of averaging time and future improvements to sampling

Measurements have also been made in HIRAC to investigate the effect of the averaging time on the measured OH reactivity. Figure 11 shows the observed OH reactivities, for a given set of conditions, as a function of the averaging time, showing successful measurements with an averaging time of 10 s and indicating the potential for further improvements for future integration of ambient OH reactivity observations with flux measurements.

Experiments described in this work using known concentrations of reactive gases have been able to reproduce recommended literature values for known rate coefficients, indicating the validity of the technique described here over the dynamic ranges investigated. However, recent work in Leeds has shown that, at higher reactivities, observed kinetics can be influenced by sampling issues related to the effects of velocity distributions on the transport time of sampled gas from the pinhole nozzle to the point at which fluorescence is excited and detected in the FAGE cell. The effects of the velocity distributions on the time taken for sampled gas to travel from the pinhole to the point of detection coupled with the

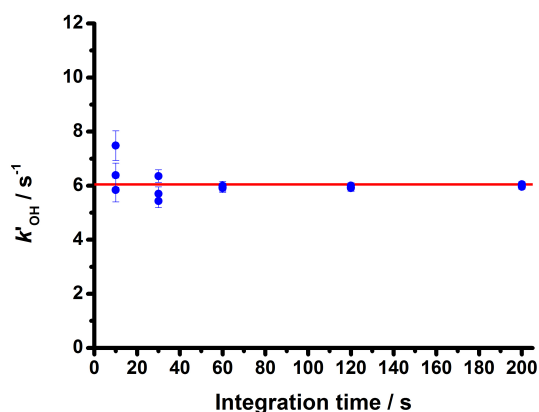


Figure 11. Observed OH reactivities, for a fixed gas composition (for which the expected OH reactivity is shown in red), as a function of averaging time, obtained using 15 mW of 308 nm probe laser power.

true kinetics of the OH decay can lead to underestimations of very high reactivities; this is described in detail by Stone et al. (2016). Successful measurements with known concentrations of CH₄ at reactivities of $\sim 150 \text{ s}^{-1}$ (Sect. 4, Fig. 4b), although scattered owing to the small number of time points over which fast decays can be measured and poorer precision compared to lower reactivities, indicate that such effects should be minimal for the instrument described in this work, even for the highest reactivities observed during the ClearfLo campaign ($> 100 \text{ s}^{-1}$). However, experiments incorporating OH reactivity measurements in chamber studies, such as those described in Sect. 8, must also ensure that the gas sampled from the chamber has been sufficiently diluted so as to avoid the measurement of high reactivities directly.

Future work will incorporate a new inlet designed to minimise the distance between the pinhole nozzle and the point of excitation fluorescence and detection, ideally such that detection occurs within the supersonic jet formed on expansion of the gas as it flows through the pinhole. The new inlet will not only increase the dynamic range over which reactivity measurements can be made, but sampling within the supersonic jet will also lead to increased signal-to-noise and enable further reductions in the averaging time required to achieve adequate signal-to-noise for measurements with high time resolution.

10 Conclusions and outlook

In this work we present the design and characterisation of an instrument to make field and chamber measurements of OH reactivity by laser flash photolysis (LFP) coupled with laser-induced fluorescence (LIF) using the FAGE technique. The LFP-LIF reactivity instrument, its operation and data analysis have been described in detail. Ambient reactivity measurements obtained during field campaigns in London, UK,

and York, UK, have been presented, and will be discussed further in future work. The instrument has also been coupled to an atmospheric chamber, and preliminary results have been shown to demonstrate the potential for reactivity measurements during future chamber experiments.

Reactivity measurements have been made using an averaging time of 10 s, indicating potential for integration of ambient OH reactivity observations with flux measurements. Future development of the instrument will increase the dynamic range over which measurements can be made and will enable reduced averaging times owing to improvements in the signal-to-noise ratio.

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