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1       **Management and valorisation of wastes through use in producing**  
2                               **alkali-activated cement materials**

3  
4       Susan A. Bernal,<sup>1,2</sup> Erich D. Rodríguez,<sup>3</sup> Ana Paula Kirchheim,<sup>3</sup> John L. Provis<sup>1\*</sup>

5  
6       <sup>1</sup>Department of Materials Science and Engineering, The University of Sheffield, Sir  
7               Robert Hadfield Building, Mappin St, Sheffield S1 3JD, United Kingdom

8       <sup>2</sup>Department of Civil and Structural Engineering, The University of Sheffield, Sir  
9               Frederick Mappin Building, Mappin St, Sheffield S1 3JD, United Kingdom

10       <sup>3</sup>Nucleo Orientado para a Inovação da Edificação, NORIE, Universidade Federal do  
11               Rio Grande do Sul, Porto Alegre, RS, Brazil

12  
13                               \*corresponding author. [j.provis@sheffield.ac.uk](mailto:j.provis@sheffield.ac.uk)

14  
15       **Abstract**

16       There is a growing global interest in maximising the re-use and recycling of waste, to  
17       minimise the environmental impacts associated with waste treatment and disposal. Use  
18       of high-volume wastes in the production of blended or novel cements (including alkali-  
19       activated cements) is well known as a key pathway by which these wastes can be re-  
20       used. This paper presents a critical overview of the urban, agricultural, mining and  
21       industrial wastes that have been identified as potential precursors for the production of  
22       alkali-activated cement materials, or that can be effectively stabilised/solidified via  
23       alkali activation, to assure their safe disposal. The central aim of this review is to  
24       elucidate the potential advantages and pitfalls associated with the application of alkali-  
25       activation technology to a wide variety of wastes that have been claimed to be suitable  
26       for the production of construction materials. A brief overview of the generation and  
27       characteristics of each waste is reported, accompanied by identification of opportunities  
28       for the use of alkali-activation technology for their valorisation and/or management.

29       **Keywords:** Engineering; Immobilisation; Clean processes; Recycling; Waste treatment  
30       and waste minimisation

32 **Contents**

33 1. Introduction .....3

34 2. Urban wastes .....7

35     2.1. Ashes from municipal solid waste incineration.....7

36     2.2. Ceramic and demolition wastes.....11

37     2.3. Wastes or sediments from water treatment plants.....15

38     2.4. Waste glass.....17

39 3. Agro-industrial waste.....20

40     3.1. Rice husk ash.....20

41     3.2. Palm oil fuel ash.....23

42     3.3. Sugar cane bagasse ashes.....25

43 4. Wastes from the mining and mineral industries.....27

44     4.1. Red mud.....27

45     4.2. Kaolin wastes.....29

46     4.3. Low purity clays.....30

47     4.4. Other mining and mineral wastes.....32

48 5. Wastes from other industries.....33

49     5.1. Coal bottom ashes.....33

50     5.2. Paper sludge ash.....36

51     5.3. Spent fluid catalytic cracking catalyst.....37

52 6. Summary and general considerations.....39

53 7. Concluding remarks .....43

54 8. Acknowledgements .....45

55 9. References .....45

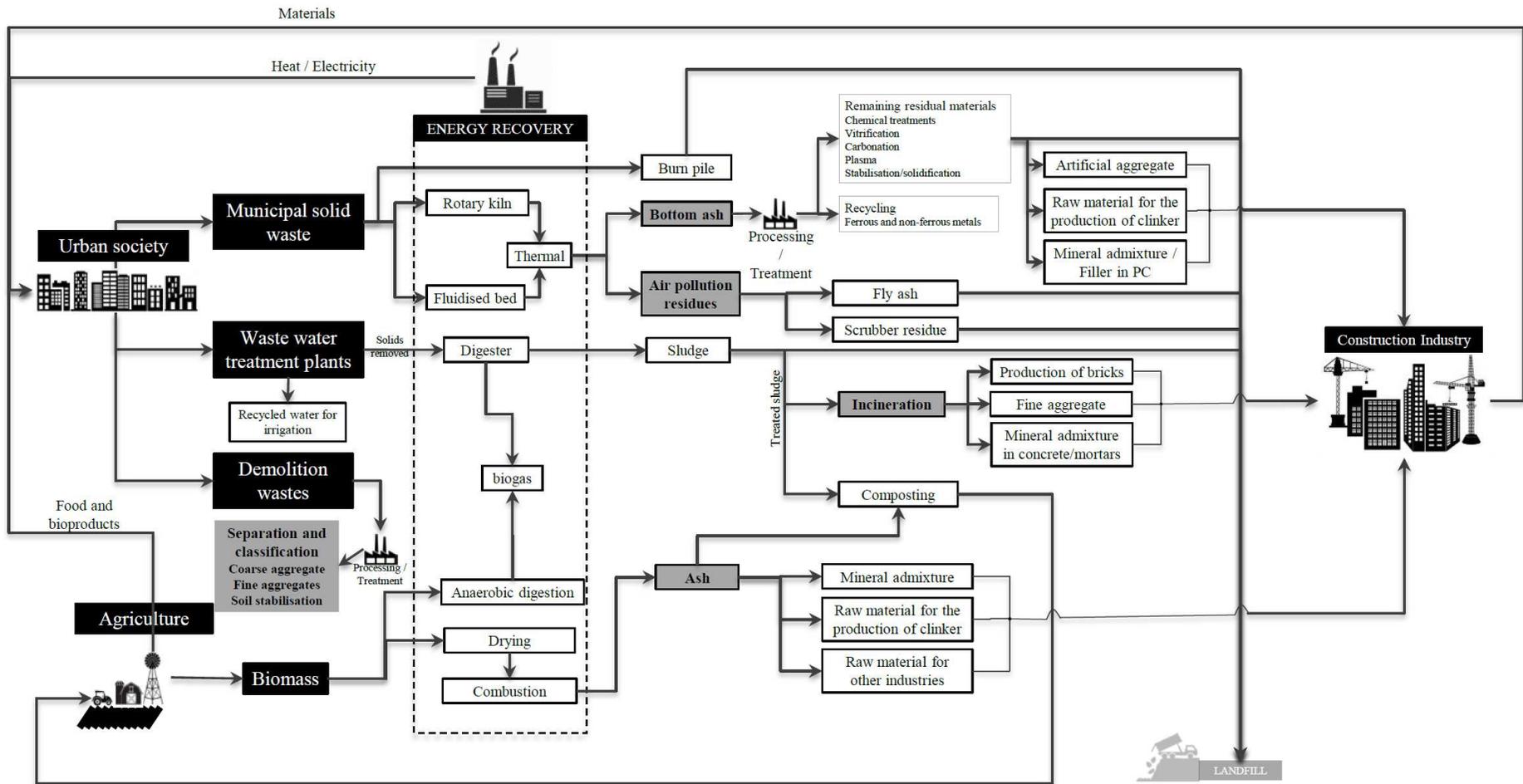
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58           **1. Introduction**

59   Over the past decades, extensive discussions about climate change have taken place  
60   around the world, analysing its potential implications for the way in which our society  
61   works, especially for the vulnerable populations in less developed regions. Within this  
62   discussion, there is a growing consensus that climate change is not just an issue of  
63   energy efficiency or industrial carbon emissions, as our approach to demanding  
64   development and economic growth has proven to be highly unsustainable in an  
65   ecological sense.<sup>1</sup> Therefore, there is an urgent need to develop new and sustainable  
66   approaches to the manufacture and consumption of materials as a key component of the  
67   move to minimise waste generation. This also requires maximising the conversion of  
68   wastes into valuable resources. Figure 1 presents some concepts related to the (current  
69   and potential) implementation of closed-loop material flows in the construction  
70   industry, focusing specifically on urban and agricultural (rather than broader industrial)  
71   wastes, and the relationships between different industry sectors and waste generators  
72   of relevance in this context. Various wastes highlighted in Figure 1 (shaded in grey) are  
73   currently under-utilised or simply discarded, but offer potential for further valorisation  
74   through alkali-activation, and will form part of the focus of this review.

75   Across modern society, concrete is the second-most widely used material of any kind  
76   (after water),<sup>2</sup> as it is the pillar of the infrastructural development of our society and the  
77   basis of a large fraction of the global built environment. Modern concrete is mainly  
78   composed of hydrated Portland cement (which acts as the binding phase in more than  
79   98% of all concrete produced worldwide) along with natural sand and rocks, and the  
80   engineering properties of the concrete as a whole are largely controlled by the chemistry  
81   and design parameters of the binder. However, Portland cement is not the only type of  
82   binder which can be used in concrete.<sup>3</sup> In the past decade, there has been rapid growth  
83   in international research efforts in the utilisation of wastes as alternative construction  
84   materials. One area of particularly rapid development has been the field of alkali-  
85   activated or “geopolymer” cements, where the reaction between an alkali source  
86   (referred to as the activator) and an aluminosilicate powder (referred to as the  
87   precursor) yields a hardened binder with performance (and often also appearance)  
88   similar to that of Portland cement,<sup>4</sup> but with a fraction of the CO<sub>2</sub> emissions.<sup>5</sup>



91 Figure 1. Schematic representation of some of the material flows related to recycling in the construction materials industry, focused on wastes  
 92 generated directly by urban society and agriculture. Wastes identified in this review as having potential for use in alkali-activation are shaded in  
 93 grey.

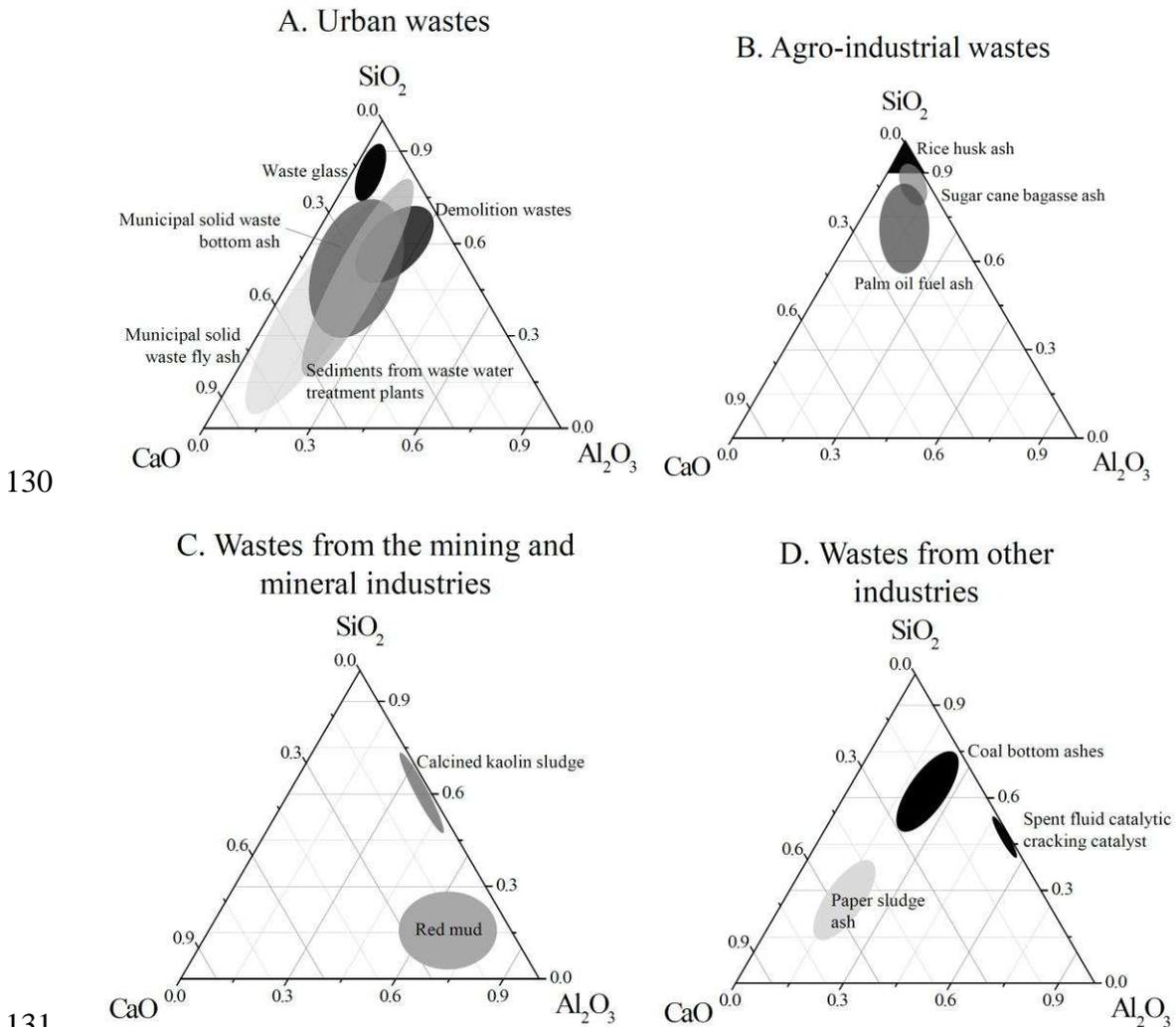
94 Precursors which are generally used in research and in the current (relatively early)  
95 stages of commercialisation of alkali-activated cements include industrial by-products  
96 such as fly ash from coal combustion, and slags from iron-making processes;<sup>6</sup> however,  
97 alkali activation can be applied to any material with a sufficiently high content of  
98 reactive  $\text{Al}_2\text{O}_3$  and  $\text{SiO}_2$  species. In recent years, there has been significant growth in  
99 the use of different urban, industrial and mining wastes as precursors for production of  
100 alkali-activated materials, as the high existing demand for blast furnace slag and fly ash  
101 in blends with Portland cement represents one of the main barriers to the further  
102 deployment of alkali-activated cements on a large industrial scale.<sup>7</sup> However, there  
103 does exist the need to increase the valorisation of some such wastes, especially for fly  
104 ash where the re-use rate can still be low: India, Middle East and Russia currently report  
105 fly ash utilisation rates of ~14%, ~11%, and ~19%, respectively.<sup>8</sup> There is also growing  
106 interest in the stabilisation/solidification of hazardous wastes via alkali-activation, to  
107 reduce the severe environmental impacts which can be associated with their chemistry  
108 and toxicity.<sup>9,10</sup>

109 In this paper, we present an overview of some of the wastes that have been used as  
110 precursors for the production of alkali-activated materials, the main material properties  
111 obtained when using those wastes in alkali-activation, and the associated development  
112 opportunities. Coal fly ashes and metallurgical slags will not be covered in detail, as  
113 their use in alkali-activation has been described in depth in recent reviews including.<sup>4,11</sup>  
114 High quality coal fly ash and ground granulated blast furnace slag are also in high  
115 demand for blending in Portland-based cements and concretes, which brings an  
116 associated cost, and thus many of the likely opportunities for growth in low-cost alkali-  
117 activated material production may be identified as being linked to precursors which are  
118 not currently used in standardised Portland cement blends.<sup>12</sup> The wastes to be discussed  
119 in detail here are outlined in Figure 2, which represents their approximate compositions  
120 on the  $\text{CaO-SiO}_2\text{-Al}_2\text{O}_3$  ternary phase plane. Based on their chemical compositions,  
121 content of amorphous phases and degree of reactivity (which are all inter-related), the  
122 potential valorisation of these wastes through alkali activation can be addressed through  
123 two general alternative pathways:

- 124 1. Use the waste as main precursor for the production of an alkali-activated  
125 binder for sale as a product in its own right, or
- 126 2. The use of alkali activation technology to develop a new outlet for a particular

127 waste, including as an alternative source of  $\text{SiO}_2$  in the alkali activator, as a secondary  
128 precursor or blending agent, or even as an aggregate.

129



132 Figure 2. Approximate compositions of the wastes discussed in this review.

133

134 A key point that is generally neglected in academic studies is the volume of material  
135 available in any particular location for the production of cements or concretes. Cement  
136 and concrete are generally produced in very large quantities (up to hundreds of  
137 thousands of tonnes per annum) from a specific production site, and so any process for  
138 their production based on wastes needs to have a long-term secure supply of the waste  
139 of at least tens of thousands of tonnes per annum. This also needs to be secured on a  
140 time horizon of multiple decades, to enable recovery of the capital cost of construction  
141 of the production facility and an economically viable degree of profitability. Academic

142 studies based on a single waste source rarely consider such aspects of scale-up when  
143 promoting the use of a particular waste as a precursor for alkali-activated cements, and  
144 so this paper will aim to provide some insight where possible, regarding these issues.

145

## 146 **2. Urban wastes**

### 147 **2.1 Ashes from municipal solid waste incineration**

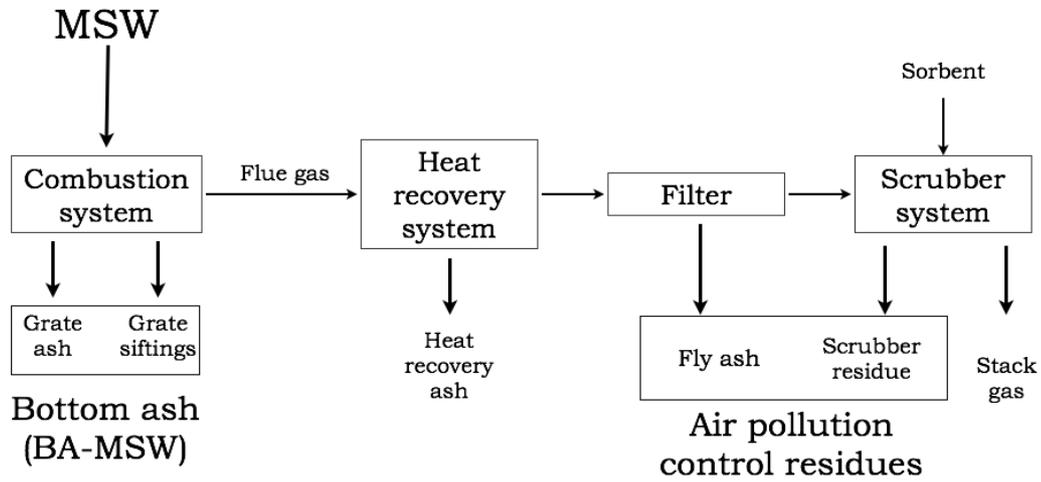
148 The local and central authorities of urban and rural areas worldwide are currently under  
149 pressure to find responsible ways to manage and dispose of the municipal solid waste  
150 (MSW) that is produced every day. China alone generates over a quarter of total global  
151 MSW (~250 Mt/y), with a reported annual growth rate of 8 to 10%,<sup>13</sup> as a consequence  
152 of its growing urbanisation and consumer-focused society. Landfill is the main strategy  
153 for MSW management in China, and only ~15% of municipal wastes are incinerated.<sup>14</sup>  
154 In the U.S., the MSW that is recyclable is less than ~35% of total MSW arisings,<sup>15</sup> and  
155 the non-recyclable wastes are landfilled, as this is an easy and currently inexpensive  
156 method for disposal.

157 Landfilling of MSW has severe environmental impacts including odour emissions,  
158 groundwater pollution from landfill leachate, and soil contamination. Therefore, the  
159 controlled incineration of municipal solid wastes (MSW) has become a more  
160 widespread way used to manage this kind of wastes. By direct incineration of MSW, it  
161 is possible to reduce the volume of waste by converting it into an ash (achieving up to  
162 80-90% volume reduction depending on the nature of the waste), and decrease the  
163 amount of waste that needs to be landfilled,<sup>16</sup> with the added value that the energy  
164 recovered from the heat that is released during the incineration of plastics, paper, other  
165 organic matter, and ferrous and non-ferrous metals can have significant financial value.

166 The main disadvantages associated with MSW incineration are the high levels of  
167 emissions of greenhouse and other problematic gases, and the large amounts of ashes  
168 which can be generated.<sup>17</sup> These ashes can be categorised essentially into two groups:  
169 bottom ash (BA-MSW), which is the material that remains in the furnace after  
170 combustion, and the air pollution control residues that are removed from the flue gas.<sup>18</sup>  
171 The BA-MSW represents ~80% of the total residues generated during incineration<sup>19,20</sup>.  
172 Scrubber residues are retained by sorbents (such as lime or sodium hydroxide), and the  
173 fly ash (FA-MSW) is separated by filters or electrostatic precipitators<sup>18</sup>, as shown in

174 Figure 3. Figure 4 shows a scanning electron microscope (SEM) micrograph of a  
175 particle of FA-MSW, which depicts its heterogeneous, highly porous structure and a  
176 particle size of around 50  $\mu\text{m}$ .

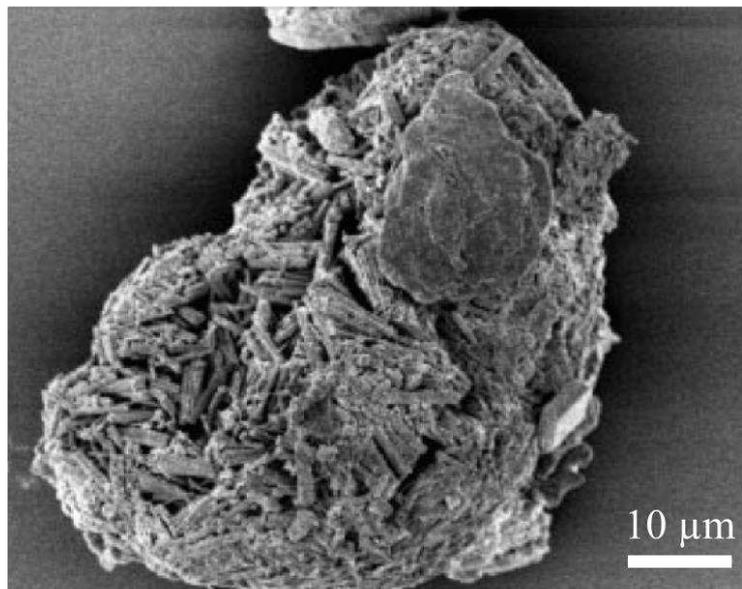
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178

179 Figure 3. Basic unit operations and mass flows of an MSW incineration plant.<sup>18</sup>

180



181

182 Figure 4. SEM image of a particle of FA-MSW showing the heterogeneous nature of  
183 this waste even within a single particle, and the intraparticle porosity. From Kersch et  
184 al.<sup>21</sup>, copyright John Wiley & Sons.

185

186 MSW ashes are often classified as hazardous due to the presence of toxic elements and  
187 organic compounds, and consequently these ashes must be treated and disposed with  
188 care, considering regulatory aspects and specifications such as the European Waste  
189 Catalogue List (19 01).<sup>22</sup> The major elements present in MSW ashes are mainly O, Si,  
190 Ca, Al, Fe, Na, and K. BA-MSW also has carbon due to unburned material. Although  
191 most of the metals are present as oxides, there are also considerable quantities of metal  
192 chlorides, metal sulfates and metal carbonates, and some non-oxidised metallic  
193 components. Some ashes may also contain significant amounts of polycyclic aromatic  
194 hydrocarbons (PAH), polychlorinated biphenyls (PCB), chlorobenzenes,  
195 chlorophenols, chlorinated compounds, benzofurans or mutagenic organic chemicals.<sup>23</sup>  
196 When the MSW ashes are used by the construction industry or as geotechnical  
197 materials, the leachability of these organics, as well as alkalis and heavy metals, is a  
198 major concern, as these can affect the properties of the concretes and the soils. Ashes  
199 with high chloride content are also severely restricted from usage in reinforced  
200 concretes due to the risk of corrosion of the embedded steel reinforcement.

201 Currently, the utilisation of ashes from MSW combustion is very limited, especially if  
202 the ash has not been pre-treated, and also due to the intrinsically high variability of this  
203 type of ash. Some ashes are decontaminated by different processes, including wet  
204 chemical treatment,<sup>24</sup> thermal or plasma vitrification,<sup>25,26</sup> carbonation,<sup>27</sup> or disposed via  
205 stabilisation/solidification (S/S) in a cementitious matrix.<sup>18</sup> Life cycle analysis has  
206 enabled quantification of the environmental benefits associated with the re-use,  
207 particularly metal recovery, of the MSW ashes; a significant reduction is observed  
208 related to the global warming impacts.<sup>28</sup>

209 The recycling of MSW ashes by the construction industry has increased worldwide over  
210 the past years, including the assessment and use of FA-MSW and BA-MSW as  
211 aggregates,<sup>29-32</sup> as raw materials for Portland clinker production,<sup>33,34</sup> and as mineral  
212 admixtures for the production of concretes.<sup>35</sup> Some studies have identified that the  
213 presence of slowly-reacting siliceous glass or metallic aluminium particles in the ashes  
214 derived from MSW might negatively affect the durability properties of cements and  
215 concretes, as these components can increase the susceptibility to degradation, via the  
216 alkali-silica reaction or the release of hydrogen gas, respectively.<sup>29,36</sup>

217 The stabilization/solidification (S/S) of MSW ashes via alkali-activation has also been  
218 assessed. The mechanisms of heavy metal immobilisation in an alkali-activated binder

219 can be physical and/or chemical, where the hazardous elements are either fixed in the  
220 gel network, linked into the structure in change balancing roles, or physically trapped  
221 in a dense and low-permeability matrix.<sup>37</sup> Luna-Galeano et al.<sup>38</sup> studied FA-MSW  
222 incorporation into alkali-activated systems based on a variety of precursors (including  
223 metakaolin, blast furnace slag and coal combustion fly ash) and alkali activators  
224 (sodium and potassium hydroxide and silicate). Although the mechanical performance  
225 of the wastefoms produced was relatively low (< 10 MPa after 28 days), the  
226 leachability of Zn, Co, Ni and Sn was greatly reduced compared to the raw MSW ash.  
227 Lancelloti et al.<sup>39</sup> showed that metakaolin-based systems can stabilise larger amounts  
228 of MSW ashes when compared with conventional cementitious S/S.

229 The use of untreated MSW ash as a precursor in the production of alkali-activated  
230 binders is limited due to its toxicity and the low contents of amorphous, reactive SiO<sub>2</sub>  
231 and Al<sub>2</sub>O<sub>3</sub>-containing phases. However, some MSW residues have been shown to be  
232 suitable to be used in this way<sup>40,41</sup>; Zheng et al.<sup>41</sup> achieved compressive strengths of up  
233 to 20 MPa after 7 days of curing for such materials. The use of CaO for flue gas  
234 treatment in MSW incineration facilities generates fly ashes rich in Ca-compounds  
235 (Ca(OH)<sub>2</sub>, CaCO<sub>3</sub>, or CaSO<sub>4</sub>)<sup>42</sup>, and these can be beneficial for strength development  
236 and permeability reduction in alkali-activated binders. Some FA-MSW materials can  
237 be treated by washing to reduce the content of undesirable elements such as Cl, Zn, Cu,  
238 Cr, Pb, Cd and Ni. Zheng et al.<sup>40</sup> also reported that after a washing treatment, an FA-  
239 MSW exhibited higher reactivity in alkali-activation, yielding a binder with improved  
240 mechanical performance due to the removal of the chloride which was affecting setting  
241 and mechanical performance.<sup>43,44</sup> This was consistent with the results of Ferone et al.<sup>45</sup>,  
242 who evaluated the effect of blending fly ash with FA-MSW which had been pre-washed  
243 to remove both chloride and sulfate, and found an improvement in terms of leaching  
244 performance. However, the washing process does itself generate a secondary liquid  
245 waste stream which requires further treatment, and this added cost must be considered  
246 when assessing the desirability of the washing step in waste treatment.

247 Diaz-Loya et al.<sup>46</sup> assessed alkali-activated systems based on blends of coal FA and  
248 FA-MSW. Their materials based solely on FA-MSW showed leachability of heavy  
249 metals (with the exception of Se) which was within the allowable limits according to  
250 the US Environment Protection Agency. The alkali-activated binders containing 60%  
251 FA-MSW exhibited mechanical performance which was suitable for the production of

252 non-structural precast products: a compressive strength of 18 MPa and flexural strength  
253 of 2.8 MPa after curing at 100 °C for 7.

254 In general, unless a decontamination treatment is applied, the use of MSW ashes as a  
255 raw material for alkali-activated cements in civil construction applications seems  
256 limited, as the products may not comply with the toxicity regulations to be used as a  
257 building material, and will tend to be variable in quality and performance. In this sense,  
258 MSW ashes present challenges related to valorisation as a construction material via  
259 alkali-activation, and future work in this area is likely to be driven predominantly by  
260 environmental arguments and the need to avoid landfilling of the waste ash, rather than  
261 any particularly desirable or unique technical properties of the materials produced.  
262 However, it does seem that solidification/stabilisation using alkali-activated matrices  
263 may be a viable route for the management of this waste via incorporation into a solid  
264 binder rather than simply landfilling it, as such a process can contribute significantly to  
265 reducing the leachability of toxic elements to the environment.

266

## 267 **2.2 Demolition and ceramic-type wastes:**

268 Roughly 45% of the total wastes arising from construction processes are ceramic-type  
269 wastes<sup>47</sup>, which are produced from two main sources:

- 270 • **Wastes generated by demolition and construction activities:** including  
271 construction and demolition wastes: concrete, bricks, roof tiles and ceramic  
272 materials.
- 273 • **Wastes generated by the ceramic industry:** including waste from thermal processes  
274 or from the manufacture of bricks, roof tiles and construction materials.

275

276 These wastes are generally classified as non-hazardous,<sup>22</sup> as long as no asbestos is  
277 present. According to Dahlbo et al.,<sup>48</sup> the current construction and demolition waste  
278 management system of the European Union needs to be significantly updated and  
279 modified in order to achieve the target of recycling a minimum of 70% in 2020 as  
280 suggested by the EU Waste Framework Directive (2008/98/EC). However, the main  
281 problems in the utilisation of wastes generated by demolition and construction materials  
282 are related to the lack of control of composition (which is very heterogeneous) and the  
283 difficulty in extracting certain contaminants, e.g. wood, paper, gypsum, glass, rubber,

284 among others.<sup>49</sup> Europe and the U.S. have made significant advances over the past  
285 decades in the correct classification and subsequent reuse of construction wastes. New  
286 techniques to ensure effective separation, instead of selective demolition and manual  
287 sorting, are now utilised, such as wet jigging,<sup>50</sup> air jigging,<sup>49</sup> heavy liquid separation,<sup>51</sup>  
288 optical sorting and near-infrared sorting technology<sup>52</sup>.

289 The main consumer of these wastes is the same construction industry which generates  
290 them, and common applications include soil stabilisation, use as a fill material for  
291 landscaping, as an artificial aggregate in the production of concrete, and/or use as a raw  
292 material for the production of Portland cement.<sup>53-56</sup> However, in growing economies  
293 where high volumes of ceramic and demolition wastes are generated, the potential for  
294 recycling and re-use of these wastes is often not reached as a consequence of the low  
295 cost and high volume availability of virgin raw materials, as well as the limited  
296 expertise available for treating wastes and the limited allocation of resources for waste  
297 management. Recently, life cycle analysis modelling has demonstrated that the re-use  
298 and valorisation of construction and demolition wastes can reduce the footprint of the  
299 industry across most environmental impact categories.<sup>57,58</sup> However, transportation is  
300 the most important impact to be considered; its contribution to the global warming  
301 impacts can be high, and may in fact dominate other benefits if local valorisation is not  
302 possible.<sup>58</sup>

303 The use of demolition wastes for the production or development of alkali-activated  
304 cements is challenging, considering the varying nature of these wastes and the  
305 consequent lack of consistency in chemical and physical properties across wastes from  
306 different sources. There is also a high energy and financial cost associated with the  
307 reduction of wastes to a sufficiently fine particle size for use as a precursor in alkali-  
308 activation, as crushing to a particle size in the range of tens of microns is very much  
309 more expensive than when targeting a normal aggregate particle size (a few millimetres  
310 to a few centimetres), and problematic dust emissions may also be associated with this  
311 process.

312 However, there do exist reports related to the use of demolition wastes as a precursor  
313 for production of alkali-activated cements. For example, Payá et al.<sup>59</sup> assessed hydrated  
314 Portland cement which had previously been carbonated in an attempt to replicate end-  
315 of-life conditions for cement in regular concretes, by alkali-activation with NaOH and  
316 waterglass. Their mortar specimens cured at 65 °C after 3 days exhibited a compressive

317 strength on the order of 10 MPa, demonstrating potential use of cement-rich fraction of  
318 the demolition wastes, which is not strongly desirable as an aggregate due to its high  
319 water demand in concrete mixtures. The applicability of cement recovered from  
320 demolition wastes as a precursor for alkali-activated materials is likely to be limited by  
321 competition from the re-use of this material in Portland cement clinker manufacture,  
322 and so further assessment will be required to elucidate the true feasibility of this option  
323 from financial, technical and environmental points of view. Recently, Komnitsas et  
324 al.<sup>60</sup> demonstrated the potential use of construction and demolition wastes (including  
325 recycled concrete, bricks and tiles) as raw materials for the synthesis of geopolymers:  
326 high mechanical strength (> 40 MPa after 7 days of curing) was achieved under specific  
327 synthesis conditions using wastes derived from tiles and bricks. However, the  
328 demolition wastes based on recycled concrete (regardless of the particle size  
329 distribution) showed a lower degree of reactivity and lower mechanical performance.  
330 These results elucidate the importance of developing an effective selection and  
331 screening process for the demolition wastes prior to use as a precursor in alkali-  
332 activation, taking into account their heterogeneity.

333 Therefore, the wastes generated by the ceramic industry can probably be reused more  
334 easily than general demolition wastes due to the greater control of composition, and  
335 thus reduced variability. The largest producers of clay-based ceramic tiles are China,  
336 Brazil, India, Italy, Iran and Spain, which together represent ~70% of global  
337 production,<sup>61</sup> and in these countries, the residues generated during the production of  
338 ceramic products are mainly disposed in landfill. These ceramic wastes consist mainly  
339 of silicate and aluminosilicate minerals obtained through the calcination of clays, such  
340 as quartz (SiO<sub>2</sub>), feldspars (MAlSi<sub>3</sub>O<sub>8</sub> where M is an alkali metal) and vitreous phases.  
341 Several studies have described<sup>62,63</sup> the use of these ceramic wastes as a coarse or fine  
342 aggregate for concrete or mortar production, or as a raw material for the production of  
343 Portland clinker.<sup>64,65</sup>

344 Some ceramic wastes do show pozzolanic reactivity, as they contain amorphous  
345 aluminosilicate phases which react with the portlandite formed during the hydration of  
346 Portland cement.<sup>66-69</sup> Although the pozzolanicity of these wastes is significantly lower  
347 than that of other calcined clays (such as metakaolin), their value as precursors in alkali-  
348 activated cement production can be optimised through control of the formulations and  
349 the activation conditions. Reig et al.<sup>47,70</sup> evaluated the alkali-activation of an

350 aluminosilicate waste obtained from red clay bricks and porcelain stoneware; mortars  
351 cured at 65 °C for 7 days developed compressive strengths exceeding 20 MPa,  
352 demonstrating that it might be feasible to reutilise these wastes for the production of  
353 alkali-activated cements. Allahverdi and Najafi Kani <sup>71</sup> produced alkali-activated pastes  
354 based on blends of waste bricks and 8-month old crushed concrete, which achieved  
355 compressive strengths of up to 40 MPa after 28 days of curing.

356 The use of recycled crushed material obtained from bricks and other clay products as  
357 raw materials for the development of alkali-activated cements is currently quite limited,  
358 although studies including those described above suggest that it may be technically  
359 achievable. One of the main limitations in a practical sense is the low volume of  
360 production of clay-based demolition waste in any particular location, compared with  
361 what might be commercially required for production of alkali-activated cements at an  
362 industrial scale, as most activities which generate such wastes are small in scale.  
363 Likewise, the growing demand for low-cost housing in many areas around the world  
364 has led to the development of improvised brick factories, whose product control is  
365 minimal, which can consequently affect the potential reactive quality of the powdered  
366 brick after recycling.

367 Conversely, ceramic wastes such as broken or off-specification porcelain stoneware,  
368 tiles, tableware and others, that can be sourced directly from the factories  
369 manufacturing these products rather than from the demolition process, could have  
370 higher potential as precursors for alkali-activated cements, as the raw materials and  
371 process of manufacture are well known, and there will be greater consistency in the  
372 properties of the wastes to enable optimisation of alkali-activated cement formulations.  
373 This is an interesting area of research that needs to be further explored, although the  
374 volumes of these wastes available from each single source tend to be rather small  
375 compared to the scale of cement production facility throughput values, and so such  
376 products may be best utilised in niche products such as refractories,<sup>72</sup> which can make  
377 use of their intrinsically high thermal resistance, rather than in production of bulk  
378 construction materials.

379

### 380 **2.3 Wastes or sediments from water treatment plants**

381 Sewage sludge is a residue generated by the wastewater treatment process, where the  
382 liquid and solids fractions are separated. Residues are collected during the primary  
383 (physical and/or chemical), secondary (biological) and tertiary (nutrient removal)  
384 treatment. The solids collected can be subjected to further treatments (including  
385 biological, thermal, long-term storage, among others) and are finally disposed. The  
386 quality of the sludge produced is affected by the degree of pollution of the effluent  
387 treated and the technical features of the water treatment plant. The physical and  
388 chemical processes involved in sewage sludge treatment tend to increase the  
389 concentrations of heavy metals, such as Zn, Cu, Ni, Cd, Pb, Hg and Cr,<sup>73</sup> as water is  
390 progressively removed from the sludge. In Europe, 35-45% of the sewage sludge  
391 generated is still landfilled, 37% is used in agriculture, 11% incinerated and the  
392 remainder is used in other areas such as forestry and land reclamation.<sup>74</sup> The presence  
393 of hazardous compounds restricts the use of sewage sludge in agriculture due to its  
394 potential ecotoxicity, and therefore it has to be assessed carefully before utilisation, to  
395 reduce any harmful effects.<sup>75</sup>

396 There exist some reports related to the co-combustion of sewage sludge in cement  
397 manufacturing, where the calorific power of the organic fraction of the sludge is used  
398 as a source of energy. The main restriction in blending the sludge with coal for  
399 combustion within the kiln is the emission of harmful elements, including heavy metals  
400 which can accumulate in the cement kiln dust. On other hand, the ashes generated  
401 during the incineration of sludge wastes have been used in the construction industry as  
402 a fine aggregate, as a mineral admixture in concrete/mortars mixes,<sup>76</sup> or as a raw  
403 material for the production of bricks.<sup>77,78</sup> There do not exist reports related to the  
404 assessment of sewage sludge ashes as the sole raw material in the production of alkali-  
405 activated cements, as these ashes tend not to contain high contents of reactive  
406 aluminosilicates; instead, alkali-activated cements have been examined as potential  
407 solidification/stabilisation matrices for these ashes, to reduce the leachability of heavy  
408 metals.

409 Yamaguchi and Ikeda<sup>79</sup> evaluated the solidification of sewage sludge slag, which is  
410 produced via the melting of the sludge at high temperature, in a fly ash based  
411 geopolymer matrix. It was identified that the sewage sludge slag was an 'active filler'  
412 and the best mechanical strength was obtained at a 25 wt.% sludge slag loading,  
413 although high temperature curing (80 °C) was required to produce monoliths. Such

414 slags could potentially be utilised in the production of alkali-activated matrices, but  
415 further research in this area would certainly be required, especially regarding  
416 immobilisation of heavy metals.

417 Reservoir sludge is a by-product resulting from the storage and treatment of potable  
418 water, mainly consisting of deposited clays and silt, and thus contains much lower  
419 levels of toxic substances than sewage sludge. It can therefore be categorised in most  
420 cases as a non-hazardous waste and may be reused in different engineering applications.  
421 Taking into account its relatively high content of clay minerals, reservoir sludge can be  
422 thermally treated to produce bricks or lightweight aggregates,<sup>80</sup> or blended with other  
423 precursor materials as a reactive component of an alkali-activated binder system. It has  
424 been demonstrated<sup>81</sup> that the compressive strength of ternary alkali-activated binders  
425 with 30 wt.% blast furnace slag, 20 wt.% metakaolin and 50 wt.% calcined reservoir  
426 sludge increases significantly when the sludge is thermally treated at 800-850 °C,  
427 consistent with the thermal activation of the clay minerals present. The maximum  
428 compressive strength reported was 56 MPa after 28 days of curing, and the mechanical  
429 performance was reduced slightly when the content of the calcined reservoir sludge was  
430 increased. Foamed alkali-activated panels based on calcined reservoir sludge with 30%  
431 blast furnace slag have also been shown to generate valuable sound-insulation  
432 properties, as expected for a low-density material based on calcined clays, offering an  
433 alternative to the use of more expensive commercial metakaolin sources in such  
434 applications.<sup>82</sup>

435 The use of calcined reservoir sludge as the sole aluminosilicate component of an alkali-  
436 activated binder was evaluated by Ferone et al.,<sup>83,84</sup> using NaOH and waterglass  
437 solutions as alkali activators. The sediments were based on quartz, feldspar, kaolinite,  
438 illite and smectite, and after being thermally treated at up to 750 °C and combined with  
439 the alkali activator, the materials developed compressive strengths lower than 12 MPa  
440 after 3 days at 60 °C. Strength development was improved greatly (38 MPa under the  
441 same conditions) when some blast furnace slag was added as a more reactive secondary  
442 constituent of the binders.

443 Alkali-activation seems to be a suitable technology for exploiting reservoir clay  
444 sediments, which do not currently have commercial value. It is important to note that  
445 the variation in clay content and nature means that mix design optimisation (including  
446 blending with other aluminosilicate materials) will be needed in each location rather

447 than using a single universal ‘ideal’ formulation. However, alkali-activation technology  
448 seems to be a suitable alternative for the manufacture of valuable products from these  
449 wastes.

450

#### 451 **2.4 Waste glass**

452 The rates of production and consumption of glass for packing differ widely between  
453 countries, and so in some countries a very high degree of reuse or recycling of waste  
454 glass is achieved, while in others (particularly countries which are high-volume  
455 importers of wine), there are a lot of waste glass bottles generated which are not suitable  
456 for domestic re-use. In EU, the glass packing waste generated was 32 kg per capita in  
457 2011. Although the 2008 target of 55% waste glass (WG) recycling has been achieved  
458 by most EU Member States, there still exists scope to increase the recycling and  
459 recovery rate.<sup>85</sup> The non-recyclable mixed-colour broken glass from used bottles, along  
460 with the glass from fluorescent lamps, can represent an environmental problem for  
461 municipal waste treatment plants as the glass is not biodegradable, and landfilling is  
462 not making effective environmental or economic use of the value and energy embodied  
463 in these residues. According to Vossberg et al.X, glass recycling shows significant  
464 energy savings (>25%) and greenhouse gas emissions reduction (~35%) when  
465 compared to landfilling.<sup>57</sup>

466 The efficiency of the glass recycling process is strongly affected by the collection  
467 method and the ability to sort the glass by colour. If glasses of different colours are  
468 correctly separated, they can be used many times without significant changes in  
469 chemical or optical properties. However, when coloured glasses are mixed, they are not  
470 suitable for reuse and then are disposed mainly in landfills. Additionally, although used  
471 fluorescent lamps are typically processed to remove the mercury and reduce its  
472 concentration to the levels recommended by the Waste Acceptance Criteria (<0.2  
473 mg/kg),<sup>86</sup> the growing adoption of fluorescent lighting systems is making difficult the  
474 safe disposal and recycling of the full range of lamps available on the worldwide  
475 market.

476 The use of waste glass in Portland cement production has generally been avoided, as it  
477 increases the alkali content in the clinker, which can generate alkali-aggregate reactions  
478 as well as the potential for flash setting due to the formation of highly soluble sulfate

479 salts.<sup>87</sup> The use of waste glass as a partial replacement of coarse or fine aggregate in the  
480 production of concrete is also limited, again due to the reaction induced between the  
481 reactive silica present in the glass and the alkalis of the Portland cement (and the glass  
482 itself). However, when the waste glass is crushed and pulverized to smaller than 300  
483  $\mu\text{m}$ , and aluminous supplementary cementitious materials such as coal fly ash are used,  
484 the deleterious effect attributed to the alkali-silica reaction decreases.<sup>88,89</sup> Some very  
485 finely ground waste glasses show pozzolanic activity, and they can be used for the  
486 partial replacement of Portland cement for concrete production, as they may enhance  
487 mechanical performance.<sup>90</sup>

488 In the context of alkali-activation of waste glasses, two main approaches have been  
489 investigated: use of the waste glass as a solid precursor for the alkali-activated cement,  
490 or as a raw material for the production of low cost sodium silicate solutions. In utilising  
491 waste glass as a precursor for alkali-activated cement production, Cyr et al.<sup>91</sup> assessed  
492 the use of a green soda-lime-silica waste glass activated by alkali hydroxide solutions,  
493 and obtained mortars with a compressive strength of up to  $\sim 60$  MPa after 56 days of  
494 curing. As the content of  $\text{SiO}_2$  in the waste glass was quite high ( $\sim 72\%$ ), the use of a  
495 silicate activator was not necessary to achieve high compressive strengths. The absence  
496 of a sodium silicate-based activator significantly reduces the cost of production of these  
497 materials.

498 Redden et al.<sup>92</sup> carried out a comparative study activating glass powder, fly ash, and  
499 blends of these materials, and identified that the glass powder-based activated cements  
500 developed higher strengths than activated fly ash cements when cured at room  
501 temperature. However, the main reaction product of glass activation was a sodium  
502 silicate gel, which was highly soluble in water and alkaline media, calling into question  
503 the stability of these cements in a real service environment in the absence of an added  
504 aluminium or calcium source that could generate an insoluble gel. Avila-López et al.<sup>93</sup>  
505 utilised urban waste glass, blended with limestone as a low-cost source of calcium, to  
506 produce alkali-activated cements. Higher reactivity of the waste glass was identified  
507 when using NaOH as an activator, which promoted the formation of a C-S-H type gel  
508 along with the hydrous Ca-Na carbonate salt pirssonite as main reaction products.  
509 Compressive strengths of up to 38 MPa were obtained in optimised mixes.

510 Badanoiu et al.<sup>94</sup> synthesised foamed alkali-activated cements using waste glass cullet,  
511 red mud, and blends of these materials, activated by solutions of NaOH and liquor

512 derived from the filtration of red mud slurry, with the aim of using waste-derived  
513 materials as both precursors and activators. These foamed cements developed a  
514 compressive strength of 25 MPa after curing at 60 °C for 24 h then at 20 °C and 85%  
515 relative humidity (RH) for 7 days.

516 These studies demonstrate that waste glasses can certainly be used as precursors for  
517 producing hardened alkali-activated cementitious materials. However, the mix designs  
518 need to be adjusted and optimised in order to produce stable reaction products, so that  
519 these cements can withstand service conditions, and therefore develop desirable  
520 durability.

521 Puertas and Torres-Carrasco have also demonstrated the production of sodium silicate  
522 solutions via chemical digestion in NaOH/Na<sub>2</sub>CO<sub>3</sub> solutions of urban waste glasses,<sup>95</sup>  
523 and have used these solutions as alkali activator for producing cements based on alkali-  
524 activated slag,<sup>96</sup> and alkali-activated fly ash.<sup>97</sup> These studies have elucidated that waste  
525 glass can be recycled for production of sodium silicate solutions, and that these  
526 solutions can act as effective activators for producing alkali-activated cements, as  
527 similar compressive strengths and phase assemblages were identified when using these  
528 alternative activators compared with those obtained when using commercial sodium  
529 silicates. This seems to be a very viable alternative for the recycling of waste glass to  
530 produce a valuable product.

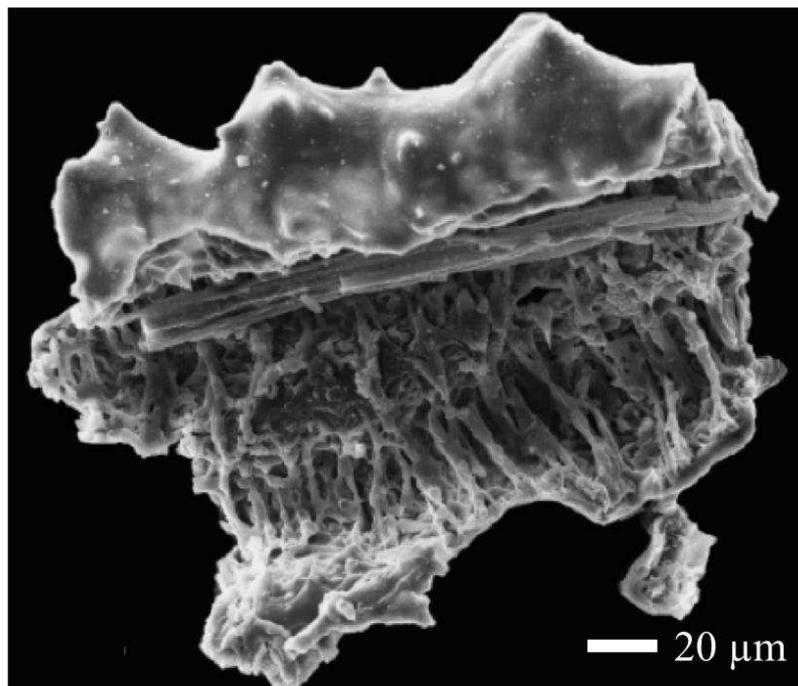
531 Other types of waste glass, such as solar panel residue glass,<sup>98</sup> have also been utilised  
532 in laboratory studies as a partial replacement material in metakaolin-based activated  
533 cements. Although material performance seemed acceptable on a lab scale, the  
534 applicability of such processes (or those including post-consumer glasses from  
535 electronic items such as display screen equipment) at an industrial scale is likely to be  
536 infeasible, considering the low volume availability of such residues worldwide or in  
537 any particular location; a very large (and expensive) number of broken panels or screens  
538 would be required to produce a useful quantity of concrete. However, as hazardous  
539 elements might be present in the waste glass, alkali-activation technology could be a  
540 suitable alternative for its safe disposal if the production of a monolithic wasteform is  
541 desired.

542

543 **3. Agro-industrial wastes**

544 **3.1 Rice husk ash**

545 Rice is a cereal grain, and is the most widely consumed staple food for a large part of  
546 the world. It is the third-highest produced crop worldwide (744 million tonnes in  
547 2014<sup>99</sup>), after sugarcane and maize.<sup>100</sup> Every five tons of rice from paddy cultivation  
548 produce one ton of rice husk waste, and in 2014 alone more than 148 million tonnes of  
549 rice husk were produced worldwide. Currently, some rice husks are utilised as fuel, and  
550 the resulting ashes, Figure 5, are a low cost source of amorphous silica that has been  
551 extensively used by the construction industry as a supplementary cementitious material  
552 for concrete production.<sup>101,102</sup> The pozzolanic activity of a rice husk ash depends on its  
553 content of amorphous silica and unburnt carbon, the particle size distribution and  
554 specific surface area, all of which are strongly affected by the combustion temperature  
555 and duration.<sup>101,103</sup>



556

557 Figure 5. SEM micrograph of a rice husk ash particle, showing its porous structure  
558 which yields a high specific surface area and thus rapid reaction. From Abreu et al.,<sup>104</sup>  
559 copyright John Wiley & Sons.

560

561 In the context of alkali-activated cements, similar to the situation discussed in the  
562 preceding section for waste glasses, rice husk ash has been used both as a secondary  
563 precursor and as a silicate source for production of sodium silicate activating solutions.

564 Detphan et al.<sup>105</sup> used rice husk ash, produced at different combustion temperatures, as  
565 partial replacement material in alkali-activated coal fly ash cements. The rice husk ash  
566 fineness and the degree of fly ash replacement strongly influenced the compressive  
567 strength; mechanical strengths of up to 56 MPa were achieved when the rice husk ash  
568 was sintered at 690 °C and the amount of small particles increased. Rattanasak et al.<sup>106</sup>  
569 blended rice husk ash with Al(OH)<sub>3</sub> to produce alkali-activated cements, adding sodium  
570 hydroxide and sodium silicate as alkali activators. Boric acid was also added to these  
571 binders to reduce their solubility in water. The formation of an aluminosilicate type gel  
572 as the main reaction product in these binders was observed, with compressive strengths  
573 between 14 and 20 MPa after 90 days of curing, depending on the Al(OH)<sub>3</sub> content.  
574 This study elucidated that hardened solids containing more than 70 wt.% rice husk ash  
575 can be produced, and that these materials can achieve moderate but useful compressive  
576 strengths.

577 He et al.<sup>107</sup> assessed the compressive strength and microstructural features of red  
578 mud/rice husk ash blended alkali-activated cements, and identified that an increased  
579 content of red mud promoted the development of higher compressive strengths,  
580 depending on the formulation of the binders. As observed by Rattanasak et al.<sup>106</sup>, an  
581 aluminosilicate type gel is forming in these cements, which is responsible for  
582 mechanical strength development over the time of curing.

583 Gastaldini et al.<sup>108</sup> produced blended concretes containing 80 wt.% Portland cement,  
584 20 wt.% rice husk ash, and 1 wt.% of either Na<sub>2</sub>SO<sub>4</sub>, K<sub>2</sub>SO<sub>4</sub> or Na<sub>2</sub>SiO<sub>3</sub>. An increase  
585 in the compressive strength development at early time of curing (7 days) was identified  
586 when alkali activators were included, along with a significant reduction in chloride  
587 permeability of the concretes.

588 The dissolution of rice husk ash into concentrated NaOH to produce sodium silicate  
589 solution as an alkali-activator is an attractive application of this waste in the field of  
590 alkali-activation technology. Bernal et al.<sup>109</sup> evaluated the effectiveness of this  
591 alternative activator in producing cements based on slag, metakaolin and their blends.  
592 This study elucidated that the mechanical performance and structural development of  
593 the alkali-activated cements produced with the waste-derived activator was comparable  
594 with the results obtained when using a commercial sodium silicate solution of  
595 corresponding chemical composition. Similar observations have been identified when

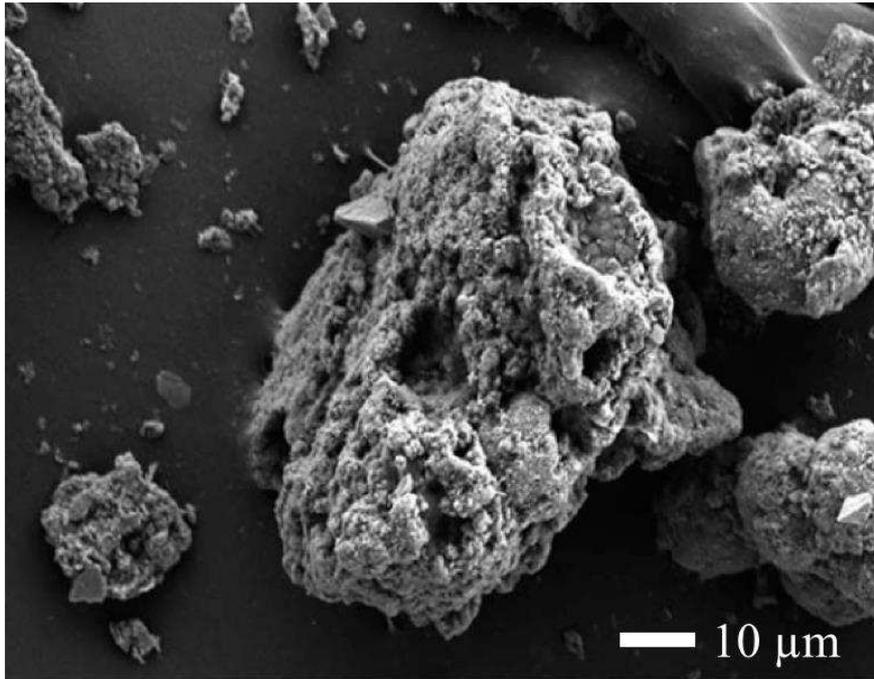
596 using these alternative activators in producing alkali-activated cements based on coal  
597 fly ash/slag blends<sup>110</sup> or spent fluid catalytic cracking catalysts.<sup>111</sup>

598 The thermal resistance of alkali-activated slag cements produced with a rice-husk ash  
599 based activator has also been assessed,<sup>112</sup> with higher retention of compressive strength  
600 after treatment at up to 1000 °C than in comparable cements produced with a  
601 commercial silicate solution. Villaquirán-Caicedo et al.<sup>113</sup> observed the formation of  
602 different crystallisation products upon high temperature exposure of alkali-activated  
603 metakaolin binders based on waste-derived or commercial sodium silicate activators,  
604 which could influence the performance of these binders under fire conditions. This was  
605 associated with the differences in the speciation of the soluble silicates available during  
606 the activation reaction when using rice husk ash based or commercial sodium silicate  
607 solutions.

608

### 609 **3.2 Palm oil fuel ash**

610 Palm oil is now a significant bio-based energy source in many parts of the world,  
611 particularly in Southeast Asia, Africa and South America. The main wastes derived  
612 from the palm oil production process are shells, palm kernel cake and fibres, among  
613 others, which are often utilised as fuel for steam production in palm oil mills. During  
614 this combustion process, a large quantity of siliceous ash is produced, and over the past  
615 decades this has begun to be utilised as a partial pozzolanic replacement for Portland  
616 cement in producing concrete.<sup>114-116</sup> As in the case of other biomass ashes, the palm oil  
617 fuel ash particles exhibit heterogeneous shape, a cellular structure and high specific  
618 surface area (Figure 6), which increase water demand when used as a mineral admixture  
619 in cements and concretes.<sup>116</sup> Recent efforts have also focused on maximising the  
620 recycling of palm oil fuel ashes via alkali-activation, as there is a rapid growth in palm  
621 oil production, and interest in biomass combustion to produce electricity as a means of  
622 reducing the cost of disposal of these wastes.



623

624 Figure 6. SEM image of a particle of palm oil fuel ash, showing the porous structure  
625 of the larger particles present. From Ooi et al.,<sup>117</sup> copyright John Wiley & Sons.

626

627 Most of these studies have been based on a single source of palm oil by-product ash,  
628 and have focused on the assessment of the effects of different mix design parameters  
629 on the strength development and basic microstructural features of alkali-activated  
630 cements based on palm oil fuel ash. However, this approach has meant that there is little  
631 broader generic information available regarding this class of ashes as a whole, as each  
632 study considers only the characteristics of a single material. There is a high degree of  
633 variability between palm oil fuel ashes in terms of composition and mineralogy,  
634 although most tend to be relatively low in reactive alumina content and thus challenging  
635 to use as a sole precursor for alkali-activated cements. Salih et al.<sup>118</sup> assessed the effect  
636 of the curing temperature and duration on the compressive strength development of  
637 these cements, identifying that comparable compressive strengths (21 - 24 MPa after 7  
638 days) were obtained in samples cured at room temperature compared with specimens  
639 cured at between 60 °C and 80 °C. This elucidated that high temperature curing is not  
640 required for these cements, if the mixes are appropriately designed.

641 The utilisation of palm oil fuel ash as a secondary precursor for production of blended  
642 alkali-activated cements has also been widely studied, and the fineness of these ashes

643 has a strong influence on reactivity and consequently strength development. Yusuf et  
644 al. produced alkali-activated cements<sup>119</sup> and concretes<sup>120</sup> based on blends of ultrafine  
645 palm oil ash and blast furnace slag. The addition of up to 20 wt.% ultrafine palm oil  
646 fuel ash to the slag-based mixes increased the compressive strength after 28 days of  
647 thermal curing, but higher volumes of ash slightly reduced mechanical performance.  
648 Conversely, Islam et al.<sup>121</sup> identified that the optimal level of blast furnace slag  
649 substitution by a coarser palm oil ash was 30 wt.%. Blended palm oil ash-slag alkali-  
650 activated cements exhibited good chemical resistance when exposed to sulfuric acid,  
651 when the content of slag was lower than 40 wt.% of the total binder (to minimise the  
652 degree of damage which could happen via decalcification and gypsum formation) and  
653 when the water content of the cement was held low.<sup>122</sup>

654 Ranjbar et al.<sup>123,124</sup> partially replaced coal fly ash by palm oil fuel ash in alkali-activated  
655 cements, where a delay in compressive strength development was observed as the  
656 fraction of palm oil fuel ash increased, in contrast to the trend identified in activated  
657 slag/palm oil fuel ash cements as noted above. These alkali-activated palm oil fuel  
658 ash/fly ash blended cements gained strength when exposed to temperatures of up to 500  
659 °C and then cooled to room temperature for testing; however, larger fractions of palm  
660 ash reduced the strength retention upon heating of these materials. High resistance to  
661 sulfuric acid exposure was also found in concretes based on these binders by Ariffin et  
662 al.,<sup>125</sup> compared with Portland cement based concretes. This was again associated with  
663 the absence of Ca-rich reaction products, which are more prone to react with the sulfuric  
664 acid to form gypsum.

665 Kupaei et al.<sup>126</sup> identified an increase in the compressive strength of foamed cements  
666 as coal fly ash was partially replaced by palm oil fuel ash, which was attributed to the  
667 higher water demand of the coal ash and thus the need to add more water to achieve  
668 satisfactory workability, and Liu et al.<sup>127</sup> also developed low-density structural  
669 insulating materials from this combination of precursors. Hawa et al.<sup>128</sup> added palm oil  
670 fuel ash to alkali-activated metakaolin, which was able to decrease the tendency  
671 towards drying shrinkage of these alkali-activated cements.

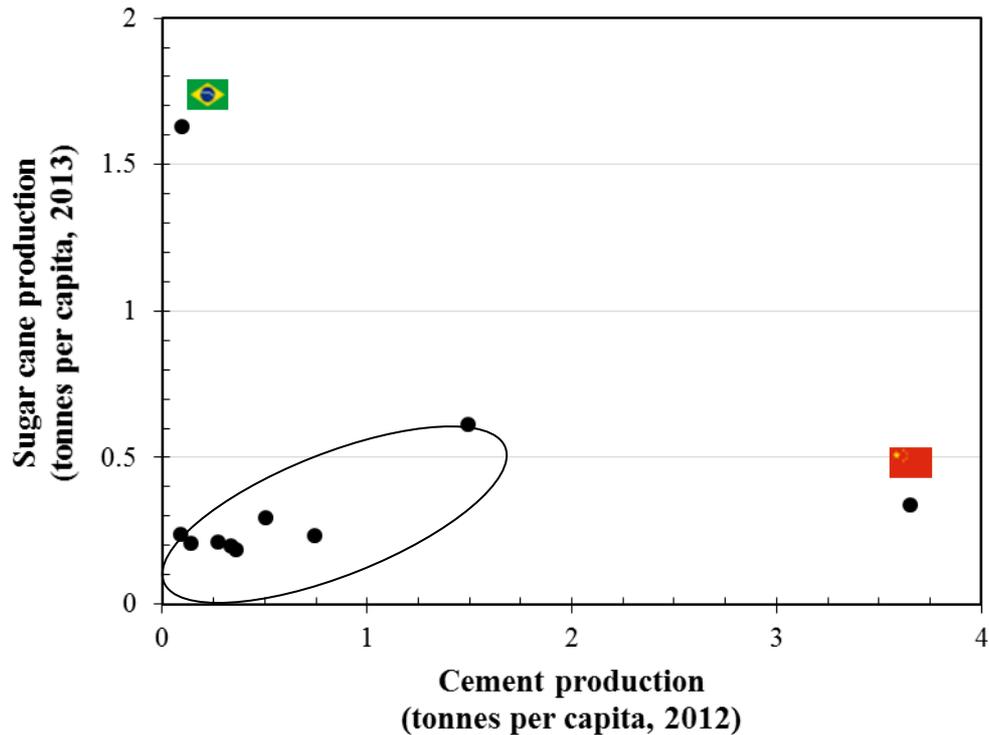
672 The growing number of studies utilising this waste, and the positive results obtained in  
673 terms of mechanical performance and durability, elucidate that alkali-activation  
674 technology is a feasible pathway for its exploitation and the production of construction  
675 materials in palm oil producing areas, some of which are underdeveloped and in need

676 of low-cost housing. The production volumes of palm oil fuel ash from major electricity  
677 generating facilities are also sufficient to make the production of alkali-activated  
678 concretes from the ash potentially economically viable, and the timescale on which  
679 these ashes are expected to be produced is also sufficiently long to make construction  
680 of dedicated facilities for their utilisation in construction materials appear worthwhile.

681

### 682 **3.3 Sugar cane bagasse ashes**

683 Sugar cane is the single most produced crop in the world,<sup>100</sup> with an estimated  
684 production of more than 2165 million tonnes in 2013,<sup>129</sup> around 30% of which is  
685 produced in Brazil, with very large volumes also generated in other warm-climate  
686 regions of the Americas and Asia. These regions in general correspond to areas of high  
687 demand for construction materials, and so any by-products generated by the sugar  
688 industry would appear to be geographically well located for use in concrete production.  
689 This is highlighted in Figure 7, which compares the per-capita cement and sugar cane  
690 production for the world's top 10 sugar cane producing countries. All of these nations  
691 have relatively high per-capita cement production, correlating well with sugar cane  
692 production (circled region) except in the cases of Brazil (high sugar cane, moderate  
693 cement) and China (high cement, moderate sugar cane) as marked in Figure 7. This  
694 indicates that there is generally likely to be good availability of sugar cane bagasse ash  
695 in areas of high demand for construction materials, which shows a strong potential for  
696 the valorisation of this waste material in construction applications.



697

698 Figure 7. Comparison of sugar cane and cement production per capita (top 10 global  
699 sugar cane producers). Data from <sup>130-132</sup>

700

701 It has been reported<sup>133</sup> that for every 10 tonnes of sugarcane crushed, a sugar factory  
702 produces nearly three tonnes of wet bagasse, which is thus a highly significant source  
703 of waste produced worldwide. Sugar cane bagasse is used for several applications,  
704 including in the production of animal feed, enzymes, amino acids, organic acids and  
705 compounds of pharmaceutical importance;<sup>134</sup> however, it is also often utilised as fuel  
706 in sugar cane mills. Bagasse combustion produces silica-rich ashes which have been  
707 studied over the past decades as supplementary cementitious materials.<sup>135-139</sup> In Brazil  
708 alone, the generation of sugar cane bagasse ash (SCBA) is equivalent to about 6% of  
709 national Portland cement production,<sup>140</sup> which could potentially mitigate more than 500  
710 kilotonnes of CO<sub>2</sub> emissions per year if the SCBA were to be used as a partial cement  
711 replacement.

712 A limited number of studies have been carried out to demonstrate the utilisation of  
713 sugar cane bagasse ashes as precursors for alkali-activated cements. Castaldelli et al.<sup>141</sup>  
714 demonstrated that it is possible to produce alkali-activated cements based on a blend of  
715 blast furnace slag and SCBA, with compressive strengths of up to 60 MPa after 55 days

716 of curing at 20 °C, and low porosity. In a later study, the same group<sup>142</sup> also produced  
717 cements from alkali-activated fly ash blended with sugar cane bagasse ash which had  
718 been thermally treated to reduce its content of organics. These cements developed good  
719 compressive strengths when cured at 65 °C, associated with the formation of an  
720 aluminosilicate type gel as the main reaction product.

721 More recently Pereira et al.<sup>143</sup> also produced blended activated cements based on blast  
722 furnace slag and SCBA, and evaluated the durability of these binders when exposed to  
723 hydrochloric acid, acetic acid, ammonium chloride, sodium sulfate and magnesium  
724 sulfate. These cements performed much better than Portland cements when exposed to  
725 ammonium chloride, acetic acid and sodium sulfate; however, little advantage was  
726 observed when the specimens were exposed to hydrochloric acid or magnesium sulfate.  
727 The partial substitution of slag by sugar cane bagasse ash did not have a significant  
728 effect in the phase assemblage or mechanical strength development of the assessed  
729 cements. Therefore, it was proposed that this might be a feasible way to reduce the  
730 production cost of alkali-activated blast furnace slag cements by achieving good  
731 performance with lower contents of this more expensive precursor, and also to  
732 maximise the re-use of sugar cane bagasse ashes, particularly where exposure of the  
733 hardened material to certain chemically aggressive conditions is likely.

734

## 735 **4 Wastes from the mining and mineral industries**

### 736 **4.1 Red mud**

737 Red mud is an alkaline waste with a pH between 9.2 to 12.8 in the untreated state,<sup>144</sup>  
738 generated from alumina extraction via the Bayer process, where the bauxite ore is  
739 treated with sodium hydroxide solutions. When most of the aluminium has been  
740 extracted from the ore, the red mud has a high quantity of entrained NaOH, and contains  
741 iron oxides that give its red colour. This waste can contain high contents of silicon, as  
742 well as some residual aluminium whose quantity depends on the efficiency of the Bayer  
743 process operations, often present as zeolites or related aluminosilicate mineral phases.  
744 The worldwide annual generation of red mud is estimated at 120 million tonnes/year,  
745 which makes its disposal an issue of great environmental importance.<sup>145</sup>

746 The development of mechanical strength through alkali-activation of red mud is limited  
747 by the low available aluminium content of most of the red mud sources which have

748 been tested. However, the use of a more aluminium-rich red mud,<sup>146</sup> or adding  
749 metakaolin<sup>147</sup> or fly ash<sup>148,149</sup> as secondary sources of aluminium, can contribute to  
750 improve the mechanical strength development of the alkali-activated binder. Kumar et  
751 al.<sup>150</sup> have produced paving blocks based on alkali-activated fly ash/red mud blended  
752 cements which comply with the relevant Indian national legislation (BIS IS  
753 15658:2006) for precast concrete blocks, and with low leachability of alkalis. Alkali-  
754 activated blast furnace slag/red mud blended binders have also been developed,<sup>151–153</sup>  
755 and the slag significantly increased the compressive strength of these materials.

756 Ye et al.<sup>153,154</sup> identified that thermal treatment of red mud increases its reactivity in  
757 alkali-activation; however, it was still not sufficiently reactive to develop a measurable  
758 compressive strength when simply mixing the calcined red mud with water, despite its  
759 high initial alkalinity. In a following study, Ke et al.<sup>155</sup> added NaOH prior to the thermal  
760 treatment of the red mud, which favoured the formation of hydraulic phases including  
761 a disordered peralkaline Na-aluminosilicate, tricalcium aluminate and  $\alpha$ -dicalcium  
762 silicate. This modified red mud reacted with water, without requiring the addition of an  
763 additional alkali-activator, and hardened monoliths with a measurable compressive  
764 strength were produced. This study demonstrated that utilisation of red mud for  
765 producing just ‘added water’ alkali-activated cements is feasible via alkali-thermal  
766 activation, although the cost-effectiveness of such a process requires further  
767 investigation and a secondary source of inexpensive alkalis.

768

769

## 770 **4.2 Kaolin wastes**

771 Kaolin is one of the most important clay minerals exploited for the manufacture of  
772 paper (~45%), ceramics (~15%), refractories (~15%), and other products. The United  
773 States, Uzbekistan, Czech Republic, Germany and Republic of Korea are the largest  
774 producers of kaolin, with an annual total production estimated at ~23 millions of metric  
775 tons.<sup>156</sup> The clay is often extracted from open-cut mines and is processed by different  
776 treatments (thermal, mechanical or chemical) to remove impurities, enhance whiteness,  
777 and/or adjust particle size distributions and shape. Wet processing is widely used to  
778 produce kaolin products for the paper industry and in filler applications. In this process,  
779 a dispersed kaolin-water suspension is passed through screens, hydroseparators, or

780 hydrocyclones to remove the coarser mineral particles. Thereafter, whitening to  
781 increase brightness is carried out. The rejected kaolin sludge is now generating a  
782 considerable environmental impact due to the large areas required for its disposal.<sup>157,158</sup>  
783 This mineral waste is formed mainly of coarse kaolinite particles and some traces of  
784 quartz and/or anatase.<sup>159</sup>

785 In recent years, the mining industry has become motivated to find a suitable application  
786 for the rejected kaolin sludge, with a view towards its potential valorisation. In this  
787 sense, dried kaolin waste has been assessed as an aggregate in asphalt concrete.<sup>160</sup>

788 The controlled thermal treatment of kaolin sludge at temperatures around 700 °C  
789 transforms the waste kaolinite into metakaolin, which is a material with higher added  
790 value. This metakaolin derived from calcined kaolin sludge (CKS) exhibits pozzolanic  
791 properties and high reactivity in cementitious systems<sup>161,162</sup> and in zeolite  
792 synthesis.<sup>163,164</sup>

793 This reactivity indicates that CKS is potentially suitable for use in the production of  
794 alkali-activated binders. Longhi et al.<sup>165,166</sup> assessed the use of a Brazilian kaolin waste,  
795 which was thermally treated at 700 °C and ball milled, then activated with sodium  
796 silicate solution. The resulting geopolymers exhibited high mechanical performance  
797 (up to 70 MPa in compression), comparable to the strengths achieved through the use  
798 of a much more expensive commercial metakaolin as precursor, and the coarser particle  
799 size of the CKS is actually to some extent beneficial in improving the fresh-state  
800 properties of the geopolymer mixes. Alkali-activation thus appears to be a technological  
801 and feasible solution for the valorisation of this industrial waste.

802

### 803 **4.3 Low purity clays**

804 The search for low cost or easily available materials for production of alkali-activated  
805 cements has led to the assessment of ‘normal clays’ such as montmorillonites, smectites  
806 and illites, among others. These clays are widely available all over the world, and may  
807 show reactivity with alkalis after thermal activation.<sup>167–169</sup> However, they tend to be  
808 more variable in composition and mineralogy than commercial kaolinites, and the  
809 parameters of the thermal activation process must be particularly precisely controlled  
810 in order to reach high reactivity.<sup>170</sup> So, extensive research is required to elucidate the

811 factors that control the performance and long term stability of alkali-activated cements  
812 based on normal clays.

813 Two particular types of clays, bentonite and lateritic soils, are the object of alkali-  
814 activation research in several countries. Laterites are soil types rich in iron and  
815 aluminium, formed in hot and wet tropical areas, and contain kaolinite in which a high  
816 proportion of  $\text{Al}^{3+}$  is replaced by  $\text{Fe}^{2+}$  or  $\text{Fe}^{3+}$ .<sup>171</sup> When thermally treated between 750  
817 °C and 800 °C, the kaolinite and gibbsite present in the soil transform into metakaolin  
818 and amorphous alumina,<sup>172</sup> which show pozzolanic activity and can be used as  
819 supplementary cementitious materials for concrete production.<sup>173</sup> In recent years, there  
820 has been a growing interest producing alkali-activated cements based on calcined  
821 lateritic soils. Silva-Neto et al.<sup>174</sup> and Gomes et al.<sup>175</sup> have demonstrated that Brazilian  
822 laterites are suitable precursors for alkali-activated cement production. In these systems  
823 the iron is seen to play a significant role in the development of the binding phases, so  
824 that iron distribution in the aluminosilicate type gels appears to occur via formation of  
825 Fe-Al-Si oxide amorphous structures. Although the structural role of  $\text{Fe}^{3+}$  as a  
826 substituent for  $\text{Al}^{3+}$  in these aluminosilicate gels remains poorly understood, screening  
827 methodologies such as those presented by McIntosh et al.<sup>176</sup> for the Fe-rich kaolinite  
828 resources of Northern Ireland offer the possibility to identify and exploit these lower-  
829 purity clay deposits, which would otherwise be of little or no economic value, as  
830 precursors for alkali-activation. The potassium silicate-activated mixes described in  
831 that study reached strengths as high as 89 MPa at 7 days.

832 Lassinanti-Gualtieri et al.<sup>177</sup> assessed the effectiveness of either acidic (phosphoric  
833 acid) or basic (sodium silicate) activation of laterite soils, before and after thermal  
834 treatment, to produce alkali-activated cements. It was demonstrated that thermal  
835 treatment of the laterite is required prior to chemical activation, and that both pathways  
836 of activation could promote the formation of hardened solid binders from a suitably  
837 calcined precursor. The acid phosphate chemistry described in this context appears in  
838 some way similar to the ‘Ceramicrete’ phosphate-bonded ceramics, and also to  
839 published work based on the combination of phosphoric acid and pure metakaolin,<sup>178</sup>  
840 but the cost of phosphoric acid is rather high and so is likely to restrict its use in large-  
841 scale applications.

842 Bentonite is a montmorillonite type clay that can be thermally treated to produce a  
843 pozzolan, and can be used by the construction industry as a supplementary cementitious

844 material.<sup>179,180</sup> There exist a limited number of studies related to alkali-activation of  
845 thermally treated bentonite. Hu et al.<sup>181</sup> carried out a study using non-treated bentonite  
846 as an additive (less than 15 wt.%) in alkali-activated fly ash binders, identifying that  
847 this clay acted as a filler and contributed to densify these binders. Chervonnyi et al.<sup>182</sup>  
848 utilised alkali-activated thermally treated bentonite for the solidification of low-level  
849 radioactive ashes from the Chernobyl accident region. Monoliths achieved 12 MPa after  
850 28 days of curing, and showed significantly lower leachability of strontium compared  
851 with Portland cement grouts. This suggested that alkali-activated cements based on  
852 bentonites could be an environmentally beneficial process for treatment of radioactive  
853 wastes.

854 More recently García-Lodeiro et al.<sup>183</sup> evaluated thermally treated bentonites as the sole  
855 precursor for producing alkali-activated cements. This study elucidated that effectively  
856 alkali-activated thermally treated bentonites produce hardened solids, whose strength  
857 is dependent on the availability of Si and Al in the system. The addition of highly  
858 soluble sources of Al, such as sodium aluminate, improved the compressive strength of  
859 these binders.

860 The alkali-activation of low cost normal clays such as bentonites and laterites, which  
861 are highly available in growing countries where the need for infrastructure is pressing  
862 and will increase in coming years, seems a viable alternative pathway to produce  
863 affordable construction materials.

864

#### 865 **4.4 Other mining and mineral wastes**

866 Mining wastes are fine and coarse mineral materials resulting from mining and mineral  
867 processes operations, which usually are collected, transported and placed in large heaps  
868 or dams.<sup>184</sup> Approximately seven billion tons of tailings are produced worldwide each  
869 year, much of which consists of clay-rich minerals which are impure and considered to  
870 be of low value, but which may offer significant value as precursors for alkali-  
871 activation, particularly in applications such as mine backfilling where the ability to  
872 replace Portland cement offers the possibility to reduce costs and gain environmental  
873 benefit.<sup>185</sup>

874 One such source of low purity clays from the mining industry is a tungsten mine waste  
875 from Portugal, which is an aluminosilicate rich in clay minerals and iron. When

876 thermally treated at 950 °C, dehydroxylation and amorphisation of this waste has been  
877 identified,<sup>186</sup> consistent with its significant content of phyllosilicate clay minerals.  
878 Pacheco-Torgal et al.<sup>187</sup> evaluated the effect of NaOH and Ca(OH)<sub>2</sub> concentrations on  
879 the mechanical performance of alkali-activated calcined tizatugsten mine waste, and  
880 used these results to develop a material with an optimised activator content,<sup>186</sup> as well  
881 as lower shrinkage than Portland cement and low water penetration. Conversely, the  
882 blending of sodium carbonate with the tungsten mine waste hindered the  
883 dehydroxylation of the waste, and even though a high compressive strength was  
884 achieved at early times of curing, a reduction in the stability of these cements was  
885 observed when immersed in water.<sup>188</sup>

886 Other mining wastes that have been utilised to produce alkali-activated cements include  
887 those obtained from copper mining, which are rich in feldspars and can be used in the  
888 production of bricks;<sup>189,190</sup> heavy metals are also able to be effectively immobilised in  
889 these materials.<sup>191</sup> The addition of a small quantity of sodium aluminate can enhance  
890 the strength development of these materials, depending on the temperature of curing,<sup>190</sup>  
891 which suggests that the availability of aluminium from the mining wastes was limiting  
892 the performance achieved. For this reason, the combination of copper mine wastes or  
893 tailings with other aluminous materials has also been identified as advantageous in  
894 alkali-activation; Zhang et al.<sup>192</sup> produced copper mine tailings/fly ash-based alkali-  
895 activated cements, where fly ash addition promoted high compressive strengths and  
896 relatively rapid strength development. Ahmari et al.<sup>193</sup> produced alkali-activated  
897 cements by blending copper mine tailings with low-calcium flash-furnace copper  
898 smelter slag and an alkali activator. The addition of the smelter slag enhanced the  
899 mechanical strength and promoted the formation of a denser microstructure, as a  
900 consequence of the high solubility of silica from the slag and its fine particle size  
901 distribution. However, elevated temperature curing was required to accelerate the  
902 hardening of the specimens. Ren et al.<sup>194</sup> also showed that aluminium sludge could be  
903 effective as a secondary source of Al<sub>2</sub>O<sub>3</sub> in an alkali-activated blend with copper mine  
904 tailings, to decrease the overall Si/Al molar ratio and improve the performance of the  
905 resulting binders.

906 Caballero et al.<sup>195</sup> utilised a silica-rich gold mining waste, derived from the grinding  
907 and subsequent separation of sulfides from quartzo-feldspathic gneiss, as the main  
908 precursor to produce alkali-activated cements, with minor Portland cement addition to

909 accelerate early reaction. These cements developed compressive strengths of up to 45  
910 MPa, and presented a high resistance to when exposed to sulphuric acid, but  
911 degradation of the specimens was identified upon exposure to nitric acid. In both  
912 sodium and magnesium sulfate solutions, these cements gained strength at extended  
913 times of immersion. In another study, the alkali-activation of thermally treated  
914 halloysite blended with volcanic glass and gold extraction tails was reported by Barrie  
915 et al.<sup>196</sup> The cements thus produced developed good compressive strength (30 MPa),  
916 and immobilisation of zinc and lead present in the tails was achieved in these alkali-  
917 activated cements. However, high leachability of arsenic and copper was identified in  
918 these specimens, which makes the material unsuitable for construction purposes, and  
919 so it was suggested that these activated cements may be most effectively used for back-  
920 fill purposes or as capping materials.<sup>196</sup>

921

## 922 **5 Wastes from other industries**

### 923 **5.1 Coal bottom ashes**

924 Coal is the most abundant fossil fuel used for electricity generation, and its relatively  
925 low cost and large deposits represent a reliable source of energy. Around 7.1 billion of  
926 tonnes of coal is used worldwide every year.<sup>197</sup> The main coal combustion wastes (or  
927 by-products) are fly ash, bottom ash, flue-gas desulfurisation products, and boiler slag.  
928 These wastes are mainly used as raw materials for the construction industry in the  
929 production of clinker or blended cements and concretes, in civil engineering (as  
930 subgrade stabilisation, pavement base course, and structural fill), and for site restoration  
931 in open cast mining.<sup>198,199</sup> However, the majority of these materials are eventually sent  
932 to landfill rather than being effectively re-used.

933 Coal fly ash (FA) is currently playing an important role in the concrete and cement  
934 market due to its low cost and pozzolanic reactivity,<sup>200</sup> and has been discussed in the  
935 context of its use in alkali-activation in several major reviews, so will not be the focus  
936 of discussion here. The second most important residue generated during coal  
937 combustion is coal bottom ash (CBA), which represents up to the 20% of the total ash  
938 generated. The CBA is collected at the bottom of the furnace and consists of larger,  
939 granular and glassy heavier particles. The total production of CBA in the European  
940 Union (EU15) is estimated to be ~4.1 Mt per annum, and only 46% of this is re-used

941 efficiently.<sup>201</sup> In the U.S., the total production of CBA reported in 2012 was 14.1 Mt  
942 with a utilisation rate of 38.8%.<sup>202</sup>

943 Although FA and CBA have similar origins, their physical and chemical features differ  
944 widely. In particular, the CBA generally contains more heavy metals than the fly ash.  
945 Therefore, in some countries, the most recent regulations and policies for the safe  
946 disposal of coal combustion wastes have modified the management of CBA.<sup>203</sup> Taking  
947 into account the large volume that is disposed in landfill, CBA is becoming an  
948 environmental and economical concern due to the large land areas used, as well as the  
949 ground and water contamination by leaching of trace elements. CBA has been used as  
950 an artificial aggregate in concrete by substitution for sand,<sup>204,205</sup> and also shows some  
951 pozzolanic reactivity, which can be improved through mechanical treatment.<sup>206,207</sup>  
952 However, its use as a supplementary cementitious material has not been widely  
953 accepted due to its high porosity and low density, which have a negative effect on water  
954 demand.<sup>207</sup>

955 A significant alternative route for the valorisation of CBA is its potential use as a raw  
956 material for the production of alkali-activated cements, as a consequence of its  
957 relatively high content of SiO<sub>2</sub> and Al<sub>2</sub>O<sub>3</sub> in reactive form.

958 However, Chindaprasirt et al.<sup>208</sup> provided a comparative assessment of alkali-activated  
959 binders produced with FA or CBA (both with CaO contents of ~16.5%), and found that  
960 the compressive strength achieved by the FA-based binders was considerably higher  
961 than was achieved with the CBA, due to the higher reactivity and higher content of  
962 amorphous phases present in the FA. As was noted above related to the utilisation of  
963 CBA as a pozzolan, the application of mechanical treatment can also increase its  
964 reactivity in alkali-activation, and thus mortars with improved mechanical performance  
965 and higher workability can be obtained.<sup>209</sup> The differences in chemical composition,  
966 degree of amorphicity and particle size distribution of the diverse CBAs generated in  
967 different thermoelectric plants lead to an intrinsically high variability in the  
968 development and optimisation of alkali-activated binder formulations based on these  
969 materials.

970 Because the development of CBA-based alkali-activated binders has increased only  
971 recently, there exist few reports related to the performance of these materials when  
972 exposed to aggressive environments. Sata et al.<sup>210</sup> studied alkali-activated binders

973 derived from a milled CBA exposed to 3% H<sub>2</sub>SO<sub>4</sub> and 5% Na<sub>2</sub>SO<sub>4</sub> solutions. The  
974 mortars exhibited excellent performance after immersion in these sulfate solutions,  
975 which is even better when finer CBA is used due to the finer pore size distribution and  
976 consequent lower permeability of the binders.<sup>211</sup>

977 As an alternative method to using alkali-activation directly to convert waste into  
978 cementitious binders, Geetha and Ramamurthy<sup>212</sup> reported the effectiveness of a  
979 pelletisation method for the production of artificial coarse aggregates through the  
980 alkali-activation of CBA using blends of NaOH, sodium silicate and Ca(OH)<sub>2</sub>.  
981 Although their results elucidate a novel potential route to valorisation and application  
982 of CBA, further assessment is required in order to understand the performance of these  
983 synthetic aggregates in concrete mixes, as well as the economic and environmental  
984 feasibility of their production through the alkali activation of CBA.

985

986 In general, the volume of CBA generated worldwide is continuing to increase as the  
987 worldwide demand for energy grows, and the development of new methods for the safe  
988 disposal or valorisation of this material is essential. Its chemical and physical properties  
989 are more challenging, and more variable, than those of the fly ash which results from  
990 the same coal combustion processes, but this also means that the competition from other  
991 potential users of CBA is much lower and so it offers significant potential for  
992 development in future years.

993

## 994 **5.2 Paper sludge ash**

995

996 It has been estimated that one tonne of paper sludge is generated per three tonnes of  
997 paper produced,<sup>213</sup> and considering the total worldwide annual production of 403  
998 million tonnes of paper,<sup>214</sup> this means that more than 130 million tonnes of paper sludge  
999 need to be valorised or disposed worldwide each year. Some of the strategies adopted  
1000 for the management of paper industry wastes include incineration with energy recovery,  
1001 pyrolysis, steam reforming, production of mineral fillers for building materials such as  
1002 cement, among others.<sup>213</sup> In particular, paper sludge ash is a by-product derived from  
1003 the incineration of paper sludge, which can contain varying quantities of thermally-  
1004 amorphised clays and partially decomposed calcium carbonate, depending on the

1005 proportions of clay and calcite used in paper production. The potential use of this ash  
1006 as a supplementary cementitious material has been studied over the past decade,<sup>215,216</sup>  
1007 considering the importance of both calcined clays and limestone as mineral admixtures  
1008 for Portland cement.

1009 A limited number of studies have been carried out using paper sludge ashes as a  
1010 precursor for alkali-activated cements. In preliminary work, Yan et al.<sup>217</sup> identified that  
1011 the partial substitution of fly ash with dried (uncalcined) paper sludge reduced the  
1012 workability and compressive strength of the alkali-activated cements; however, it did  
1013 promote a refinement of the pore structure which led to a reduced drying shrinkage of  
1014 the material. Antunes Boca Santa et al.<sup>218</sup> produced alkali-activated calcined paper  
1015 sludge cements blended with coal bottom ashes, as the calcined paper sludge utilised  
1016 was partially crystalline and not highly reactive. Higher contents of bottom ash  
1017 contributed to increase the mechanical strength and density of the cements.

1018

1019 More recently, Gluth et al.<sup>219</sup> reported higher compressive strengths in water-hydrated  
1020 paper sludge ash paste compared to the same ash activated by NaOH or KOH, after 28  
1021 days of curing. All of the portlandite formed by hydration of the free lime in the ash  
1022 was consumed during the first 7 days of curing. Bernal et al.<sup>220</sup> utilised a paper sludge  
1023 ash rich in free lime as a precursor for production of alkali-activated cements. This  
1024 particular paper sludge ash was highly reactive, and when combined with either water  
1025 or an alkaline solution, it formed hydrated reaction products including AFm-type  
1026 phases, portlandite and a highly disordered C-A-S-H type phase. The inclusion of an  
1027 alkaline solution (either sodium hydroxide or silicate) increased the dissolution rate of  
1028 free lime, and consequently favoured the formation of more Ca-rich phases compared  
1029 to the water-hydrated paper sludge ash.

1030

1031 Considering the significant differences in composition, particularly the content of free  
1032 lime, between paper sludge ashes from different sources, it cannot be stated that this  
1033 waste will generically be suitable for production of alkali-activated cements, as the  
1034 activation reaction will proceed in a different way depending on the content of calcium  
1035 present in the ash. However, with the correct combination of ash, activator and  
1036 secondary (likely siliceous) precursors, it does appear possible to produce good-quality  
1037 alkali-activated materials from paper sludge ash, and this would seem to be a high  
1038 value-added end usage for these ashes.

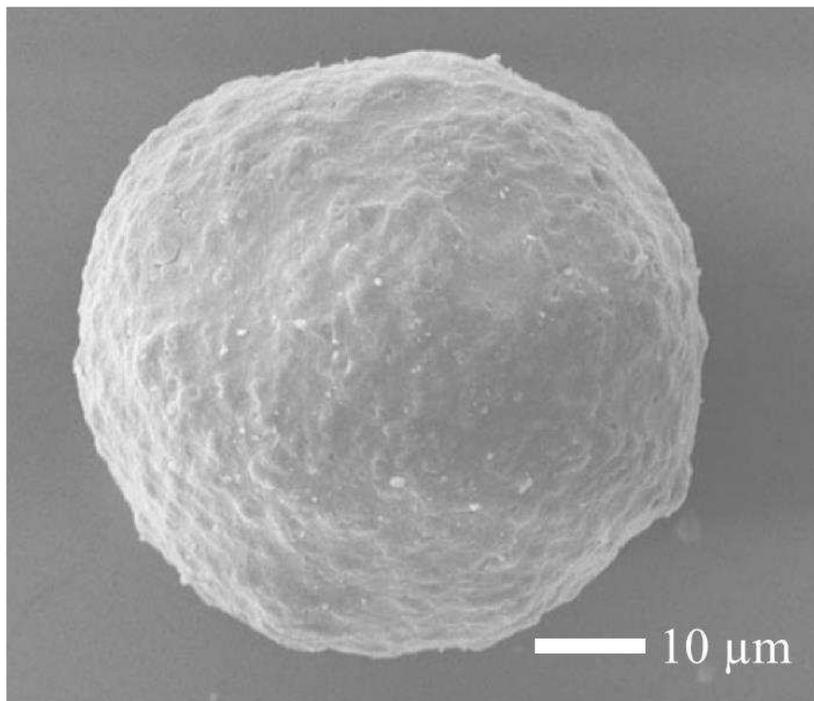
1039

### 1040 5.3 Spent fluid catalytic cracking catalyst

1041

1042 Fluid catalytic cracking catalyst (Figure 8) is an aluminosilicate product, often based  
1043 on a zeolitic framework, used extensively in oil refineries. Once this catalyst loses its  
1044 activity (becomes 'spent'), and if it cannot be effectively or economically regenerated,  
1045 it is discarded and treated as waste. This waste catalyst has been studied as a potential  
1046 supplementary cementitious material for the production of blended cements,<sup>221,222</sup> and  
1047 high performance mortars and concretes have been produced in this manner. The  
1048 reactivity of this waste varies depending on the nature of the initial catalyst used,<sup>221,223</sup>  
1049 therefore optimisation studies are required when using materials from different sources.  
1050 The production of this waste is relatively low, around 800,000 tons per year worldwide  
1051 in 2010,<sup>224</sup> which has limited its large-scale adoption as a partial replacement of  
1052 Portland cements in concrete production.

1053



1054

1055 Figure 8. SEM image of a spent fluid cracking catalyst particle, showing a spherical  
1056 particle morphology and absence of micron-scale pores, as well as bright regions  
1057 which are likely to correspond to high local concentrations of heavy metals. From

1058

Bare et al.,<sup>225</sup> copyright John Wiley & Sons.

1059

1060 In recent years, Tashima et al.,<sup>226,227</sup> Rodríguez et al.<sup>228</sup> and Trochez et al.<sup>229</sup> utilised  
1061 fluid catalytic cracking catalyst residues as sole precursors for producing alkali  
1062 activated cements. These studies have been focused on evaluating the effects of  
1063 different formulation parameters on the microstructural development of these materials,  
1064 their phase assemblage and compressive strength. There is a good consensus that this  
1065 waste is a suitable precursor for producing alkali-activated cements, which can develop  
1066 a high compressive strength depending on the formulation adopted for its production.  
1067 In the case of Tashima et al.<sup>226,227</sup> high temperature curing (65 °C) was utilised, while  
1068 Rodríguez et al.<sup>228</sup> and Trochez et al.<sup>229</sup> cured their samples at 40 °C and 25 °C,  
1069 respectively, and the materials obtained developed compressive strengths comparable  
1070 to those reported for high temperature cured specimens. Significant differences in the  
1071 nature of the alkali activation reaction products between sources of spent fluid catalytic  
1072 cracking catalyst waste have been identified across these studies, and therefore it is  
1073 necessary to identify the characteristics of the waste, particularly mineralogy and  
1074 particle size distribution, that control its performance when used as a precursor for  
1075 alkali-activated cements.

1076 The alkali-activation of this waste might be of interest for its treatment or valorisation,  
1077 depending on the content of toxic and hazardous elements present, as both catalytic  
1078 heavy metals and contaminants deposited on the catalyst in use can be important in  
1079 determining the availability of hazardous species from the waste catalysts. Further  
1080 investigation of these systems is required to elucidate whether these cements can  
1081 develop specialised technical properties to make their development sufficiently  
1082 attractive for commercial purposes.

1083

## 1084 **6 Summary and general considerations**

1085 Table 1 provides a summary of the nature and production of the wastes discussed in  
1086 this review, and their characteristics which are particularly relevant to use in the  
1087 production of alkali-activated cements and concretes.

1089 Table 1. Summary of wastes considered, and key factors defining their utilisation in alkali-activated cement materials.

	Quantities available	Use in alkali activation technology	Disadvantages if used in alkali-activation	Potential advantages for use in alkali-activation	Waste classification <sup>230</sup>
Ashes from municipal waste incineration	<p>EU-27 incinerates ~58 Mt of MSW (2012), producing between 6-18 Mt of BA.<sup>231</sup></p> <p>The main cities in China generated more than 172 Mt in 2014.<sup>232</sup></p> <p>The US generated 254 Mt of MSW in 2013, where 13% (~33 Mt) was incinerated and ~8 Mt of BA was produced.<sup>15</sup></p>	<p>As precursor.</p> <p>As a secondary precursor</p> <p>As aggregate</p>	<ul style="list-style-type: none"> <li>- Presence of toxic compounds including: metal chlorides, metal sulfates, metal carbonates, polycyclic aromatic hydrocarbons, polychlorinated biphenyls, chlorobenzenes, chlorophenols, chlorinated compounds, benzofurans and heavy metals.</li> <li>- Lower reactivity when compared to traditional precursors.</li> <li>- High heterogeneity in chemical and physical properties among batches.</li> <li>- High water demand due to its high porosity and specific surface area.</li> <li>- A decontamination process could be necessary.</li> <li>- Absence of policies for its re-use in other production processes.</li> <li>- Most of the alkali-activated products will likely require thermal curing</li> <li>- The production of materials with high mechanical performance is limited.</li> </ul>	<ul style="list-style-type: none"> <li>- Reduction of harmful substances released to the environment due to their encapsulation.</li> <li>- High interest to find alternative routes for disposal.</li> </ul>	19.01.11/19.01.12: Mirror hazardous / Mirror non-hazardous
Ceramic and demolition wastes	<ul style="list-style-type: none"> <li>- Construction and demolition waste: EU-27 generates ~860 Mt. China generates ~2.19 Gt.<sup>233</sup></li> <li>- Demolition wastes are not rigorously tracked in U.S. However, the amount estimated in 2012 was approximately 480 Mt.<sup>234</sup></li> <li>- Ceramic waste: Ceramic tile production climbed to 11.913 billion square metres with growth overwhelmingly confined to Asia and non-EU Europe.<sup>61</sup></li> <li>- China, Spain and Italy are the three largest exporter countries, accounting for 66% of world exports.</li> <li>- China, Brazil and India remain the top three tile producer and consumer countries.</li> <li>- The ceramic tile industry generates a large volume of ceramic waste outputs to landfill estimated at 85 kt in 2007 from both excess stock and defective products.<sup>235</sup></li> </ul>	<p>As precursor</p> <p>As a secondary precursor</p> <p>As aggregate</p>	<p><u>Construction and demolition waste:</u></p> <ul style="list-style-type: none"> <li>- High heterogeneity in chemical and physical properties.</li> <li>- Requirement of a classification process due to the presence of different materials (wood, plastic, glass, metal, etc), as well as a milling treatment.</li> <li>- Low reactivity when compared to other precursors.</li> <li>- The alkali-activated products will likely require thermal curing.</li> </ul> <p><u>Ceramic waste:</u></p> <ul style="list-style-type: none"> <li>- Low reactivity when compared to other precursors.</li> </ul>	<p><u>Construction and demolition waste:</u></p> <ul style="list-style-type: none"> <li>- High interest to find alternative routes for disposal.</li> </ul> <p><u>Ceramic waste:</u></p> <ul style="list-style-type: none"> <li>- Better homogeneity in chemical and physical properties when compared to demolition wastes</li> </ul>	17.01/17.01.07: Mirror non-hazardous
Wastes or sediments from water plants	<p>According to the FAO/AQUASTAT database,<sup>236</sup> the values reported between 2008-2015 for municipal waste water production are: Africa: 12.47 Gt/y; Americas: 94.27 Gt/y; Asia: 123.46 Gt/y; EU: 35.54 Gt/y.</p> <p>The estimated sewage sludge production rates in dry metric tons per annum are: EU-27: 8909 (2010); US: 6514 (2004), and China: 2966 (2006).<sup>237</sup></p>	<p>As a secondary precursor</p> <p>Immobilisation</p>	<ul style="list-style-type: none"> <li>- Limited availability of sewage sludge.</li> <li>- Low reactivity due to its low content of amorphous aluminosilicate compounds.</li> <li>- Requires the use of a primary aluminosilicate precursor with high reactivity.</li> <li>- Presence of heavy metals (including Zn, Pb, Cd, Cu, Hg, Zn, and Ni).</li> <li>- Depending on its mineral composition a thermal process could be required (particularly for clay-rich sediment sludges).</li> <li>- Waste water treatment capacity is strongly related to national development.</li> <li>- Absence of policies for its re-use in other production processes.</li> <li>- The alkali-activated products will likely require thermal curing</li> <li>- The production of materials with high mechanical performance is limited.</li> </ul>	<p>Reduction of harmful substances released to the environment due to their encapsulation.</p>	9.02.06/19.08.12: Mirror hazardous/ Mirror non-hazardous
Waste glass	<p>EU-28 glass production 20.85 Mt with a recycling rate of 71% (2013).<sup>238</sup></p> <p>In U.S. the glass container generation and recovery in 2012 were 11.57 Mt and 3.2 Mt, respectively.<sup>239</sup></p>	<p>As a source of SiO<sub>2</sub> for the production of the alkali activator</p>	<ul style="list-style-type: none"> <li>- Limited availability of the residue.</li> <li>- Requirement for a classification process</li> <li>- Presence of high content of Hg when the waste contains used fluorescent lamps.</li> <li>- Low volumes of waste can be valorised due to the low amount of extra SiO<sub>2</sub> required during alkali activation.</li> <li>- Chemical dissolution of amorphous phases can be required.</li> </ul>	<ul style="list-style-type: none"> <li>- There exist targets to achieve higher reuse rate</li> <li>- Reduction of cost of binder production due to the substitution of waterglass, which is the component with the highest price.</li> <li>- Improved performance of alkali-activated systems when used as a soluble source of SiO<sub>2</sub>.</li> </ul>	15.01.07/19.12.05/20.01.02: Absolute non-hazardous 17.02.02: Mirror-non hazardous
Rice husk ash	<p>In 2014 the global production of paddy rice was 746 million metric tonnes.<sup>100</sup> Assuming that 20% of paddy rice is husk, ~150 Mt of this residue was generated. When the husk is burned, 25% of ashes is generated, which represents ~38 Mt.</p>	<p>As a source of SiO<sub>2</sub> for the production of the alkali activator.</p>	<ul style="list-style-type: none"> <li>- Depending on the control of the thermal process, high contents of unburned material can be obtained.</li> <li>- Other potential applications are available, which could increase cost.</li> <li>- The transport cost of the residue can be high due to its low density.</li> <li>- Activator solutions can exhibit a dark color, which might affect the aesthetics of the final product.</li> <li>- Requires an extra investment within the alkali-activation technology/process for its dissolution in order to obtain a high quality activator.</li> <li>- Lower volume utilisation when compared to materials used as precursors, due to the low requirements for soluble silicates during the activation.</li> </ul>	<ul style="list-style-type: none"> <li>- Reduction of cost of binder production due to the substitution of waterglass solution, which is the component with the highest price.</li> <li>- Alkali activator with a specific M<sub>2</sub>O/SiO<sub>2</sub> ratio can be produced.</li> <li>- When produced under optimal conditions, similar performance can be achieved compared to commercial soluble silicate solutions.</li> <li>- Activator solutions with other alkaline cations can be also produced.</li> <li>- High number of reports elucidate its feasibility for use in activator production.</li> </ul>	Not specified in this standard.
Palm oil fuel ash	<p>The global palm oil production for 2015 was 62.6 Mt.<sup>240</sup> Assuming that ash equivalent to 10% of this mass is generated, approximately 6.3 Mt of waste is obtained.</p>	<p>As precursor</p> <p>As a secondary precursor</p>	<ul style="list-style-type: none"> <li>- Low content of reactive alumina.</li> <li>- Most of the systems likely will require thermal curing</li> <li>- Few reports related to its performance and effectiveness as a precursor. More studies are required.</li> </ul>	<ul style="list-style-type: none"> <li>- The presence of calcium (5-15%) can improve its performance as precursor.</li> </ul>	Not specified in this standard.
Sugar cane bagasse ash	<p>Brazil is the world's largest sugar cane producer (around 650 Mt in 2013), which corresponds to 30% of the world's production.<sup>129</sup> Brazilian sugarcane industry generates a considerable amount of sugarcane bagasse ash, estimated at about 2.5 Mt/y (Cordeiro, 2006).</p>	<p>As a secondary precursor</p>	<ul style="list-style-type: none"> <li>- The content of Al<sub>2</sub>O<sub>3</sub> is not sufficient to be used as a main precursor.</li> </ul>	<ul style="list-style-type: none"> <li>- High production in markets with high demand for construction materials.</li> </ul>	Not specified in this standard.
Red mud	<p>120 Mt/y of red mud is generated<sup>241</sup> and currently a quantity in storage of more than 2.7 Bt is estimated.<sup>144</sup></p>	<p>As precursor</p> <p>As a secondary precursor</p>	<ul style="list-style-type: none"> <li>- High content of Fe<sub>2</sub>O<sub>3</sub>, whose participation during the alkali-activation technology and mechanical performance improvement is not well understood (may be positive or negative).</li> <li>- According to the efficiency and effectiveness of the Bayer process, the content of reactive Al<sub>2</sub>O<sub>3</sub> can be extremely low.</li> </ul>	<ul style="list-style-type: none"> <li>- After thermal treatment the red mud can be considered a good alternative to produce one-part alkali-activated systems (just adding water).<sup>155</sup></li> <li>- Alkaline residue (mainly with high contents of dissolved NaOH).</li> </ul>	01.03.09: Mirror non-hazardous
Kaolin wastes	<p>The United States, Uzbekistan, Czech Republic, Germany and Republic of Korea are the largest producers of kaolin, with an annual total production estimated at 23 million metric tonnes.<sup>156</sup> The Brazilian mining industry generates ~0.5 Mt/y of kaolin sludge waste, with a stockpile of ~10 Mt.<sup>242</sup></p>	<p>As precursor</p>	<ul style="list-style-type: none"> <li>- Requires thermal treatment to increase its reactivity</li> <li>- Particle shape reduces the workability of the fresh mixtures</li> <li>- Reactivity degree is dependent on the kaolinite content.</li> <li>- Kaolin sludge can be re-used for other industries and applications.</li> </ul>	<ul style="list-style-type: none"> <li>- Materials with high mechanical performance can be obtained (even comparable to pure MK-based systems).</li> <li>- Depending on the source, the chemical and mineralogical composition might be homogeneous.</li> </ul>	Not specified in this standard.
Coal bottom ashes	<p>In 2010 the global production of coal combustion products (CCP) was estimated at 780 Mt. Considering that the ~15% of the overall CCP is CBA, the generated estimated value is around 117 Mt.<sup>8</sup></p> <p>Annual production quantities of bottom ash in US and EU were about 14 (American Coal Ash Association (ACAA), 2014) and 4 (European Coal Combustion Products Association (ECOBA), 2012) million tonnes in the last decade, respectively.<sup>243</sup></p>	<p>As precursor</p> <p>As a secondary precursor</p>	<ul style="list-style-type: none"> <li>- Low reactivity.</li> <li>- High heterogeneity in chemical and physical properties among batches.</li> <li>- The production of materials with high mechanical performance is limited.</li> <li>- The alkali-activated products will likely require thermal curing</li> </ul>	<ul style="list-style-type: none"> <li>- High interest to find alternative routes for disposal.</li> </ul>	10.01.01: Absolute non-hazardous

	Coal fired thermal plants in India produce about 131 million tons of coal ash, which comprises about 25 million tons of coal bottom ash <sup>204</sup>				
Paper sludge ash	Production of 125 kt per annum in the UK. <sup>244</sup> Confederation of European Paper Industries (CEPI, 2014) states that pulp and paper industry landfill disposal has declined by 55% over the last 12 years, from 32.7 to 14.3 kg/tonne of product. <sup>245</sup>	As precursor As a secondary precursor	- Requires thermal treatment in order to increase its reactivity. - Particle shape may reduce the workability of the fresh mixtures - Reactivity is dependent on the kaolinite content.	- Thermal treatment conditions for this material are similar to those used for pure kaolinite - Optimisation considers the decomposition of organic material and the prevention of free lime formation from calcite.	03.03.02: Absolute non-hazardous
Spent fluid catalytic cracking catalyst	The global production is estimated at ~200 kt/y. <sup>246</sup>	As precursor	- Low production when compared to the other residues. - The residue requires and previous treatment in order to reduce the content of harmful elements, including V, La, and others.	- High reactivity - Homogeneity in its chemical composition among different batches. - The waste is constituted mainly of SiO <sub>2</sub> and Al <sub>2</sub> O <sub>3</sub> . - Materials (mainly mortars) with high mechanical performance can be produced.	16.08.04: Mirror non-hazardous

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1092

1093 One additional key consideration, which is relevant across many of the wastes  
1094 discussed in this review, is organic carbon content. The content of organic carbon,  
1095 particularly when present as unburned material in wastes generated via thermal  
1096 processes, must be considered carefully in the design of alkali-activated cements. The  
1097 presence of a high content of porous and non-reactive organic particles, with a high  
1098 specific surface area, significantly increases the water demand of the fresh mixtures  
1099 with a consequent negative effect on the rheological and mechanical properties of the  
1100 material. These particles can also absorb the activator solution, which reduce the alkali  
1101 concentration during the reaction process. Fernandez-Jiménez and Palomo suggested  
1102 that a suitable coal FA must have loss on ignition values lower than 5%.<sup>247</sup> However,  
1103 there exist studies related to the production of alkali-activated materials using different  
1104 industrial wastes or by-products derived from thermal processes with higher contents  
1105 of organic matter, including coal fly ash,<sup>248–251</sup> coal bottom ash,<sup>212,252–255</sup> municipal  
1106 solid waste ashes,<sup>256,257</sup> palm oil fuel ash,<sup>120,122,128</sup> and sugar cane bagasse ash.<sup>141</sup> Taking  
1107 into account that the high content of un-reacted material reduces the effectiveness and  
1108 reactivity of these wastes as precursors, blending with another more-reactive  
1109 aluminosilicate may be required. When the mechanical performance requirements for  
1110 the material are higher, the use of precursors with a high content of unburned material  
1111 can be restricted.

1112 One of the methods which is often used to reduce the organic carbon content of waste  
1113 ashes is a more extended (or higher temperature) combustion process, which consumes  
1114 the carbon, but often at the cost of inducing partial crystallisation of the silicate or  
1115 aluminosilicate phases and thus reducing their reactivity. A balance is therefore  
1116 required between carbon elimination and reactivity retention, which necessitates  
1117 careful process control and parametric optimisation to achieve the best results when  
1118 producing alkali-activated cements using siliceous wastes.

1119 Additionally, as discussed in section 3, it is very unlikely that pure siliceous wastes  
1120 would be suitable for use as a sole precursor in alkali-activation due to their low Al  
1121 content; blending with an aluminous material will always be necessary. For these  
1122 reasons, the Si-rich wastes including SCBA, RHA and glass waste have generally been  
1123 used as a source of amorphous silica for the alkaline activator. Although some of the  
1124 residues included in this review have been chemically modified in order to be used as  
1125 alternative alkali activators, the open literature also reports the use of other industrial

1126 wastes that are suitable for potential re-use as waste derived activators. A sodium  
1127 aluminate and NaOH-based solution from the aluminium anodising process has been  
1128 successfully incorporated as an activator in fly ash / blast furnace slag blends. Even  
1129 though the time of setting of these alkali-activated systems were considerably longer,  
1130 these materials were able to generate a 28-day compressive strength higher than 80  
1131 MPa.<sup>258,259</sup> This work, along with other reports of aluminate activation in fly ash-based  
1132 alkali-activated binder systems,<sup>260,261</sup> offers yet another opportunity for the valorisation  
1133 of problematic wastes in the production of this class of construction materials.

1134

## 1135 **7 Concluding remarks**

1136 This paper has summarised the most important research findings related to different  
1137 wastes that could be used for the synthesis of alkali-activated binders. Valorisation of  
1138 a wide variety of metallurgical, societal and agricultural wastes can be achieved through  
1139 the use of these materials as precursors or alternative sources of SiO<sub>2</sub> in the activator  
1140 for alkali-activated binders and concretes. Most alkali-activated mixes are currently  
1141 based on ground granulated blast furnace slag or on fly ash, with alternative wastes  
1142 generally used in lower volumes. Blending of specific wastes in defined combinations,  
1143 often involving one of these better-understood materials in conjunction with another  
1144 alternative material, can offer a lower-risk and potentially highly attractive path to the  
1145 utilisation of a broader range of wastes, as the quality control and metals leachability  
1146 issues which are often associated with many of these materials are reduced through  
1147 dilution.

1148

1149 Standardisation and large-scale commercial deployment of alkali-activation technology  
1150 is taking place rapidly in many jurisdictions worldwide, and although most of the mixes  
1151 now being used at production scale are based on a fairly narrow selection of precursors  
1152 (coal fly ash, blast furnace slag, and calcined clays), a performance-based approach to  
1153 standardisation does certainly offer scope for the utilisation and valorisation of a much  
1154 wider range of silicate and aluminosilicate slags as precursors for the production of  
1155 alkali-activated concretes.

1156

1157 In developing any new material or process for large-scale deployment, it is essential to  
1158 ensure that there is a robust supply chain in place. This is particularly critical in the

1159 construction materials industry because of the enormous volumes which must be  
1160 processed for an operation to be economically viable; a modern cement kiln has a  
1161 throughput on the order of thousands of tonnes per day, whereas in most process  
1162 industries this could easily represent the annual throughput of a large plant. The cement  
1163 and concrete industry, the agriculture industry and the extractive metallurgy industry,  
1164 are arguably the only process sectors which are equipped to handle a such a large  
1165 volume of solids as both precursor and product, and this raises important questions  
1166 when analysing a potential new route to market, or a new product. When defining  
1167 whether a particular alkali-activated binder formulation will be worthy of commercial  
1168 attention, the key question often becomes: is it possible to make enough of this material  
1169 to become commercially viable? A large number of academic studies are conducted,  
1170 and published, which describe the production of an alkali-activated binder system from  
1171 particular combinations of industrial wastes and chemical feedstocks. However, if a  
1172 particular waste material is available only in quantities of a few tens of tonnes per day,  
1173 it will be very difficult to produce a commercially useful volume of alkali-activated  
1174 concrete for general construction or infrastructure applications.

1175

1176 This means that the production of alkali-activated concretes based on waste streams of  
1177 low to moderate volume will require some form of driver other than simply the  
1178 production of a low-cost, standard-performance concrete to enable their use in a  
1179 practical and profitable context. Specific environmental or cost benefits can arise from  
1180 the use of a particular solid waste material (through diversion of materials from landfill)  
1181 or source of waste alkalis (replacing some of the more costly sodium silicate activator)  
1182 in large-scale alkali-activated concrete production), and sometimes the performance of  
1183 alkali-activated materials derived from a specific lower-volume precursor can offer  
1184 attractive opportunities for niche applications. Such properties include chemical and  
1185 thermal resistance, and concretes displaying good performance in these areas can  
1186 command a significant price premium over standard products. This is likely to be the  
1187 area in which alkali-activation of waste materials will lead to commercially and  
1188 technologically significant outcomes, and will enable the true valorisation of wastes  
1189 from a wide range of industries and areas of society, as has been outlined in this review.

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