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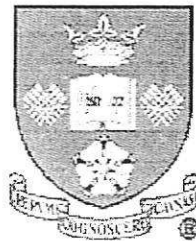
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Adaptive MIMO Multi-periodic Repetitive Control System: Liapunov Analysis

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Research report No. 853

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Abstract

This paper presents a simple feed forward adaptive plus multi-periodic repetitive control scheme for the ASPR(Almost Strictly Positive Real) or ASNR(Almost Strictly Negative Real, see Appendix for definition) plant to asymptotically track or reject multi-periodic reference or disturbance signals. The Liapunov stability analysis is given. This is an extension work of the Liapunov stability analysis for multi-periodic repetitive control system under a positive real condition. A simulation is included. The extension of the Liapunov stability analysis to ASPR or ASNR plant under certain non-linear perturbations and an exponential stability scheme are discussed as well. Finally an adaptive proportional plus MRC(multi-periodic repetitive control) scheme is proposed.

1 Introduction

For a system to track/reject periodic reference/disturbance signal, repetitive control was developed several years ago. This control method, which is based on the internal model principle, has proven to be very effective in practical applications. In most existing repetitive control approaches [1] [2] [4] [8] [12], the asymptotic convergence of the state to the origin and internal stability of the system are guaranteed under some strict assumption on the dynamic system. Hara [2] derived the sufficient conditions for the stability of repetitive and modified repetitive control systems by applying the small gain theorem and the stability theorem for time-lag systems. It is shown that the plant $P(s)$ should satisfy $\|f(s)(1 - P(s))\|_{\infty} < 1$ where $f(s)$ is a low-pass filter introduced to improve the system stability at a cost of losing tracking accuracy at high frequencies. Owens et al [12] [13] gave the Liapunov stability analysis and proved that asymptotic/exponential stability is guaranteed if the linear plant is positive real/strictly positive real or the nonlinear plant



is passive. Similar lyapunov stability analysis was done in [1] [4] [8] and some strict assumptions, which are actually passive condition as in [13], were made on the nominal system of the plant. In this paper, we will alleviate such restrictive assumptions on the plant to some extent.

In many cases, the reference and/or disturbance periodic signals may contain different fundamental frequencies and the ratio of these frequencies can be irrational. So the so-called multi-periodic repetitive control was analysed by several authors (Weiss [18] [19]; Owens et al., 2002 [12]; Li et al., 2002 [9]). Weiss [18] [19] gave a H^∞ stability condition based on input-output transfer function for linear SISO/MIMO single/multi-periodic system. The Liapunov stability analysis is given by Owens et al [12] and it is studied by Li et al [9] that a feed forward and feedback compensation can be employed when the real plants are not necessarily positive real. However, the method in [9] needs some plant parameter information and such information is based on off-line frequency domain system identification of a particular system. Also the plant is restricted to be minimum phase, strictly proper and with relative degree one and positive high-frequency gain.

Adaptive repetitive control design and implementation, which includes internal model principle, have been discussed by many authors [3] [8] [14] [15] [16] [17] [20] both in the discrete-time and continuous-time domain. Most of them [3] [14] [15] [16] [17] are indirect adaptive control algorithms. Several estimation algorithms were used to identify the plant models and certainty equivalence principles were applied to design the adaptive control schemes. On the other hand, Jiang [8] gave a direct adaptive control scheme and applied an adaptively adjusted gain in the feedback controller when the upper bound of the plant uncertainty exists, however unknown. Ye [20] designed a global adaptive control of a class of nonlinear systems when the signs of certain system parameters are unknown for learning control system.

In this paper we will use the non-identifier-based direct adaptive control technique [5] [7] to design adaptive controllers for a class of ASPR or ASNR MIMO LTI systems, which actually are minimum-phase, with relative degree m and unknown high-frequency gain, to track/reject multi-periodic reference/disturbance signals. The Lyapunov stability analysis is applied.

The adaptive MIMO multi-periodic repetitive control system is shown in Figure 1. The R , D , Y , U , E are reference, disturbance, output, control input and error respectively. The plant Σ_G is finite-dimensional, linear time-invariant, and described by

$$\begin{aligned} \dot{x}(t) &= Ax(t) + B(u(t) + d(t)) \\ y(t) &= Cx(t), x(0) = x_0 \end{aligned} \quad (1)$$

where $x(t) \in R^n, u(t) \in R^m, y(t) \in R^m$ and the dimensions of constant matrices A, B, C are $n \times n, n \times m, m \times n$ respectively. Both reference $r(t)$ and disturbance $d(t)$ are multi-periodic with components of period $\tau_i, i = 1, \dots, p$. These periods are assumed known. The multi-periodic repetitive controller is

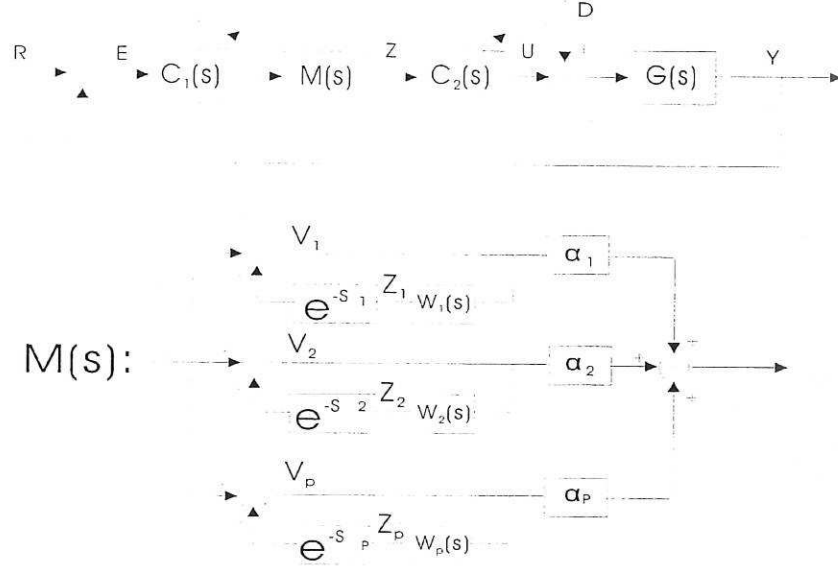


Figure 1: Adaptive MIMO multi-periodic repetitive control system

$M(s) = \sum_{i=1}^p \frac{\alpha_i I}{1 - W_i(s)e^{-s\tau_i}}$, we select $\sum_{i=1}^p \alpha_i = 1$ without loss of generality. $W_i(s)$ is a low-pass filter. $C_1(s), C_2(s)$ are both feed forward matrix gains given in the following sections designed to guarantee the Lyapunov stability of the whole system including the plant.

The paper is organized as follows. In section 2, we introduce a simple high constant feed forward gain, which realizes the stability of the MRC system for an ASPR plant. In section 3, we adopt an adaptive feed forward gain, which alleviate the assumption made in section 2. In section 4, the general problem is solved for the ASPR or ASNR plant and here we introduce a Nussbaum-type feed forward gain. Simulation results are presented in section 5. Section 6 discusses the extension of the Liapunov analysis to the ASPR or ASNR plant under certain non-linear perturbations. Section 7 gives an exponential stabilization control scheme via exponential weighting factor. Section 8 gives an adaptive proportional plus MRC scheme. For every control schemes, the Lyapunov stability proof is given. Finally in section 9, conclusions are given.

2 Stabilization by high constant feed forward gain

Assume the MIMO, LTI plant Σ_G is ASPR, that is there exists an unknown constant matrix $\lambda^* \in \mathbb{R}^{m \times m}$ such that the closed-loop system ($A -$

$B\lambda^*C, B, C)$ satisfies the strict-positive-realness conditions, that is

$$\begin{aligned} P(A - B\lambda^*C) + (A - B\lambda^*C)^T P &< -Q \\ PB &= C^T \end{aligned} \quad (2)$$

Theorem 1 Consider the ASPR system Σ_G described by (1). Suppose that both reference $r(t)$ and disturbance $d(t)$ are identically zero. The feedforward gain $C_1(s) = k\Gamma$ and $C_2(s) = \Gamma$, where k is a positive constant and is selected to be larger than $\gamma := \|\lambda^{*T} + \lambda^*\|$. $\Gamma \in R^{m \times m}$ is a matrix such that $\Gamma + \Gamma^T > 0$ and is selected to be $I_{m \times m}$ without loss of generality. Then the multi-periodic repetitive system in Figure 1 is globally asymptotically stable in the sense that the state $x(\cdot) \in L_\infty^n[0, \infty)$, control signal $v_i(\cdot) \in L_2^m[0, \infty)$, and output $y(\cdot) \in L_2^m[0, \infty)$.

Proof: Assume

$$\begin{aligned} \dot{x}_{W_i}(t) &= A_{W_i}x_{W_i}(t) + B_{W_i}v_i(t) \\ z_i(t) &= C_{W_i}x_{W_i}(t) \end{aligned} \quad (3)$$

is a minimal realization of strictly bounded real $W_i(s)$. Then according to Corollary 1 and the inequality (10) in [12], we have $(x_{W_i}^T P_{W_i} x_{W_i})' \leq \mu^2 v_i^T v_i - z_i^T z_i$, where $0 < \mu < 1$ is a constant. Introduce a positive definitive Lyapunov function V of the form

$$V = x^T P x + \frac{1}{k} \sum_{i=1}^p \alpha_i \int_{t-\tau_i}^t \|z_i(\theta)\|^2 d\theta + \frac{1}{k} \sum_{i=1}^p \alpha_i x_{W_i}^T P_{W_i} x_{W_i} \quad (4)$$

The system (1) can be rewritten as follows:

$$\begin{aligned} \dot{x}(t) &= (A - B\lambda^*C)x(t) + B \sum_{i=1}^p \alpha_i v_i + B\lambda^*y(t) \\ y(t) &= Cx(t) \end{aligned} \quad (5)$$

By differentiating V along (5) and using (2) we have

$$\begin{aligned} &(x^T P x)' \\ &< -x^T Q x + \sum_{i=1}^p \alpha_i v_i^T y + \sum_{i=1}^p \alpha_i y^T v_i + \gamma y^T y \\ &+ \left(\frac{1}{k} \sum_{i=1}^p \alpha_i \int_{t-\tau_i}^t \|z_i(\theta)\|^2 d\theta \right)' \\ &= \frac{1}{k} \sum_{i=1}^p \alpha_i [z_i^T z_i - z_i^T(t - \tau_i) z_i(t - \tau_i)] \\ &= \frac{1}{k} \sum_{i=1}^p \alpha_i [z_i^T z_i - (v_i^T + ky^T)(v_i + ky)] \\ &= \frac{1}{k} \sum_{i=1}^p \alpha_i z_i^T z_i - \frac{1}{k} \sum_{i=1}^p \alpha_i v_i^T v_i - \sum_{i=1}^p \alpha_i v_i^T y - \sum_{i=1}^p \alpha_i y^T v_i - ky^T y \\ &+ \left(\frac{1}{k} \sum_{i=1}^p \alpha_i x_{W_i}^T P_{W_i} x_{W_i} \right)' \leq \frac{1}{k} \sum_{i=1}^p \alpha_i \mu^2 v_i^T v_i - \frac{1}{k} \sum_{i=1}^p \alpha_i z_i^T z_i \\ &\frac{dV}{dt} < -x^T Q x - (k - \gamma) y^T y - \frac{1}{k} \sum_{i=1}^p \alpha_i (1 - \mu^2) v_i^T v_i < 0 \end{aligned} \quad (6)$$

Integrating (6) and using (4) and the positivity of V yield

$$V(0) > V(t) + \int_0^t x^T Q x dt + \int_0^t (k - \gamma) \|y\|^2 dt + \int_0^t (1 - \mu^2) \frac{1}{k} \sum_{i=1}^p \alpha_i v_i^T v_i dt \quad (7)$$

from which $x(\cdot) \in L_\infty^n[0, \infty)$, $v_i(\cdot) \in L_2^m[0, \infty)$ and $y(\cdot) \in L_2^m[0, \infty)$, which proves the result. \square

Here we assume γ is known and it is a restrictive assumption which will be excluded in the following section.

3 Stabilization by adaptive feed forward gain

Theorem 2 Consider the ASPR system Σ_G described by (1). Suppose that both reference $r(t)$ and disturbance $d(t)$ are identically zero. The feedforward gain $C_1(s) = k(s)\Gamma$ and $C_2(s) = \Gamma$, where $k(t)$ is an adaptive scale gain with adaptive law $\dot{k}(t) = e^T(t)e(t)$, $k(0) > 0$, $\Gamma = I_{m \times m}$. Then the adaptive multi-periodic non-linear repetitive system in Figure 1 is globally asymptotically stable in the sense that $x(\cdot) \in L_\infty^n[0, \infty)$, $v_i(\cdot) \in L_2^m[0, \infty)$, $y(\cdot) \in L_2^m[0, \infty)$, $k(\cdot) \in L_\infty[0, \infty)$ and $\lim_{t \rightarrow \infty} k(t) = k_\infty < \infty$.

Proof: The proof is an extension of that in section 2. By differentiating (4) we have

$$\begin{aligned} \frac{dV}{dt} &< -x^T Q x - (k - \gamma) y^T y - \frac{1}{k^2} \frac{dk}{dt} \sum_{i=1}^p \alpha_i \int_{t-\tau_i}^t \|z_i(\theta)\|^2 d\theta \\ &\quad - (1 - \mu^2) \frac{1}{k} \sum_{i=1}^p \alpha_i v_i^T v_i - \frac{1}{k^2} \frac{dk}{dt} \sum_{i=1}^p \alpha_i x_{W_i}^T P_{W_i} x_{W_i} \end{aligned} \quad (8)$$

Integrating (8) and using the adapting law $\dot{k}(t) = e(t)^T e(t) = y(t)^T y(t)$ yields

$$\begin{aligned} V(t') - V(0) &< -\int_0^{t'} x^T Q x dt - \int_{k(0)}^{k(t')} (\tau - \gamma) d\tau - \int_0^{t'} \frac{1}{k^2} \frac{dk}{dt} \sum_{i=1}^p \alpha_i \int_{t-\tau_i}^t \|z_i(\theta)\|^2 d\theta dt \\ &\quad - \int_0^{t'} (1 - \mu^2) \frac{1}{k} \sum_{i=1}^p \alpha_i v_i^T v_i dt - \int_0^{t'} \frac{1}{k^2} \frac{dk}{dt} \sum_{i=1}^p \alpha_i x_{W_i}^T P_{W_i} x_{W_i} dt \\ &= -\int_0^{t'} x^T Q x dt - \left[\frac{k(t')^2}{2} - \gamma k(t') - \frac{k(0)^2}{2} + \gamma k(0) \right] \\ &\quad - \int_0^{t'} \frac{1}{k^2} \frac{dk}{dt} \sum_{i=1}^p \alpha_i \int_{t-\tau_i}^t \|z_i(\theta)\|^2 d\theta dt \\ &\quad - \int_0^{t'} (1 - \mu^2) \frac{1}{k} \sum_{i=1}^p \alpha_i v_i^T v_i dt - \int_0^{t'} \frac{1}{k^2} \frac{dk}{dt} \sum_{i=1}^p \alpha_i x_{W_i}^T P_{W_i} x_{W_i} dt \end{aligned} \quad (9)$$

We will establish $k(t) \in L_\infty[0, t')$ by contradiction. Suppose $k(t) \notin L_\infty[0, t')$, the term $-\left[\frac{k(t')^2}{2} - \gamma k(t') - \frac{k(0)^2}{2} + \gamma k(0)\right]$ will be negative infinity because $f(x) := x^2$ becomes infinite of a higher order than $g(x) := x$ as x increases to infinity. The other items of the right part of (9) are definitely negative due to $\frac{dk(t)}{dt} \geq 0$ and $0 < \mu < 1$, hence contradicting the non-negativity of the left hand side of (9). Therefore, we have $k(t) \in L_\infty[0, t')$.

When $t' = \infty$, we have $k(t) \in L_\infty[0, \infty)$. Due to the monotonic increase of $k(t)$, we have $\lim_{t \rightarrow \infty} k(t) = k_\infty < \infty$. Also we have $x(\cdot) \in L_\infty^n[0, \infty)$, $v_i(\cdot) \in L_2^m[0, \infty)$ and $y(\cdot) \in L_2^m[0, \infty)$ as before, which proves the result. \square

4 Stabilization via Nussbaum-type switching

Assume the MIMO, LTI plant Σ_G is ASPR or ASNR, that is there exists an unknown positive definite matrix λ^* such that the closed-loop system $(A - \sigma B\lambda^*C, \sigma B, C)$ satisfies the strict-positive-realness conditions, that is

$$\begin{aligned} P(A - \sigma B\lambda^*C) + (A - \sigma B\lambda^*C)^T P &< -Q \\ \sigma PB &= C^T \end{aligned} \quad (10)$$

where $\sigma := \text{sign}(CB)$ is assumed unknown.

Now we introduce a Nussbaum-type adaptive controller as follows:

$$u(t) = N(\lambda(t))\Gamma z(t) \quad (11)$$

$\Gamma = I_{m \times m}$, $N(\cdot) : \mathbb{R} \rightarrow \mathbb{R}$ is any continuous function of Nussbaum type (Nussbaum, 1983 [11]), that is, $N(\cdot)$ has the properties

$$\sup_{k > k_0} \frac{1}{k - k_0} \int_{k_0}^k N(\tau) d\tau = +\infty \text{ and } \inf_{k > k_0} \frac{1}{k - k_0} \int_{k_0}^k N(\tau) d\tau = -\infty.$$

For example, $N(\cdot) : \tau \rightarrow \tau^2 \cos \tau$ suffices.

Theorem 3 Consider the ASPR or ASNR system Σ_G described by (1). The feedforward gain $C_1(s) = k(s)\Gamma$ and $C_2(s) = N(s)\Gamma$, where $k(t)$ and $\lambda(t)$ are both adaptive scalar gains with adaptive law $\dot{k}(t) = e(t)^T e(t)$, $k(0) > 0$ and $\dot{\lambda}(t) = e(t)^T z(t)$, $\lambda(0) \geq 0$. Then the adaptive multi-periodic non-linear repetitive system in Figure 1 is globally asymptotically stable in the sense that $x(\cdot) \in L_\infty^n[0, \infty)$, $y(\cdot) \in L_2^m[0, \infty)$, $\lambda(\cdot) \in L_\infty[0, \infty)$, $k(\cdot) \in L_\infty[0, \infty)$ and $\lim_{t \rightarrow \infty} k(t) = k_\infty < \infty$.

Proof: We set the low-pass filter $W_i(s)$ to be 1 for sake of simplicity. The system can be rewritten as follows:

$$\begin{aligned} \dot{x}(t) &= (A - \sigma B\lambda^*C)x(t) + B(N(\lambda)z(t) + d(t)) + \sigma B\lambda^*y(t) \\ y(t) &= Cx(t), \quad z(t) = \sum_{i=1}^p \alpha_i z_i(t) \end{aligned} \quad (12)$$

Also due to the minimum phase property of Σ_G , there exists an invariant set, made up of periodic trajectories vanishing with $r(t)$ and $d(t)$, which is contained in the ker of the output. That is, if the control input u_∞ is carefully selected under some state x_∞ , the output of the system output y_∞ will be r . So we have

$$\begin{aligned} \dot{x}_\infty(t) &= Ax_\infty(t) + Bu_\infty(t) \\ r(t) &= Cx_\infty(t) \end{aligned} \quad (13)$$

Then we define $e(t) := r(t) - y(t)$, $e_x(t) := x_\infty(t) - x(t)$, we have

$$\begin{aligned} \dot{e}_x(t) &= (A - \sigma B\lambda^*C)e_x(t) + \sigma B\lambda^*e(t) - BN(\lambda)z(t) - Bd(t) + Bu_\infty(t) \\ e(t) &= Ce_x(t) \end{aligned} \quad (14)$$

Similar to $d(t) = \sum_{i=1}^p \alpha_i d_i(t)$, we have $u_\infty(t) = \sum_{i=1}^p \alpha_i u_{\infty i}(t)$. Introducing a positive definite Liapunov function V :

$$V = e_x^T P e_x + \frac{1}{k} \sum_{i=1}^p \alpha_i \int_{t-\tau_i}^t \|z_i(\theta) - \sigma u_{\infty i}(\theta) + \sigma d_i(\theta)\|^2 d\theta \quad (15)$$

By differentiating V , we have

$$\begin{aligned} & (e_x^T P e_x)' \\ & < -e_x^T Q e_x + \gamma e^T e - 2\sigma N(\lambda) z^T e - 2\sigma d^T e + 2\sigma u_\infty^T e \\ & \left(\frac{1}{k} \sum_{i=1}^p \alpha_i \int_{t-\tau_i}^t \|z_i(\theta) - \sigma u_{\infty i}(\theta) + \sigma d_i(\theta)\|^2 d\theta \right)' \\ & = z^T e + e^T z - \sigma u_\infty^T e - \sigma e^T u_\infty + \sigma d^T e + \sigma e^T d - k e^T e \\ & - \frac{1}{k^2} \frac{dk}{dt} \sum_{i=1}^p \alpha_i \int_{t-\tau_i}^t \|z_i(\theta) - \sigma u_{\infty i}(\theta) + \sigma d_i(\theta)\|^2 d\theta \end{aligned} \quad (16)$$

$$\begin{aligned} \frac{dV}{dt} & < -e_x^T Q e_x - (2\sigma N(\lambda) - 2) z^T e - (k - \gamma) e^T e \\ & - \frac{1}{k^2} \frac{dk}{dt} \sum_{i=1}^p \alpha_i \int_{t-\tau_i}^t \|z_i(\theta) - \sigma u_{\infty i}(\theta) + \sigma d_i(\theta)\|^2 d\theta \end{aligned}$$

Integrating (16) and using law $\dot{k}(t) = e(t)^T e(t)$, $\dot{\lambda}(t) = e(t)^T z(t)$ yield

$$\begin{aligned} & V(t') - V(0) \\ & < - \int_0^{t'} e_x^T Q e_x dt - \int_{k(0)}^{k(t')} (\tau - \gamma) d\tau - \int_{\lambda(0)}^{\lambda(t')} (2\sigma N(\tau) - 2) d\tau \\ & - \int_0^{t'} -\frac{1}{k^2} \frac{dk}{dt} \sum_{i=1}^p \alpha_i \int_{t-\tau_i}^t \|z_i(\theta) - \sigma u_{\infty i}(\theta) + \sigma d_i(\theta)\|^2 d\theta dt \\ & = - \int_0^{t'} e_x^T Q e_x dt - \left[\frac{k(t')^2}{2} - \gamma k(t') - \frac{k(0)^2}{2} + \gamma k(0) \right] - \int_{\lambda(0)}^{\lambda(t')} (2\sigma N(\tau) - 2) d\tau \\ & - \int_0^{t'} -\frac{1}{k^2} \frac{dk}{dt} \sum_{i=1}^p \alpha_i \int_{t-\tau_i}^t \|z_i(\theta) - \sigma u_{\infty i}(\theta) + \sigma d_i(\theta)\|^2 d\theta dt \end{aligned} \quad (17)$$

We will establish $\lambda(t) \in L_\infty[0, t']$, $k(t) \in L_\infty[0, t']$ by contradiction. Suppose $\lambda(t) \notin L_\infty[0, t']$, $k(t) \notin L_\infty[0, t']$, the term $-\left[\frac{k(t')^2}{2} - \gamma k(t') - \frac{k(0)^2}{2} + \gamma k(0)\right]$ will be negative infinity as in section 3. The term $-\int_{\lambda(0)}^{\lambda(t')} (2\sigma N(\tau) - 2) d\tau$ will take arbitrary large negative or positive value when $\lambda(t') = \infty$ according to Theorem A.1 in Appendix. For example, if we select $N(\lambda) = \lambda^2 \cos \lambda$ and $\lambda(0) = 0$ without loss of generality, then we have $-\int_0^{\lambda(t')} (2\sigma N(\tau) - 2) d\tau = -2\sigma[\lambda(t')^2 \sin \lambda(t') + 2\lambda(t') \cos \lambda(t') - 2 \sin \lambda(t')] + 2\lambda(t')$ and it will take arbitrary large negative or positive value when $\lambda(t') = \infty$. So when it takes arbitrary large negative, the right hand side of (17) will be negative, hence contradicting the non-negativity of the left hand side of (17). Therefore, we have $\lambda(t) \in L_\infty[0, t']$, $k(t) \in L_\infty[0, t']$.

When $t' = \infty$, we have $\lambda(t) \in L_\infty[0, \infty)$, $k(t) \in L_\infty[0, \infty)$. As in section 3, we have $\lim_{t \rightarrow \infty} k(t) = k_\infty < \infty$, $x(t) \in L_\infty^n[0, \infty)$ and $y(t) \in L_2^n[0, \infty)$, which proves the result. \square

It should be pointed out that we can't prove that $\lim_{t \rightarrow \infty} \lambda(t) = \lambda_\infty < \infty$ although the simulation seems to show λ converges. Also $W_i(s)$ can only be set as 1 for above analysis because otherwise $\tilde{z}_i(t) = z_i(t) - \sigma u_{\infty i}(t) + \sigma d_i(t)$

doesn't satisfy the same evolution equation as $z_i(t)$. It's easy to understand because zero-tracking/full-rejection will be lost when $W_i(s)$ isn't equal to 1.

5 Simulation

For sake of simplicity, a SISO system is examined to illustrate the control system performance. The ASPR or ASNR plant under control is described as (1) where

$$A = \begin{pmatrix} -1 & 1 \\ 2 & 0 \end{pmatrix}, B = \begin{pmatrix} \pm 1 \\ 0 \end{pmatrix}, C = \begin{pmatrix} 1 & 0.5 \end{pmatrix}, x(0) = \begin{pmatrix} 1 \\ -1 \end{pmatrix}$$

or $G(s) = \frac{\pm(s+1)}{(s-1)(s+2)}$. The reference is $r = r_1 + r_2$, where $r_1 = \sin \omega_1 t + 1.5 \sin 5\omega_1 t$, $r_2 = \sin \omega_2 t$ and $\omega_1 = 0.2 \times 2\pi \text{rad/sec}$, $\omega_2 = 0.3 \times 2\pi \text{rad/sec}$. The disturbance is a square wave at a period of $7Hz$ and with peak value ± 2 . A square wave is chosen to indicate the scheme can cope with signals with infinite frequency content. The weightings are chosen to be 0.4, 0.4, 0.2 (for the disturbance rejection repetitive sub-controller). We select $k(0) = 1$, $\lambda(0) = 0$, $W_i(s) = 1$ and $N(\lambda) = \lambda^2 \cos(\lambda)$. The simulation result is given in Figure 2 and 3. Figure 2 is for $G(s) = \frac{(s+1)}{(s-1)(s+2)}$ and Figure 3 is for $G(s) = \frac{-(s+1)}{(s-1)(s+2)}$. The simulation result shows that the control scheme is capable for the ASPR or ASNR plant to asymptotically track/reject a multi-periodic reference/disturbance signal.

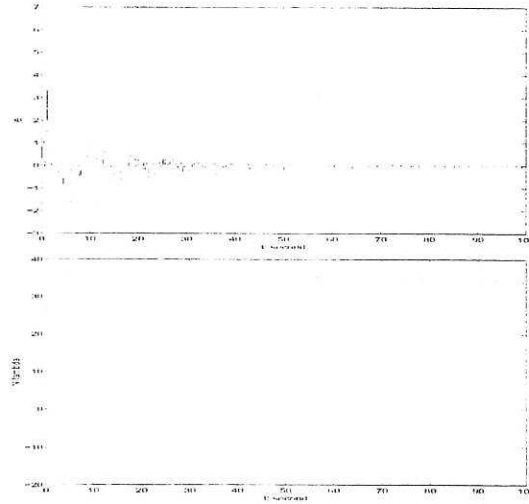


Figure 2: Error $e(t)$ and Nussbaum-type gain $N(\lambda)$ for ASPR plant

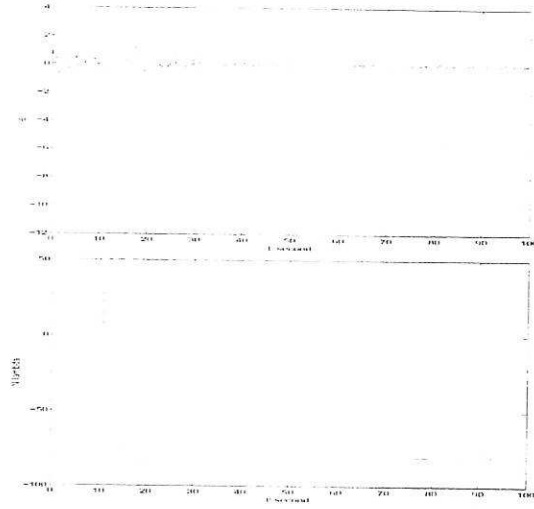


Figure 3: Error $e(t)$ and Nussbaum-type gain $N(\lambda)$ for ASNR plant

6 Effect of non-linear perturbation

The above Liapunov stability can be extended to the system under certain non-linear perturbations. The plant is described by

$$\begin{aligned} \dot{x}(t) &= Ax(t) + B(u(t) + d(t)) + g_1(t, x(t)) + g_2(t, y(t)) + d'(t) \\ y(t) &= Cx(t) \end{aligned} \quad (18)$$

The nominal system is ASPR or ASNR as in section 4 and the non-linear perturbations satisfy

$$\begin{aligned} g_1(\cdot, \cdot) : R \times R^n &\rightarrow R^n, \|g_1(t, x)\| \leq \hat{g}_1 \|x\| \\ g_2(\cdot, \cdot) : R \times R^m &\rightarrow R^n, \|g_2(t, y)\| \leq \hat{g}_2 \|y\| \\ d'(\cdot) &\in L_2^n[0, \infty) \end{aligned} \quad (19)$$

Here $g_1(\cdot, \cdot), g_2(\cdot, \cdot), d'(\cdot)$ are assumed to be Carathedory function, which, for some unknown $\hat{g}_1, \hat{g}_2 \geq 0$, are linearly bounded for almost all $t \in R$ and for all $x \in R^n, u, y \in R^m$.

Theorem 4 Consider the system Σ_G described by (18) and (19). Suppose that both reference $r(t)$ and disturbance $d(t)$ are identically zero. Then the adaptive multi-periodic non-linear repetitive system in Figure 1 where the feedforward gain $C_1(s) = k(s)\Gamma$ and $C_2(s) = N(s)\Gamma$ with $\dot{k}(t) = e(t)^T e(t), k(0) > 0, \dot{\lambda}(t) = e(t)^T z(t), \lambda(0) \geq 0$ is globally asymptotically stable in the sense that $x(\cdot) \in L_\infty^n[0, \infty), y(\cdot) \in L_2^m[0, \infty), \lambda(\cdot) \in L_\infty[0, \infty), k(\cdot) \in L_\infty[0, \infty)$ and $\lim_{t \rightarrow \infty} k(t) = k_\infty < \infty$.

Proof: The proof is similar to that in section 4 and here we only outline below. Introducing a positive definite Liapunov function V :

$$V = x^T P x + \frac{1}{k} \sum_{i=1}^p \alpha_i \int_{t-\tau_i}^t \|z_i(\theta)\|^2 d\theta \quad (20)$$

Differentiating V along (18) and using (10) yield

$$\begin{aligned} & (x^T P x)' \\ & < -x^T Q x + 2\sigma N(\lambda) z^T y + \gamma y^T y + g_1^T P x + x^T P g_1 + g_2^T P x + x^T P g_2 + \\ & d'^T P y + y^T P d' \\ & \leq -x^T Q x + 2\sigma N(\lambda) z^T y + \gamma y^T y + 2\hat{g}_1 \|P\| \|x\|^2 + 2\hat{g}_2 \|P\| \|x\| \|y\| + 2\|P\| \|d'\| \|x\| \\ & \leq -x^T Q x + 2\sigma N(\lambda) z^T y + \gamma y^T y + 2\hat{g}_1 \|P\| \|x\|^2 + \hat{g}_2 \|P\| a_1^{-2} \|x\|^2 + \hat{g}_2 \|P\| a_1^2 \|y\|^2 + \\ & \|P\| a_2^{-2} \|x\|^2 + \|P\| a_2^2 \|d'\|^2 \\ & < -x^T (Q - 2\hat{g}_1 \|P\| I - \hat{g}_2 \|P\| a_1^{-2} I - \|P\| a_2^{-2} I) x + 2\sigma N(\lambda) z^T y + (\gamma + \\ & \hat{g}_2 \|P\| a_1^2) y^T y + \|P\| a_2^2 \|d'\|^2 \\ & \quad a_1, a_2 > 0 \\ & \frac{1}{k} \left(\sum_{i=1}^p \alpha_i \int_{t-\tau_i}^t \|z_i(\theta)\|^2 d\theta \right)' \\ & = -z^T y - y^T z - k y^T y - \frac{1}{k^2} \frac{dk}{dt} \sum_{i=1}^p \alpha_i \int_{t-\tau_i}^t \|z_i(\theta)\|^2 d\theta \end{aligned}$$

When the linear bounds $\hat{g}_1, \hat{g}_2 > 0$ are sufficiently small in terms of the system entries (A, B, C) and $a_1, a_2 > 0$ are chosen to be sufficiently large so that $\hat{Q} := Q - 2\hat{g}_1 \|P\| I - \hat{g}_2 \|P\| a_1^{-2} I - \|P\| a_2^{-2} I$ is also positive definite. Therefore, we have

$$\begin{aligned} \frac{dV}{dt} & < -x^T \hat{Q} x - (2\sigma N(\lambda) - 2) z^T (-y) - (k - \gamma - \hat{g}_2 \|P\| a_1^2) y^T y \\ & - \frac{1}{k^2} \frac{dk}{dt} \sum_{i=1}^p \alpha_i \int_{t-\tau_i}^t \|z_i(\theta)\|^2 d\theta + \|P\| a_2^2 \|d'\|^2 \end{aligned} \quad (21)$$

Integrating (21) yields

$$\begin{aligned} & V(t') - V(0) \\ & < - \int_0^{t'} x^T \hat{Q} x dt - \int_{k(0)}^{k(t')} (\tau - \gamma - \hat{g}_2 \|P\| a_1^2) d\tau - \int_{\lambda(0)}^{\lambda(t')} (2\sigma N(\tau) - 2) d\tau \\ & - \int_0^{t'} \frac{1}{k^2} \frac{dk}{dt} \sum_{i=1}^p \alpha_i \int_{t-\tau_i}^t \|z_i(\theta)\|^2 d\theta dt + \int_0^{t'} \|P\| a_2^2 \|d'\|^2 dt \end{aligned} \quad (22)$$

The item $\int_0^{t'} \|P\| a_2^2 \|d'\|^2 dt$ is bounded as $d'(\cdot) \in L_2[0, \infty)$. Therefore, it can be shown that $\lambda(\cdot) \in L_\infty[0, \infty)$, $k(\cdot) \in L_\infty[0, \infty)$ as before. Also we have $y(\cdot) \in L_2^m[0, \infty)$, $x(\cdot) \in L_\infty^n[0, \infty)$ and $\lim_{t \rightarrow \infty} k(t) = k_\infty < \infty$ as before, which proves the result. \square

7 Exponential stabilization via exponential weighting factor

It has been proved that asymptotical stability of MRC system can be guaranteed if the plant \sum_G is ASPR or ASNR. While when it strictly satisfies

a ASPR or ASNR condition, now we show that the system is exponentially stable when modifying the adaptive scheme. According to definition A.1 and A.3 in Appendix, each almost strictly positive real system is almost ϵ -strictly positive real for some sufficiently small but unknown $\epsilon^* > 0$, that is, $(A + \epsilon^* I, \sigma B, C)$ is Almost Strictly Positive Real. Our aim is to find $\epsilon^* > 0$ adaptively by using an exponential weighting factor tuned by $k(t)$. We introduce a function $\epsilon(k(t))$ (for example $\frac{0.1}{k(t)+1}$) with following properties: i) $\epsilon(k(t)) > 0$ for all $k(t) > 0$. ii) It is non-increasing for all $k(t) > 0$. iii) $\lim_{t \rightarrow \infty} \epsilon(k(t)) = \epsilon_\infty > 0$.

Theorem 5 Consider the system Σ_G described by (1). Suppose that both reference $r(t)$ and disturbance $d(t)$ are identically zero. Then the adaptive multi-periodic non-linear repetitive system in Figure 1 where the feedforward gain $C_1(s) = k(s)\Gamma$ and $C_2(s) = N(s)\Gamma$ with $\dot{k}(t) = e_\epsilon(t)^T e_\epsilon(t)$, $k(0) > 0$, $\lambda(t) = e_\epsilon(t)^T v_\epsilon(t)$, $\lambda(0) \geq 0$ by denoting $x_\epsilon(t) := e^{\epsilon(k(t))t} x(t)$ is globally exponentially stable in the sense that $x(\cdot) \in L_\infty^n[0, \infty)$, $y(\cdot) \in L_2^m[0, \infty)$, $\lambda(\cdot) \in L_\infty[0, \infty)$, $k(\cdot) \in L_\infty[0, \infty)$, $\lim_{t \rightarrow \infty} k(t) = k_\infty < \infty$, $\lim_{t \rightarrow \infty} \epsilon(k(t)) = \epsilon_\infty > 0$ and also $\|x(t)\| \leq M_1 e^{-\epsilon t}$ for all $t \geq 0$ and some $M_1 > 0, \epsilon > 0$.

Proof: With the notation $x_\epsilon(t) := e^{\epsilon(k(t))t} x(t)$, the plant can be written as

$$\begin{aligned} \dot{x}_\epsilon(t) &= [A + \epsilon^* I - \sigma B \lambda^* C] x_\epsilon(t) + \epsilon(k(t)) x_\epsilon(t) - \epsilon^* x_\epsilon(t) \\ &\quad + \frac{d\epsilon(k(t))}{dt} t x_\epsilon(t) + \sigma B \lambda^* C x_\epsilon(t) + N(\lambda) B v_\epsilon(t) \\ y_\epsilon(t) &= C x_\epsilon(t), \quad v_\epsilon(t) = \sum_{i=1}^p \alpha_i v_{i\epsilon}(t) \end{aligned} \quad (23)$$

Also we have

$$\begin{aligned} & z_{i\epsilon}^T(t - \tau_i) z_{i\epsilon}(t - \tau_i) \\ &= e^{2\epsilon(k(t-\tau_i))(t-\tau_i)} z_i^T(t - \tau_i) z_i(t - \tau_i) \\ &\geq e^{2\epsilon(k(t))(t-\tau_i)} z_i^T(t - \tau_i) z_i(t - \tau_i) \\ &= e^{2\epsilon(k(t))t} e^{-2\epsilon(k(t))\tau_i} (v_i(t) + k(t)y(t))^T (v_i(t) + k(t)y(t)) \\ &= e^{-2\epsilon(k(t))\tau_i} (v_{i\epsilon}(t) + k(t)y_\epsilon(t))^T (v_{i\epsilon}(t) + k(t)y_\epsilon(t)) \\ &\geq e^{-2\epsilon(k(0))\tau} (v_{i\epsilon}(t) + k(t)y_\epsilon(t))^T (v_{i\epsilon}(t) + k(t)y_\epsilon(t)) \\ &\quad \tau := \max(\tau_i) \end{aligned} \quad (24)$$

Introducing a positive definite Liapunov function V :

$$V = x_\epsilon^T P x_\epsilon + \frac{1}{k} \sum_{i=1}^p \alpha_i \int_{t-\tau_i}^t \|z_{i\epsilon}(\theta)\|^2 d\theta + \frac{1}{k} \sum_{i=1}^p \alpha_i x_{W_{i\epsilon}}^T P_{W_{i\epsilon}} x_{W_{i\epsilon}} \quad (25)$$

Differentiating V along (23) and using (24) yields

$$\begin{aligned} (x_\epsilon^T P x_\epsilon)' &< -x_\epsilon^T Q x_\epsilon - 2\epsilon^* x_\epsilon^T P x_\epsilon + 2\epsilon(k) x_\epsilon^T P x_\epsilon + 2 \frac{d\epsilon(k)}{dt} t x_\epsilon^T P x_\epsilon - 2\sigma N(\lambda) (-y_\epsilon)^T v_\epsilon + \gamma y_\epsilon^T y_\epsilon \\ &\quad \left(\frac{1}{k} \sum_{i=1}^p \alpha_i x_{W_{i\epsilon}}^T P_{W_{i\epsilon}} x_{W_{i\epsilon}} \right)' \leq \frac{1}{k} \sum_{i=1}^p \alpha_i \mu^2 v_{i\epsilon}^T v_{i\epsilon} - \frac{1}{k} \sum_{i=1}^p \alpha_i z_{i\epsilon}^T z_{i\epsilon} - \frac{1}{k^2} \frac{dk}{dt} \sum_{i=1}^p \alpha_i x_{W_{i\epsilon}}^T P_{W_{i\epsilon}} x_{W_{i\epsilon}} \end{aligned}$$

$$\begin{aligned}
& \left(\frac{1}{k} \sum_{i=1}^p \alpha_i \int_{t-\tau_i}^t \|z_{i\epsilon}(\theta)\|^2 d\theta \right)' \\
&= \frac{1}{k} \sum_{i=1}^p \alpha_i [z_{i\epsilon}^T z_{i\epsilon} - z_{i\epsilon}^T(t - \tau_i) z_{i\epsilon}(t - \tau_i)] - \frac{1}{k^2} \frac{dk}{dt} \sum_{i=1}^p \alpha_i \int_{t-\tau_i}^t \|z_{i\epsilon}(\theta)\|^2 d\theta \\
&\leq \frac{1}{k} \sum_{i=1}^p \alpha_i [z_{i\epsilon}^T z_{i\epsilon} - e^{-2\epsilon(k(0))\tau} (v_{i\epsilon} + ky_{i\epsilon})^T (v_{i\epsilon} + ky_{i\epsilon})] \\
&\quad - \frac{1}{k^2} \frac{dk}{dt} \sum_{i=1}^p \alpha_i \int_{t-\tau_i}^t \|z_{i\epsilon}(\theta)\|^2 d\theta \\
&= \frac{1}{k} \sum_{i=1}^p \alpha_i z_{i\epsilon}^T z_{i\epsilon} - \frac{1}{k} e^{-2\epsilon(k(0))\tau} \sum_{i=1}^p \alpha_i v_{i\epsilon}^T v_{i\epsilon} - 2e^{-2\epsilon(k(0))\tau} y_{i\epsilon}^T z_{i\epsilon} \\
&\quad - k e^{-2\epsilon(k(0))\tau} y_{i\epsilon}^T y_{i\epsilon} - \frac{1}{k^2} \frac{dk}{dt} \sum_{i=1}^p \alpha_i \int_{t-\tau_i}^t \|z_{i\epsilon}(\theta)\|^2 d\theta
\end{aligned} \tag{26}$$

Therefore, we have

$$\begin{aligned}
\frac{dV}{dt} &< -x_{i\epsilon}^T Q x_{i\epsilon} - 2\epsilon^* x_{i\epsilon}^T P x_{i\epsilon} + 2\epsilon(k) x_{i\epsilon}^T P x_{i\epsilon} + 2 \frac{d\epsilon(k)}{dt} t x_{i\epsilon}^T P x_{i\epsilon} \\
&\quad + (2e^{-2\epsilon(k(0))\tau} - 2\sigma N(\lambda)) (-y_{i\epsilon})^T v_{i\epsilon} + (\gamma - k e^{-2\epsilon(k(0))\tau}) y_{i\epsilon}^T y_{i\epsilon} \\
&\quad - \frac{1}{k} (e^{-2\epsilon(k(0))\tau} - \mu^2) \sum_{i=1}^p \alpha_i v_{i\epsilon}^T v_{i\epsilon} \\
&\quad - \frac{1}{k^2} \frac{dk}{dt} \sum_{i=1}^p \alpha_i \int_{t-\tau_i}^t \|z_{i\epsilon}(\theta)\|^2 d\theta - \frac{1}{k^2} \frac{dk}{dt} \sum_{i=1}^p \alpha_i x_{i\epsilon}^T P_{W_{i\epsilon}} P_{W_{i\epsilon}} x_{W_{i\epsilon}}
\end{aligned} \tag{27}$$

Integrating (27) and using the adaptive law yields

$$\begin{aligned}
V(t') - V(0) &< - \int_0^{t'} x_{i\epsilon}^T Q x_{i\epsilon} dt - 2 \int_0^{t'} (\epsilon^* - \epsilon(k)) x_{i\epsilon}^T P x_{i\epsilon} dt + 2 \int_0^{t'} \frac{d\epsilon(k)}{dt} t x_{i\epsilon}^T P x_{i\epsilon} dt \\
&\quad + \int_{\lambda(0)}^{\lambda(t')} (2e^{-2\epsilon(k(0))\tau} - 2\sigma N(s)) ds + \int_{k(0)}^{k(t')} (\gamma - s e^{-2\epsilon(k(0))\tau}) ds \\
&\quad - \int_0^{t'} \frac{1}{k^2} \frac{dk}{dt} \sum_{i=1}^p \alpha_i \int_{t-\tau_i}^t \|z_{i\epsilon}(\theta)\|^2 d\theta dt + \int_0^{t'} \frac{1}{k} \sum_{i=1}^p \alpha_i (\mu^2 - e^{-2\epsilon(k(0))\tau}) z_{i\epsilon}^T z_{i\epsilon} dt \\
&\quad - \int_0^{t'} \frac{1}{k^2} \frac{dk}{dt} \sum_{i=1}^p \alpha_i \int_{t-\tau_i}^t x_{W_{i\epsilon}}^T P_{W_{i\epsilon}} P_{W_{i\epsilon}} x_{W_{i\epsilon}} d\theta dt
\end{aligned} \tag{28}$$

We will establish $\lambda(\cdot) \in L_\infty[0, \infty)$ $k(\cdot) \in L_\infty[0, \infty)$ by contradiction. Suppose $\lambda(\cdot) \notin L_\infty[0, \infty)$ $k(\cdot) \notin L_\infty[0, \infty)$. Assume $\epsilon(k(0)) > \epsilon^*$ $(-2 \int_0^{t'} (\epsilon^* - \epsilon(k)) x_{i\epsilon}^T P x_{i\epsilon} dt)$ is definitely negative when $\epsilon(k(0)) \leq \epsilon^*$, $-2 \int_0^{t'} (\epsilon^* - \epsilon(k)) x_{i\epsilon}^T P x_{i\epsilon} dt = -2 \int_0^{t_1} (\epsilon^* - \epsilon(k)) x_{i\epsilon}^T P x_{i\epsilon} dt - 2 \int_{t_1}^{t'} (\epsilon^* - \epsilon(k)) x_{i\epsilon}^T P x_{i\epsilon} dt$, $\epsilon(k(t_1)) = \epsilon^*$. According to Theorem A.2 in Appendix and without loss of generality, we can assume $x_{i\epsilon} = (y_{i\epsilon}^T, \eta_{i\epsilon}^T)^T$, so then $P = \begin{pmatrix} (\sigma C B)^{-1} & 0 \\ 0 & P_4 \end{pmatrix}$. Due to $y_{i\epsilon}(\cdot) \in L_\infty[0, t_1)$ and A_4 is asymptotically stable, we have $\eta_{i\epsilon}(\cdot) \in L_\infty[0, t_1)$, then $-2 \int_0^{t_1} (\epsilon^* - \epsilon(k)) x_{i\epsilon}^T P x_{i\epsilon} dt$ is a positive finite. So $-2 \int_0^{t'} (\epsilon^* - \epsilon(k)) x_{i\epsilon}^T P x_{i\epsilon} dt$ is negative infinity. $+\int_{k(0)}^{k(t')} (\gamma - s e^{-2\epsilon(k(0))\tau}) ds$ is negative infinity as before. $+\int_{\lambda(0)}^{\lambda(t')} (2e^{-2\epsilon(k(0))\tau} - 2\sigma N(s)) ds$ is arbitrarily negative or positive infinity as before. When we select $k(0)$ so that $|e^{-\epsilon(k(0))\tau}| < \mu$, $+\int_0^{t'} \frac{1}{k} \sum_{i=1}^p \alpha_i (\mu^2 - e^{-2\epsilon(k(0))\tau}) z_{i\epsilon}^T z_{i\epsilon} dt$ is negative. The other items are definitely negative due to $\frac{dk}{dt} > 0$ and $\frac{d\epsilon}{dt} < 0$. So when $+\int_{\lambda(0)}^{\lambda(t')} (2e^{-2\epsilon(k(0))\tau} - 2\sigma N(s)) ds$ takes arbitrarily negative, the right hand side of (28) will be negative, hence contradicting the non-negativity of the left hand side. Then from $\int_0^{+\infty} x^T Q x dt \leq \int_0^{+\infty} x_{i\epsilon}^T Q x_{i\epsilon} dt \leq +\infty$, we have $x(\cdot) \in L_\infty^n[0, \infty)$. Similar as before, we have

$y(\cdot) \in L_2^m[0, \infty)$, $\lambda(\cdot) \in L_\infty[0, \infty)$, $k(\cdot) \in L_\infty[0, \infty)$ and $\lim_{t \rightarrow \infty} k(t) = k_\infty < \infty$. Then we have $\lim_{t \rightarrow \infty} \epsilon(k(t)) = \epsilon_\infty > 0$. As $x_\epsilon(t)$ is uniformly bounded such that $\|x_\epsilon(t)\| \leq M_1$, we have $\|x(t)\| \leq M_1 e^{-\epsilon t}$ for some $M_1 > 0, \epsilon > 0$, which indicates exponential stability of the state. \square

However, perfect zero-tracking/full-rejecting for periodic reference/disturbance signals will be lost if the low-pass filter is not selected to be 1. So the state can only exponentially decrease to a bound as $\|x(t)\| \leq M_1 e^{-\epsilon t} + M_2$ for all $t \geq 0$ and some $M_1 > 0, M_2 > 0, \epsilon > 0$. Now we need to revise the adaptive scheme of $k(t)$ as

$$\dot{k}(t) = \begin{cases} \|e(t)\|(\|e(t)\| - \delta) & \text{if } \|e(t)\| \geq \delta \\ 0 & \text{if } \|e(t)\| < \delta \end{cases}$$

to prevent the divergence of adaptive gain $k(t)$.

8 Adaptive Proportional plus MRC system

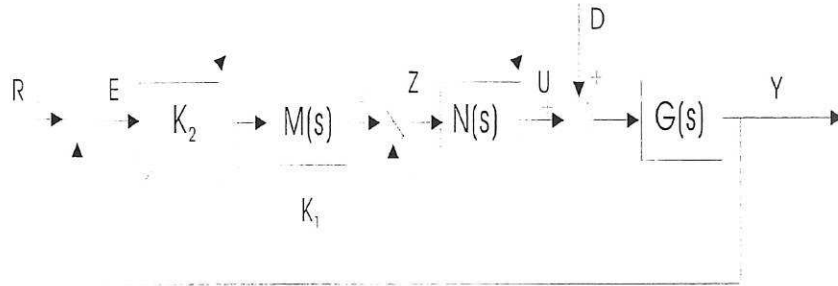


Figure 4: Adaptive MIMO Proportional plus MRC system

Theorem 6 Consider the ASPR or ASNR system Σ_G described by (1). Suppose that both reference $r(t)$ and disturbance $d(t)$ are identically zero. Then the adaptive multi-periodic non-linear repetitive system in Figure 4 with k_1 being a positive constant, $k_2(t) = e(t)^T e(t)$, $k_2(0) > 0$ and $\dot{\lambda}(t) = e(t)^T z(t) + k_1 k_2(t) e(t)^T e(t)$, $\lambda(0) \geq 0$ is globally asymptotically stable in the sense that $x(\cdot) \in L_\infty^n[0, \infty)$, $y(\cdot) \in L_2^m[0, \infty)$, $\lambda(\cdot) \in L_\infty[0, \infty)$, $k_2(\cdot) \in L_\infty[0, \infty)$ and $\lim_{t \rightarrow \infty} k_2(t) = k_{2\infty} < \infty$.

Proof: We set the low-pass filter $W_i(s)$ to be 1 for sake of simplicity. The system can be rewritten as follows:

$$\begin{aligned} \dot{x}(t) &= (A - \sigma B \lambda^* C) x(t) + B N(\lambda) z(t) - B N(\lambda) k_1 k_2(t) y(t) + \sigma B \lambda^* y(t) \\ y(t) &= C x(t), \quad z(t) = \sum_{i=1}^p \alpha_i z_i(t) \end{aligned} \quad (29)$$

Introducing a positive definite Liapunov function V :

$$V = x^T P x + \frac{1}{k_2} \sum_{i=1}^p \alpha_i \int_{t-\tau_i}^t \|z_i(\theta)\|^2 d\theta \quad (30)$$

By differentiating V we have

$$\begin{aligned} \frac{dV}{dt} &< -x^T Q x - (k_2 + 2k_1 k_2 - \gamma) y^T y - (2\sigma N(\lambda) - 2)(k_1 k_2 y^T y - z^T y) \\ &\quad - \frac{1}{k_2^2} \frac{dk_2}{dt} \sum_{i=1}^p \alpha_i \int_{t-\tau_i}^t \|z_i(\theta)\|^2 d\theta \end{aligned} \quad (31)$$

Integrating (31) yields

$$\begin{aligned} V(t') - V(0) &< - \int_0^{t'} x^T Q x dt - \int_{k_2(0)}^{k_2(t')} (\tau + 2k_1 \tau - \gamma) d\tau - \int_{\lambda(0)}^{\lambda(t')} (2\sigma N(\tau) - 2) d\tau \\ &\quad - \int_0^{t'} \frac{1}{k_2^2} \frac{dk_2}{dt} \sum_{i=1}^p \alpha_i \int_{t-\tau_i}^t \|z_i(\theta)\|^2 d\theta dt \end{aligned} \quad (32)$$

Similar to that in section 4, we can conclude $x(\cdot) \in L_\infty^n[0, \infty)$, $y(\cdot) \in L_2^m[0, \infty)$, $\lambda(\cdot) \in L_\infty[0, \infty)$, $k_2(\cdot) \in L_\infty[0, \infty)$ and $\lim_{t \rightarrow \infty} k_2(t) = k_{2\infty} < \infty$, which proves the result. \square

Also the simulation results show that a higher proportional gain k_1 is helpful for the performance.

9 Conclusion

A kind of adaptive MIMO multi-periodic repetitive control system is studied. An adaptive feed forward adaptive gain plus multi-periodic repetitive controller is applied to make the ASPR or ASNR plant output to asymptotically track/reject multi-periodic reference/disturbance signals. The stability is analysed in the sense of Liapunov stability. The adapting gains are proved to be bounded and the error decays asymptotically to zero. The similar Liapunov stability analysis is also extended to ASPR or ASNR plant under certain non-linear perturbations. It is also shown that exponential stability can be guaranteed by modifying the adaptive schemes. Finally, an proportional plus adaptive MRC system is proposed and its stability is proven in the sense of Liapunov stability as well.

10 Appendix

Theorem A. 1 [20]. Let $V(t)$ and $k(t)$ be smooth functions defined on $[0, +\infty)$ with $V(t) \geq 0, \forall t \in [0, +\infty)$, $N(t)$ a Nussbaum-type function, and b a nonzero constant. If the following inequality holds: $V(t) \leq \int_0^{k(t)} [bN(\omega) + 1] d\omega + c, \forall t \in [0, +\infty)$ where c is an arbitrary constant, then $V(t)$, $k(t)$ and $\int_0^{k(t)} [bN(\omega) + 1] d\omega$ must be bounded on $[0, +\infty)$.

Theorem A. 2 [7]. Consider the system (1) with $\det(CB) \neq 0$ and let $V \in R^{n \times (n-m)}$ denote a basis matrix of $\ker C$. It follows that $S := [B(CB)^{-1}, V]$ has the inverse $S^{-1} = [C^T, N^T]^T$, where $N := (V^T V)^{-1} V^T [I_n - B(CB)^{-1} C]$. Hence the state space transformation $(y^T, \eta^T)^T = S^{-1}x = ((Cx)^T, (Nx)^T)^T$ converts (1) into

$$\begin{aligned}\dot{y}(t) &= A_1 y(t) + A_2 \eta(t) + CB(u(t) + d(t)) \\ \dot{\eta}(t) &= A_3 y(t) + A_4 \eta(t)\end{aligned}\quad (33)$$

Here $A_1 \in R^{m \times m}$, $A_2 \in R^{m \times (n-m)}$, $A_3 \in R^{(n-m) \times m}$, $A_4 \in R^{(n-m) \times (n-m)}$, so that

$$\begin{pmatrix} A_1 & A_2 \\ A_3 & A_4 \end{pmatrix} = S^{-1}AS$$

If (A, B, C) is minimum phase, then A_4 in (33) is asymptotically stable.

Lemma A. 3 (Barbalet) If the function $f(t)$ is uniformly continuous, such that $\lim_{t \rightarrow \infty} \int_0^t |f(s)| ds$ exists and is finite, then we have $\lim_{t \rightarrow \infty} f(t) = 0$.

Definition A. 1 Almost Strictly Positive Real: A system

$$\begin{aligned}\dot{x}(t) &= Ax(t) + Bu(t) \\ y(t) &= Cx(t) + Du(t), x(0) = x_0\end{aligned}\quad (34)$$

where $(A, B, C, D) \in R^{n \times n} \times R^{n \times m} \times R^{m \times n} \times R^{m \times m}$, is called Strictly Positive Real, if it satisfies equation (35) for $\mu > 0$ and we say it is Almost Strictly Positive Real, if there exists a $K \in R^{m \times m}$, so that the feedback $u(t) = -Ky(t) + r(t)$ yields a Strictly Positive Real system.

$$\begin{aligned}PA + A^T P &= -QQ^T - 2\mu P \\ PB &= C^T - QW \\ W^T W &= D + D^T\end{aligned}\quad (35)$$

Definition A. 2 Almost Strictly Negative Real: The system $G(s)$ defined by (34) is called Almost Strictly Negative Real, if $-G(s)$ is a Almost Strictly Positive Real system.

Definition A. 3 Almost ϵ -Strictly Positive/Negative Real: Let $\epsilon > 0$, the system (34) is called ϵ -Strictly Positive Real, if it satisfies equation (35) for $\mu > \epsilon$ and we say it is Almost ϵ -Strictly Positive Real, if there exists a $K \in R^{m \times m}$, so that the feedback $u(t) = -Ky(t) + r(t)$ yields a ϵ -Strictly Positive Real system. It is called Almost ϵ -Strictly Negative Real, if $-G(s)$ is a Almost ϵ -Strictly Positive Real system.

References

- [1] Dixon W. E., Zergeroglu E., Dawson D.M., Costic B.T., Repetitive Learning Control: A Lyapunov-Based Approach, Proceedings of the 2001 International Conference on Control Applications, Mexico City, Mexico, Sep, 2001.
- [2] Hara S., Yamamoto Y., Omata T., and Nakano M., Repetitive control system: A new type servo system for periodic exogenous signals, IEEE Trans. on Automatic Control, Vol. 33, No. 7, P659-668, 1988.
- [3] Hillerstrom G, Adaptive Suppression of Vibrations: A Repetitive Control Approach, IEEE Trans. on Control Systems Technology, Vol. 4, No 1, P72-78, 1996.
- [4] Horowitz R., Messner W., Moore J. B., Exponential Convergence of a Learning Controller for Robot Manipulators, IEEE Trans. on Automatic Control, Vol. 36, No 7, P890-897, 1991.
- [5] Howard Kaufman, Itzhak Barkana, and Kenneth Sobel, Direct Adaptive Control Algorithms: Theory and Applications. Second Edition, Springer, New York, 1997.
- [6] Ilchmann A., Owens, D.H., Adaptive Stabilization with Exponential Decay, Systems and Control Letters, 14, P437-443, 1990.
- [7] Ilchmann A., Non-Identifier-Based High-Gain Adaptive Control, Lecture Notes in Control and Information Sciences 189, Springer-Verlag, London, 1993.
- [8] Jiang Y.A., Clements D.J., Hesketh T., Adaptive Repetitive Control of Nonlinear Systems, Proceedings of the 34th Conference on Decision and Control, New Orleans, LA, Dec, 1995.
- [9] Li L.M., Owens D.H., and Banks S.P., Multi-periodic Repetitive Control System Part II: Robustness and Practical Issues, submitted for publication, 2002.
- [10] Lucibello P., Exact repetitive control of minimum phase linear systems, Proceedings of the 1993 IEEE/RSJ International Conference on Intelligent Robots and Systems, Yokohama, Japan 1993.
- [11] Nussbaum R.D., Some remarks on a conjecture in parameter adaptive control, Systems Control Letters, Vol 3, PP243-246, 1983.
- [12] Owens D.H., Li L.M. and Banks S.P., Multi-periodic Repetitive Control System Part I: A Liapunov analysis for MIMO systems, submitted for publication, 2002.

- [13] Owens D.H., Li L.M. and Banks S.P., Multi-periodic Non-linear Repetitive Control: Feedback Stability Analysis, LETTER NOTES IN CONTROL AND INFORMATION SCIENCES 281: Nonlinear and Adaptive Control. P275-283, 2003.
- [14] Sun Z., Tsao T., Adaptive Control with Asymptotic Tracking Performance and its Application to an Electro-Hydraulic Servo System, Journal of Dynamic Systems Measurement and Control: Trans. of the ASME, Vol 122, MAR, PP188-195, 2000.
- [15] Tomizuka M., Tsao T., Chew K., Analysis and Synthesis of Discrete-Time Repetitive Controllers, Journal of Dynamic Systems Measurement and Control: Trans. of the ASME, Vol 111, SEP, PP353-358, 1989.
- [16] Tsao T., Tomizuka M., Robust Adaptive and Repetitive Digital Tracking Control and Application to a Hydraulic Servo for Noncircular Marching, Journal of Dynamic Systems Measurement and Control: Trans. of the ASME, Vol 116, MAR, PP24-32, 1994.
- [17] Tzou Y., Jung S., Yeh H., Adaptive Repetitive Control of PWM Inverters for Very Low THD AC-Voltage Regulation with Unknown Loads, IEEE Trans. on Power Electronics, Vol. 15, No. 5, PP973-980, 1999.
- [18] Weiss G., Repetitive control systems: old and new ideas, System and Control in the Twenty-first Century, editors: C. Byrnes, B. Datta, D. Gilliam and C. Martin, Birkhauser-Verlag, Basel, PP389-404, 1997.
- [19] Weiss G., Hafele M., Repetitive control of MIMO systems using H^∞ design, Automatica, Vol. 35, PP1185-1199, 1999.
- [20] Ye X.D. and Jiang J.P., Adaptive nonlinear design without a priori knowledge of control directions, IEEE Trans. Automat. Contr., 43(11), 1617-1621, 1998.

