



This is a repository copy of *Magnetic and structural characterization of NiFe/Fe<sub>30</sub>Co<sub>70</sub> Bilayers*.

White Rose Research Online URL for this paper:  
<http://eprints.whiterose.ac.uk/83443/>

Version: Accepted Version

---

**Article:**

Morley, N.A., Finkel, A.C., Yang, W. et al. (1 more author) (2014) Magnetic and structural characterization of NiFe/Fe<sub>30</sub>Co<sub>70</sub> Bilayers. *IEEE Transactions on Magnetics*, 50 (11). 2503704. ISSN 0018-9464

<https://doi.org/10.1109/TMAG.2014.2330001>

---

**Reuse**

Unless indicated otherwise, fulltext items are protected by copyright with all rights reserved. The copyright exception in section 29 of the Copyright, Designs and Patents Act 1988 allows the making of a single copy solely for the purpose of non-commercial research or private study within the limits of fair dealing. The publisher or other rights-holder may allow further reproduction and re-use of this version - refer to the White Rose Research Online record for this item. Where records identify the publisher as the copyright holder, users can verify any specific terms of use on the publisher's website.

**Takedown**

If you consider content in White Rose Research Online to be in breach of UK law, please notify us by emailing [eprints@whiterose.ac.uk](mailto:eprints@whiterose.ac.uk) including the URL of the record and the reason for the withdrawal request.



[eprints@whiterose.ac.uk](mailto:eprints@whiterose.ac.uk)  
<https://eprints.whiterose.ac.uk/>

# Magnetic and Structural Characterisation of NiFe/Fe<sub>30</sub>Co<sub>70</sub> bilayers

Nicola A. Morley, Member, IEEE, Anastasia Caruana Finkel, Weigang Yang and Nik Reeves-McLaren.

**Abstract**— Magnetostrictive films are required for a wide range of device applications; by increasing the magnetostriction constant and decreasing the anisotropy field, the devices will become more efficient. This paper has studied Fe<sub>30</sub>Co<sub>70</sub> films on different thicknesses of the soft magnetic underlayer Ni<sub>81</sub>Fe<sub>19</sub>, to determine how the structural and magnetic properties change. It was found that the anisotropy field of the Fe<sub>30</sub>Co<sub>70</sub> film could be reduced by 50% to 10kA/m and the magnetostriction constant increased by a factor 4 to 65ppm when grown on 30nm Ni<sub>81</sub>Fe<sub>19</sub>. This was due to the NiFe underlayer inducing a BCC(110) texture within the Fe<sub>30</sub>Co<sub>70</sub> film and reducing the in-plane stress.

**Index Terms**—magnetostrictive films, MEMS, soft magnetic underlayers

## I. INTRODUCTION

MAGNETIC microelectromechanical systems (MEMS) devices are being developed for a range of applications including magnetostrictive energy harvesters [1] and wireless mass sensors for detection of airborne toxins and water based nutrients [2]. To achieve the sensitivities required for these applications the magnetic films used must have a large magnetostriction constant ( $\lambda_s > 50\text{ppm}$ ) and a small anisotropy field ( $H_s < 10\text{kA/m}$ ) [1, 2]. Possible candidate materials for these applications include Fe-Co [3-6], Fe-Ga [7-9] and Metglas films [10].

Previous work by Hunter et al [3] showed that the magnetostriction constants of Fe-Co films could be as high as 250ppm, but strongly depended on fabrication procedure, which influenced the film microstructure. While the magnetostriction constants were high in these films, the anisotropy fields were also high i.e.  $H_s \sim 40\text{kA/m}$  for the quenched Fe<sub>34</sub>Co<sub>66</sub> film. Similarly, work by Javed et al [7, 8] and Hatrick-Simpers et al [9] showed the magnetostriction constants for Fe-Ga films ranged from 50ppm to 150ppm depending on the fabrication method, but again the anisotropy fields were in general  $> 50\text{kA/m}$ , with the lowest measured at 32 kA/m for a 50nm Fe<sub>77</sub>Ga<sub>23</sub> film [7]. Both Fe-Co and Fe-Ga films would be ideal for the MEMS applications if the

anisotropy field could be reduced. One method to achieve this, is to grow the films on thin underlayers, such as Cu, Rb, and NiFe. Jung et al [4] determined that Ta, Cu, NiFe and Ru underlayers strongly reduce the anisotropy field and coercive field of Fe<sub>65</sub>Co<sub>35</sub> films by changing the film texture. Kotapati et al. [5] determined that when grown on a thicker NiFe underlayer, smaller anisotropy fields and larger magnetostriction constants can be achieved for 15nm Fe<sub>50</sub>Co<sub>50</sub> films. Caruana Finkel et al. [6] also showed that increasing NiFe underlayer thickness led to smaller anisotropy fields in 25nm Fe<sub>10</sub>Co<sub>90</sub> films; the magnetostriction constant could be tuned by varying NiFe thickness.

This work has studied 50nm Fe<sub>30</sub>Co<sub>70</sub> films on soft magnetic underlayers, with the aim to achieve the large magnetostriction constants achieved by Hunter et al [3], in thinner films, but with anisotropy fields  $< 10\text{kA/m}$ .

## II. EXPERIMENTAL PROCEDURE

Bilayer films were grown on cleaned silicon substrates with the native oxide layer still in place. The films were grown in a Nordiko RF sputterer, which had the capability for the soft magnetic underlayer and the Fe<sub>30</sub>Co<sub>70</sub> film to be grown in sequence without exposing the underlayer to atmosphere. The soft magnetic underlayer was Ni<sub>81</sub>Fe<sub>19</sub> (NiFe), grown at 4.8mTorr pressure and a power density of  $1\text{kW/m}^2$ , which was the lowest pressure and power for the system which allowed for uniform NiFe film growth [11]. The thickness of the NiFe films ranged from 0 to 30nm. The Fe<sub>30</sub>Co<sub>70</sub> film was then deposited on top at 4.8mTorr pressure and a power density of  $2\text{kW/m}^2$ . The thickness of the Fe<sub>30</sub>Co<sub>70</sub> films was 50nm. The thickness calibration of each layer deposited using the RF sputterer was checked before the bilayer growths, by measuring three monolith films of different thicknesses using an atomic force microscope. This ensured that the film thickness for each layer was  $\pm 1\text{nm}$ .

A Siemens D5000 diffractometer with a Cu K $\alpha$  source ( $\lambda = 1.5418\text{\AA}$ ) was used to collect the x-ray diffraction (XRD) patterns of the films. The XRD data were fitted in Fityk software package [12], to determine line position  $2\theta$  and full width at half maximum (FWHM) values. From these measured

This paragraph of the first footnote will contain the date on which you submitted your paper for review.

N. A. Morley, Department of Materials Science and Engineering, University of Sheffield, Sheffield, S1 3JD (e-mail: n.a.morley@sheffield.ac.uk).

A. Caruana Finkel, Department of Materials Science and Engineering, University of Sheffield, Sheffield, S1 3JD (e-mail: anastasia.finkel@gmail.com)

W. Yang, Department of Materials Science and Engineering, University of Sheffield, Sheffield, S1 3JD (e-mail: mtp12wy@sheffield.ac.uk)

N. Reeves-McLaren, Department of Materials Science and Engineering, University of Sheffield, Sheffield, S1 3JD (e-mail: n.reeves@sheffield.ac.uk)

values, the lattice constant ( $a$ ) was determined using Bragg's law, along with the homogenous strain ( $\varepsilon$ ) and stress ( $\sigma$ ) [13]. The minimum grain size ( $D$ ) was determined from the XRD data using the Scherrer equation [13]. The magnetic properties were measured on a Magneto-optic Kerr Effect (MOKE) magnetometer [6-8]. From the normalised hysteresis loops, the anisotropy fields ( $H_s$ ) and coercive fields ( $H_c$ ) were determined, while the anisotropy was inferred from the normalised remanent magnetisation. The effective magnetostriction constant ( $\lambda_{eff}$ ) was determined using the Villari Effect technique [6-8]. This involves bending the film along the hard axis over a known bend radius within a MOKE magnetometer. The change in anisotropy field as a function of bend radii ( $R$ ) is then plotted (Fig. 3a), and the effective magnetostriction constant determined using the equation:

$$\lambda_{eff} = \frac{dH_s}{d^1/R} \frac{\mu_0 M_s E}{3\nu\tau} \quad (1)$$

Where  $\mu_0 M_s$  is saturation magnetization (2.2T for  $Fe_{30}Co_{70}$ ),  $\nu$  is the Poisson ratio of the substrate,  $E$  is the Young's Modulus of the substrate and  $\tau$  is the substrate thickness. The values of the Poisson ratio and Young's modulus of the 380 $\mu$ m silicon substrate are known from the literature [14]. The saturation magnetization of the 50nm  $Fe_{30}Co_{70}$  films is assumed to be the same as bulk  $Fe_{30}Co_{70}$ , as previous work on thin films found that the magnetization was reduced from the bulk value for films thinner than 2.5nm [15], thus at 50nm the saturation magnetization can be taken as the bulk value.

### III. RESULTS AND DISCUSSION

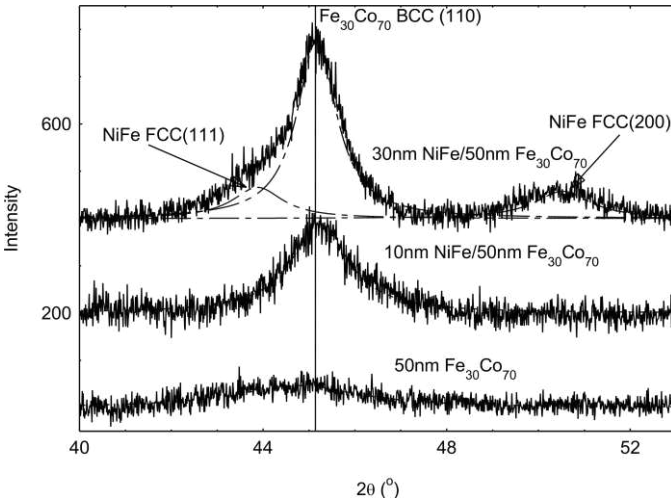


Fig. 1. XRD data for the 50nm  $Fe_{30}Co_{70}$  films grown on NiFe underlayers. The dashed lines are a fit to the data.

XRD data, Fig. 1, showed a peak at  $2\theta \sim 45^\circ$ , for all three  $Fe_{30}Co_{70}$  films, which increasing in sharpness with NiFe layer thickness. This peak is attributed to the BCC(110) peak, which occurs at  $2\theta = 45.14^\circ$  for bulk  $Fe_{30}Co_{70}$  (solid line in Fig. 1). The peaks were fitted using Fityk [12], and this fitting is plotted as dashed lines in Fig. 1. For the 30nm NiFe/50nm  $Fe_{30}Co_{70}$  film, two extra peaks are observed in the data along with the expected BCC(110) peak. These peaks are attributed to the NiFe underlayer and are the FCC (111) peak at  $43.87^\circ$  and the FCC(200) peak at  $50.52^\circ$ . As the BCC(110) peak increases in

TABLE I  
SUMMARY OF THE LATTICE CONSTANTS, STRAINS, STRESSES AND GRAIN SIZE FOR THE  $Fe_{30}Co_{70}$  FILMS

Film	Lattice constant, $a$ (Å)	Strain, $\varepsilon$	Stress, $\sigma$ (GPa)	Grain Size, $D$ (nm)
50nm $Fe_{30}Co_{70}$	$2.86 \pm 0.03$	-	-	$3 \pm 1$
10nm NiFe/ 50nm $Fe_{30}Co_{70}$	$2.831 \pm 0.004$	$-0.0021 \pm 2 \times 10^{-5}$	$1.42 \pm 0.01$	$7 \pm 0.5$
30nm NiFe/ 50nm $Fe_{30}Co_{70}$	$2.836 \pm 0.004$	$-0.0004 \pm 1 \times 10^{-5}$	$0.24 \pm 0.01$	$10 \pm 0.5$

sharpness with NiFe thickness, this means that growing on the NiFe underlayer has improved the texture within the  $Fe_{30}Co_{70}$  film. For the  $Fe_{30}Co_{70}$  film grown with no underlayer, XRD data shows no preferred texture within the film, with all textures as likely. For the  $Fe_{30}Co_{70}$  films grown on a NiFe underlayer, the NiFe has caused the BCC(110) direction in the  $Fe_{30}Co_{70}$  films to become aligned perpendicular to the substrate, thus providing the  $Fe_{30}Co_{70}$  films with a strong texture direction within it.

The lattice constant, grain size, homogenous strain and stress for each film are given in table 1. For the 50nm  $Fe_{30}Co_{70}$  film grown with no underlayer, the lattice constant is larger than the bulk  $Fe_{30}Co_{70}$  lattice constant ( $a_0 = 2.837 \text{Å}$ ), suggesting there is a small compressive stress within the film. Due to the broad width of the peak and the low signal to noise ratio (SNR = 4), the error on the lattice constant is larger than the bilayer films. This means that although the fitted peak  $2\theta$  is smaller than the bulk value, the large error on it means that it is within error of the bulk value. Thus no strain and stress values are given, due to the large uncertainty in the data. For the  $Fe_{30}Co_{70}$  films grown on NiFe, the lattice constants are smaller than the bulk constant, though within errors, suggesting a small in-plane tensile stress within the film. The in-plane stress is also a factor 6 smaller in the 30nm NiFe/50nm  $Fe_{30}Co_{70}$  film compared to the 10nm NiFe/50nm  $Fe_{30}Co_{70}$  film. This means growing  $Fe_{30}Co_{70}$  films on NiFe films has changed both overall texture within the film and in-plane stress. The growth on NiFe has also affected the grain size within the  $Fe_{30}Co_{70}$  films. The grain size was determined using the Scherrer equation [13], which depends on the  $2\theta$  peak as well as the full width at half maximum (FWHM) of the XRD peak. Thus again due to the SNR and broad peak width of the 50nm  $Fe_{30}Co_{70}$  film with no underlayer, the grain size quoted is a minimum value, as the grain size increases with decreasing FWHM. Therefore the data suggests that the 50nm  $Fe_{30}Co_{70}$  film with no underlayer had a grain size of 3nm, while for the 30nm NiFe/50nm  $Fe_{30}Co_{70}$  film the grain size had increased to 10nm, which will in part be due to the BCC(110) texture in the film, improving the FWHM of the XRD peak.

From Fig. 2, it is observed that the shape of the hard axis magnetisation loop changes as the thickness of the NiFe underlayer thickness increases. The anisotropy field decreases by 50%, from  $20 \pm 2$  kA/m for the  $Fe_{30}Co_{70}$  film to  $10 \pm 2$  kA/m for the 30nm NiFe/50nm  $Fe_{30}Co_{70}$  film. This will be due to the NiFe underlayer, which has reduced the stress and increased the BCC(110) texture in the films. This is because the anisotropy field is directly proportional to the stress in the film [16], thus a decrease in the in-plane stress, will reduce the anisotropy field of the film, as observed in Fig.2.

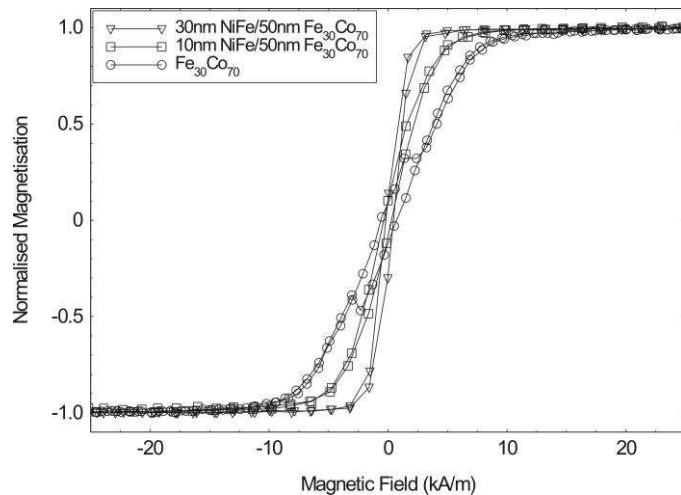


Fig. 2. Normalised hard axis magnetisation loops as a function of magnetic field for the 50nm Fe<sub>30</sub>Co<sub>70</sub> films grown on NiFe underlayers

From Fig. 2, the coercive field reduces by a half as well, from  $0.7 \pm 0.2$  kA/m for the Fe<sub>30</sub>Co<sub>70</sub> film to  $0.35 \pm 0.2$  kA/m for the 10nm NiFe/50nm Fe<sub>30</sub>Co<sub>70</sub> film. The coercive field depends on the microstructure and grain size within the film [4]. For Fe<sub>30</sub>Co<sub>70</sub> films, the film structure went from no defined texture for the Fe<sub>30</sub>Co<sub>70</sub> film to strong BCC(110) texture for the Fe<sub>30</sub>Co<sub>70</sub> films grown on NiFe; this change in microstructure will be the cause for the reduction in the H<sub>c</sub>. Although the anisotropy fields and coercive fields were reduced when growing on NiFe underlayers, the overall uniaxial anisotropy within the films was maintained.

The effective magnetostriction constants of the Fe<sub>30</sub>Co<sub>70</sub> films were measured using the Villari Effect (eqn (1)) and are plotted in Fig. 3b, along with the change in anisotropy field as a function of inverse bend radii (Fig. 3a). For the 50nm Fe<sub>30</sub>Co<sub>70</sub> film with no underlayer, the effective magnetostriction constant was  $+17 \pm 4$  ppm, while for the 10nm NiFe/50nm Fe<sub>30</sub>Co<sub>70</sub> the effective magnetostriction constant was  $+14 \pm 4$  ppm, therefore within error of the monolith film. Thus growing on the thin NiFe layer did not effect the overall effective magnetostriction constant. The slight decrease in effective magnetostriction constant could be due to the effective magnetostriction constant of 10nm NiFe on silicon being  $-2.25$  ppm [17]. For the 30nm NiFe/50nm Fe<sub>30</sub>Co<sub>70</sub>, the effective magnetostriction constant was  $+65 \pm 4$  ppm, thus growing on the thicker NiFe film has increased the effective magnetostriction constant to larger than the bulk polycrystalline value ( $\sim 57$  ppm [18]). A similar effect was observed in the effective magnetostriction constants of 15nm Fe<sub>50</sub>Co<sub>50</sub> films [5] grown on NiFe underlayers. Hunter et al [3] measured the effective magnetostriction constants of 500nm Fe<sub>30</sub>Co<sub>70</sub> films, for different processing methods. The values they achieved were  $\lambda_{\text{eff}} \sim 75$  ppm for the as grown films,  $\lambda_{\text{eff}} \sim 140$  ppm for the slow cooled films and  $\lambda_{\text{eff}} \sim 250$  ppm for the quenched films. The texture and phases in the films changed with the different processed, which shows that the effective magnetostriction constant is strongly linked to the film structure. For the 30nm NiFe/50nm Fe<sub>30</sub>Co<sub>70</sub> film, the effective magnetostriction constant is in agreement with Hunter's as-grown films value.

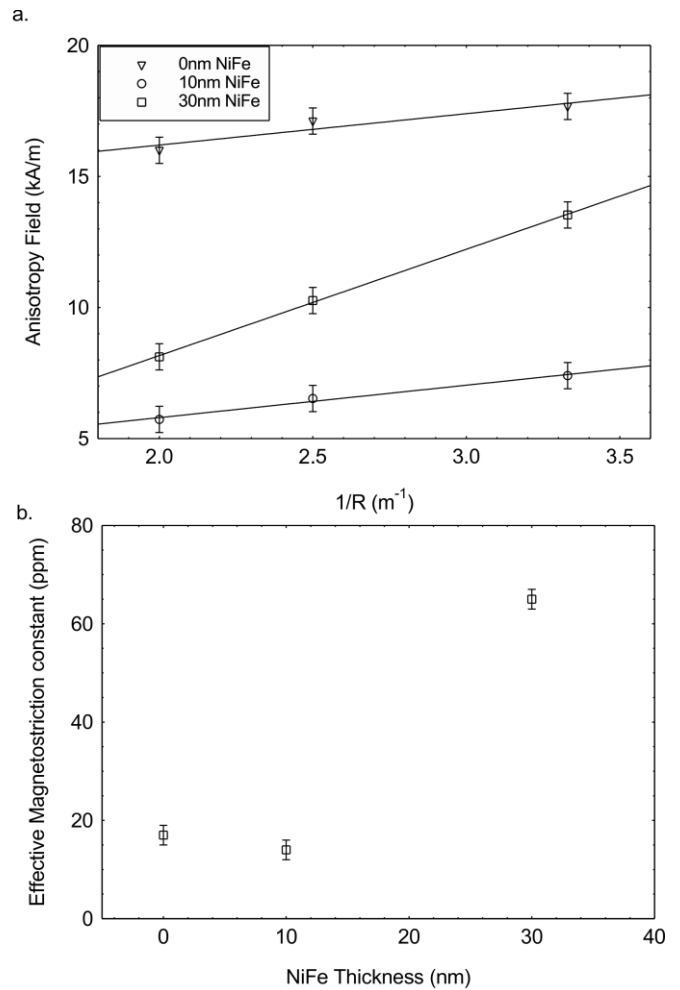


Fig 3a. Anisotropy field as a function of inverse bend radii for the Fe<sub>30</sub>Co<sub>70</sub> films Fig. 3b. Effective magnetostriction constants as a function of NiFe thickness for Fe<sub>30</sub>Co<sub>70</sub> films.

From Hunter et al [3] work, the increase in the effective magnetostriction constant is likely to be due to two effects, the first the changing of texture from randomly orientated to (110) texture and the second is the reduction in stress in the Fe<sub>30</sub>Co<sub>70</sub> films. For a randomly orientated polycrystalline film, such as the 50nm Fe<sub>30</sub>Co<sub>70</sub> film without an underlayer, the effective magnetostriction constant is given by [19]:

$$\lambda_{\text{isotropic}} = \frac{2}{5} \lambda_{100} + \frac{3}{5} \lambda_{111} \quad (2)$$

Where  $\lambda_{100}$  is the magnetostriction constant along the (100) direction and  $\lambda_{111}$  is the magnetostriction constant along the (111) direction. While for a textured (110) film, such as the 30nm NiFe/50nm Fe<sub>30</sub>Co<sub>70</sub> film the effective magnetostriction constant is given by [19]:

$$\lambda_{(110)} = \frac{1}{5} \lambda_{100} + \frac{4}{5} \lambda_{111} \quad (3)$$

Thus both effective magnetostriction constants depend differently on the  $\lambda_{100}$  and  $\lambda_{111}$  values. For bulk Fe<sub>30</sub>Co<sub>70</sub>, the values of  $\lambda_{100}$  and  $\lambda_{111}$  have not been published, with Hall [20] only measuring  $\lambda_{100}$  and  $\lambda_{111}$  up to 60% Co in Fe. Bozorth [18] presented effective magnetostriction constants for bulk Fe<sub>30</sub>Co<sub>70</sub> polycrystalline samples, with the largest value being

130ppm for a hard rolled tape, which had oriented domains compared to 57ppm for bulk polycrystalline samples. Therefore the difference in the effective magnetostriction constants between the 50nm Fe<sub>30</sub>Co<sub>70</sub> film and the 30nm NiFe/50nm Fe<sub>30</sub>Co<sub>70</sub> film could arise from the change in texture in the films.

The effective magnetostriction constant is also influenced by the stress in the film and can be predicted by [16]:  $\lambda_{\text{net}} = \frac{\mu_0 M_s H_s}{3\sigma}$ , where  $\mu_0 M_s$  is the saturation magnetisation (for Fe<sub>30</sub>Co<sub>70</sub> films is 2.2T),  $H_s$  is the anisotropy field and  $\sigma$  is the in-plane stress. Putting the variables in for the films grown on NiFe underlayers, as the XRD peak for the 50nm Fe<sub>30</sub>Co<sub>70</sub> film with no underlayer (Fig. 1) was too broad to determine a stress for the film, gives  $\lambda_{\text{net}} = 2.5\text{ppm}$  for the 10nm NiFe/50nm Fe<sub>30</sub>Co<sub>70</sub> film and  $\lambda_{\text{net}} = 31\text{ppm}$  for the 30nm NiFe/50nm Fe<sub>30</sub>Co<sub>70</sub> film. Although they are smaller than the measured effective magnetostriction constants, there is a large difference between the 10nm NiFe/50nm Fe<sub>30</sub>Co<sub>70</sub> film and the 30nm NiFe/50nm Fe<sub>30</sub>Co<sub>70</sub> film effective magnetostriction constants. Thus showing that changes in stress in the films lead to the large change in the effective magnetostriction constant. This suggests that the large effective magnetostriction constant measured for the 30nm NiFe/50nm Fe<sub>30</sub>Co<sub>70</sub> film is due to both the reduction in stress and increase in the BCC(110) texture in the film.

#### IV. CONCLUSIONS

Growing Fe<sub>30</sub>Co<sub>70</sub> films on thin NiFe underlayers has improved the magnetic properties of the Fe<sub>30</sub>Co<sub>70</sub> films, such that they could be considered for MEMS applications. For example growing the 50nm Fe<sub>30</sub>Co<sub>70</sub> film on a 30nm NiFe underlayer, reduced the anisotropy field by 50% to 10kA/m, while the effective magnetostriction constant increased to 65ppm. From XRD data, the Fe<sub>30</sub>Co<sub>70</sub> films grown on NiFe underlayers had strong BCC(110) texture within the film compared against the Fe<sub>30</sub>Co<sub>70</sub> film grown with no underlayer. Growing Fe<sub>30</sub>Co<sub>70</sub> films on NiFe improved the film texture in the films, with a concomitant reduction in the anisotropy fields and increased effective magnetostriction constant.

#### REFERENCES

- [1] O. Gutfleisch, M. A. Willard, W. E. Bruck, C. H. Chen, S. G. Sankar, and J. Ping Liu, "Magnetic Materials and Devices for the 21st Century: Stronger Lighter and More Energy Efficient," *Adv. Mats*, vol. 23, pp. 821-842, 2011.
- [2] M. R. J. Gibbs, E. W. Hill, and P. J. Wright, "Magnetic materials for MEMS applications," *J. Phys D: Appl. Phys.*, vol. 37, pp. R237 - R244, 2004.
- [3] D. Hunter, W. Osborn, K. Wang, N. Kazantseva, J. Hattrick-Simpers, R. Suchoski, R. Takahashi, M. L. Young, A. Mehta, L. A. Bendersky, S. E. Lofland, M. Wuttig, and I. Takeuchi, "Giant Magnetostriction in annealed CoFe thin-films," *Nat. Commun.*, vol. 1529, pp. 1 - 7, 2011.
- [4] H. S. Jung, W. D. Doyle, and S. Matsunuma, "Influence of underlayers on the soft properties of high magnetisation FeCo films," *J. Appl. Phys.*, vol. 93, pp. 6462 - 6464, 2003.
- [5] S. Kotapati, A. Javed, N. Reeves-McLaren, M. R. J. Gibbs and N. A. Morley, "Effect of the NiFe thickness on the magnetic properties of NiFe/FeCo bilayers", *J. Magn. Magn. Mats*, vol. 331, pp 67-71, 2013
- [6] A. Caruana Finkel, N. Reeves-McLaren and N. A. Morley, "Influence of soft magnetic underlayers on the magnetic properties of Co<sub>90</sub>Fe<sub>10</sub> films" *J. Magn. Magn. Mats*, vol. 357, pp 87-92, 2014
- [7] A. Javed, T. Szumiata, N. A. Morley, and M. R. J. Gibbs, "An investigation of the effect of structural order on magnetostriction and

- magnetic behaviour of Fe-Ga thin films," *Acta Mat*, vol. 58, pp. 4003, 2010.
- [8] A. Javed, N. A. Morley, and M. R. J. Gibbs, "Structure, Magnetic and Magnetostrictive Properties of as-deposited Fe-Ga Thin Films," *J. Magn. Magn. Mats*, vol. 321, pp. 2877, 2008.
- [9] J. R. Hattrick-Simpers, D. Hunter, C. M. Craciunescu, K. S. Jang, M. Murakami, J. Cullen, M. Wuttig, I. Takeuchi, S. E. Lofland, L. Bendersky, N. Woo, R. B. Van Dover, T. Takahashi, and Y. Furuya, "Combinatorial investigation of magnetostriction in Fe-Ga and Fe-Ga-Al," *Appl. Phys. Letts*, vol. 93, pp. 102507, 2008.
- [10] H. Szymczak and R. Zuberek, "Models of stress-induced anisotropy and magnetostriction in metallic glasses", *IEEE Trans Magn*, vol. 26, pp. 2551-2553, 1987
- [11] A. V. Svalov, I. R. Aseguinolaza, A. Garcia-Arribas, I. Orue, J. M. Barandiaran, J. Alonso, M. L. Fernandez-Gubieda and G. V. Kurlyandskaya, "Structure and Magnetic Properties of Thin Permalloy Films near the "Transcritical" state", *IEEE. Trans. Mag*, vol. 46, pp. 333-336, 2010
- [12] M. Wojdyr, "Fityk: a general purpose peak fitting programme," *J. Appl. Crystall*, vol. 43, pp. 1126-1128, 2010.
- [13] C. Hammond, "The Basics of Crystallography and Diffraction", 3<sup>rd</sup> ed. Oxford: Oxford University Press, 2009
- [14] D. R. Franca and A. Blouin, "All-optical measurement of in-plane and out-of-plane Young's modulus and Poisson's ratio in silicon wafers by means of vibration modes", *Meas. Sci. Technol.* Vol 15, pp. 859-868, 2004
- [15] C. A. Neugebauer, "Saturation Magnetisation of Nickel Films of Thickness less than 100Å", *Phys. Rev.* Vol 116, pp1441-1446, 1959
- [16] N. A. Morley, S. Rigby, and M. R. J. Gibbs, "Anisotropy and magnetostriction constants of nanostructured FeCo films," *J. Optoelec Adv. Mats*, vol. 1, pp. 109 - 113, 2009.
- [17] M. P. Hollingworth, M. R. J. Gibbs and S. J. Murdoch, "Magnetostriction and surface roughness of ultrathin NiFe films
- [18] R.M. Bozorth, "Ferromagnetism", IEEE Press, New York, 1978
- [19] A. Javed, N. A. Morley, T. Szumiata and M. R. J. Gibbs, "A comparative study of the microstructural and magnetic properties of <110> textured thin polycrystalline Fe<sub>100-x</sub>Ga<sub>x</sub> (10 <x < 35) films", *Appl. Surf. Sci.*, vol. 257, pp. 5977 - 5983, 2011
- [20] R. C. Hall, "Magnetic Anisotropy and Magnetostriction of Ordered and Disordered Cobalt-Iron Alloys", *J. Appl. Phys.* Vol 31, pp 157S - 158S 1960