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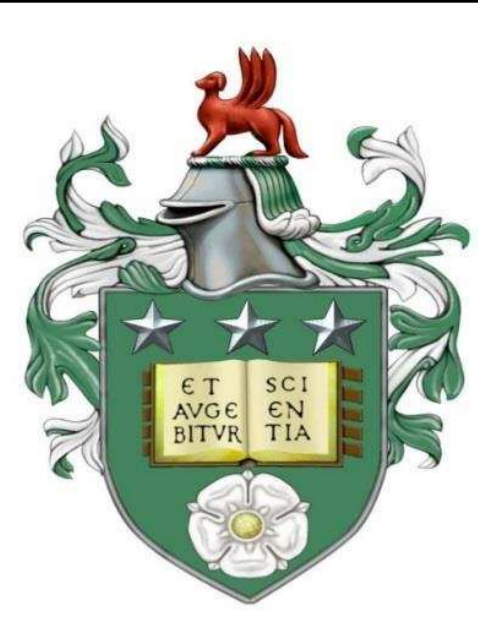
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THE VIBRATION RESPONSE OF A NOVEL COMPOSITE FLOORING SYSTEM INCORPORATING PERFORATED STEEL ULTRA SHALLOW FLOOR BEAMS (USFBs) FOR SUSTAINABLE CONSTRUCTION



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1.0 INTRODUCTION

- Steel concrete composite (SCC) flooring solutions are widely used nowadays as they are lightweight and are quick to erect.
- Recent research initiatives seek to develop slim floors by minimising the structural depth of the floor section.
- Ultra Shallow Floor Beams (USFBs) are used to reduce structural depth compared to traditional slabs (Fig 1).
- USFBs provide an overall reduction in floor-floor height. Concept is shown in Fig 2.

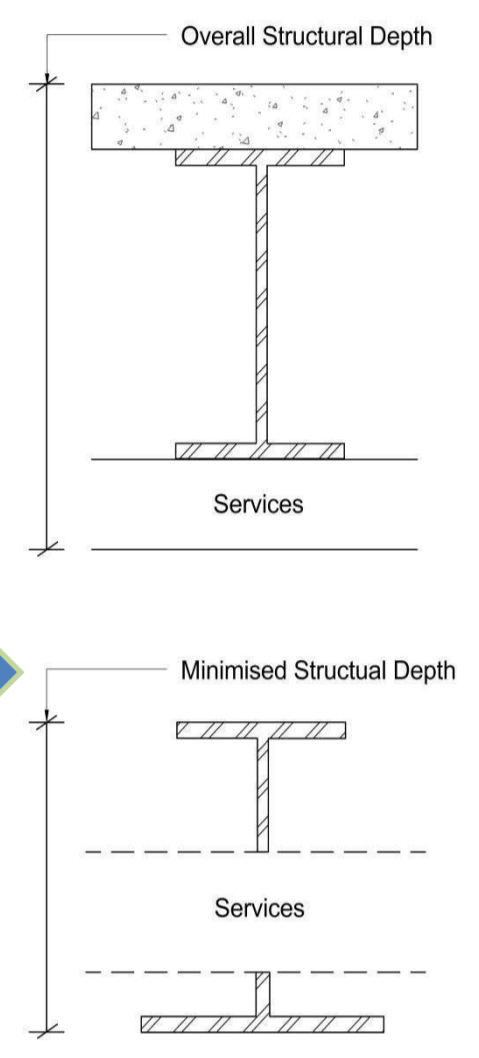


Fig 1: Reduced Depth

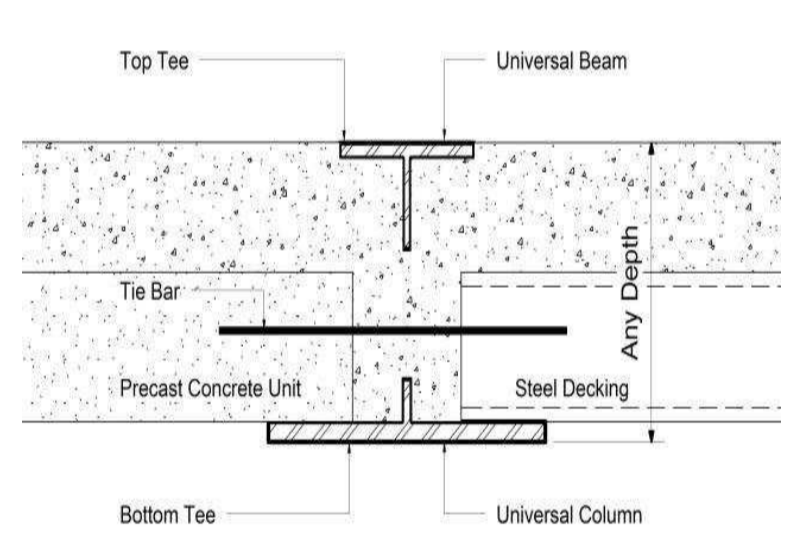


Fig 2: Concept of USFB

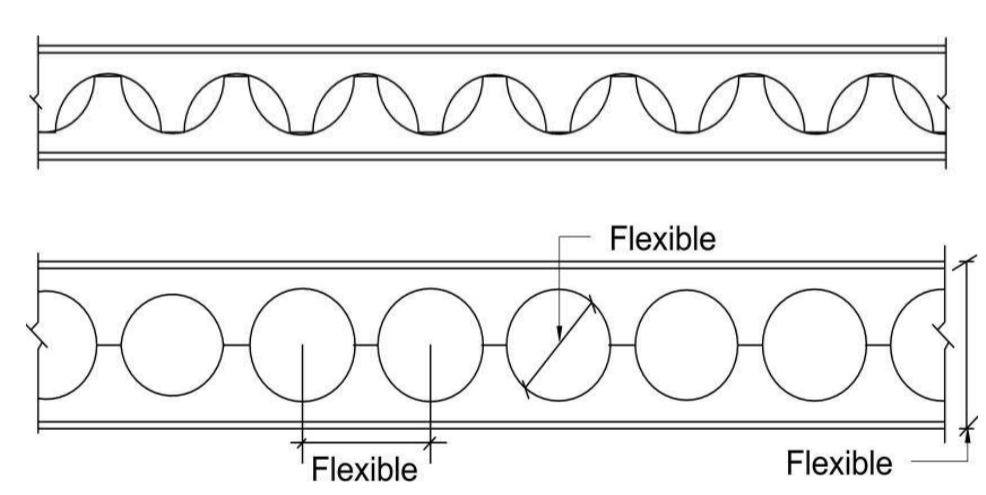


Fig 3: Fabrication Process

2.0 WHY USE PERFORATED USFBs

- A lighter flooring solution in the means of thinner and wider slabs (Fig 4).
- A section with greater second moment of inertia.
- Shear stud connectors in traditional SCC (i.e. concrete slab situated on top of steel beam) are not needed (Fig 5).
- Concrete encasement between structural depth offers a fire resistance of 60mins.
- Longitudinal shear resistance of composite section is enhanced.
- Possible service integration (Fig 6).



Fig 4: Wider Spans

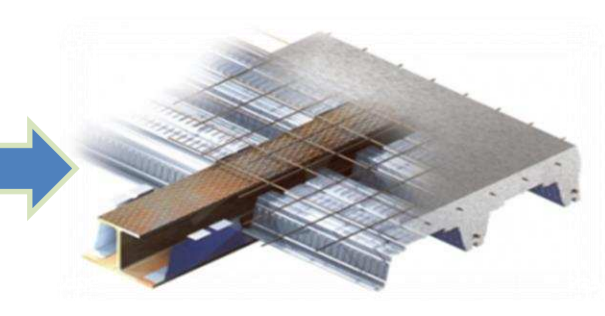


Fig 5: No Shear Studs

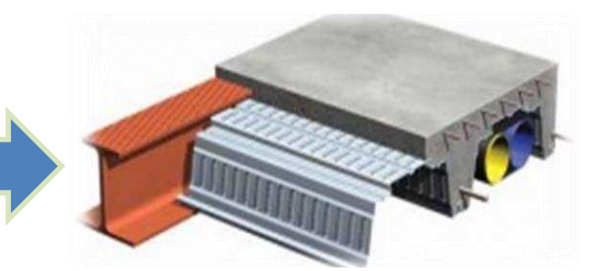


Fig 6: Service Integration

3.0 THE PROBLEM

- It is expected that lightweight, thin and long span slabs will vibrate under certain loads.
- Resonance creates excessive floor vibrations when the floor's natural frequency coincides with excitation frequencies e.g. walking, dancing, etc.

4.0 PROJECT AIM & OBJECTIVES

- The main aim was:
- To provide design guidelines of slabs with perforated USFBs.
- The objectives were as follows:
- To extract the dynamic properties of a bare steel perforated USFB.
 - To generate the natural frequencies and modes shapes of the novel USFB slab by investigating the influence of concrete depth, support conditions and web opening spacing.
 - To develop frequency design limits for various floor spans.
 - To develop equivalent geometric properties for the USFB corresponding to the Euler Bernoulli beam of constant cross-section.

5.0 EXPERIMENTAL RESULTS

- Experimental test was performed on a bare steel 210x124/255x55 USFB.
- The testing found the 1st in plane natural frequency to be 11.77 Hz. Satisfactory performance is achieved as $f_{01} > 3\text{Hz}$.

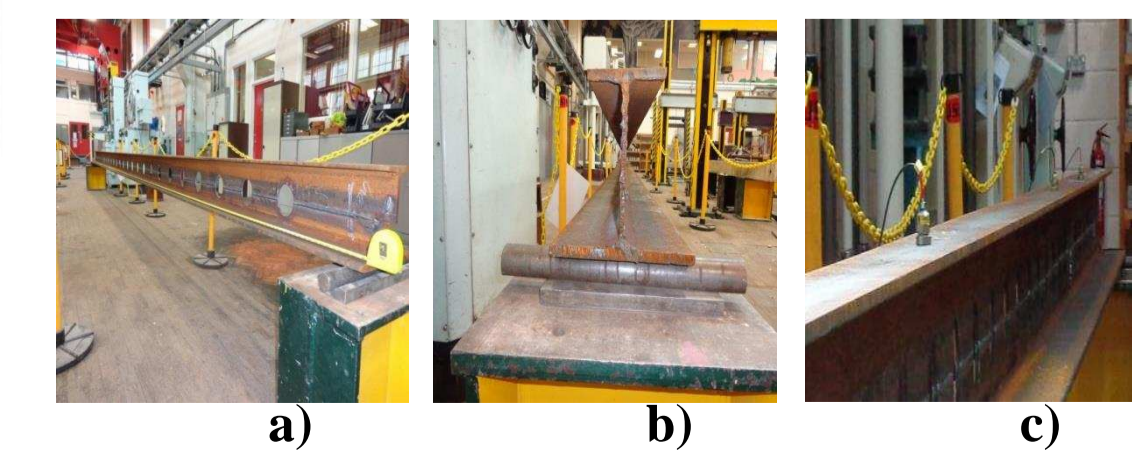


Fig 7: a) Isometric View. b) Cross Section. c) Accelerometers

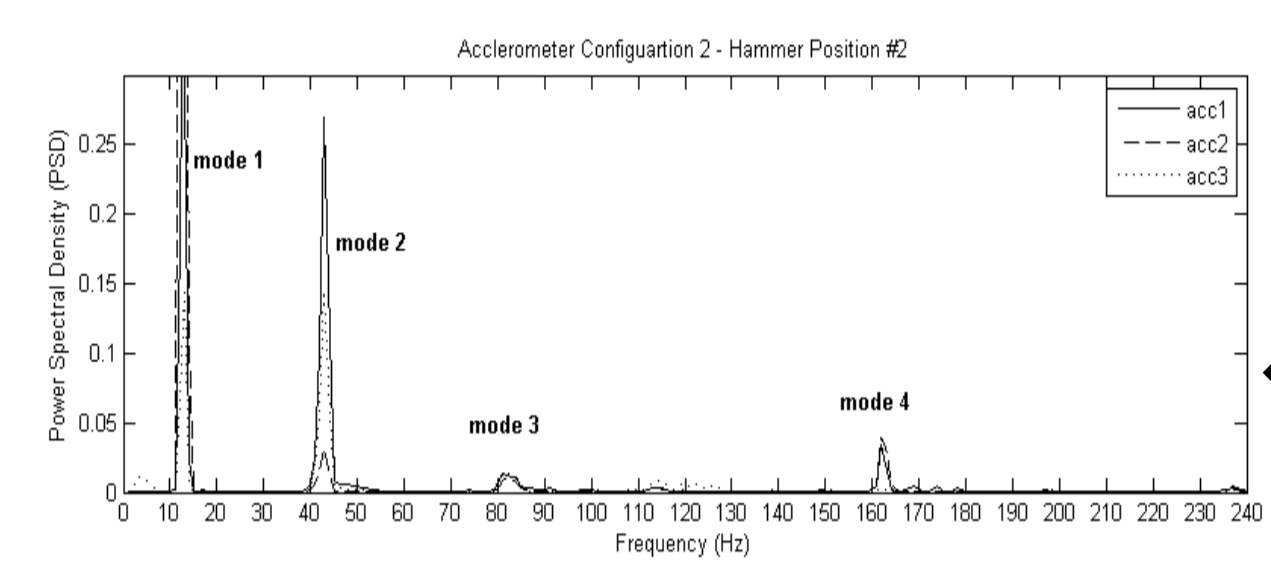


Fig 8: Matlab Results, $f_{01} = 11.77\text{Hz}$

6.0 VALIDATION OF FE MODELS

- Calibrating FE models was done against existing studies.
- 3D solid FE elements were built similar to Tsavdaridis and Giaralis (2011) and Mello et al. (2008).
- Good corroboration was observed thereby allowing the parametric models to be built and evaluated (Fig 9).

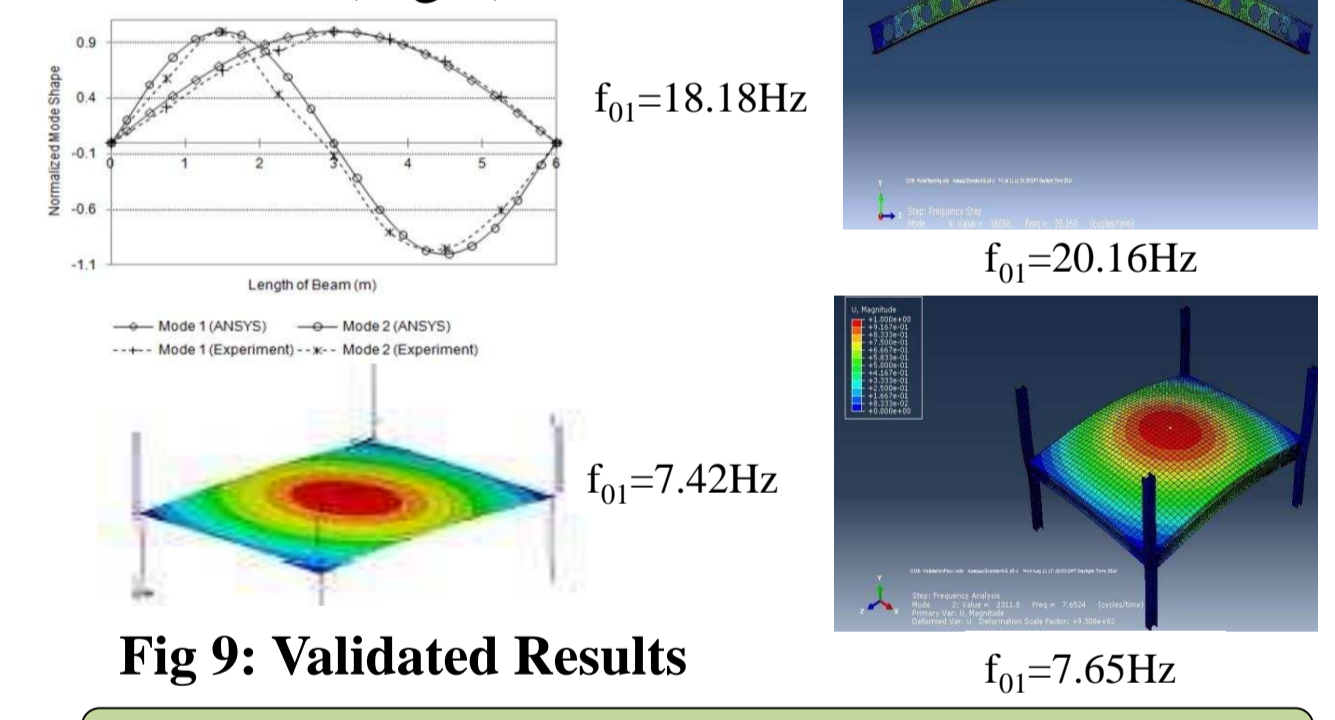


Fig 9: Validated Results

7.0 COMPARATIVE STUDY

- Economic savings are possible with USFBs whilst satisfying minimum floor frequency of 3Hz.

Mode	Comparative Model Natural Frequencies (Hz)		
	Model 1 – Concrete on top Perforated USFB	Model 2 – Concrete encasing Perforated USFB	(Mello et al., 2008) Natural Frequencies (Hz)
1	6.69	5.55	7.42
2	12.610	10.876	14.70
3	13.463	11.295	15.23
4	17.061	14.418	20.32
5	25.419	22.687	30.82
6	29.157	26.595	31.86

Table 1 : Results from Comparative Analyses

8.0 PARAMETRIC STUDY

- The results from this study revealed that:
- Increasing concrete thicknesses resulted in a parabolic behaviour of the 1st vibration mode. Higher modes were linear (Fig 11a, 11b).

- Higher natural frequencies with fixed supports but similar results to pinned supports were seen in higher vibration modes (Fig 11c).
- Decreasing web opening spacing stiffened the section resulting in higher natural frequencies (Fig 11d).

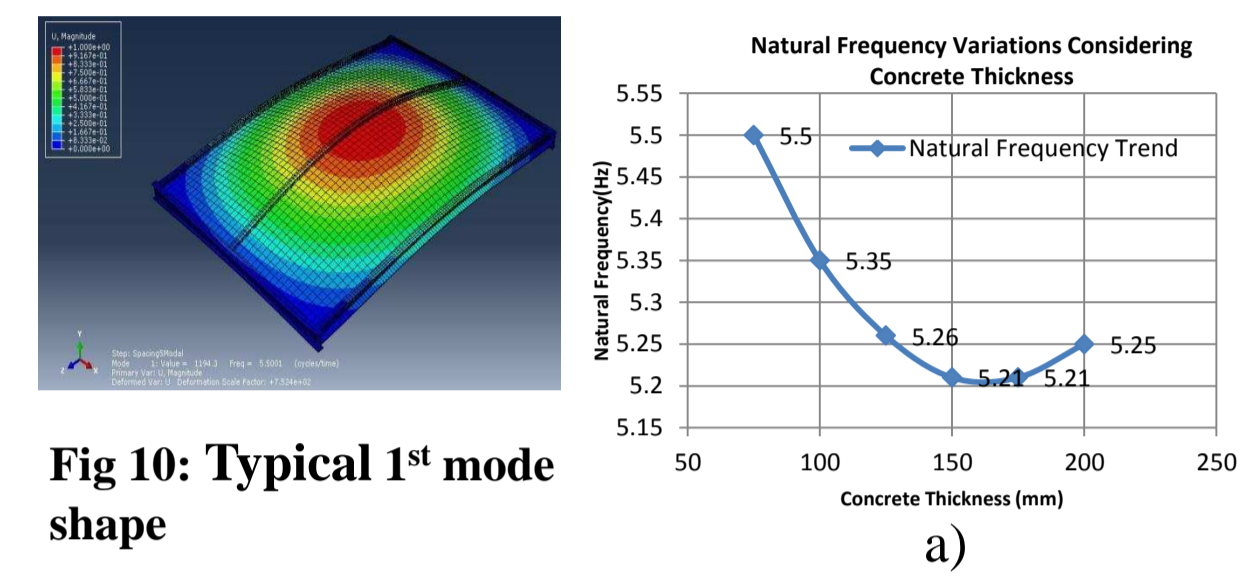


Fig 10: Typical 1st mode shape

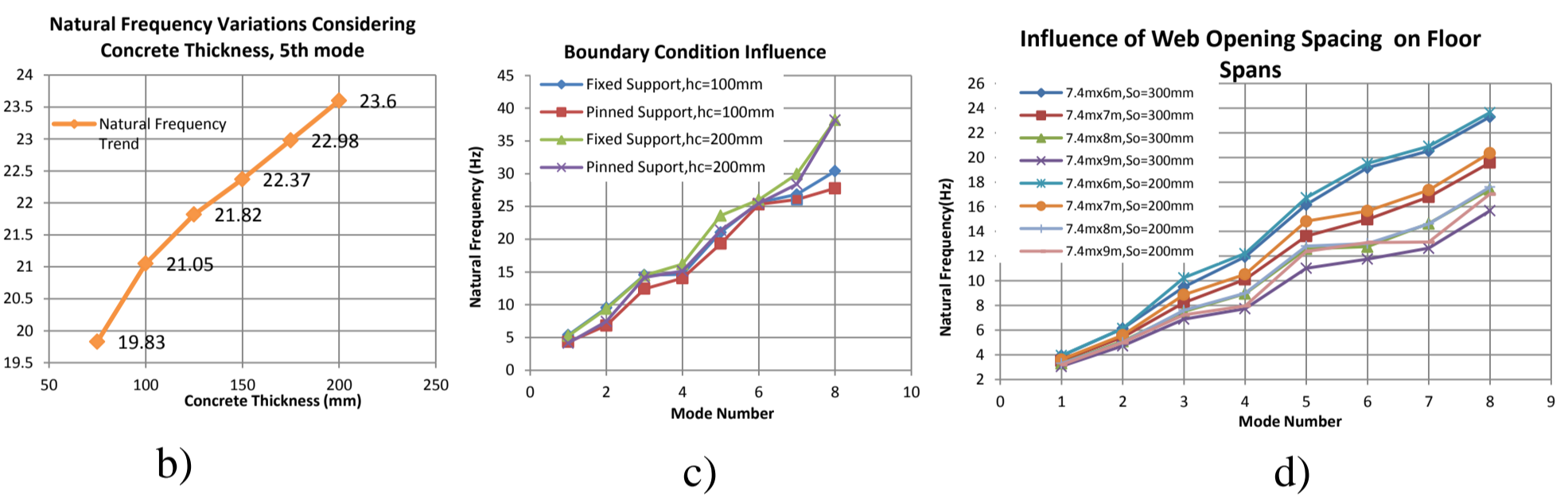


Fig 11a,b,c,d: Parametric Results

9.0 EQUIVALENT GEOMETRIC PROPERTIES

- Favourable results were obtained with equivalent geometric properties corresponding to Euler Bernoulli beam (Table 2).

Floor Dimension (max)	Concrete Thickness (m)	1 st In Plane Natural Frequency (EE) (Hz)	Equivalent Composite Area A_{eq} (m ²)	Equivalent Composite Moment of Inertia I_{eq} (m ⁴)	1 st In-Plane Natural Frequency with equivalent properties (Hz) Eql.	Percentage of error (%)
7.4x9	0.075	3.17	0.0324	1.54*10 ⁻³	3.11	1.9
	0.100	3.06	0.0412	1.83*10 ⁻³	3.06	0
	0.125	3.02	0.0500	2.16*10 ⁻³	3.05	0.99
	0.150	3.02	0.0588	2.53*10 ⁻³	3.07	1.7
	0.175	3.05	0.0676	2.92*10 ⁻³	3.10	1.6
0.200	3.10	0.0764	3.48*10 ⁻³	3.20	3.2	

Table 2: Results with Equivalent Properties

10.0 FINAL REMARKS

- The research concluded:
- Less participation of increased mass in the 1st mode.
 - Slabs modelled with fixed supports are preferable.
 - Reduced web opening spacing improves the slab response.

12.0 REFERENCES

- Mello, A.V.A. et al., 2008. Dynamic Analysis of Composite Systems made of Concrete Slabs and Steel Beams. Journal of Constructional Steel Research, Volume 64, pp. 1142-1151.
- Tsavdaridis, K.D. and Giaralis, A., 2011. Derivation of the Dynamic Properties of Steel Asymmetric Perforated Ultra Shallow Floor Beams via Finite Element Modal Analysis and Experimental Verification. Greece, City University London

11.0 FURTHER WORK

- Consider influence of beam-column joints.
- Influence of various size and shape of web openings.
- Influence of shear studs welded to the web and re-bars through web openings.
- Determining response factor (R).
- Testing of the system in its bare, construction and final states.